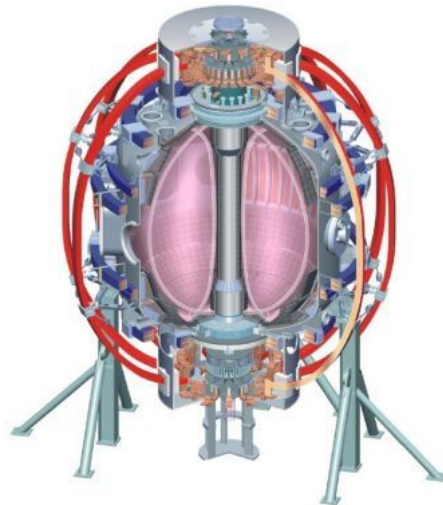


# NSTX Liquid Lithium Divertor (LLD) Design Status and Plans

**H. W. Kugel, PPPL**

*For the NSTX Research Team*

**NSTX 5 Year Plan Review for 2009-13  
Conference Room LSB-B318, PPPL  
July 28-30, 2008**



College W&M  
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TRINITI  
KBSI  
KAIST  
POSTECH  
ASIPP  
ENEA, Frascati  
CEA, Cadarache  
IPP, Jülich  
IPP, Garching  
ASCR, Czech Rep  
U Quebec

# Motivation for NSTX Lithium Research

- NSTX research with solid lithium is aimed initially towards using liquid lithium to control density, edge collisionality, impurity influxes, and eventually power handling.
  - *Solid Li provides short pulse capability but can saturate; liquid Li has much higher LiD capacity, and has potential for power handling and self healing.*
- Over the longer term, NSTX will investigate if liquid lithium can help integrate 4 important potential benefits for fusion
  - a. Divertor pumping over large surface area compatible with high flux expansion solutions for power exhaust and low collisionality
  - b. Improved confinement (reported in FY08)
  - c. ELM reduction and elimination (reported in FY08)
  - d. High-heat flux handling (via capillary flowing Li, swirl tubes, hypervaportrons, evaporative cooling)

# NSTX Has a 3 Phase Lithium Plan

- The 3 Phase NSTX Lithium Plan for Particle Control and Power Handling is moving aggressively toward the 3rd Phase:

## *I. Lithium Injection Experiments (2005-2008)*

- Li pellet injection: 2-5 mg pellets, on graphite divertor (2005)
- Li powder tests: 50  $\mu\text{m}$  Li powder on graphite divertor (2007-2008)

## *II. Lithium Evaporator [LITER] (2006-2009)*

- 1 LITER: deposition on graphite divertor (2006-2007)
- 2 LITER: deposition on graphite divertor (2008)
- 2 LITER: deposition on graphite and LLD-1 (2009-2010)

## *III. Liquid Lithium Divertor [ SNL - NSTX Collaboration] (2009-2013)*

- LLD-1: Li evaporated on thin porous Mo/SS on Cu baseplate
- LLD-2: Li capillary flow to load a Mo mesh surface over wider area
- LLD-3: long pulse (5s) power handling capillary surface with active cooling (via capillary flowing Li, swirl tubes, hypervaportrons, evaporative cooling) for high-power 16 MW (10 MW NBI + 6 MW RF) operations

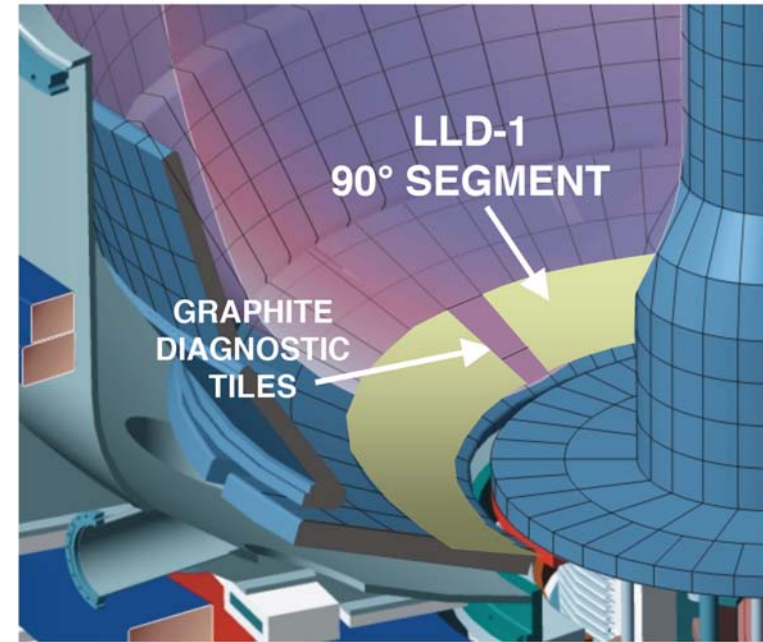
# Liquid Lithium Divertor Physics Design Goals

- Physics Design Goals

- 1) LLD-1: Achieve density control for increased neutral beam current drive capability in the range (from recent simulations):
  - $n_e \sim 5 \times 10^{19} \text{ m}^{-3}$  at  $I_p = 750 \text{ kA}$ 
    - (15-25%  $n_e$  decrease from present expts)
  - highest non-inductive fraction discharges presently often evolve toward  $n_e/n_{GW} \rightarrow 1$
- 2) LLD-2: Enable  $n_e$  scan capability in long pulse H-mode (e.g.,  $\sim x2$ ) by varying lithium thickness
  - Increase filling rate (e.g. capillary flow, powder dropper) to wider area mesh surface
  - Test ability to operate at significantly lower density
  - NHTX ( $n_e/n_{GW} = 0.5$ ) and ST-CTF ( $n_e/n_{GW} = 0.25$ )
- 3) LLD-3: Investigate LLD with long-pulse (5s), high heat flux for 16 MW (10MW (2 NBI) + 6 MW RF) power handling capability

# LLD-1 Plate Design With Thin Lithium Film on High-Z Bonded to Copper is Highest Confidence Approach

- Location - lower outer divertor in four 90° sections.
- Width - 20 cm starting 5 cm outboard of CHI gap.
- Shape - replaces present graphite tiles.
- Structure - 0.01 cm Mo flame-sprayed on 0.02 cm SS brazed to 1.9 cm Cu. Resistive heaters and cooling lines maintain 200-400°C.
- Li Loading - 2 lithium evaporators.



- Each toroidal section electrically grounded to vessel at one mid-segment location to control eddy currents
- Each toroidal section fastened at 4 corners to divertor copper baseplate with fasteners providing structural support, electrical isolation, and accommodating thermal expansion (design adopted from JET PPPL collaboration)
- Narrow graphite tile transition regions between sections contain thermocouples, an array of Langmuir probes, and magnetic & current sensors

# Particle Balance and Recycling Model Used to Estimate 0-D LLD-1 Pumping Projections and Sensitivities

$$\eta_{pump} \cong \gamma_{Li}^{sticking} \frac{\int_{R_{min, tray}}^{R_{max, tray}} \Gamma_{\perp}(R) R dR}{\int_{R_{min}}^{R_{max}} \Gamma_{\perp}(R) R dR} \left( \frac{\Gamma_{out}}{\Gamma_{in} + \Gamma_{out}} \right) \left( \frac{\Gamma_{down}}{\Gamma_{up} + \Gamma_{down}} \right) f_{\phi}$$

Li surface particle sticking probability - 0.85

In/out particle flux ratio - 0.8

(LLD) Tray toroidal coverage - 0.9

Impact of  $R_{tray}$ ,  $\Delta_{tray}$ ,  $(R_{OSP} - R_{tray})$  ( $\Gamma$  available from Vlad)

Up/down particle flux ratio 0.5 ( $\delta_r^{sep}$  important)

