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Supersonic gas jet fueling in NSTX (XP 626)

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Acknowledgements:

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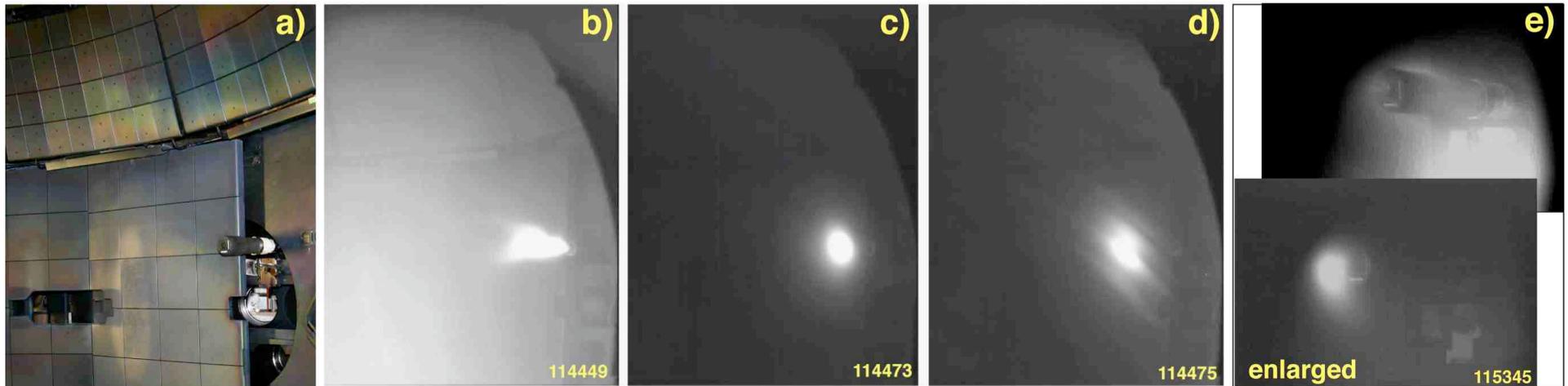
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**2006 NSTX Results Review
Princeton, NJ
27 July 2006**

XP 626 summary

- Low field side (LFS) supersonic gas injector (SGI) has been used for fueling of ohmic and 2-6 MW NBI-heated L- and H-mode plasmas
- SGI-fueled H-mode power threshold low (< 2 MW NBI), H-mode access reliable
- Developed H-mode scenario with SGI fueling and reduced x 20 high field side (HFS) fueling rate demonstrating the possibility of density control
- SGI-fueled double-null H-mode plasmas demonstrate different ELM regime (type III ELMs vs small and type I ELMs with HFS fueling)
- SGI injects deuterium at $\Gamma < 5 \times 10^{21}$ particles/s in quantities 0.1 - 0.3 of NSTX plasma inventory in a multi-pulse, continuous fashion with measured fueling efficiency 0.1 - 0.3
- SGI has been used “commercially” in several XPs

Supersonic gas jet does not perturb plasma edge



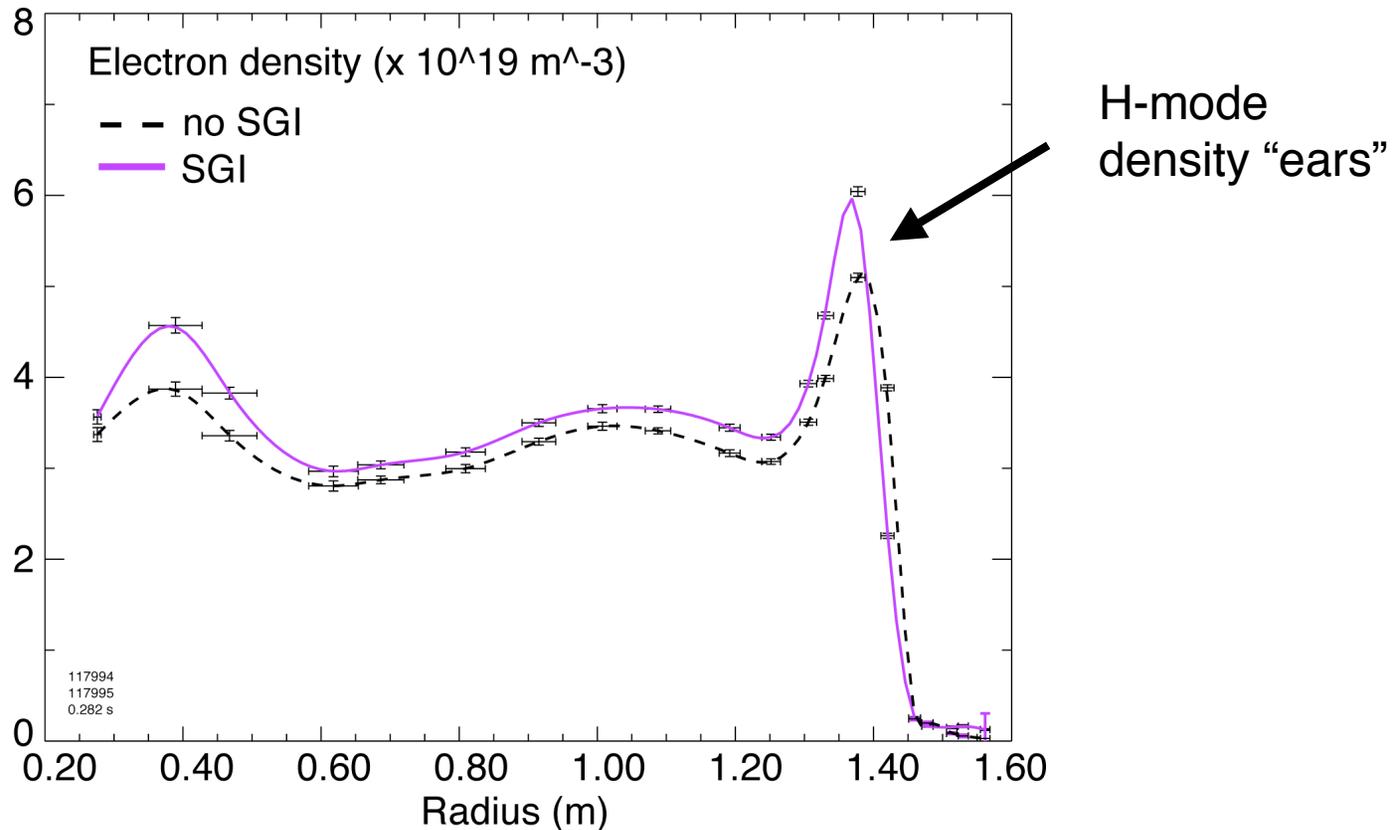
- Used Canadian Photonic camera with 0.5-2 ms framing rate
- Example frames above: (a) SGI in NSTX vacuum vessel, (b) SGI injecting gas into collapsing plasma with a wide $T_e = 3$ eV, $n_e = (2-2.5) \times 10^{18} \text{ m}^{-3}$ scrape-off layer, (c) 6 MW NBI-heated L-mode plasmas, (d) 4 MW NBI-heated H-mode plasmas, (e) ohmic plasmas at 3 cm distance from LCFS
- Plasma filaments (“blobs”) are often observed to traverse through gas jet
- During supersonic gas injection
 - SGI Langmuir probe does not typically show T_e reduction or I_{sat} increase
 - Magnetic sensors do not show any EM perturbations

