

# Phased Array Operation with HHFW



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**NSTX Results Review**

**PPPL**

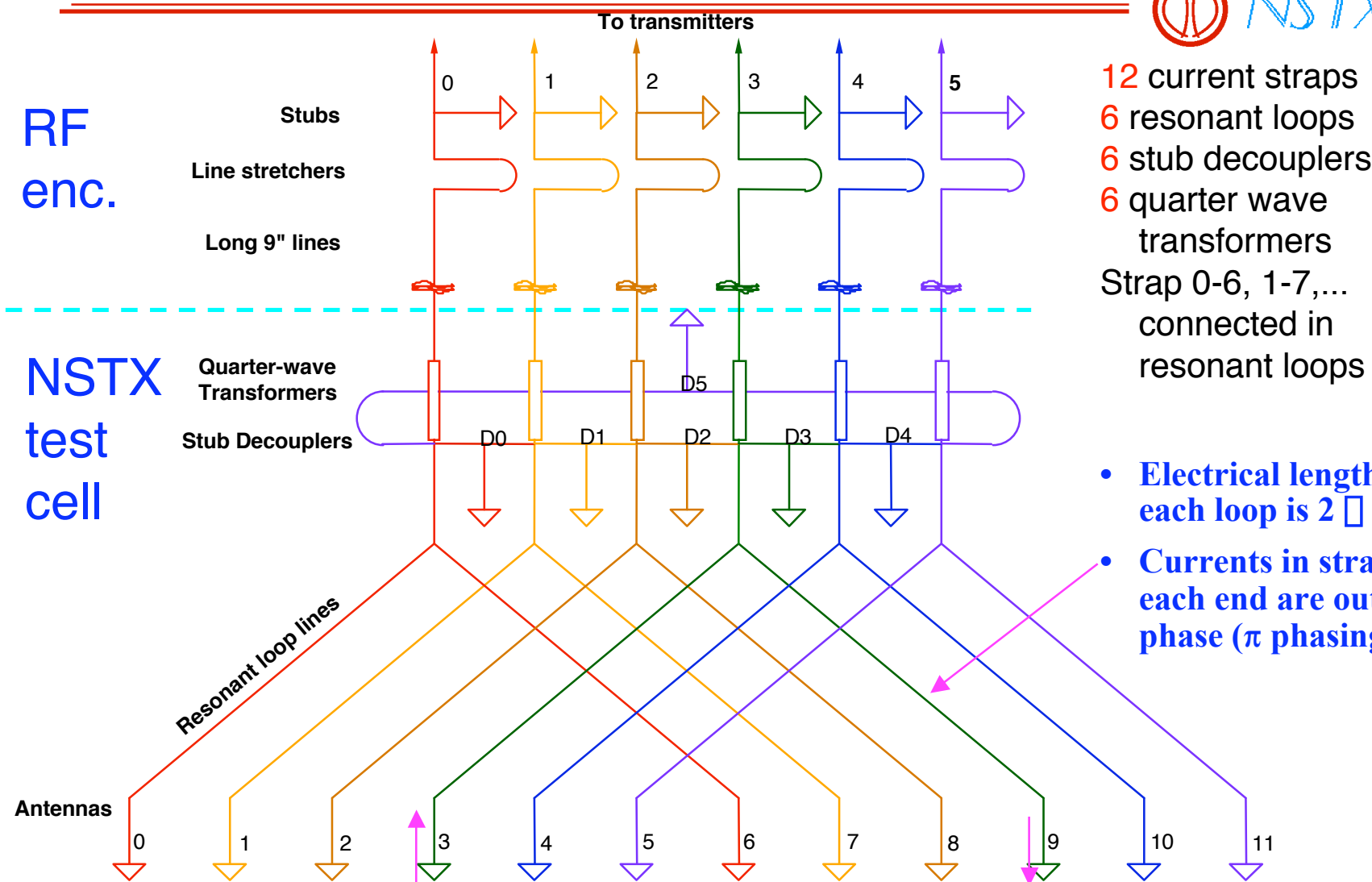
**September 10, 2002**

# Phased Array Operation with HHFW



- **Improved phase control**
- **Heating vs. array phasing ( $k_{\parallel} = 8 \text{ m}^{-1}$ )**
- **Plasma loading vs. array phasing**
- **Wave spectra**
- **Evidence for current drive**

# 6 transmitters: Fixed frequency, 30 MHz, drive resonant loops



- 12 current straps
- 6 resonant loops
- 6 stub decouplers
- 6 quarter wave transformers
- Strap 0-6, 1-7, ... connected in resonant loops

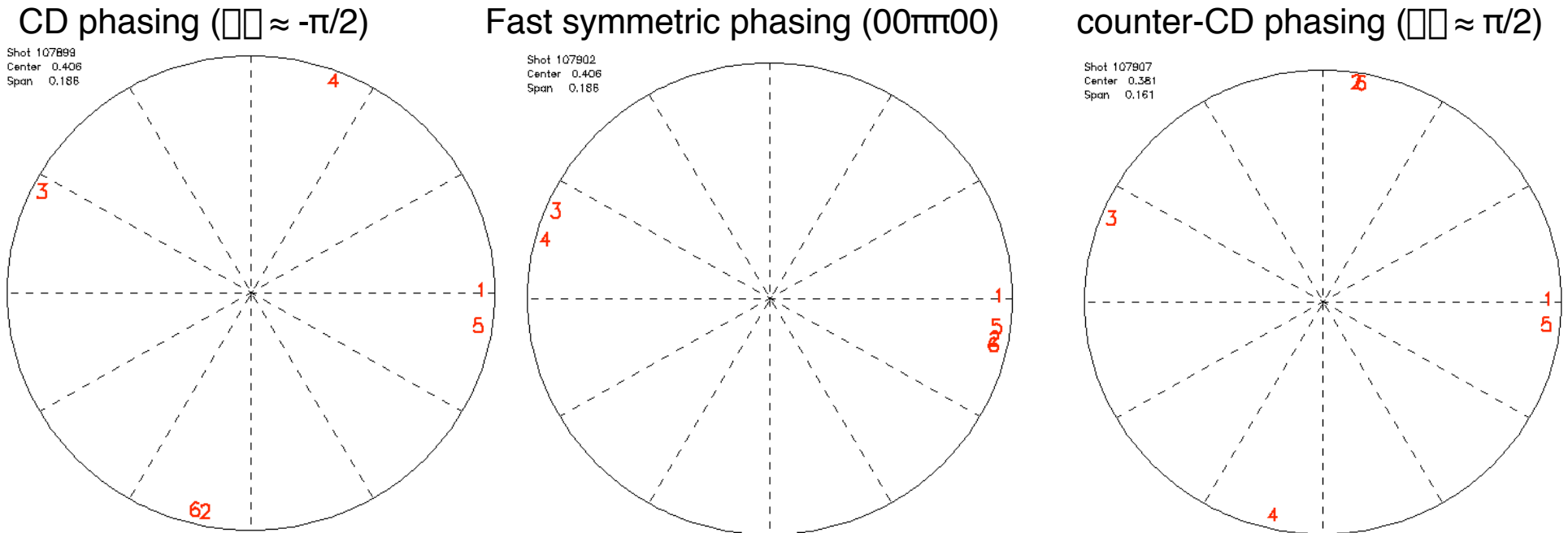
- Electrical length of each loop is  $2\lambda$
- Currents in straps at each end are out of phase ( $\pi$  phasing)

# Improved phase control system- dynamic phase change now possible



- **Inter-source phase control**
  - Set electronically via a computerized waveform generator
  - Feedback control of source phases to fix the phases of antenna currents
- **Can set for any inter-source phasing, and can vary with time during a shot**
  - Pre-programmed phase(t)
  - Operated with constant  $\Delta\phi$ , and changed  $\Delta\phi$  by  $45^\circ$  during a shot (e.g,  $90^\circ$  to  $45^\circ$ )

We have operated with some “Standard” phase settings....