\* Red items estimated from CCD camera data  
(V. Soukhanovskii, LLNL)

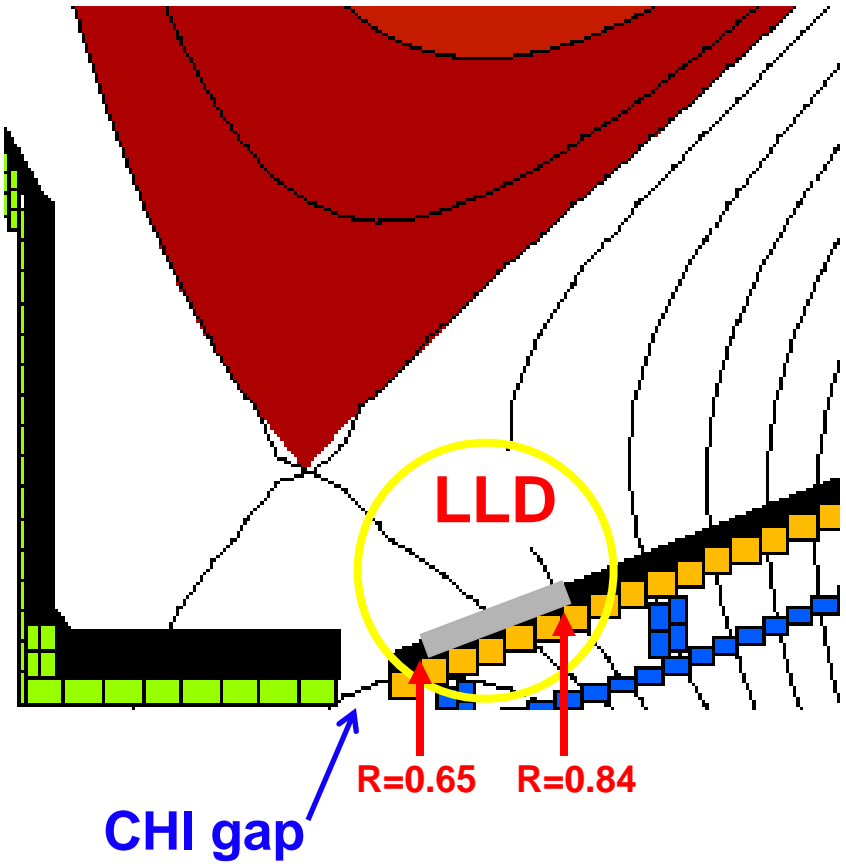
## Iterative Procedure

- Convert measured  $D\alpha$  luminosity to particle flux using 20 ionizations per photon
- Estimate LLD-1 flux intercept fraction from candidate discharge data for a given time slice
- Vary  $R_{LLD}$  in steps of 1 cm
- Repeat for different  $W_{LLD}$ ,  $R_P$ ,  $\eta_{CORE}$  and other input parameters

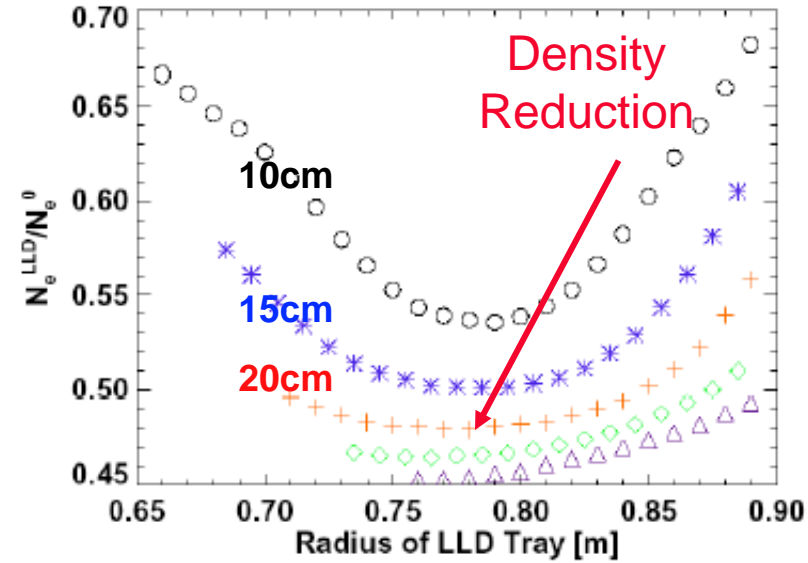
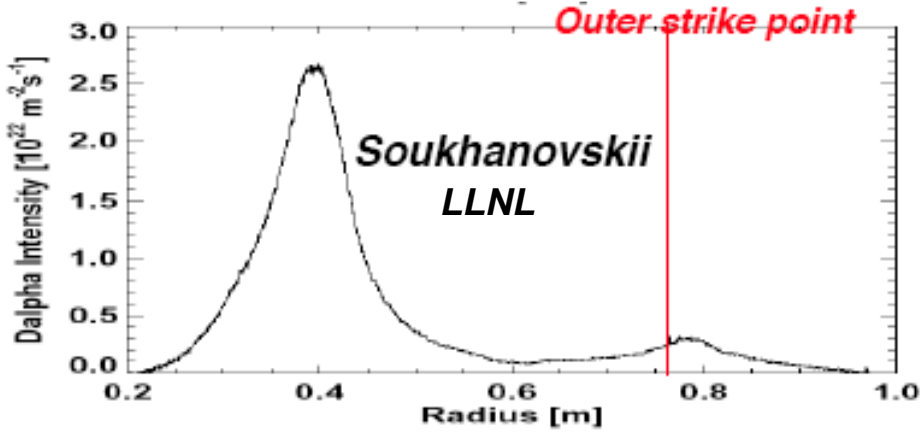
R.Maingi, ORNL