SGI-fueled H-mode plasmas demonstrate different properties (low power threshold, type III ELMs)

| I_p (MA) | P_{NBI} (MW) | Magnetic configuration | Fueling | Power threshold (MW) | ELM type | Comment |
|---------------|--------------------------|------------------------------------|-----------|-------------------------|---------------|---|
| 0.7-1.0 | 2-6 | LSN, $\delta=0.4, \kappa < 2.2$ | HFS | 1-2 | I, small | Uncontrolled density rise due to HFS fueling |
| 0.7-1.0 | 2-6 | DN, $\delta=0.8, \kappa < 2.2$ | HFS | 1-2 | I, small | |
| 0.7-1.0 | 2-4 | LSN, $\delta=0.4, \kappa < 2.2$ | HFS + SGI | < 2 | small | HFS fueling can be reduced or eliminated |
| 0.8-1.0 | 4-6 | DN, $\delta=0.8, \kappa < 2.2$ | HFS + SGI | < 2 | small, III | |

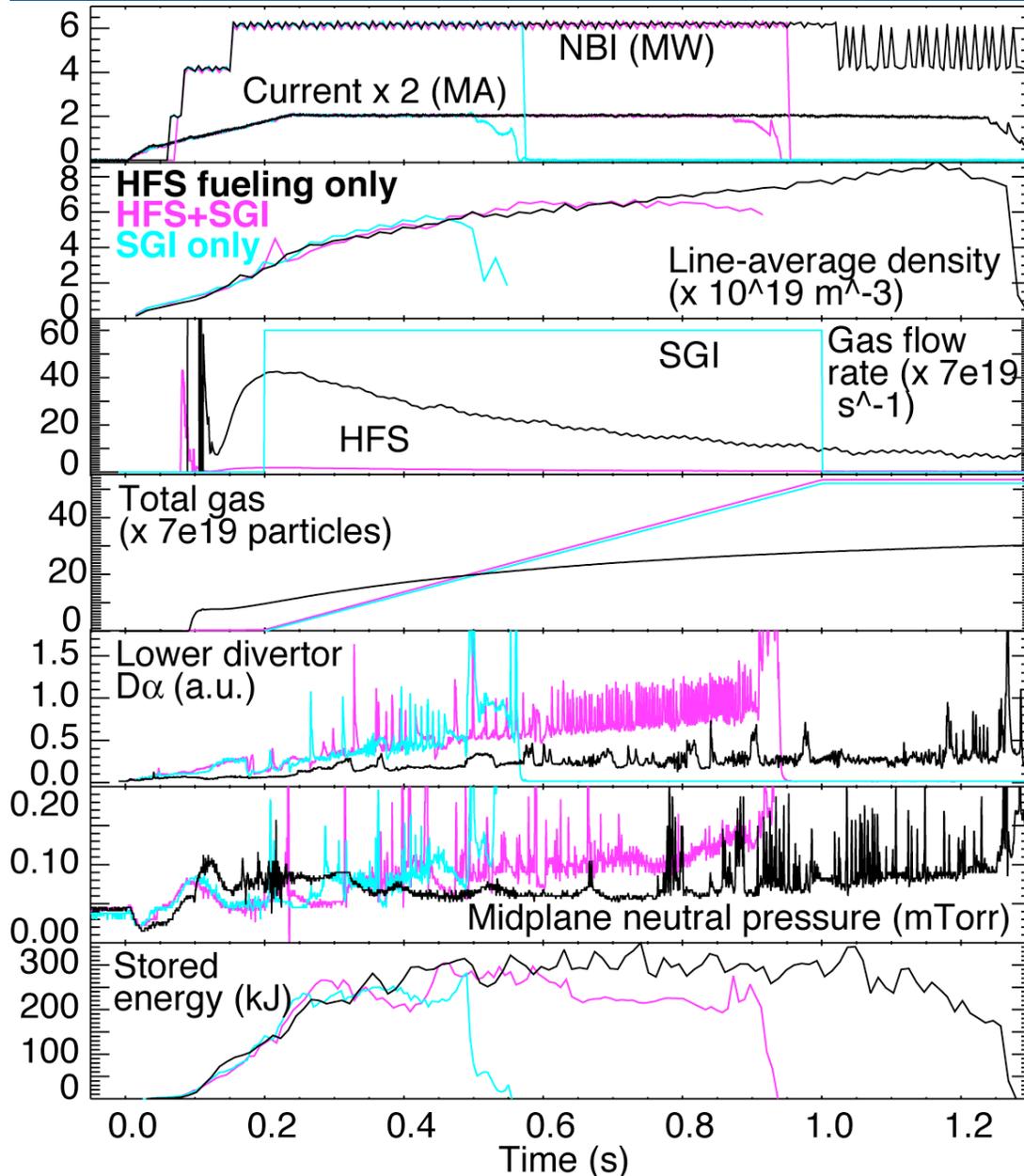
- Purpose of H-mode fueling experiments: eliminate uncontrolled density rise observed in HFS-fueled H-mode plasmas
- H-mode power threshold is low with LFS SGI fueling (high with LFS gas)
- With SGI fueling - transition from type I to type III ELMs in Double Null
- H-mode references: R. Maingi et al. PPCF 46 (2004) A305, NF 43 (2003) 969

