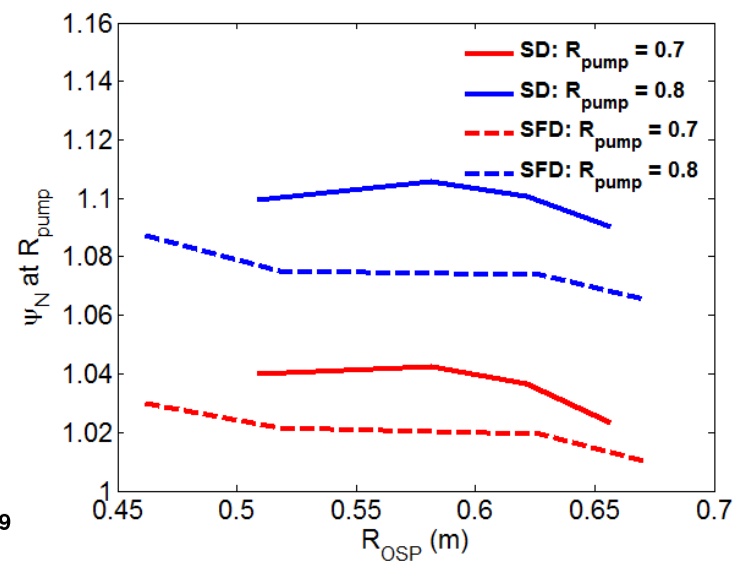
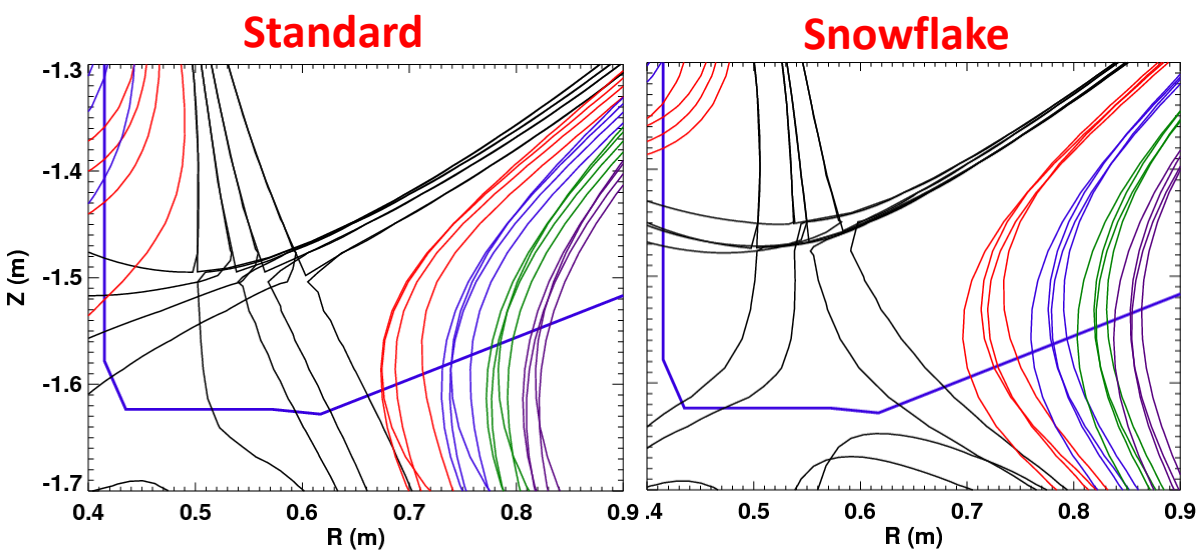