# NSTX Data Used to Enable Analysis of Expected Performance of LLD-1 for Low $\delta$ Plasmas

Low  $\delta$  : reduce  $n_e$  by 50%



R. Maingi  
ORNL

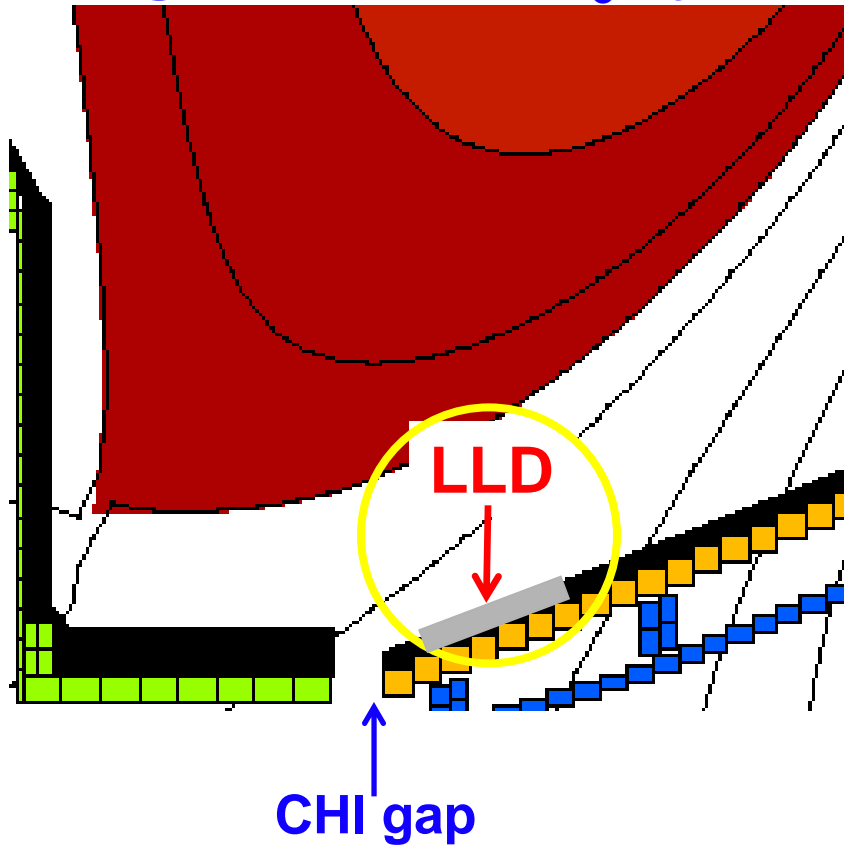


Shown for different LLD-1 widths

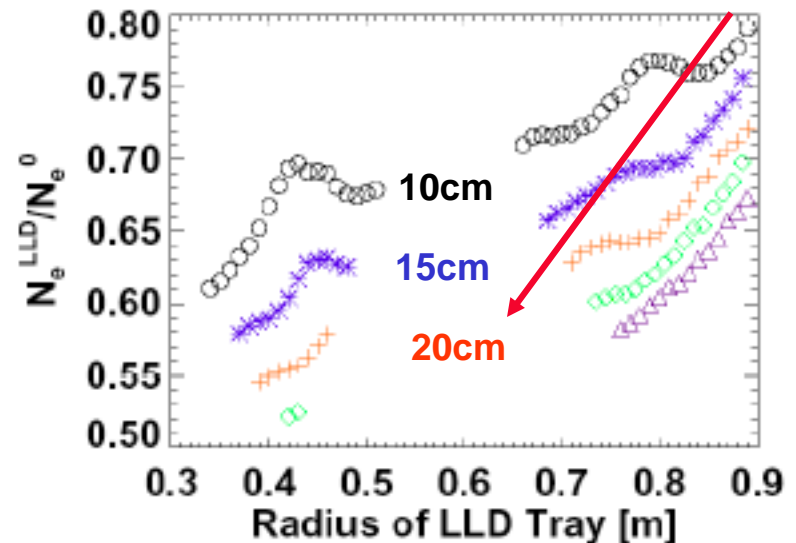
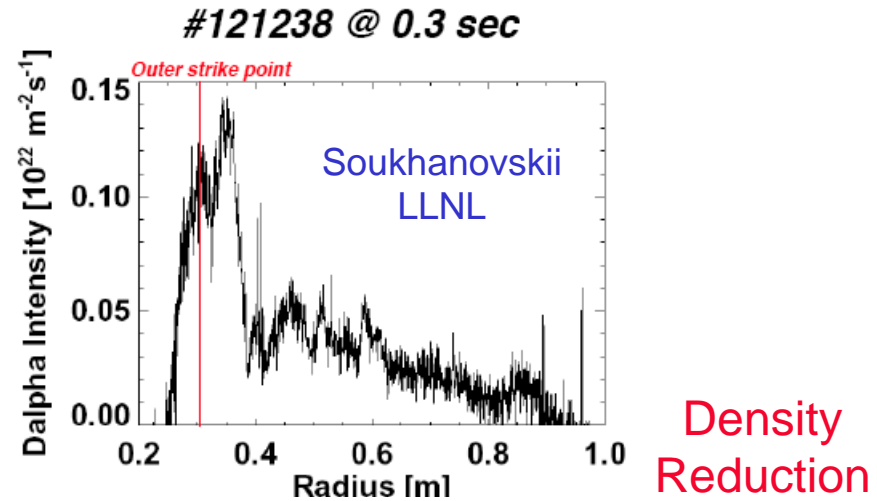
# Pumping by LLD-1 20 cm Wide on Outer Divertor Will Provide Density Control for Inner Divertor Broad SOL $D\alpha$ Profile High $\delta$ Plasmas

- Density reduction will depend on proximity of outer strike point to LLD-1

High  $\delta$  : reduce  $n_e$  by 25%



R. Maingi, ORNL



Shown for different LLD-1 widths



# LLD-1 Design Derives from Extensive International Liquid Lithium R&D

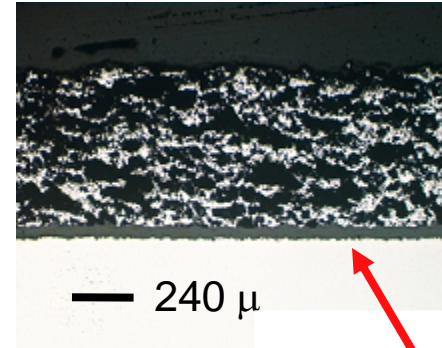
- Lithium surface tension forces in capillary media (metal wire meshes, metal felts, sintered metals, flame-sprayed porous metals) have been shown to form, control, confine, and redistribute liquid Li uniformly over plasma-wetted surface in presence of  $J \times B$  forces, gravity, and thermal gradients.
  - No thermal induced cracking in lithium filled medium
  - No fatigue
  - No radiation swelling
  - Exiting flows can remove codeposition
  - Continuous flow provides replenishment during erosion
  - ➔ – *Provides recycling control*
  - ➔ – *Provides impurity control*
  - ➔ – *Provides low collisionality edge conditions*
  - ➔ – *Maximum allowable incident heat fluxes  $> 100 \text{ MW/m}^2$* 
    - **Examples: Mo wire meshes [T-11, FTU], flame-sprayed porous Mo [LTX]**
- LLD-1 design and plans are following an integrated R&D approach

# Integrated Approach: LTX R&D Aiding in Performance Projections and Design of NSTX LLD-1

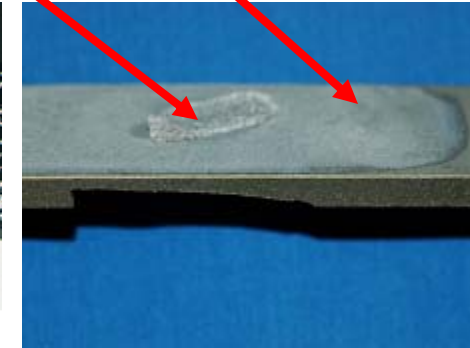
- LTX is preparing to begin lithium operations
  - Recycling on liquid Li at more relevant edge parameters than CDX-U
  - Test plasma fueling w/ gas puffing, jets when recycling particle source is small
  - Examine Li sputtering w/ hotter edge

- LLD-1 relevant lithium wall implementations developed for LTX
  - NSTX & LTX have been working closely with Sandia to determine LLD-1 design for operations in FY09
  - Flame-sprayed porous Mo adopted for NSTX LLD-1 capillary surface

- **Solid Li melting**
- **Liquid Li flowing over porous Mo**



Micrograph of highly porous moly



Successful lithium wetting test on porous moly

- **Candidate LLD-1 porous molybdenum surface -**
  - Originally developed for 2<sup>nd</sup> LTX shell (Phase II SBIR w/ Plasma Processes, Inc.)

R. Majeski, R.Kaita



# NSTX-SNL Collaboration Has Considered Two Candidate Surfaces for LLD-1

- Two candidate Li surfaces have been under investigation

➔ 1) Thin flame sprayed porous Mo, on thin SS on thick Cu baseplate is highest confidence initial approach

- LTX style plate (tested offline)  
(prepared by Plasma Processes Inc.)