In H-mode plasmas supersonic gas jet deposits particles in SOL and edge



- Supersonic gas jet does not penetrate further than 1-4 cm from separatrix
- Density rise is often seen in H-mode density profile “ears”, often “ears” width increases. Pedestal width/height analysis in progress...
- T_e profiles indicate pedestal and core reduction by up to 10-15 %

HFS fueling can be replaced by SGI fueling without H-mode density reduction



- Shown three discharges with full HFS fueling, reduced HFS fueling and SGI, and SGI fueling only
- Note **ELM** regime change from small and type I to **type III** in SGI-fueled plasmas
- Total gas input is greater with SGI fueling
- HFS fueling reduced by x 9
- Experiment was run when multi-pulse SGI capability was not yet available

Future work

- Hardware improvements under consideration:
 - Independent gas handling system
 - Increased plenum pressure (presently limited to 2500 Torr)
 - New supersonic nozzles
 - Density feedback with SGI using Plasma Control System

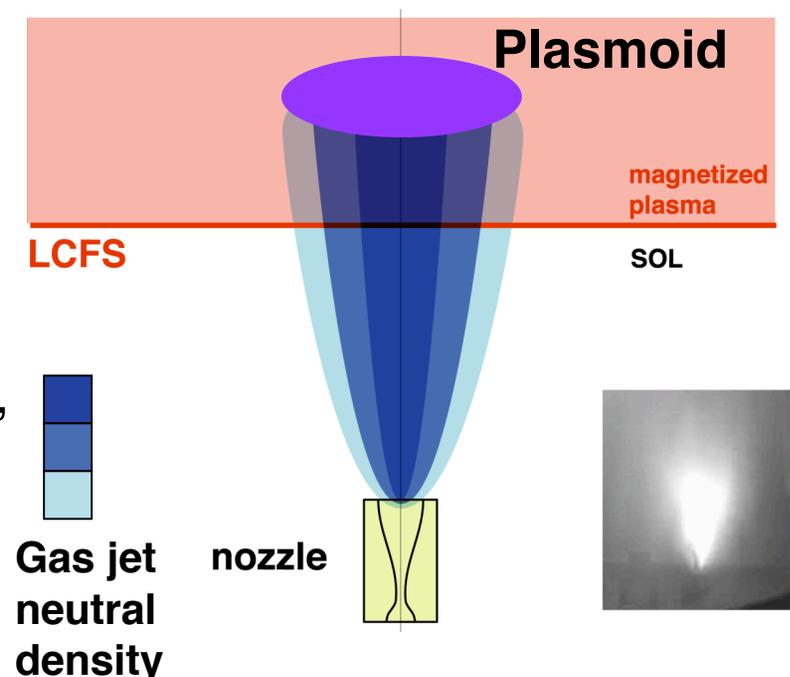
- Experiments under consideration
 - Low density H-mode plasma development
 - H-mode density control with SGI
 - ELM regimes characterization - power and gas injection scan
 - ELM control with SGI