# ANTENNA ARRAY PHASING EXPERIMENTS

## Heating, loading, current drive, etc.



We have done a series of experiments with different phasings to study the effects of phasing changes and to look for current drive.

- Heating efficiency *fairly insensitive* to phasing, as measured by stored energy
  - ◆ Possible improvement in stored energy with counter-CD ( $\phi = +\pi/2$ ) rel. to co-CD ( $\phi = -\pi/2$ )
  - ◆ Limited data at other phasings ( $\pm 60^\circ$ ,  $\pm 45^\circ$ ,  $\pm 30^\circ$ )
  - ◆ Counter-CD phasing gives higher central electron temperatures.
- Substantial *difference in loading* of the antennas for co- vs. counter current drive phasing
  - ◆ Agrees with theory when large pitch angle of the magnetic field is taken into account
- Current drive experiments *encouraging but not conclusive*, because we have no diagnostic yet for measuring central current density.

# Heating: confinement follows usual scaling



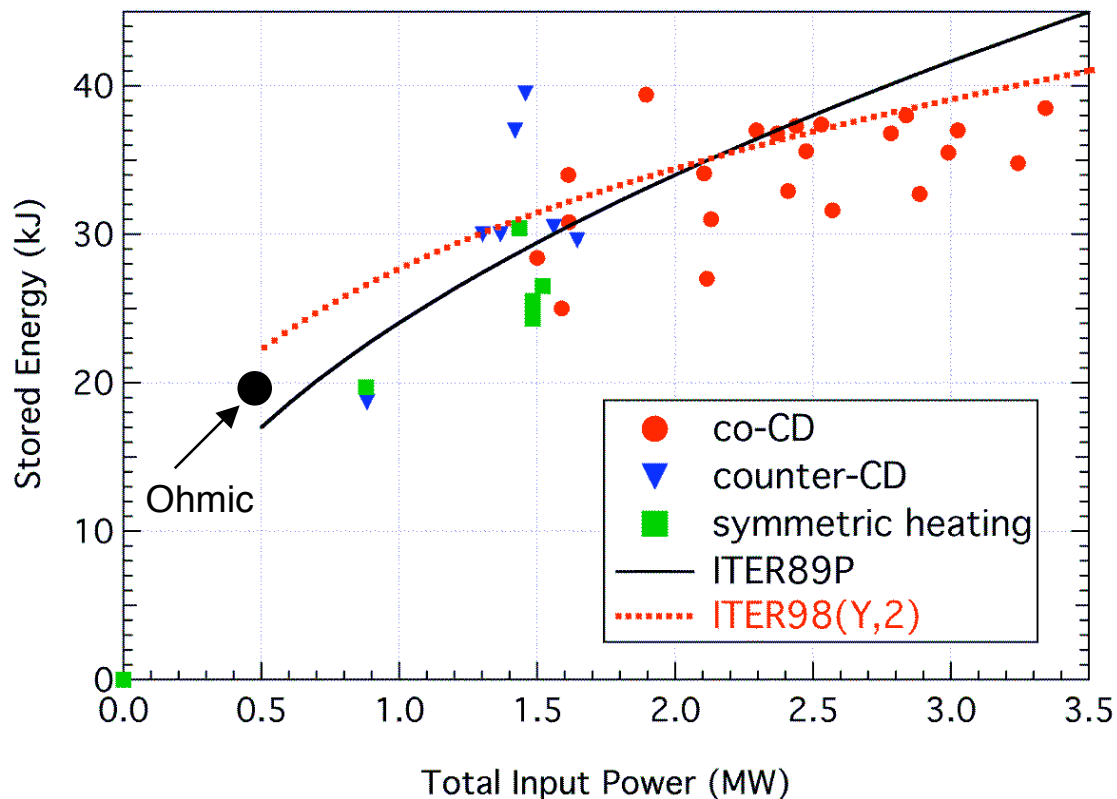
- Heating efficiency (as measured by total stored energy in plasma from EFIT) is *fairly insensitive* to phasing (slightly better for counter-CD?)
- Confinement comparable to calculated values using

- ITER89P scaling (black curve)
- ITER98(y,2) scaling (red curve)

Scaling calc. parameters:

- $I_p = 500$  kA
- $B_0 = 0.45$  T
- $\langle n_{20} \rangle = 0.1$
- $M = 2$
- $R_0 = 0.85$  m
- $a = 0.65$  m
- $\kappa = 1.7$
- $H = 1$

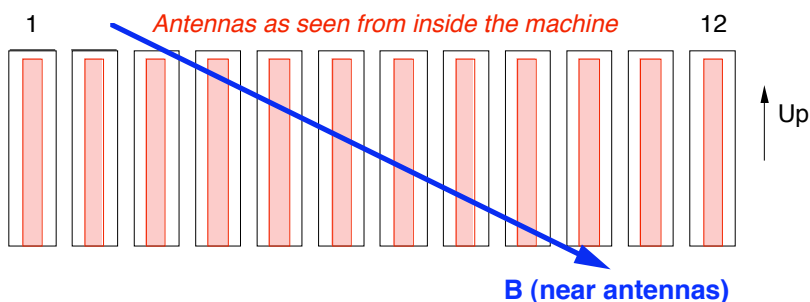
Stored energy vs. input power for co, counter, and symmetric phasing at  $8 \text{ m}^{-1}$



# Asymmetric plasma response to the wave direction results from large pitch angle of magnetic field

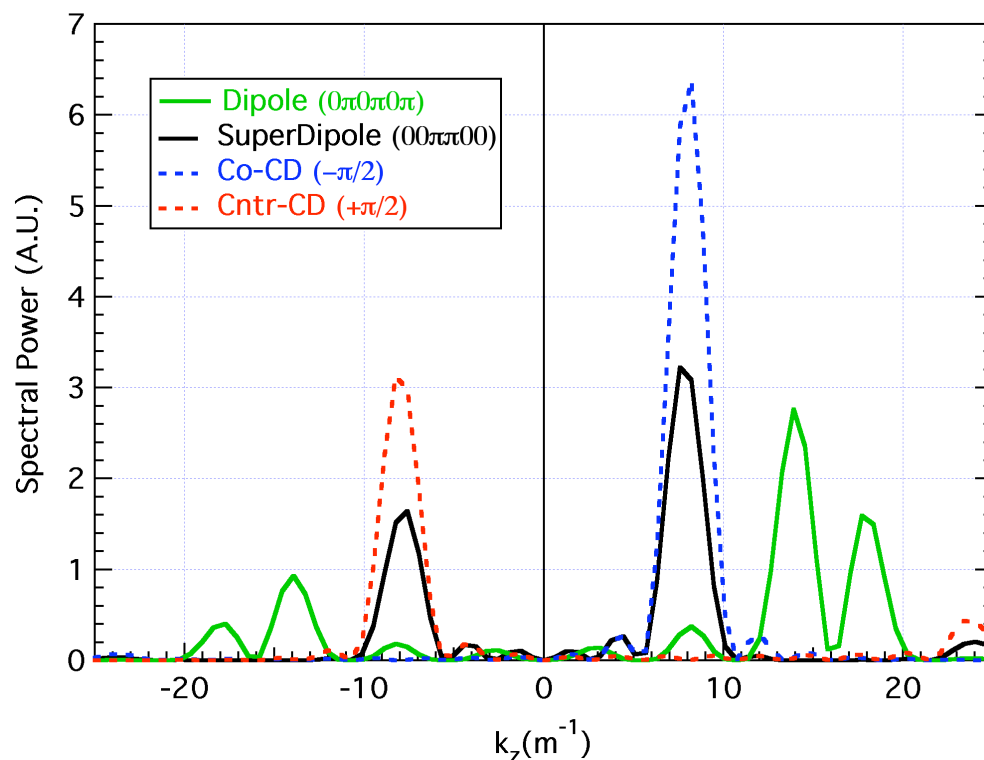


Pitch angle of the magnetic field at the antennas can be as large as  $45^\circ$



- Asymmetries between co-CD and counter-CD directions are more pronounced at higher wavenumbers.
- Asymmetric plasma response means even symmetric phasings can give rise to directional wave spectra.
- CD and “super-dipole” phasings give wave velocities resonant with 1.2 keV electrons.
- Dipole phasing gives rise to waves resonant with 250 and 400 eV electrons