- Experiments and simulations of LLD-1 behavior (porosity, gravity, thermal, JxB forces) in progress (N. Morley, UCLA)

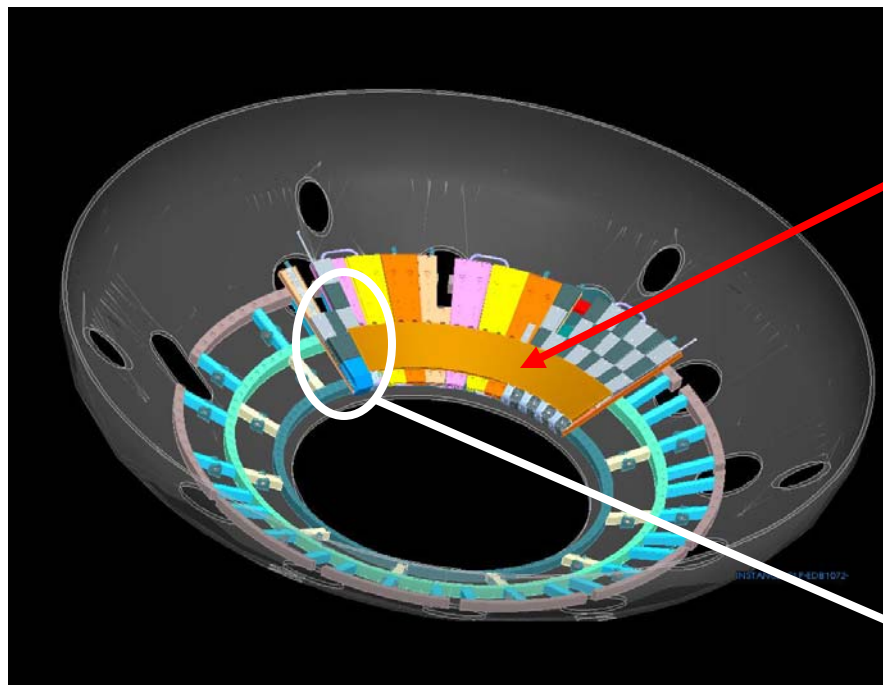
2) Chemical vapor deposited Mo on vitreous carbon mesh

- under investigation at SNL (not tested; testing planned)  
(prepared by Ultramet Inc.)

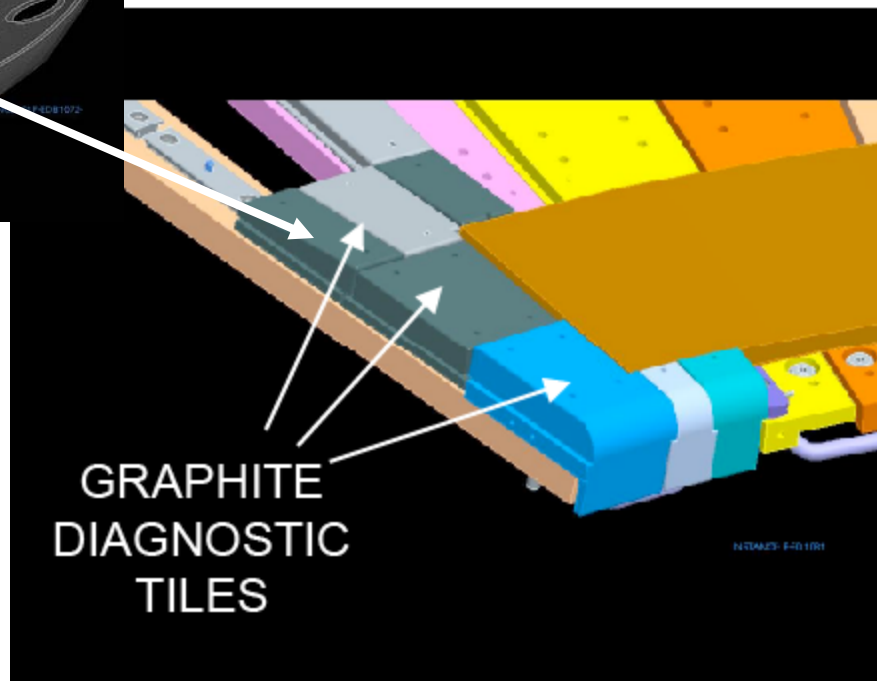
## • Key properties for an acceptable LLD-1 lithium surface

- ability of liquid Li to flow across a metal surface (wetting capability)
- minimize temperature rate of rise of Li → rapid heat transfer from Li to baseplate

# Plasma Facing Views of the Basic LLD-1 Copper Plate Substrate



- 4 Toroidal 90° segments separated by graphite Diagnostic Tiles

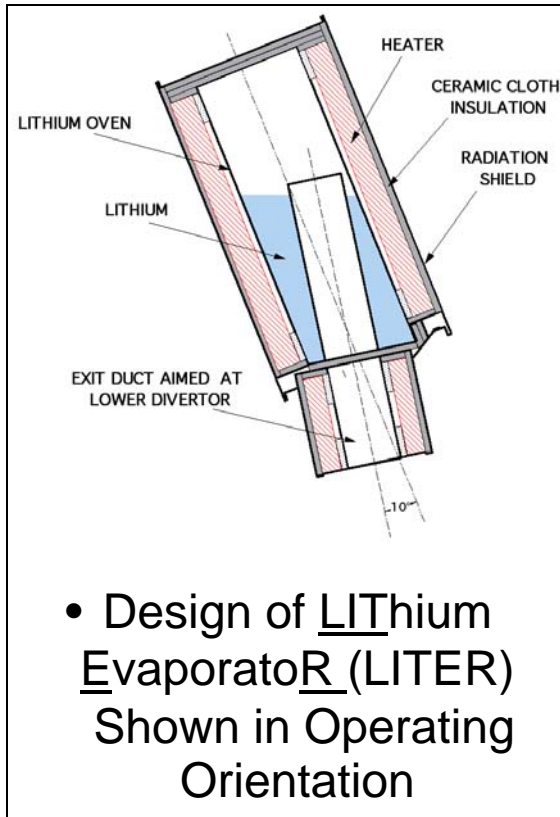


GRAPHITE  
DIAGNOSTIC  
TILES

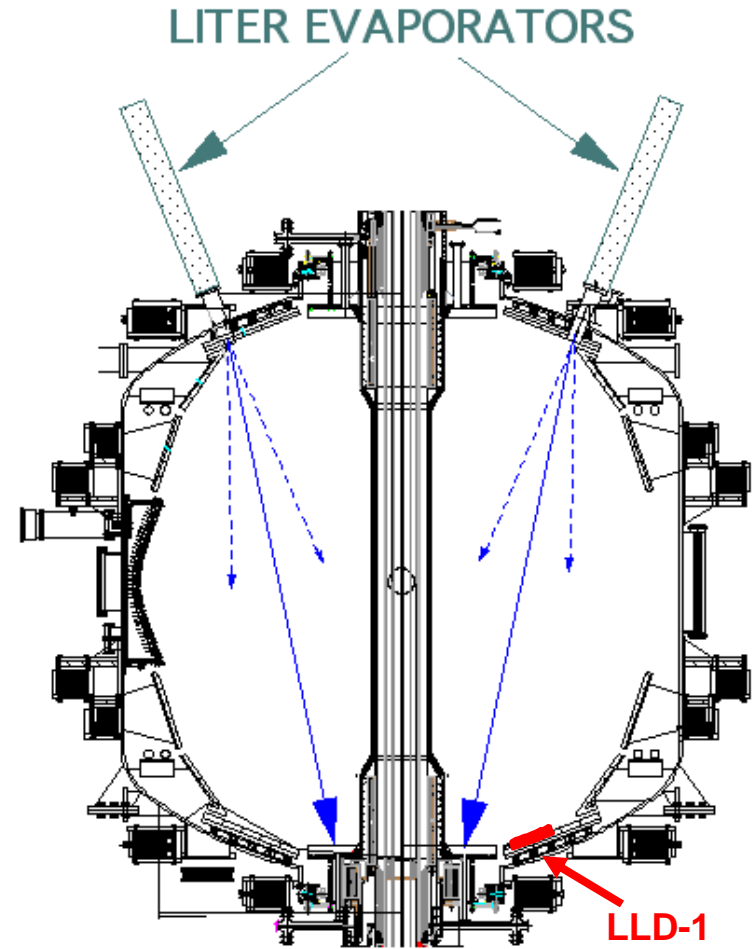
# LLD-1 Operation Requires Additional Diagnostics for NSTX Control and Characterization for Step Devices