Supersonic gas jet is a unique fueling technique studied on NSTX

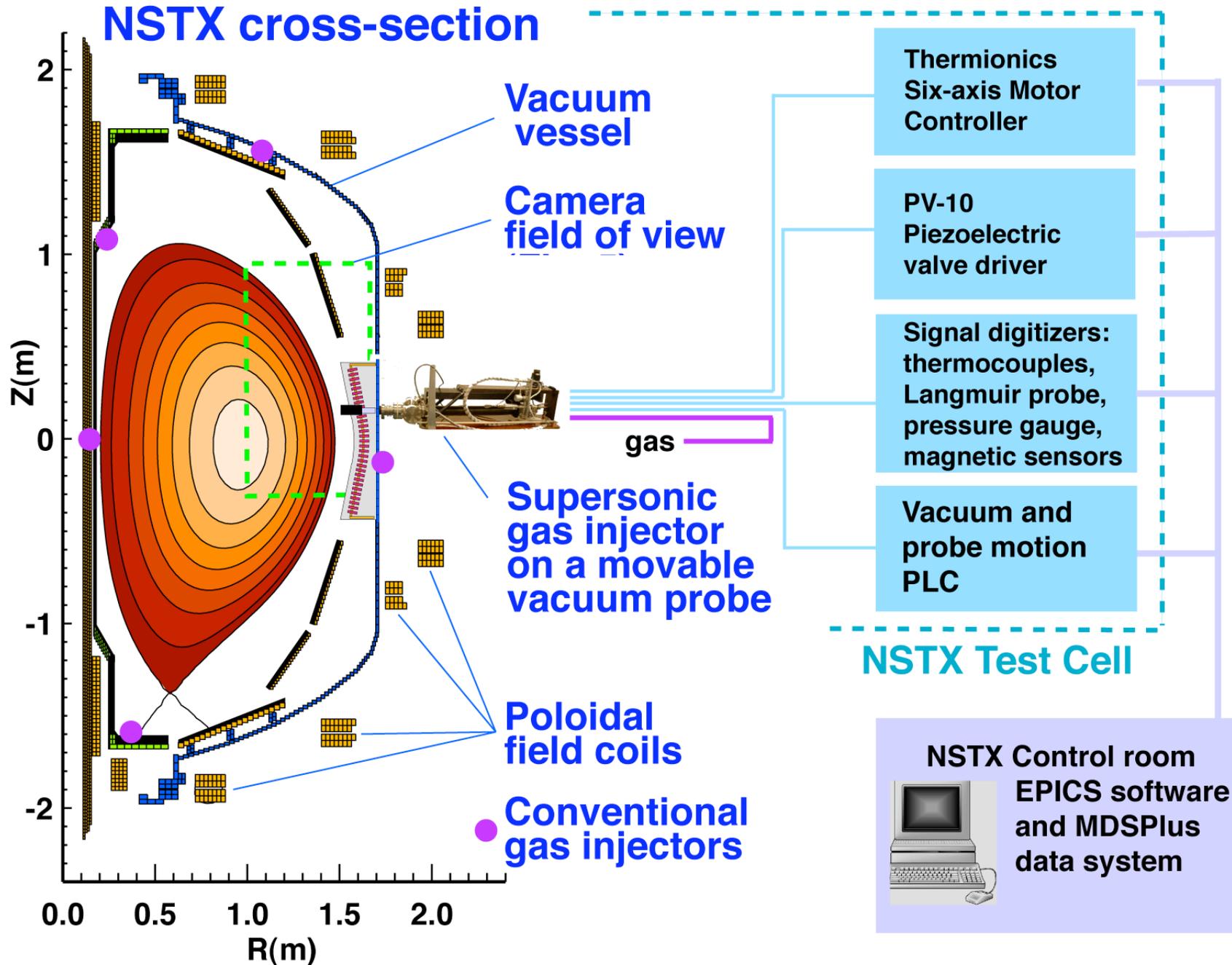
- **Improve and optimize gas fueling**
 - ITER will rely on central fueling (pellet, compact toroid), however plasma start-up and edge fueling will use gas puffing
- Supersonic gas injector installed on NSTX in 2004, experiments conducted in ohmic and NBI H-mode plasmas in 2005-2006
- Supersonic gas jet fueling was studied on other facilities
 - limiter tokamaks (HL-1M, Tore Supra): injected 0.2-0.9 of total plasma inventory in several ms, perturbative, fueling efficiency 0.3-0.6
 - divertor tokamak (AUG), divertor stellarator (W7-AS): similar gas jet parameters, but fueling efficiency $\sim 0.1-0.3$

Supersonic gas jet penetration mechanism

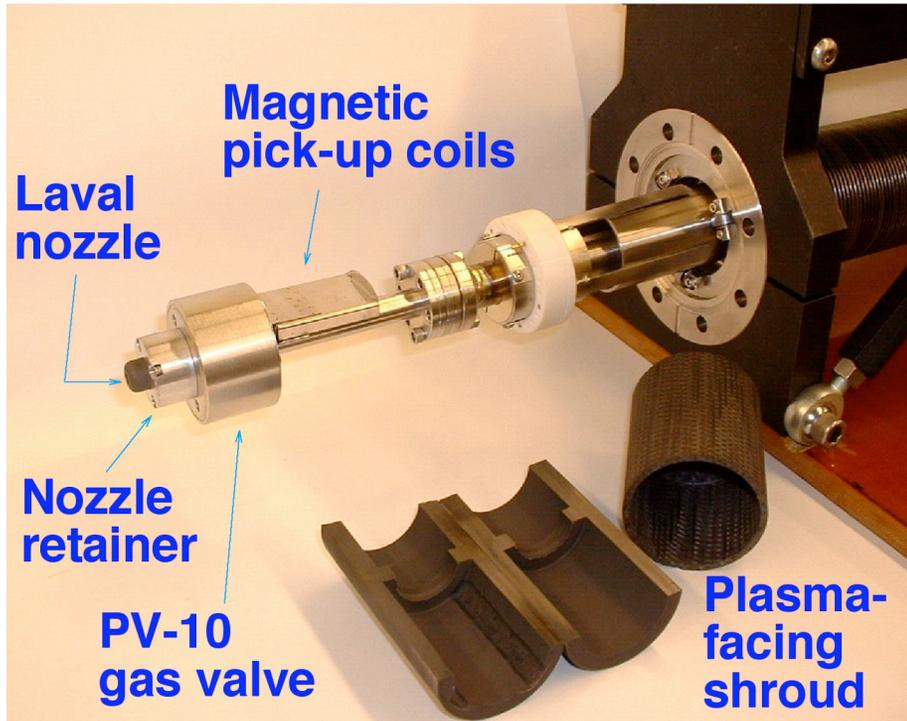
- Supersonic gas jet is a low divergence high pressure, high density gas stream
- Velocity distribution function is drifting narrowed Maxwellian with $u_{\text{drift}} = u_{\text{flow}}$
 $u_{\text{flow}} = M c = M \sqrt{\gamma kT/m} > v_{\text{therm}}$
- SOL/edge electrons with low T_e do not fully penetrate gas jet, gas jet retains neutral (molecular-atomic) -ion structure, eventually ionizes and creates a plasmoid
- High density plasmoid blocks jet from deep penetration into magnetized plasma
- Depth of penetration is determined by jet pressure (density) and plasma kinetic and magnetic pressure
- Single particle ionization / charge exchange penetration model is inapplicable
- Modeling must include continuity, momentum, energy balance (Braginskii) equations with detailed reaction rates and neutral transport