$k_z$  power spectrum from GLOSI/RANT3D calculations

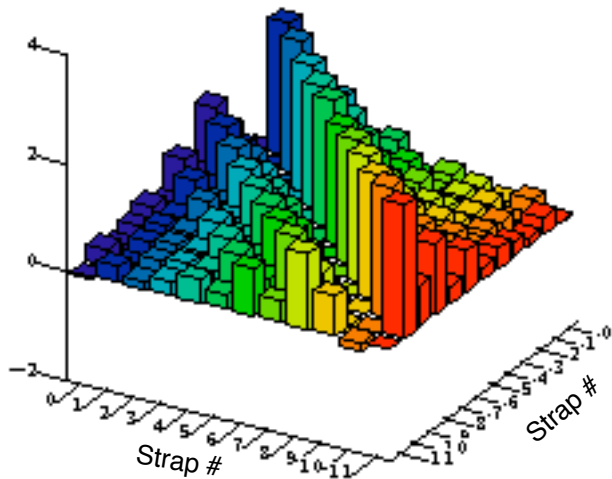


## We understand the loading asymmetry between co-CD and counter-CD phasing and can calculate the full 12x12 strap impedance matrix

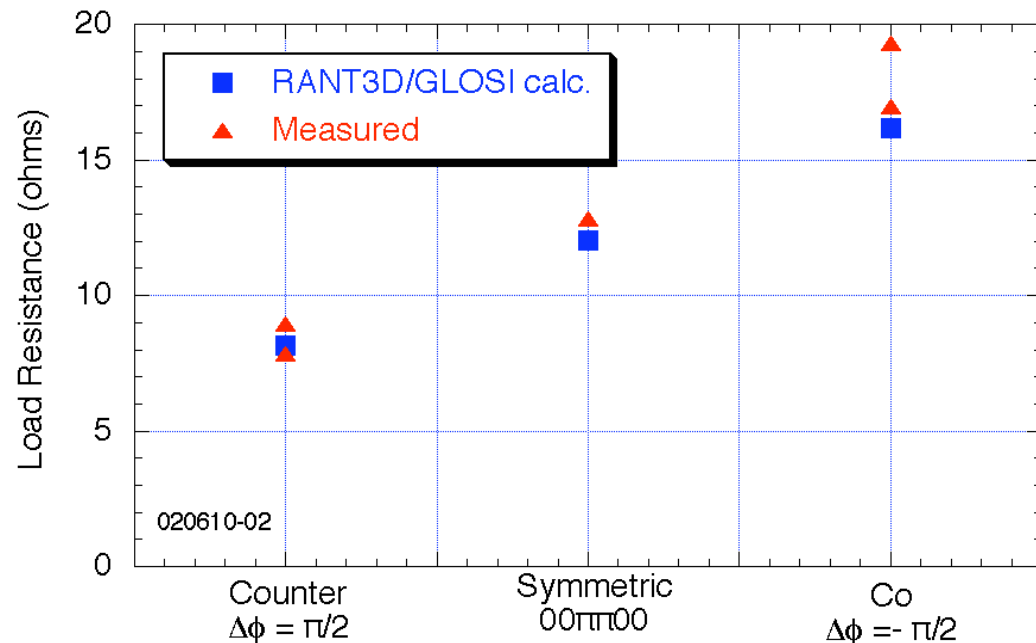


- Loading of antennas with  $\Delta\phi = -\pi/2$  phasing is  $\approx$  twice the loading with  $+\pi/2$
- Asymmetry caused by pitch angle of magnetic field in front of antenna.
  - RANT3D/GLOSI used to calculate 12x12 impedance matrix of antennas
  - 12-strap, 6-loop circuit model used to calculate load resistance  $R_{load}$
  - Calculations in good agreement with measured loading

12x12 impedance matrix from RANT3D (Im part, diag. term suppressed) shows asymmetry



Measured load resistance  $R_{load}^*$  for co-, counter-, and  $00\pi\pi00$  phasing agrees with calculations