- *Each LLD-1 90° segment has control and monitoring sensors:*
  - 12 thermocouples embedded in the heaters for monitoring heater limits
  - 12 thermocouples embedded in copper baseplate for monitoring heat transfer
  - 2 strips of 4 thermocouples each for torodial and radial temperature variations
  - 1 center post halo current Rogowski for monitoring JxB effects
- *Each set of inter-segment graphite tiles has diagnostic sensors:*
  - Bay H: existing 2D magnetic sensor array and 2 thermocouples
  - Bay B: 120 LP array with some UIUC signal conditioners for triple probes
  - Bay E and Bay K: 2 biased electrodes, 5 LP, 1 thermocouples
- *External Diagnostics:*
  - Bay H: Slow IR camera, Bay E: Fast IR camera
  - Bay G: Lyman- $\alpha$  Diode Array for recycling measurements at the LLD-1 highly reflective liquid lithium surface

# LLD-1 Li Surface Will Be Supplied Using the 2 LITER Units



- Photo of LITER on probe & loaded with Li under argon

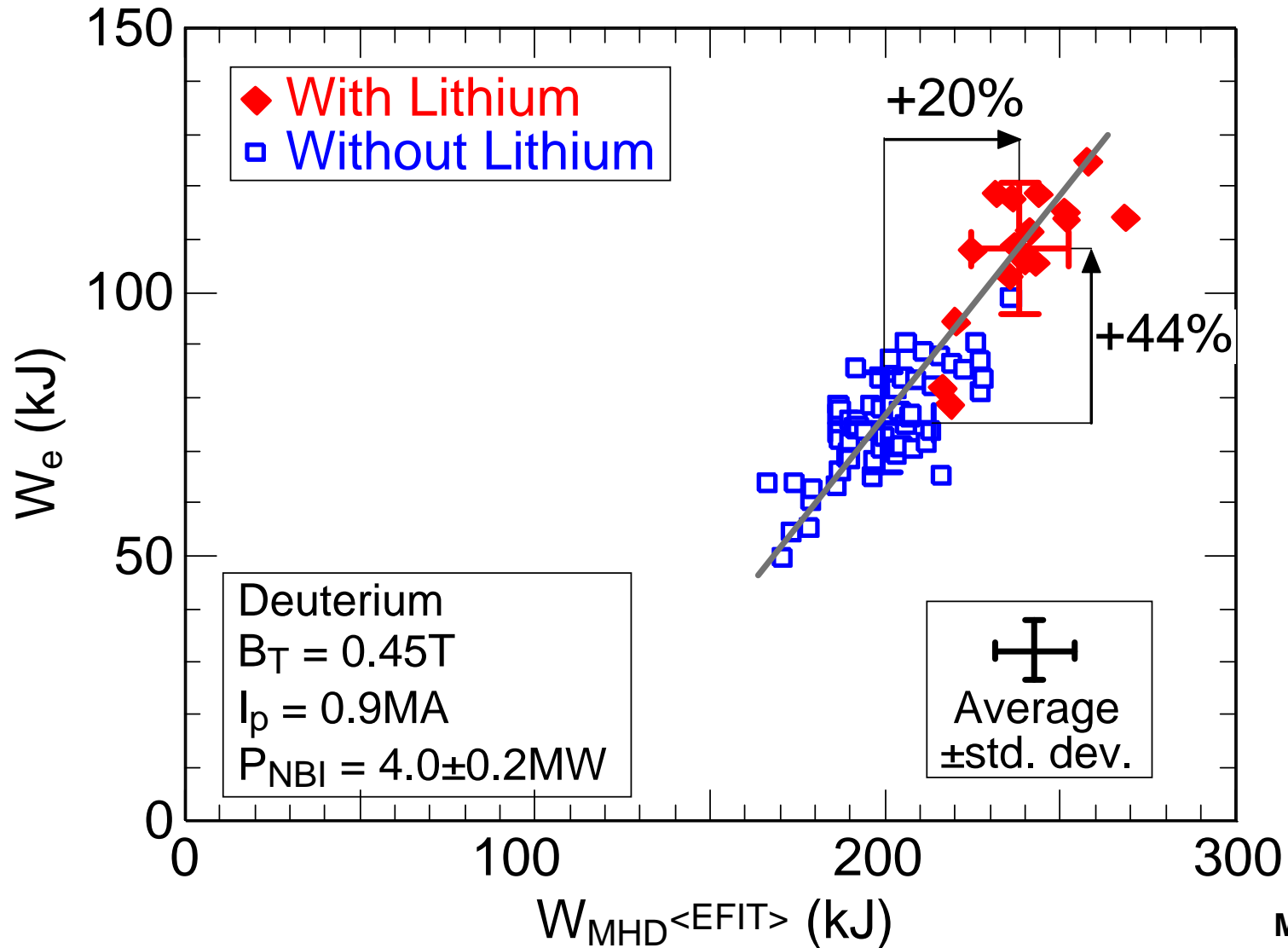


- LITER central aiming axis to graphite divertor and gaussian angle at 1/e (dashed)

# Dual LITER System Used Routinely as a New Operational Capability for Establishing Lithium Wall Conditions

- In recent experiments, the dual LITHium EvaporatoR (LITER) evaporated 120g of Li into NSTX (+60 g on LITER shutters)
  - The LITERs deposited lithium on the lower divertor target for 10 min, at combined rates of 10-70 mg/min
  - Prior to each discharge, the LITERs were withdrawn behind shutters
  - If HeGDC was applied, the shutters remained closed
  - The shutters were then reopened as soon as the diagnostic window shutters closed, and the deposition cycle repeated
  - Became routine operational tool used to establish lithium wall conditions
    - used for many FY08 experiments; the next slides show some of the initial results.