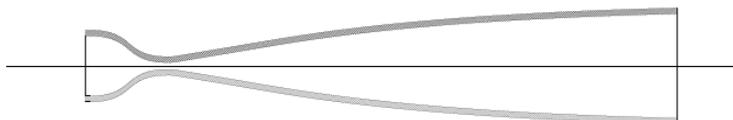
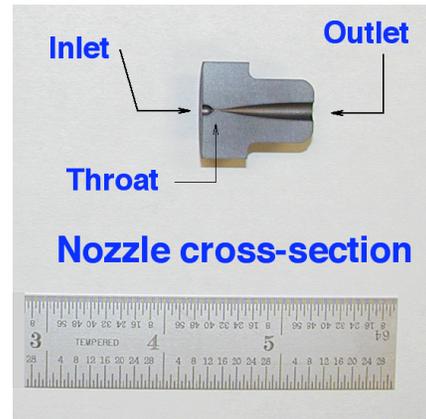
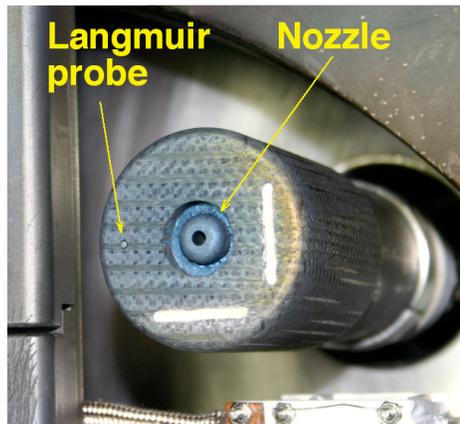
SGI on NSTX: placement and control elements



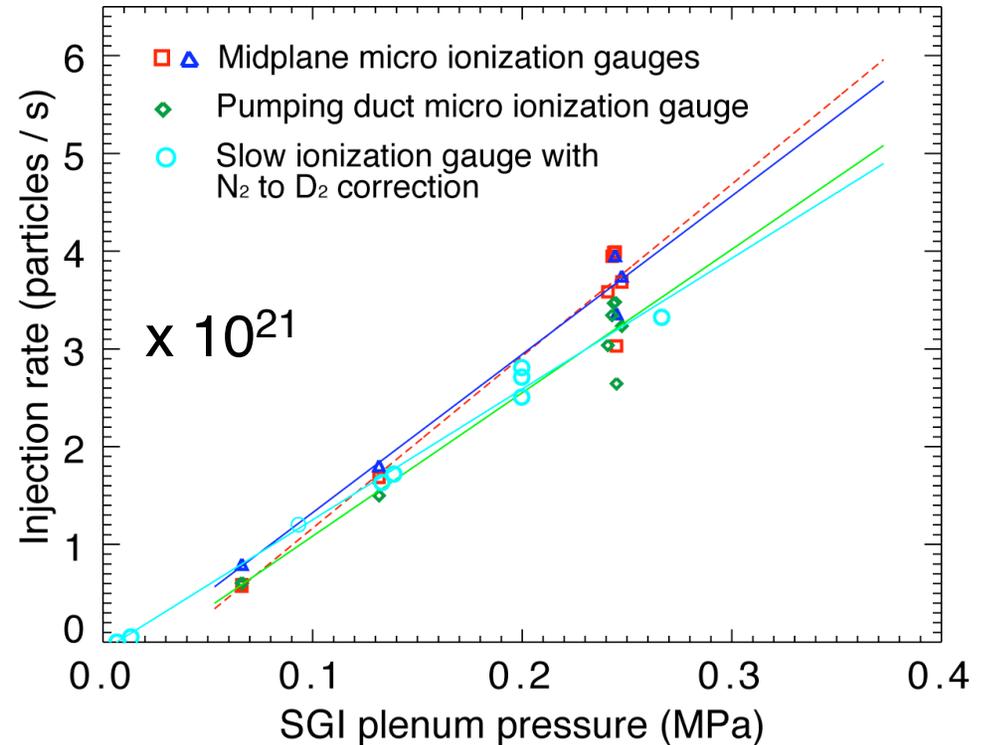
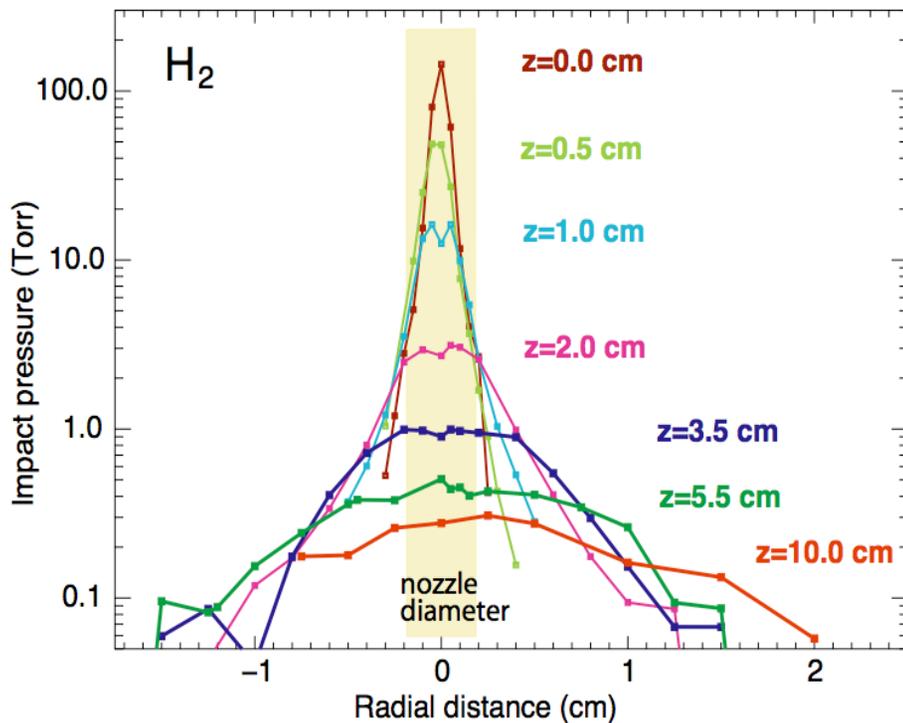
SGL head is a densely packed apparatus



