Locked Modes and Error Fields in NSTX

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NSTX Results Review Wednesday, September 19, 2001



Measurement of low-frequency n=1 modes



6 large B_r sensors

- Opposing sensors are differenced in analog, then integrated
 - MDS+ tree archives uncompensated δB_r
 - J/K-D/E, A/L-F/G, B/C-H/I
 - Remaining calibration done in software (IDL)
- B_r sensors are mounted on PF5 coils
 - PF5 generates large apparent δB_r caused by:
 - Sensor misalignment
 - PF5 non-circularity

Nulling vacuum B_r requires several additional sensors



(B_R sensors designed by E. Fredrickson)



- Each B_r sensor has 2 B_v and B_{ϕ} sensors for misalignment correction
 - Signals summed for spatial averaging
- Flux loops
 - Wall loops used for B_r gain correction
 - Flux loop voltages used as source terms for modeling circulating eddy currents in passive plates and wall
- Flux loops essential to modeling vacuum response

Calibration steps for locked mode sensors (for deducing plasma-induced δB_r)

- 1. Calibrate VF and TF compensation sensors using PF3U/L, and TF
- 2. Correct for sensor misalignment with respect to TF
- 3. Correct for sensor misalignment with respect to VF from PF3U/L
- 4. Correct for sensor gain differences using B_r from wall flux loops
- 5. Subtract remaining static δB_r using coil currents
- 6. Subtract PF-induced δB_r using low-pass filtered loop voltages *Plate and wall 3D circulating eddy-currents* \Rightarrow 2-6 Gauss error fields
- 7. Subtract TF-induced δB_r using low-pass filtered dB_T/dt at sensors
- 8. Subtract any remaining TF pickup due to alignment changes
- 9. Subtract non-linear filtered I_{OH} x I_{TF} term, sometimes unipolar *Indicative of TF coil movement due to torque near CS, up to 6 Gauss error*
- 10. Remove PF5 supply switching noise with band-pass filter

Ohmic shots: often early and prolonged locking

VSTX

- "Reconnection event" collapse occurs near t=220ms
- Mode growth starts near t=160ms
- Mode persists for 100ms after collapse event



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Most NBI heated shots quiescent until internal modes are driven unstable

 $I_{\rm P}=1.2{\rm MA}$

 $\beta_{\rm t} = 17\%, \ \beta_{\rm N} = 3$

• No obvious early mode onset time

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• n=1 mode locks near Bays E-G



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Multiple IRE's exhibit successive locking

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- Again, no obvious early onset time
- Each IRE-driven mode locks near Bay G



Rotation dynamics of modes (a few examples)



- Long mode duration of 150 ms
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10 cm outboard gap

PF5 dominates δB_r pickup after compensation



- *Align with PF3U/L* ⇒ pickup from all other non-PF5 coils is small
- PF5 pickup is 2 orders of magnitude larger
 - Sensors in near-field
 - Coils are not circular
 - $-\delta B_r = 30-150$ Gauss measured at sensor

PF5-U/L coil shape inferred from δB_r and B_V

DNSTX

PF5L error field dominates



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n=1 error field contours from PF5 at 10kA



• Error field is localized to lower PF5 coil

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- 30-50 Gauss n=1 error field for typical PF5 current and 0cm gap
- 20-30 Gauss peak error field for 10cm gap

Expected locking position from PF5 error field



- Dominant expected locking position also localized to lower vessel
- Locking near Bays G or H predicted for modes near lower outboard mid-plane
- Nearly all modes should lock between C through H

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Summary

- Locked-mode detectors calibrated to ~ 1-2 Gauss level
 - Plasma n=1 mode amplitudes > 2 Gauss are obvious
 - Inferences about smaller mode amplitudes require some care
- High-current NSTX plasmas routinely show locking behavior
 - Many 400-600kA HHFW target shots are relatively quiet
- Infer from data that NBI-driven plasma rotation/shear likely suppresses locking activity (compare to HHFW, ohmic)
- Modes most often lock then decay near Bays G or H
 ⇒ Consistent with significant PF5 induced error field
- Likely difficult to take advantage of wall stabilization without fixing PF5 coils and/or adding correction/feedback coils.
 - Shifting PF5L and forcing it to be more circular would be helpful