# Stored Energy ( $W_{MHD}$ ) Increases After Li Deposition Mostly Through Increase in Electron Stored Energy ( $W_e$ )



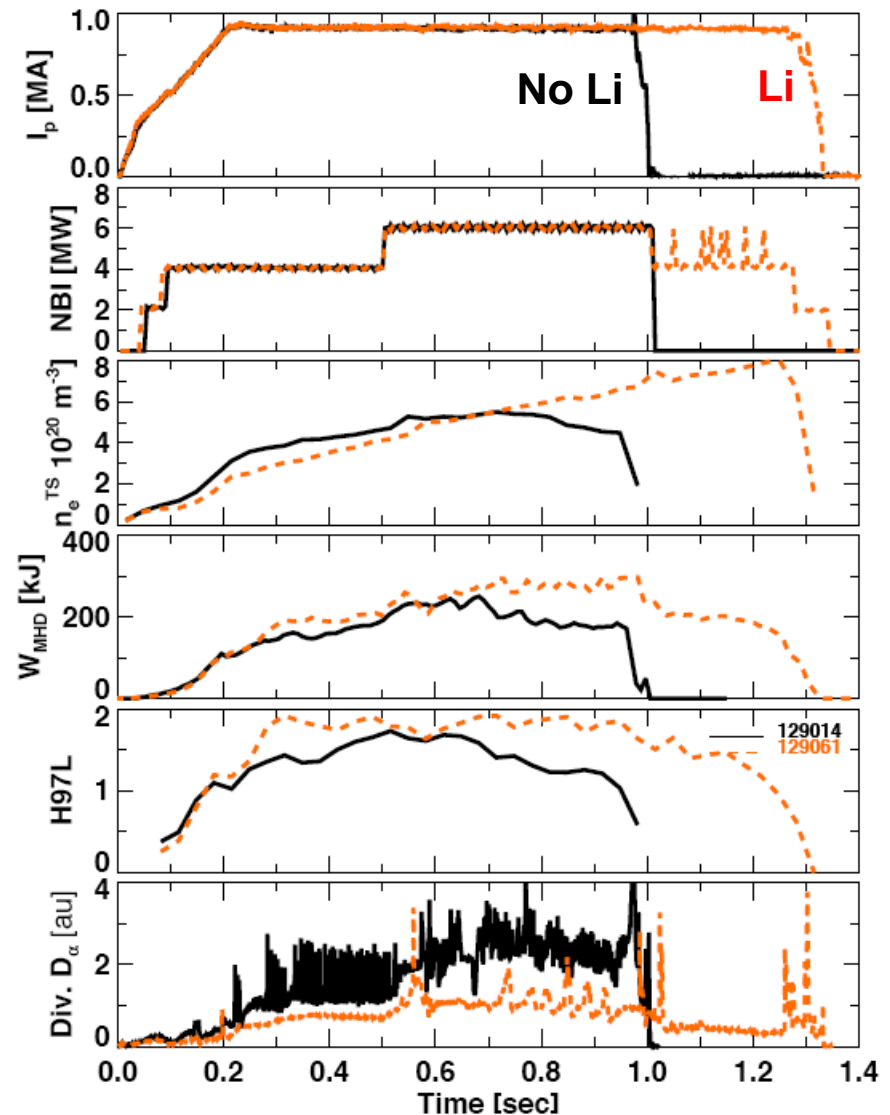
M. G. Bell



# Solid Lithium Surface Coatings

## Increase Confinement, Stored Energy, and Pulse Length

- Comparison for pre-Li and post-Li reference shots with constant NBI, constant external gas, etc.
- Lithium (188 mg) reduced density in initial period up to 0.6s
  - pre-Li discharge was ELMy
  - ELMs were absent on Li shot
- In time, the lack of ELMs causes the density in the discharge with Li to overtake the shot without Li.

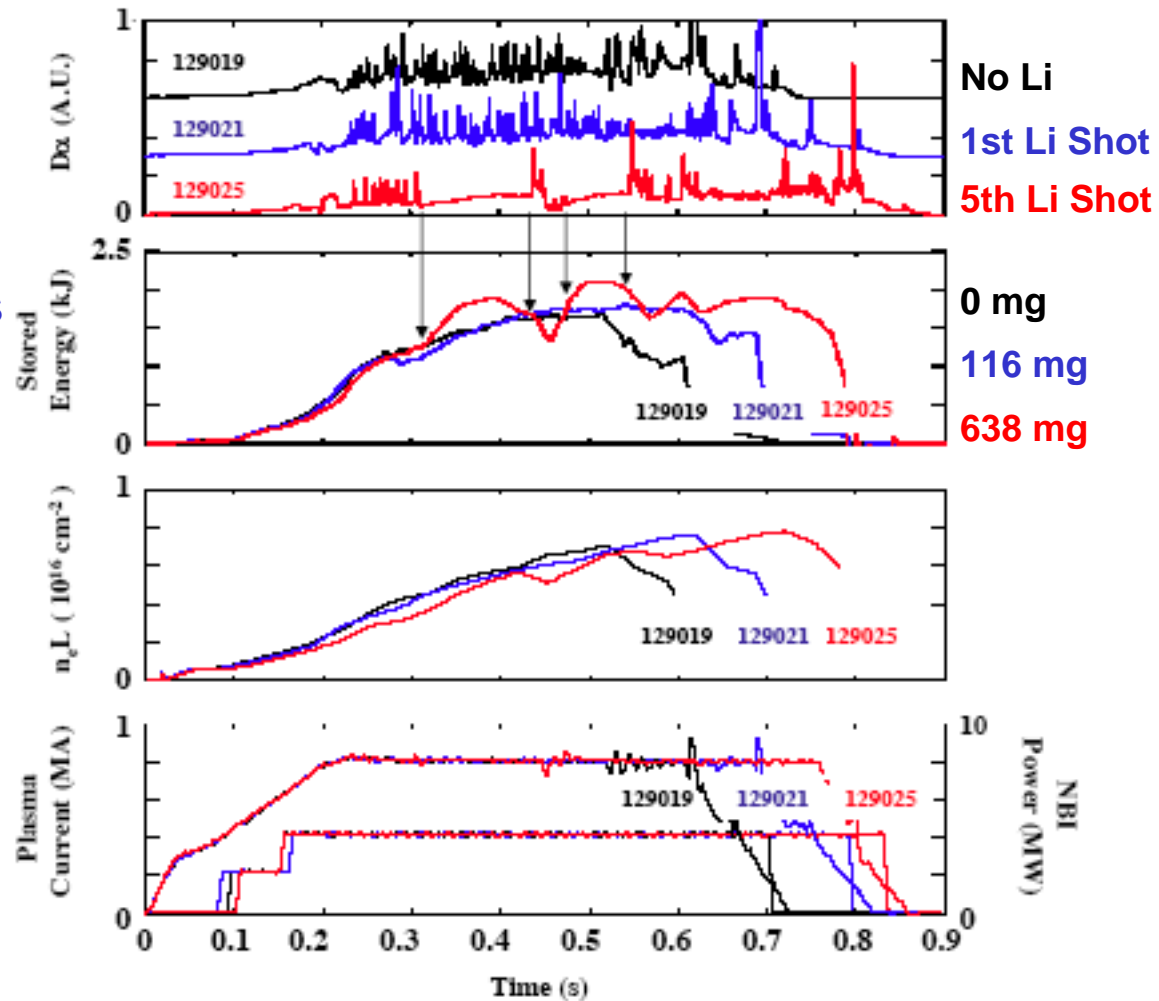


R. Maingi, ORNL

# ELM Suppression by 5<sup>th</sup> Discharge With Li

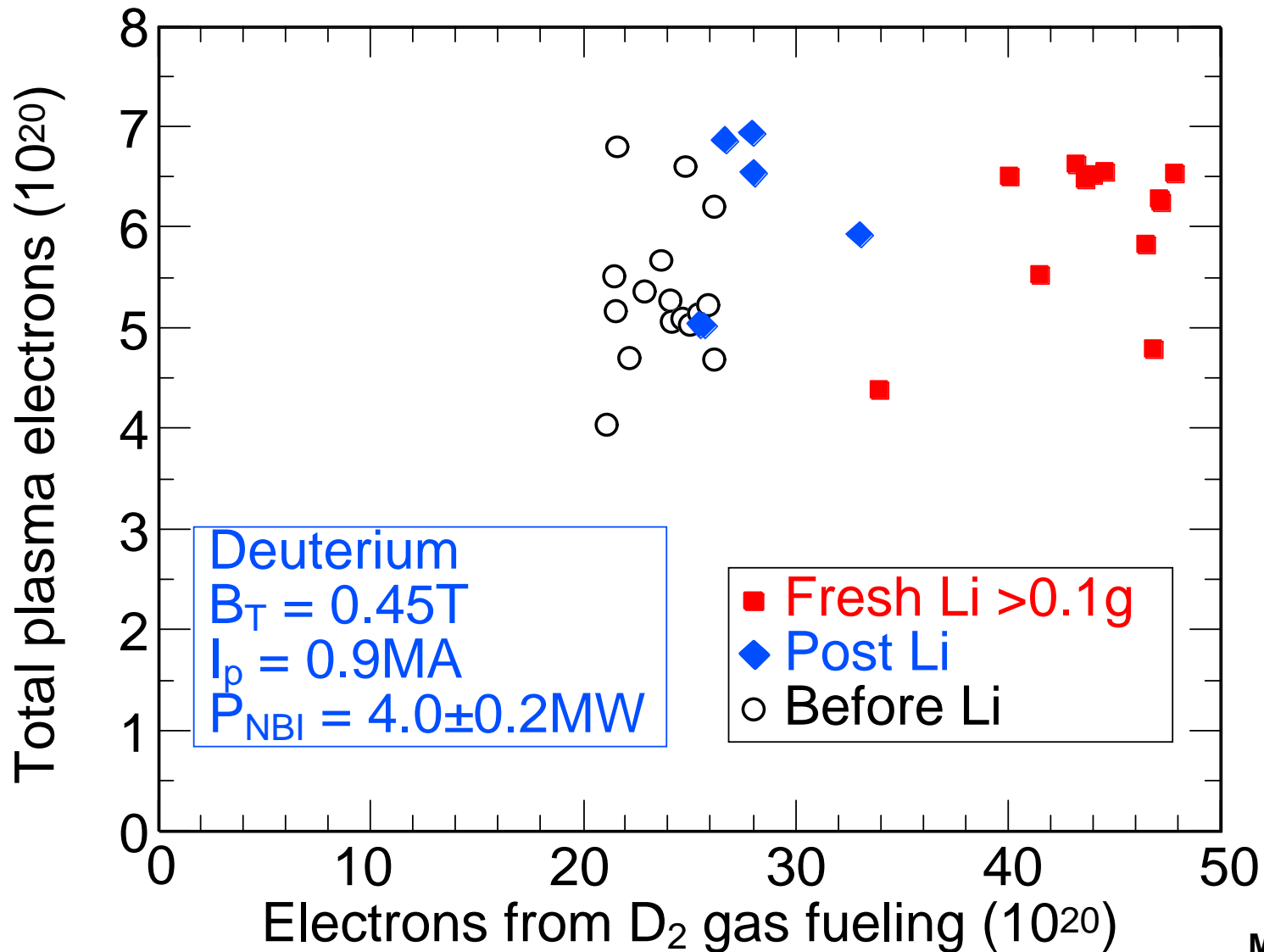
## No ELMs $\Rightarrow$ Immediate Increase in Stored Energy