- Shroud: CFC and ATJ graphite
- Gas valve: Veeco PV-10 piezoelectric type, $d_{throat}=0.02''$, typical opening time 1-2 ms, driving voltage 150 V
- Thermocouples in shroud and in gas valve
- Two magnetic pick-up coils on shroud front surface for B_z , B_t measurements
- Three magnetic pick-up coils in shielded box inside shroud for B_z , B_r and magnetic fluctuations measurement
- Langmuir probe: flush-mounted design, $d_{tip}=1.75$ mm, $I-V$ recorded at 5 kHz, $-50 < V < 50$
- Nozzle: True Laval geometry, $L = 23.4$ mm, $d_{throat} = 0.01''$

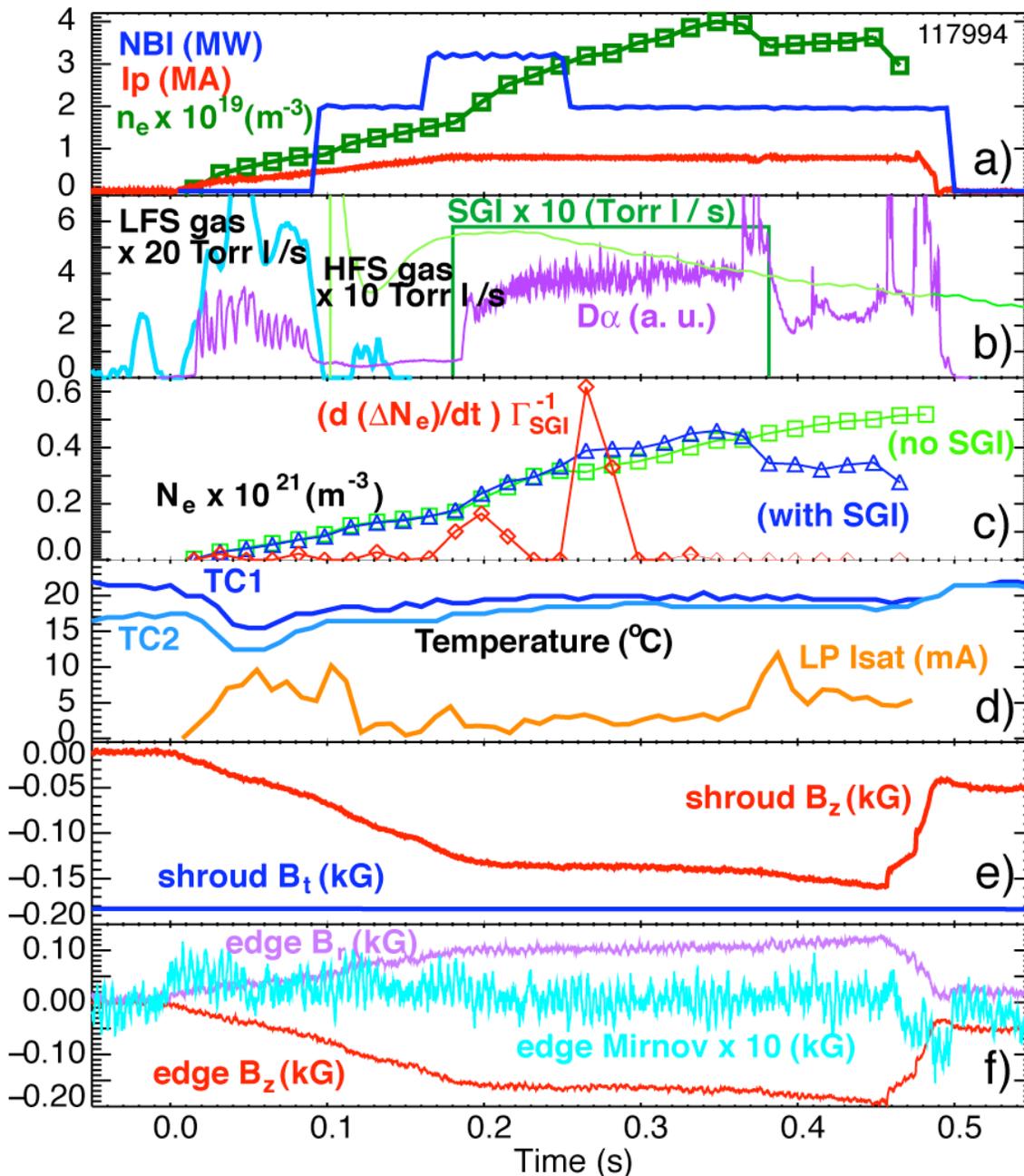


SGI parameters characterized off-line and *in situ*



- NSTX SGI is operated at 45-60 Torr I /s ($\sim (3.2 - 5) \times 10^{21}$ mol/s)
- Jet divergence half-angle: $6^\circ - 25^\circ$
- Hydrogen / Deuterium: $M = 4$, $T \sim 60 - 160$ K, $\rho < 5 \times 10^{17}$ cm⁻³,
 $Re = 6000$, $v_{therm} \sim 1100$ m/s, $v_{flow} = 2400$ m/s

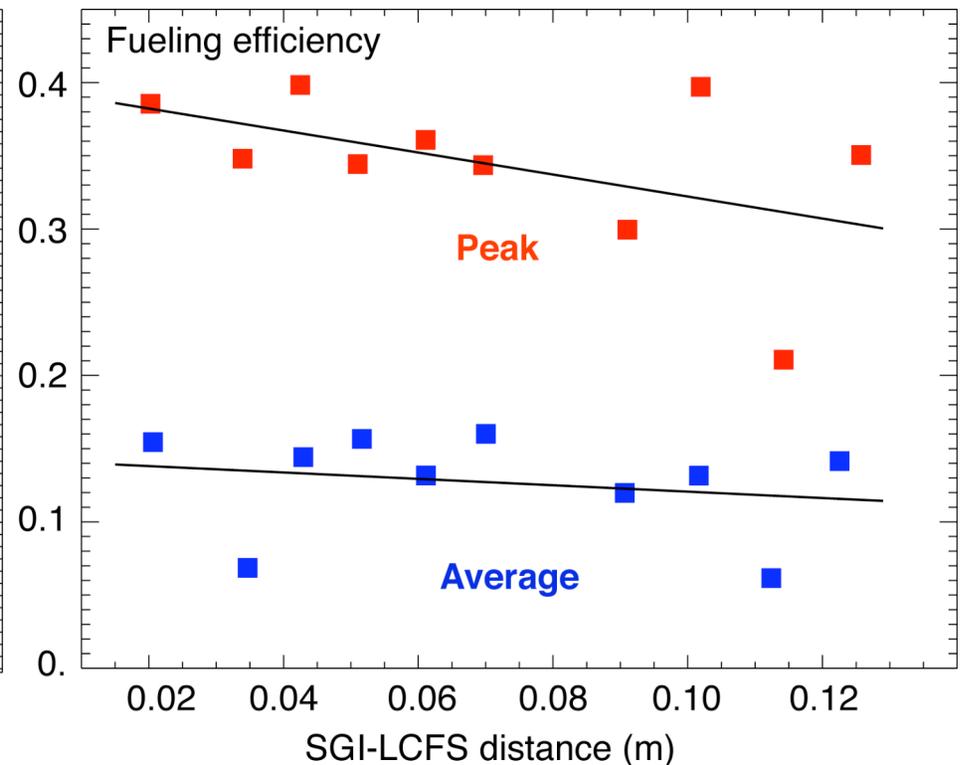
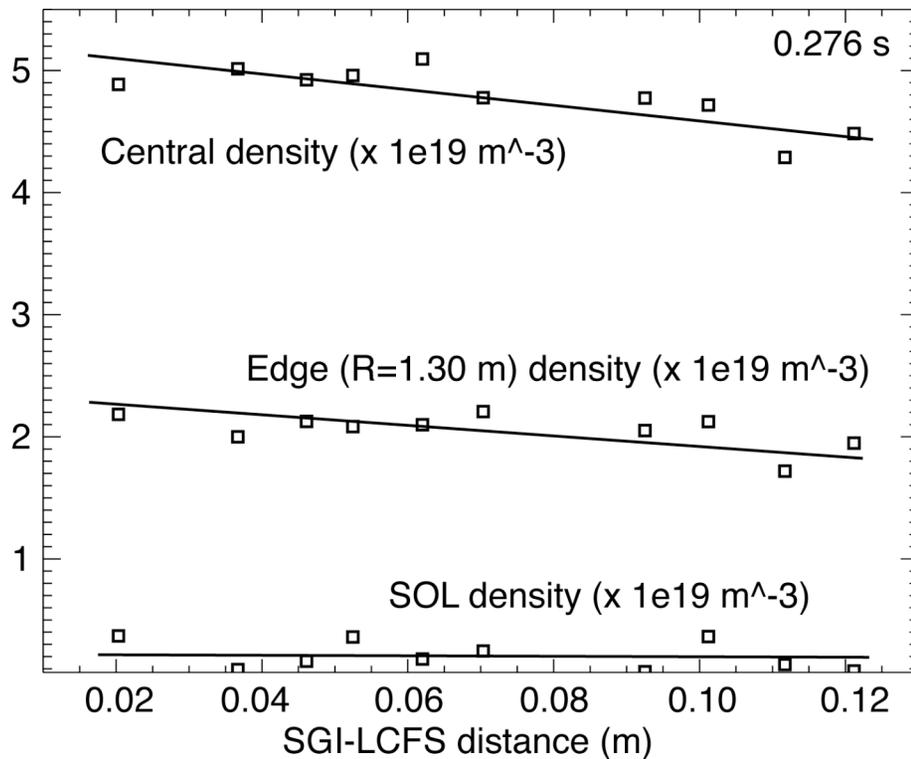
SGI H-mode fueling efficiency 0.1-0.3