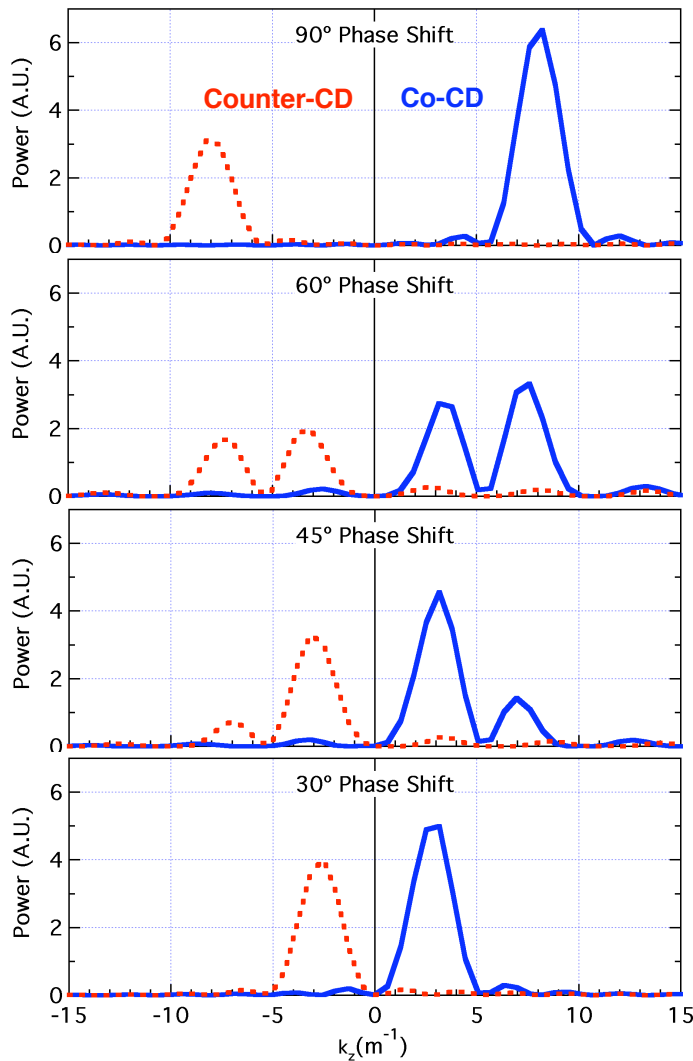




# Due to the fixed 180° phase between straps 1-7, 2-8, ... the wave spectra are not continuously variable

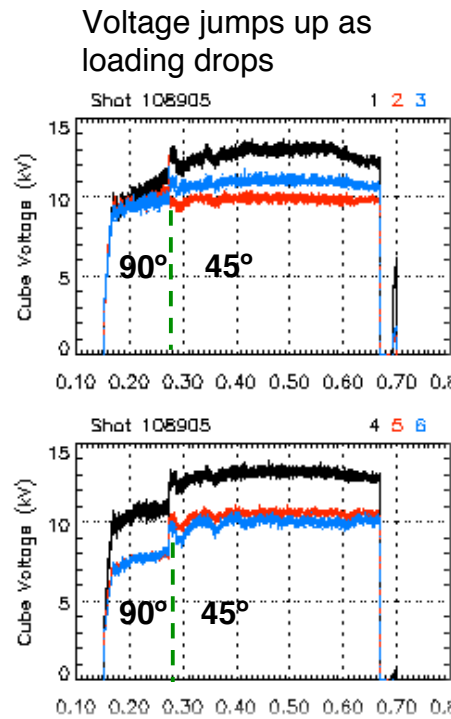


Calculated Spectra From RANT3D

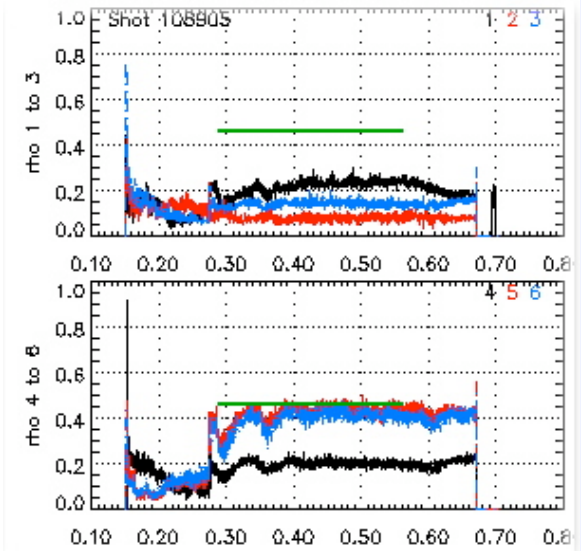


- 30° and 90° relative phasing give single-peaked spectra at  $m = 5, 13$  ( $k_{||} = 3, 8 \text{ m}^{-1}$ ).
- 45° and 60° give double-peaked spectra at the same wave numbers.