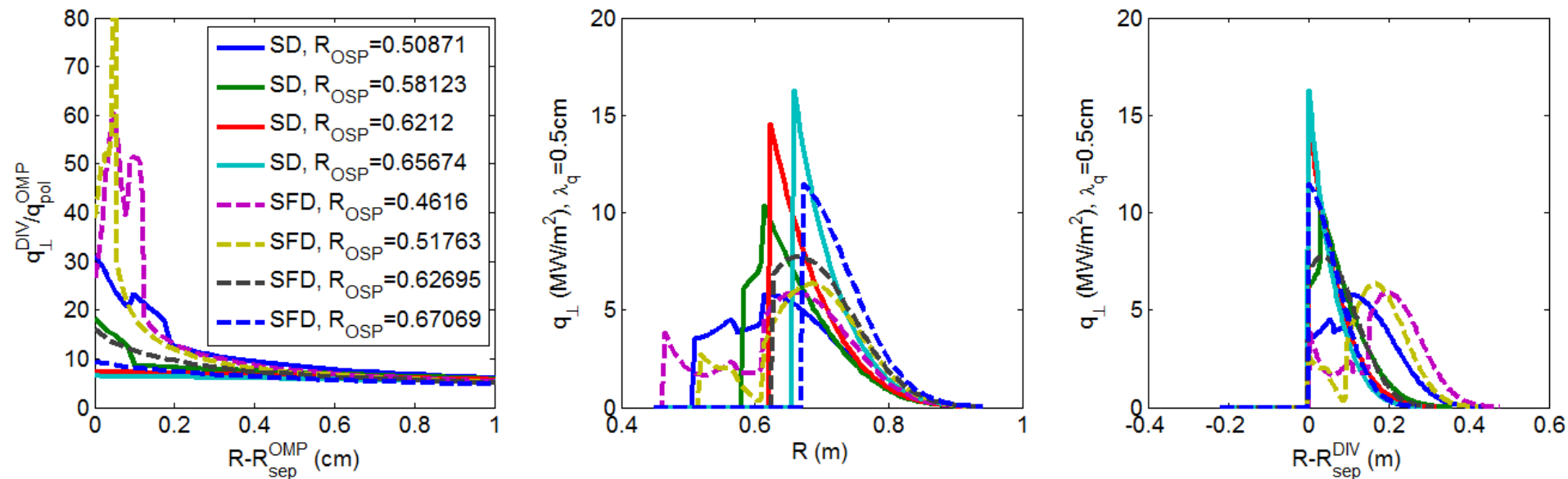
Moving R_{OSP} doesn't change ψ_N at pump entrance very much

- Two sets of equilibria considered
 - Standard divertor, R_{OSP} at four positions
 - Snowflake, again R_{OSP} scan
- Contours: $\psi_N = 1.0, 1.03, 1.06, 1.09, 1.12$
- Strike points for $\psi_N > 1.0$ move much less than separatrix
 - ψ_N at likely pump positions varies weakly with R_{OSP}
 - Moving R_{OSP} outwards towards pump doesn't help much until R_{OSP} is very close to pump