- As Li increases
  - ELMs decrease
  - Stored energy increases
  - Pulse lengthens
- At higher Li evaporation rates and higher PFC accumulations, complete ELM suppression occurs  $\Rightarrow$  higher confinement\*



\* D. Mansfield, PSI08, O-28

# Lithium Edge Conditions Require Large Fueling Increases to Maintain Density

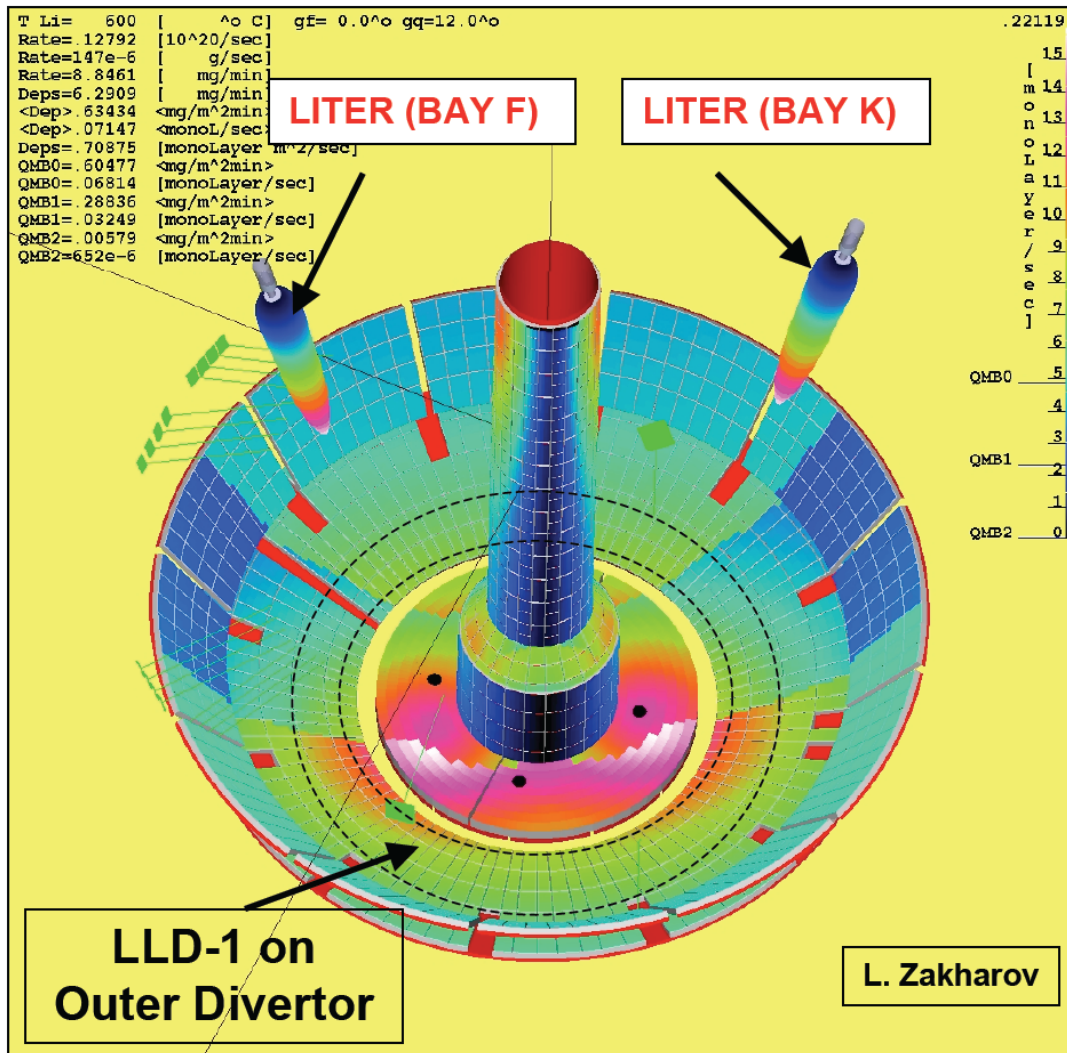


M. G. Bell

# LITER Technical Success Demonstrated by Initial Results of Evaporated Lithium Surface Coatings

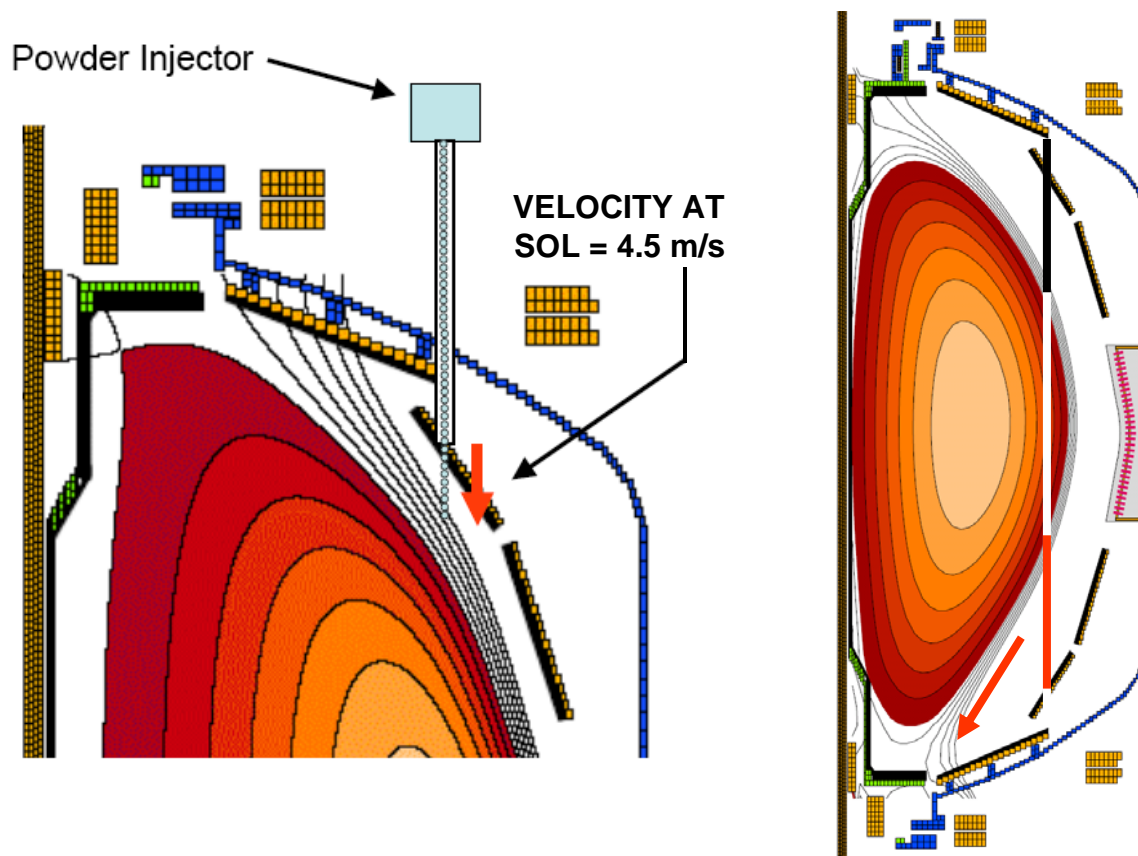
- The effects of the active lithium surface coatings on standard discharge scenarios include:
  1. Reduced plasma density in the early phase of the discharge
  2. Suppression of ELMs
  3. Improved energy confinement
  4. Reduced flux consumption and increased pulse length for standard, high-triangularity discharges
  5. Reduced HeGDC time between discharges to maintain the H-mode
  6. Increased pedestal electron and ion temperature
  7. Reduced SOL plasma density and edge neutral density
  8. Discharges after lithium also benefited from  $n=1$  and  $n=3$  mode control by the external non-axisymmetric coils to reduce deleterious MHD activity.

# LLD-1 Will Be Loaded With Lithium Using LITER



- **LITER Deposition Capability**
  - for LLD-1 to pump NSTX plasma from  $7 \times 10^{13} \text{ cm}^{-3}$   $\rightarrow$   $5 \times 10^{13} \text{ cm}^{-3}$  will require the absorption of  $2.4 \times 10^{20}$  D particles, every particle confinement time ( $\sim 50 \text{ ms}$ ), for 1000 ms, for a total of  $4.8 \times 10^{21}$  D particles absorbed.
  - for a 1:1 D/Li ratio requires at least  $5.5 \times 10^{-2} \text{ g}$  of lithium ( $2 \mu\text{m}$ ).
  - present LITER deposition efficiency on to LLD  $\sim 7\%$  of it total output, then the total lithium need is 0.79 g.
  - using two evaporators at 30 mg /min (FY07 typ) will require about 13 min to coat the LLD-1.
  - if lower concentration ratio 0.1D/Li is required, then need 7.9 g of lithium ( $20 \mu\text{m}$ ), or 4 g per LITER, operating at 100 mg/min for 40 min.