Phase has been changed from 90° to 45° during shot at 1.9 MW



Reflection coefficient increases as match changes

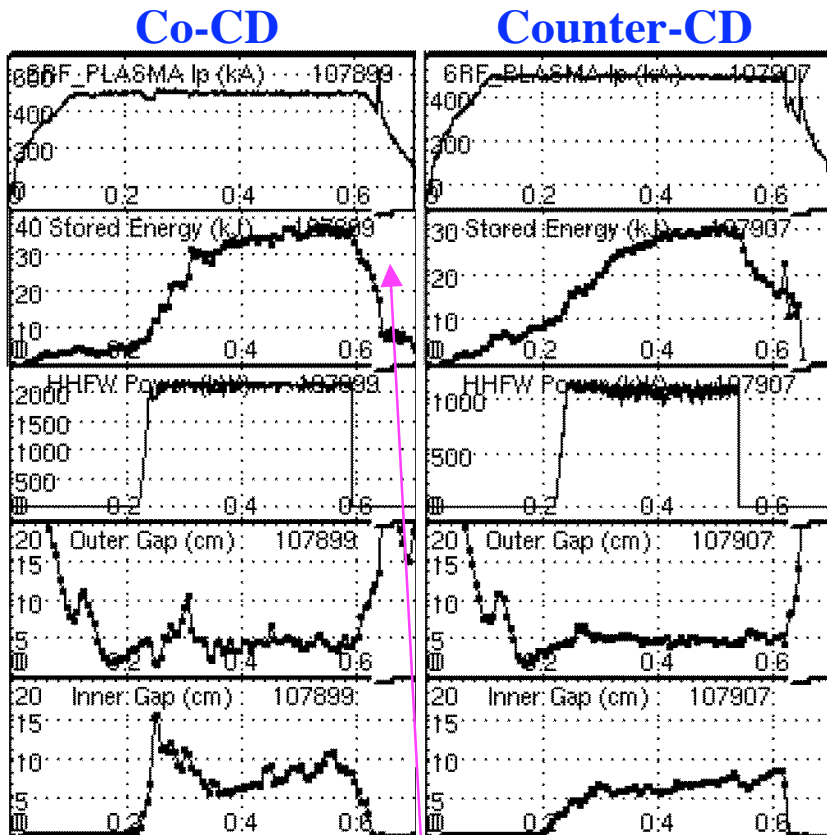


# HHFW CD: measurements and analysis

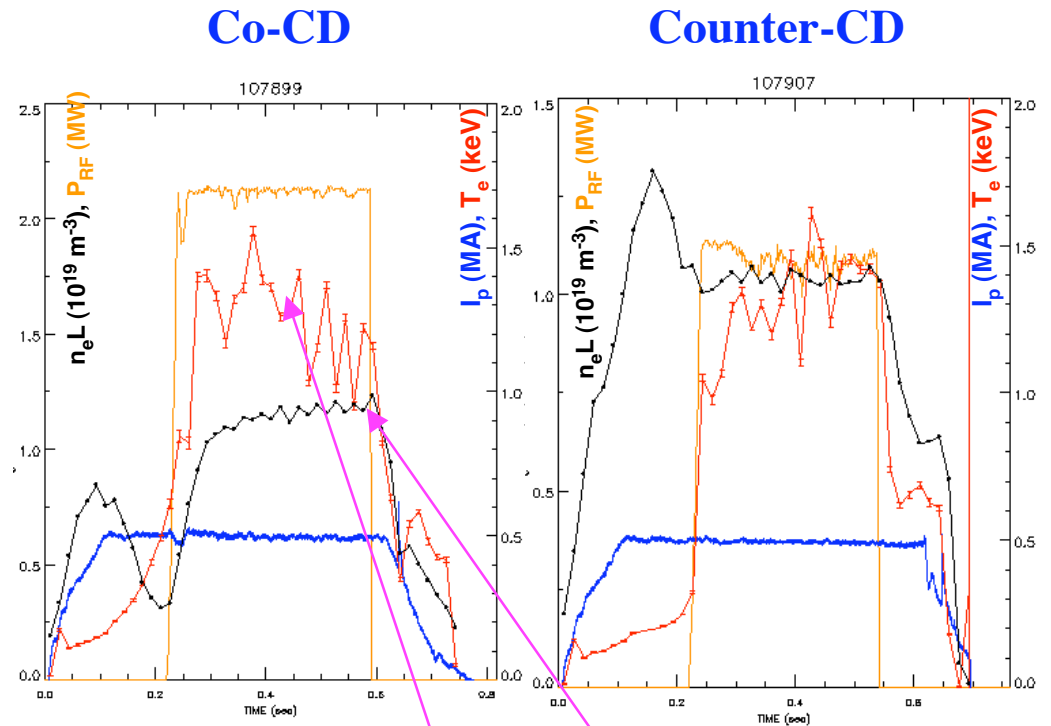


107899: Co-CD,  $P_{\text{HHFW}} = 2.1\text{MW}$

108907: Counter-CD,  $P_{\text{HHFW}} = 1.2\text{MW}$



Similar plasma stored energy



Similar  $T_e$  and density



# Current drive: significant difference in loop voltage seen between co- and counter-CD



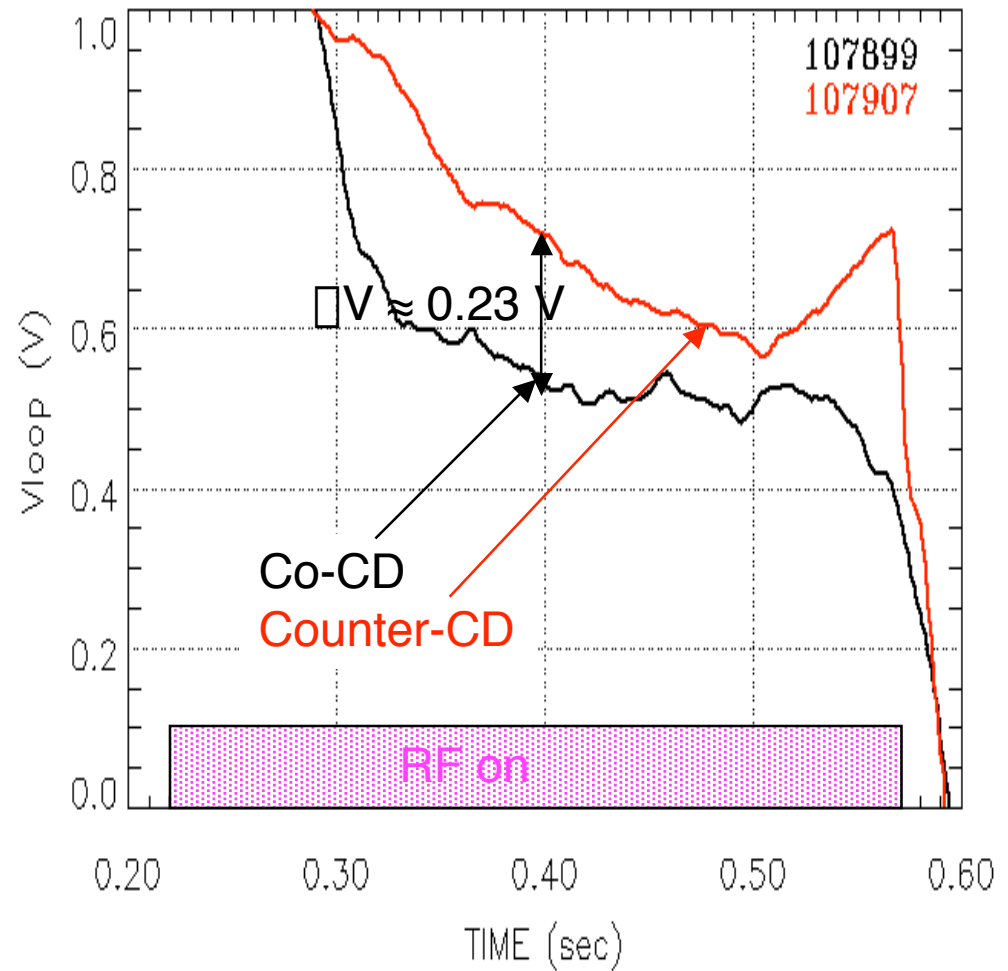
**No direct current-profile diagnostics yet.**

**Because of lack of Motional Stark Effect diagnostic, we must look for differences in loop voltage.**

$I_p$  is held constant on NSTX through feedback.

It takes less loop voltage to maintain  $I_p$  for identical plasma conditions when driving current in the co-CD direction.

Modeling predicts ~200 ms for the effect to show up on loop voltage.

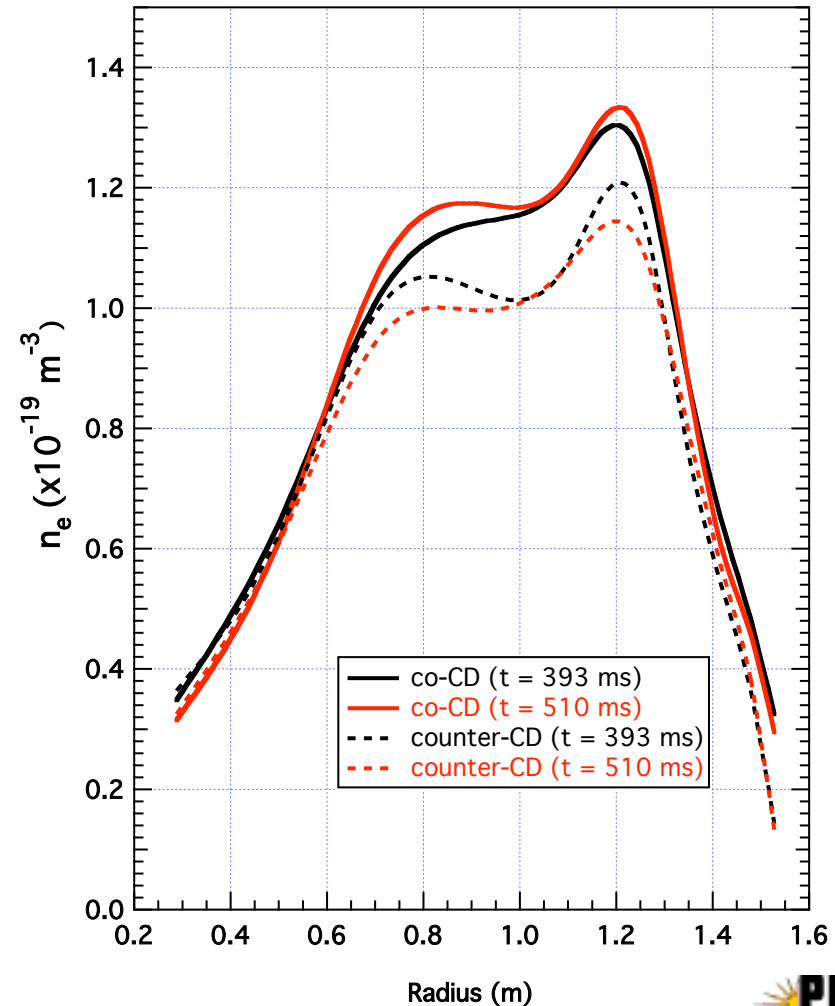
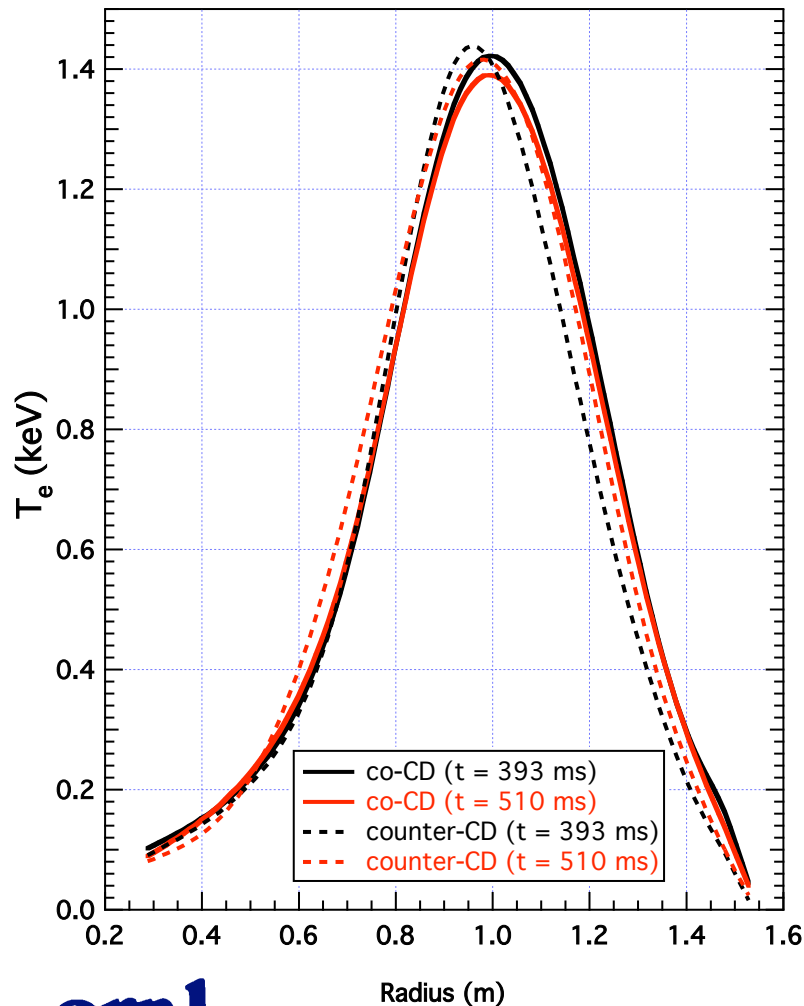