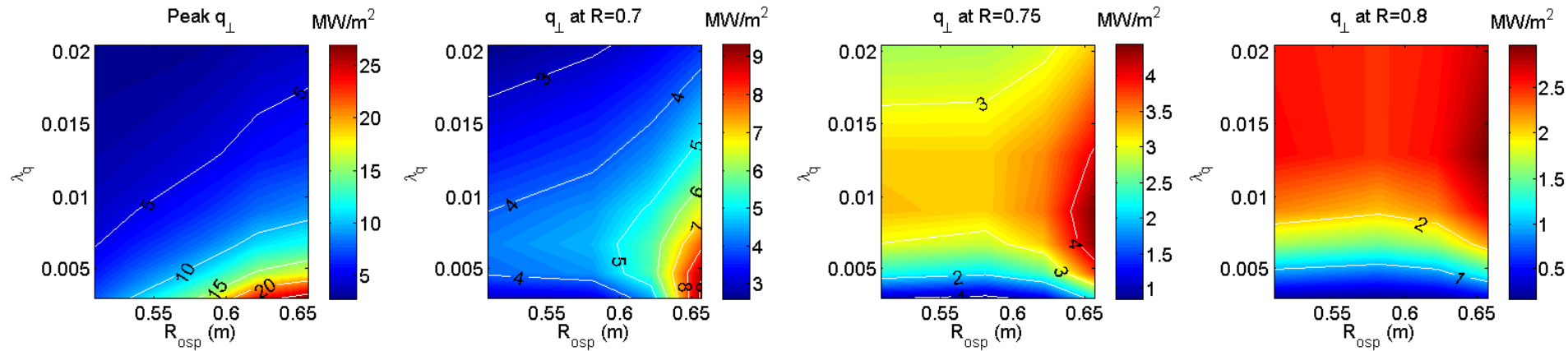


Projecting heat flux profiles

- Exponential poloidal heat flux profile imposed at midplane
 - P=5 MW (e.g., 1/2 of 10 MW goes to outer divertor)
 - $\lambda_q^{\text{OMP}} \sim 0.3\text{-}2.0$ cm
- Mapped along field lines to divertor
 - Total geometric heat flux reduction factor shown on left
 - Example heat flux profiles showing for $\lambda_q^{\text{OMP}}=5\text{mm}$
 - Lots of heat flux at R=0.7, not much at 0.8

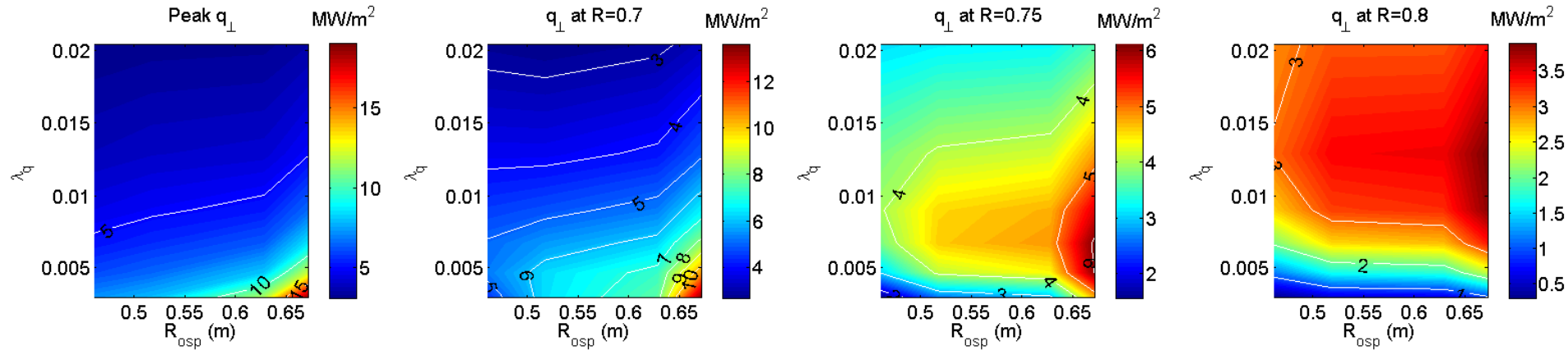


Heat flux at pump locations: standard divertor



- To keep peak heat flux $< 10 \text{ MW/m}^2$
 - $R_{\text{OSP}} < 0.55 \text{ m}$ **OR**
 - $\lambda_q > 8 \text{ mm}$
- With pump entrance at $R=0.7\text{m}$, heat flux is $>3 \text{ MW/m}^2$ for all heat flux widths, OSP positions
- $R=0.75 \text{ m}$: pumping only ok ($q_{\perp} > 2 \text{ MW/m}^2$) for $\lambda > 5 \text{ mm}$
 - Can't beat this by moving OSP to larger $R \Rightarrow q_{\text{pk}}$ becomes too large
- $R=0.8 \text{ m}$: pumping works only for $\lambda > 8 \text{ mm}$