# New Li Powder Injection Capability Will Be Tested Offline for Potential for Reloading LLD-1 Prior to Discharges



- Li powder injected during breakdown and early in discharge reaches lower divertor
- Recent initial results indicate Li powder (50  $\mu\text{m}$ ) injected early in discharge yielded higher, and broader temperature profiles earlier in the discharge

D. Mansfield DPP, APS, 2008

- Laboratory experiments are planned to test if this new capability for present discharges can be used to reload the LLD-1 prior to a series of discharges

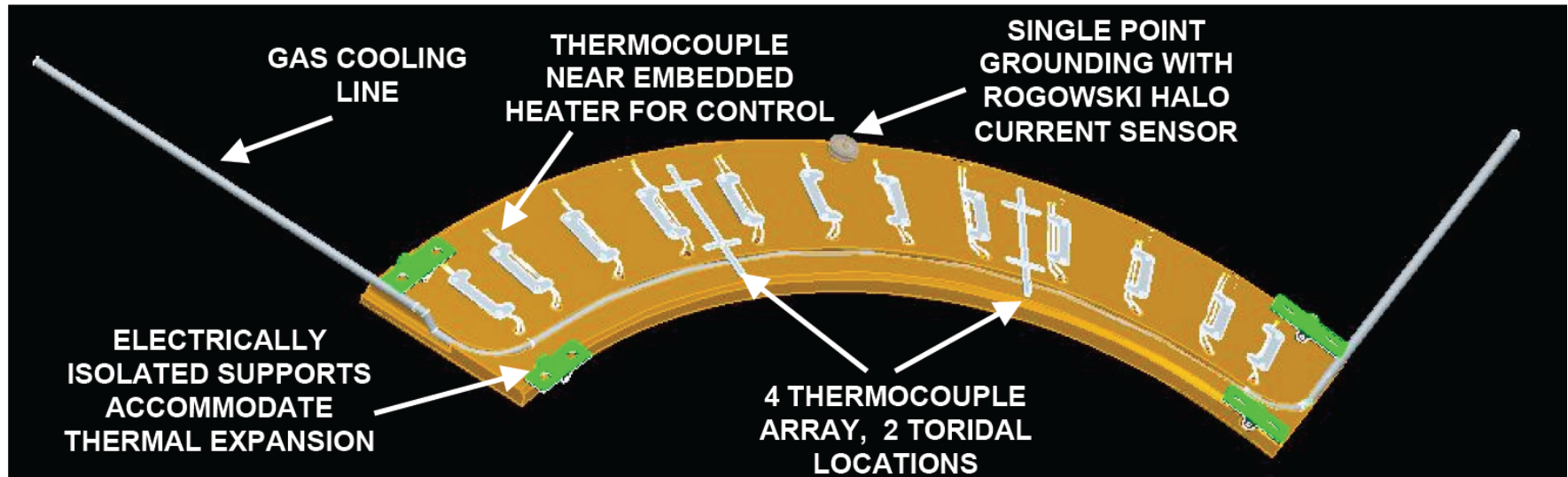
# NSTX Will Test the Potential Benefits of Liquid Lithium Divertor for Integrating High Plasma and PSI Performance

- LLD-1
    - *The Outer Divertor is the initial lowest technical and programmatic risk location for LLD-1 to the high performance, high  $\delta$ , ST research program*
    - LLD-1, 20 cm wide pumping on Outer Divertor provides reduction in density for increased neutral beam current drive capability
  - LLD-2
    - Enable  $n_e$  scan capability in long pulse H-mode
      - Increase filling rate ( powder, capillary) to wider area Mo mesh surface
      - Test ability to operate at significantly lower density (NHTX, CTF)
  - LLD-3
    - Investigate power handling for long-pulse with high heat-flux
      - *long pulse (5s) power handling surface with active cooling (capillary flows, swirl tubes, hypervaportrons, evaporative cooling) for 16 MW (2NBI + RF) operation*
      - Higher lithium fill rates (capillary flow replenishment planned for FTU)
- LLD-1 Status
    - Final Design Review successful. Final drawings submitted by SNL for procurement.
    - Successful CDR for LLD-1 Diagnostics. LLD Controls FDR scheduled for Sept.
    - Planning to complete installation in 2008 for FY09 operation.

# Backup



# Bottom View of LLD-1 Copper Substrate Plate Showing Controls and Sensors



- 12 heaters (240v) each with embedded TC for monitoring heater limits
- 12 TC embedded in copper baseplate for monitoring heat transfer
- 2 strips of 4 TC each for monitoring torodial and radial temperature variations
- 1 Center post halo current Rogowski coil for monitoring JxB effects