# Temperature and density profiles for co- and counter-CD shots are very similar



Electron Temperature for co-, counter-CD Phasing  
(107899, 107907)

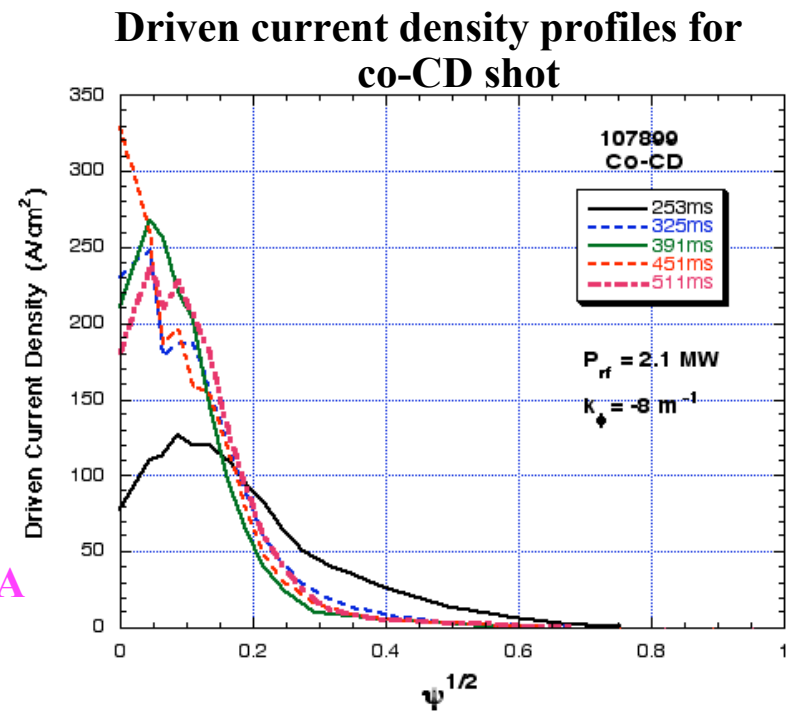
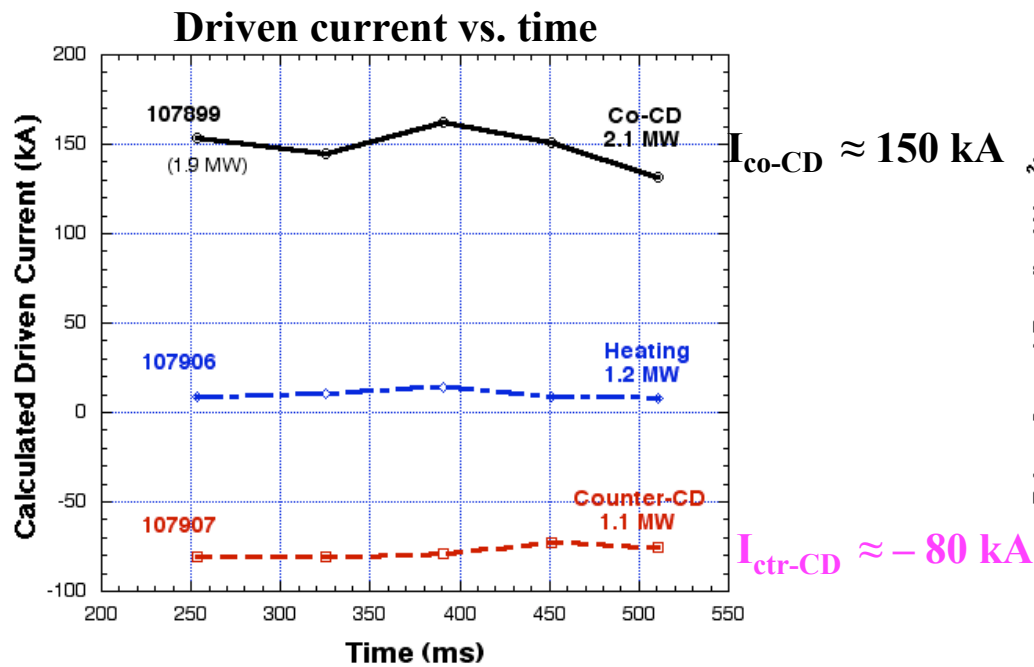
Plasma Density for co-, counter-CD Phasing  
(107899, 107907)



# CURRAY calculations of driven current (T. K. Mau)



- Used  $k_{\text{tor}} = \pm 8 \text{ m}^{-1}$  for co-CD,  $-8 \text{ m}^{-1}$  for ctr-CD, both w.  $P(-8 \text{ m}^{-1})/P(+8 \text{ m}^{-1}) = 1.25$  for symmetric phasing
- Temp and dens profiles from Thomson scattering data (assumed  $T_e \approx T_i$ )
- $Z_{\text{eff}} \approx 3.25$
- Geometry from EFIT
- Self-adjoint calculation of  $I_{\text{CD}}$



$$\square I_{\text{CD}} = I_{\text{co-CD}} - I_{\text{ctr-CD}} \approx 230 \text{ kA from CURRAY}$$

# Zero-D calculation of driven current (D. Swain)



## Parameters:

$$I_p = 500 \text{ kA}$$

$$P_{co} = 2.1 \text{ MW} \quad P_{ctr} = 1.1 \text{ MW}$$

$$V_{co} = 0.5 \text{ V} \quad V_{ctr} = 0.7 \text{ V}$$

$$\text{so } V_{co}/V_{ctr} = r_v \approx 0.7$$

$$I_p = I_{OH} + I_{BS} + I_{CD} \text{ where } I_{BS} \approx 40 \text{ kA (bootstrap current)}$$

## Assume

Steady-state has been achieved

$$I_{OH} R_p = V, \text{ and that}$$

$R_p$  is the same for both shots

$$-I_{co-CD}/I_{ctr-CD} = P_{co}/P_{ctr} = r_{pwr} \approx 0.5 \text{ (assumes } I_{CD} \sim \text{CD power)}$$