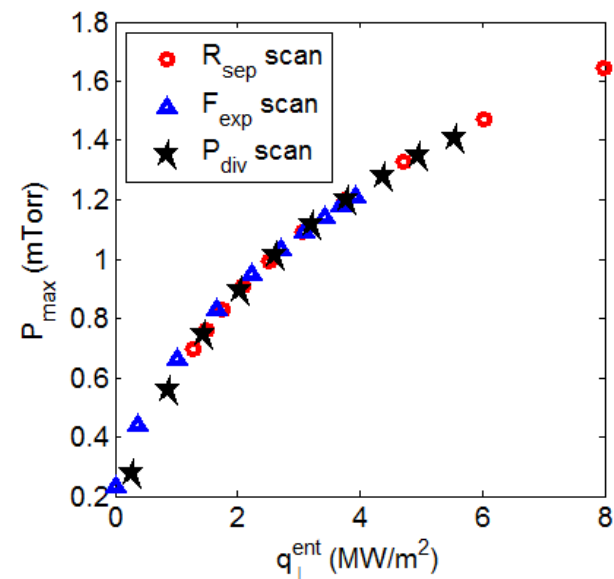
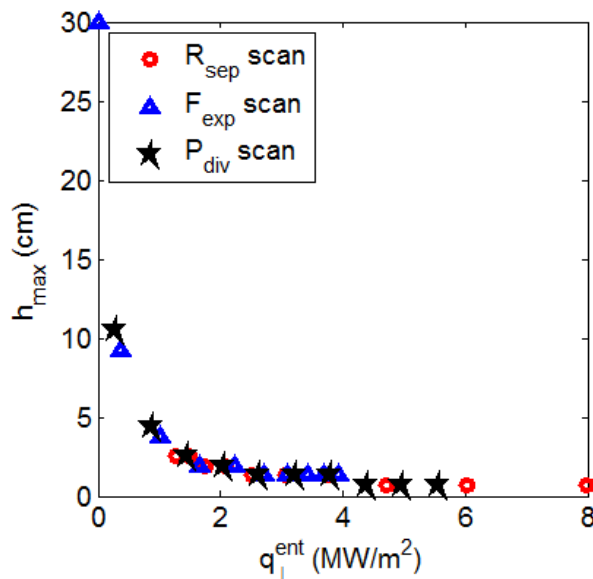
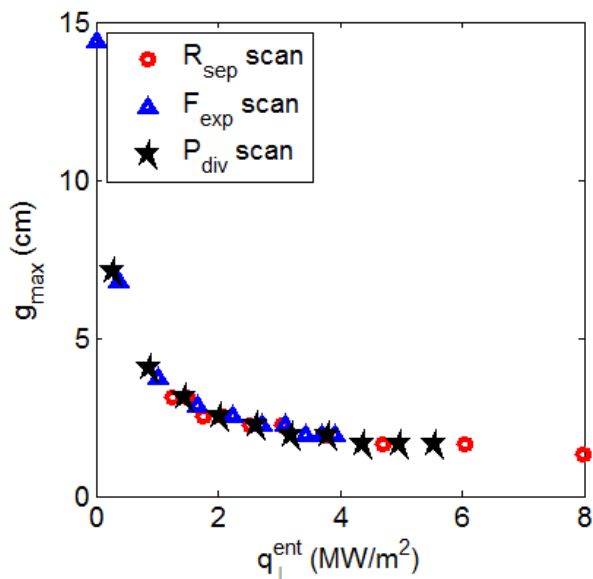
Heat flux at pump locations: snowflake divertor



- Power handling:
 - Region with $q_{pk} < 10$ MW/m² is a bit larger than SD
 - R_{OSP} can be moved out to ~ 0.6 m even for the narrowest SOL
- Pumping:
 - Works a little bit better than SD
 - Large flux expansion puts higher fluxes in the far SOL locations of the pump
 - Pump entrance at either R=0.7 or 0.75 m should work for basically any SOL width
 - R=0.8 only works for $\lambda > 5$ mm

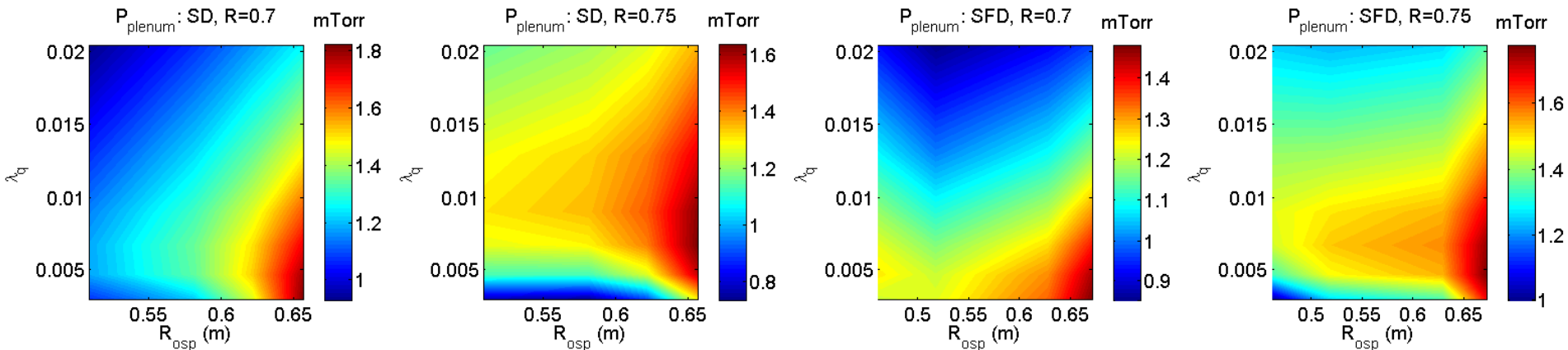
Updating duct optimization for likely entrance position