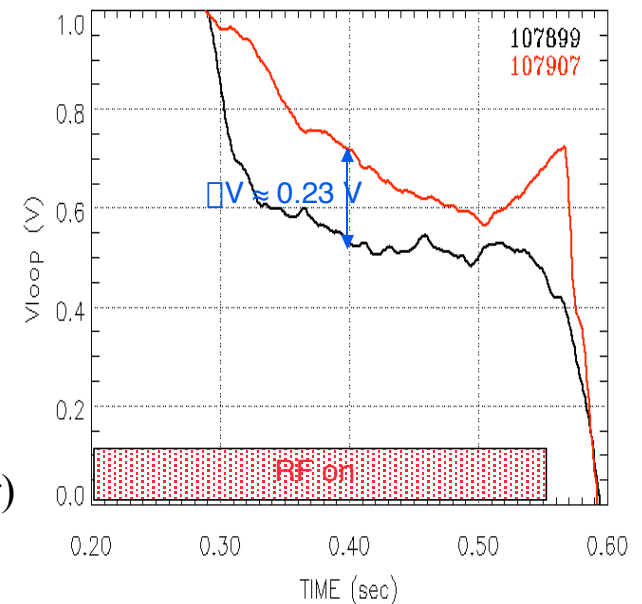
## Then

$$I_{co} = (I_p - I_{BS}) (1 - r_v) / (1 + r_v r_{pwr}) \approx 100 \text{ kA}$$

$$I_{ctr} \approx 0.5 I_{co} = 50 \text{ kA}$$

- $I_{CD} \approx 150 \text{ kA}$  from 0D calculation

$$I_{CD}/P_{RF} \approx 48 \text{ kA/MW at } n_e L = 1.7 \times 10^{15} \text{ cm}^{-2}$$

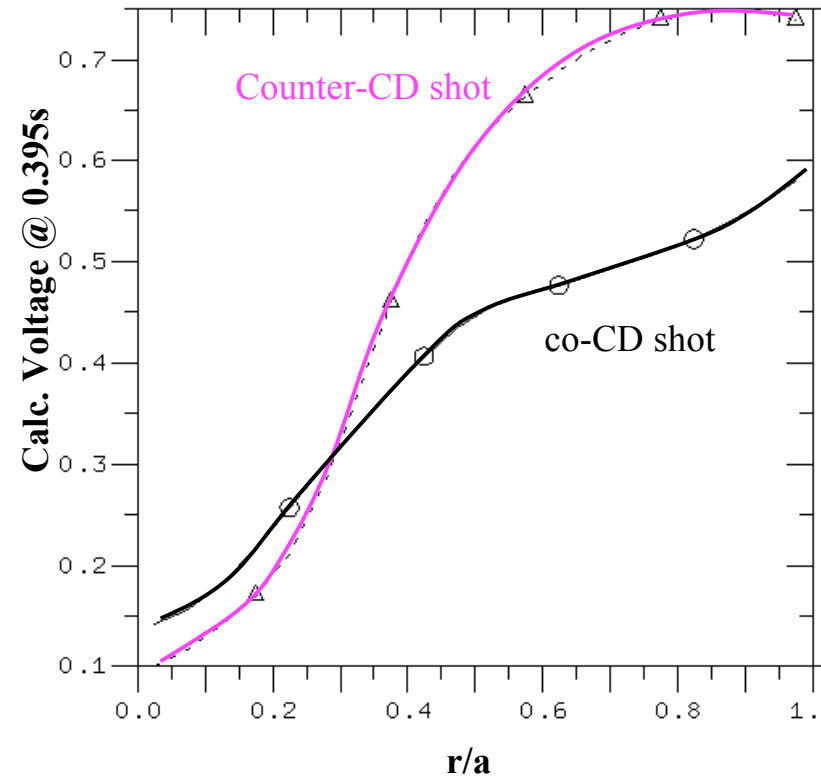


# Current drive calculation using TRANSP (S. Kaye)



- Use TRANSP to compute current profile evolution
  - Use measured  $V_{loop}(t)$ ,  $T_e(r,t)$ ,  $n_e(r,t)$ ,  $I_p(t)$  as input
  - Compute  $V(r,t)$  for co- and counter-CD shots
  - Compute  $\Delta E(r,t) = E_{co}(r,t) - E_{ctr}(r,t)$
  - Assume neoclassical resistivity
  - Compute  $\Delta j(r,t) = \Delta j_{NC}(r,t) - \Delta j_{E}(r,t)$
  - Integrate to get  $\Delta I_{CD}$

•  $\Delta I_{CD} \approx 90$  kA from TRANSP



- Summary:  $\Delta I_{CD} \approx$ 
  - 230 kA from CURRAY
  - 150 kA from zero-D
  - 90 kA from TRANSP

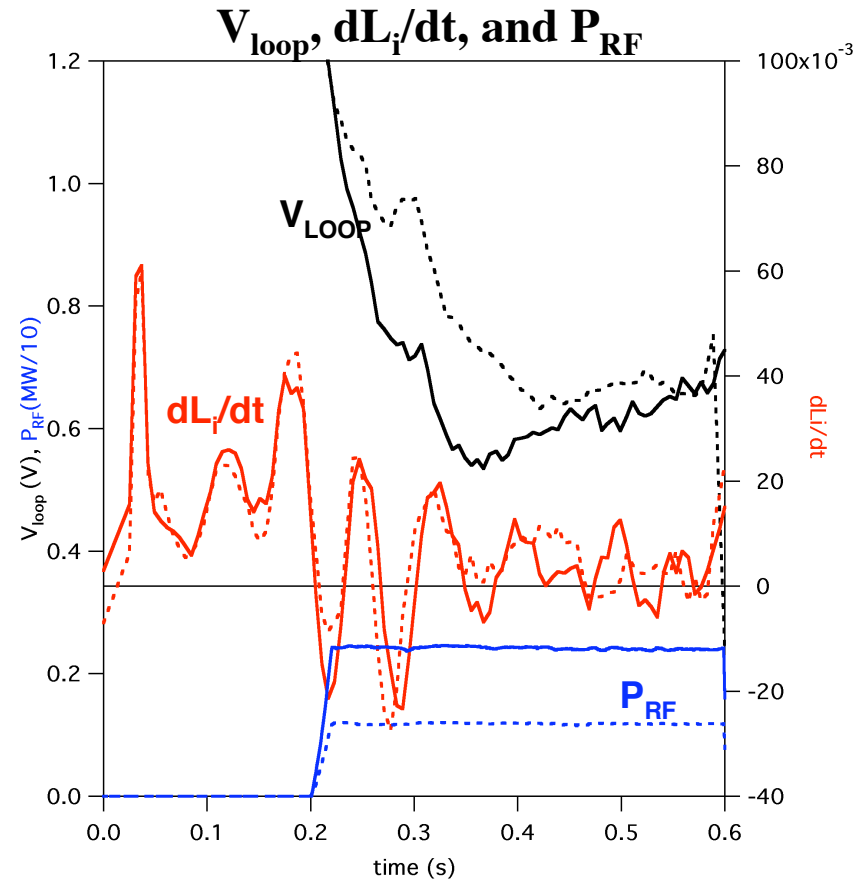
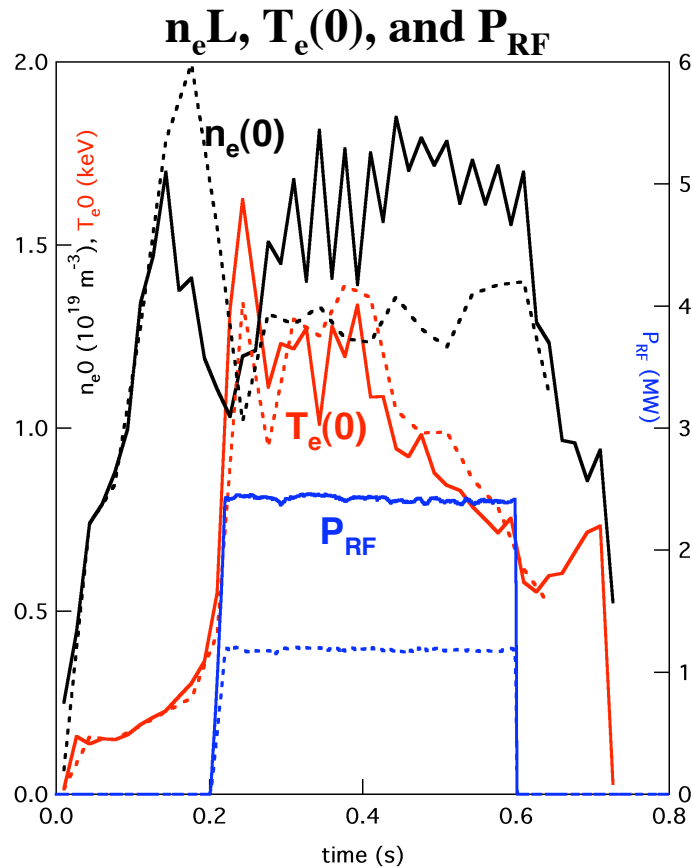
- Conclusions:
  - Current drive observed.
  - Difficult to interpret because steady-state not obtained
  - Magnitude of driven current uncertain, more work is needed.

# Difference in loop voltage (30%) observed at $\pm\pi/2$ phasing for comparable plasma conditions ( $D_2$ , 500 kA, 0.5 T)



Shot 108751: counter-CD ( $+\pi/2$ ) - dotted  
 Shot 108748: co-CD ( $-\pi/2$ ) - solid

$I_{CD}/P_{RF} \sim 35 \text{ kA/MW}$  for  $n_e L \approx 1.6 \times 10^{15} \text{ cm}^{-2}$   
 (0D estimate)





# Higher phase velocity ( $\pm\pi/4$ phasing) gives similar estimated current drive efficiency but at higher plasma density

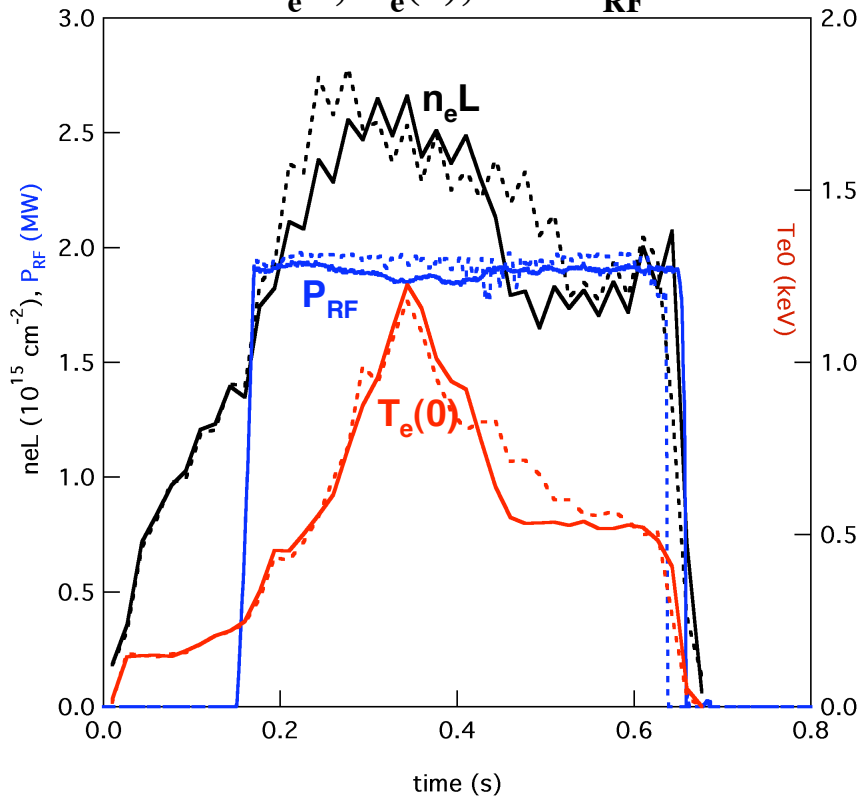


Shot 108901: counter-CD ( $+\pi/4$ ) - dotted  
 Shot 108903: co-CD ( $-\pi/4$ ) - solid

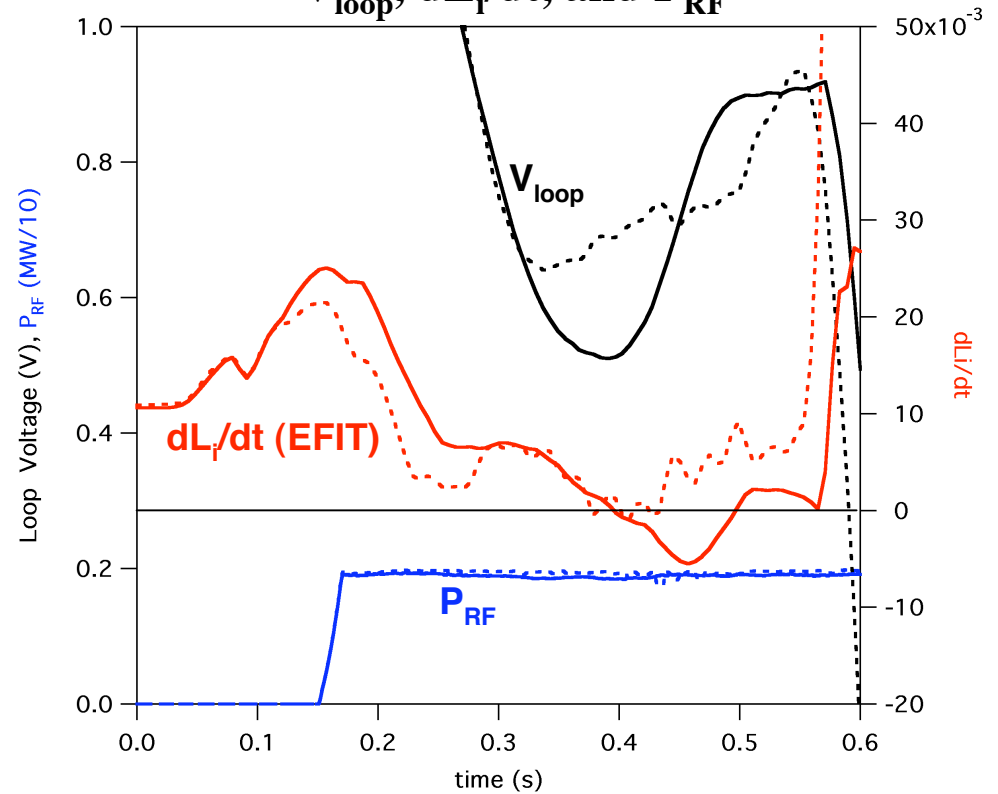
$I_{CD}/P_{RF} \sim 35 \text{ kA/MW}$  at  $n_e L \approx 2.5 \times 10^{15} \text{ cm}^{-2}$   
 (0D estimate)

$D_2$ , 500 kA, 0.5 T

$n_e L$ ,  $T_e(0)$ , and  $P_{RF}$



$V_{loop}$ ,  $dL_i/dt$ , and  $P_{RF}$



# Work to do



- **TRANSP and CURRAY analysis of:**
  - ± $\pi/2$  phasing (108748 and 108751)
  - ± $\pi/4$  phasing (108901 and 108903)
- **More detailed 0-D analysis of these shots.**
- **Analyze density fluctuations in the edge as a function of antenna phasing.**