- Looks like $R=0.7$ is good position for duct entrance
- New analytic calcs performed for new (old) parameters
 - $R_{\text{ent}} = 0.7$ (0.9) m
 - Field line angle = 3.0° (5.0°)
 - $T_e = 15.0$ (10.0) eV
- Need $q_{\perp} \sim 2 \text{ MW/m}^2$ to reach 1 mTorr
 - $g \sim 2.5 \text{ cm}$, $h \sim 2.0 \text{ cm}$



Projecting plenum pressure

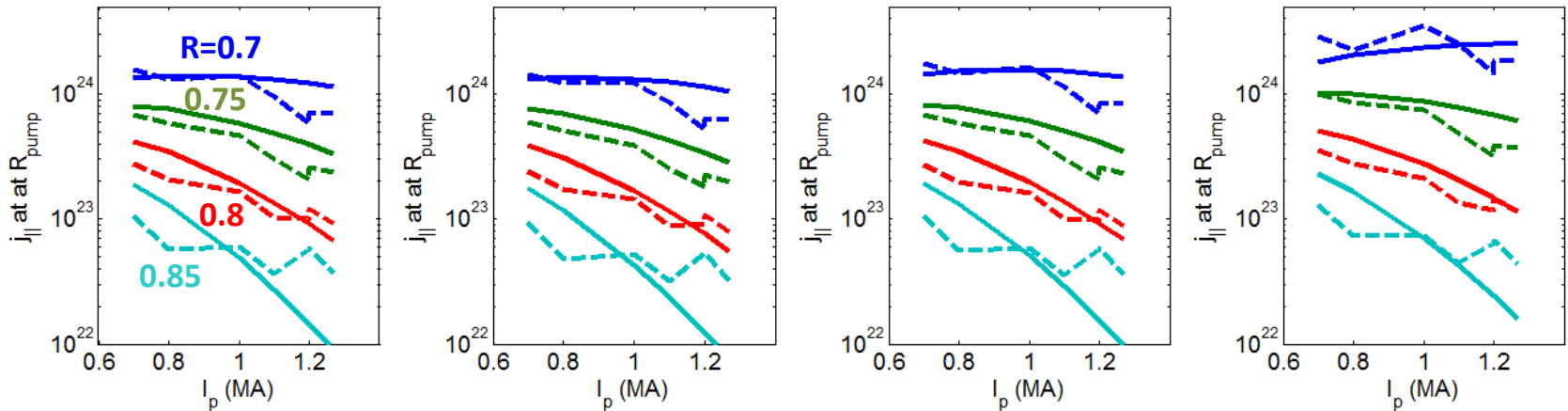
- Fix g/h of entrance at 2.5/2.0
- Use profiles directly in pressure calculation (including angles)
- Results consistent with heat flux arguments
 - R=0.7 or 0.75 should ~work for all R_{OSP} , λ_q
 - Moving R_{OSP} increases pressure some, need R_{OSP} near R_{pump} to really make a difference
 - Snowflake has somewhat lower maximum pressure, but has better pumping at low λ_q
 - And you can move ROSP close to pump in snowflake without exceeding q_{\perp} limits



Sanity check of flux projections against LP data

- Probe flux at pump entrances ($R=0.7, 0.75, 0.8, 0.85$): dashed
 - From Mike's fits vs. ψ_N
- Projections based on heat flux: solid
 - λ_q from the same data set
- Not too shabby-especially if you plot it on a log scale

Standard



Snowflake