- Example of 2-3 MW NBI HFS and SGI fueled LSN H-mode plasmas
- Density approaching Greenwald scaling limit
- SGI turns on at 0.180 s
- Supersonic gas jet does not perturb plasma edge

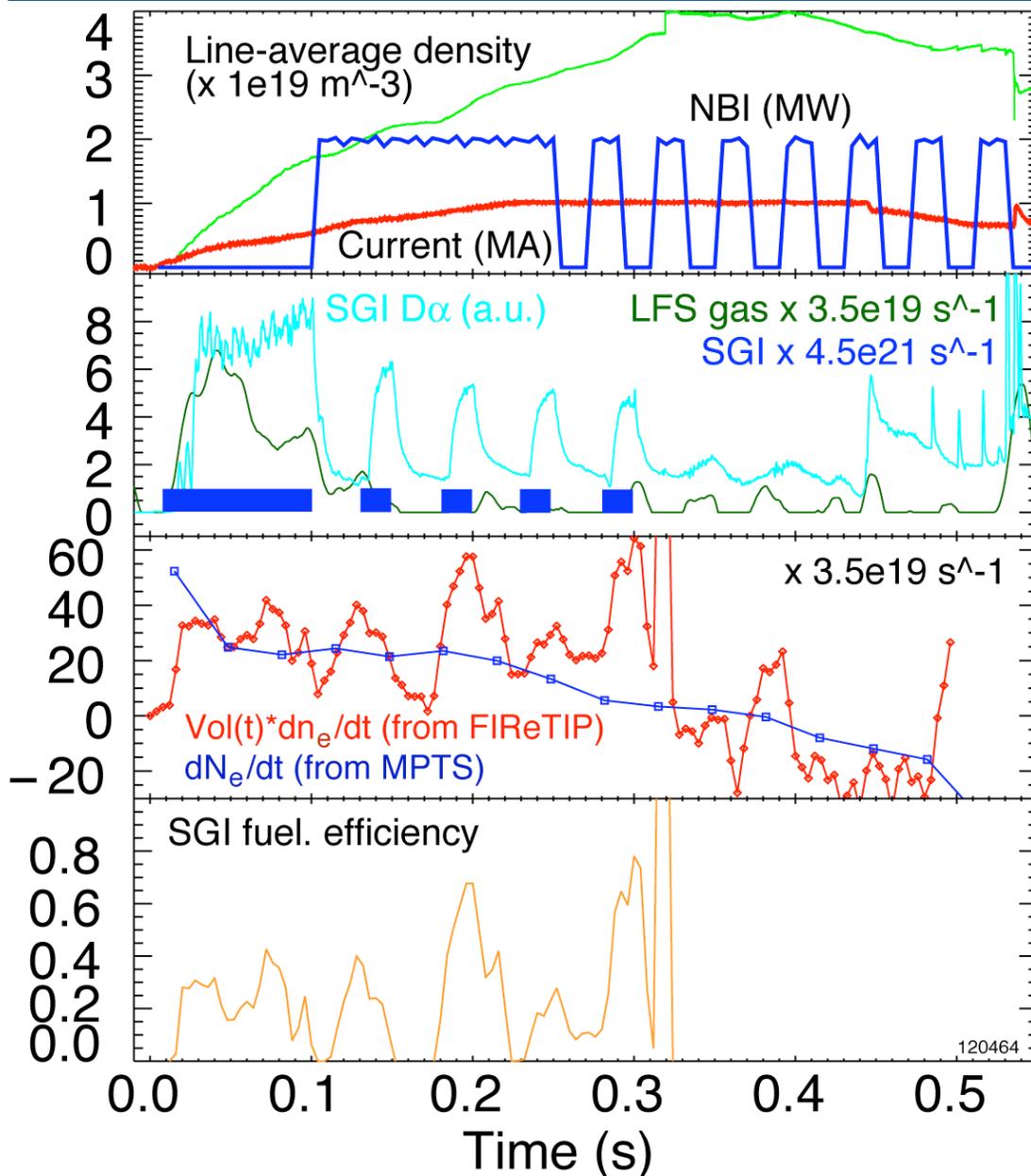
- (a) I_p , P_{NBI} , n_e
- (b) Gas injection rates, $D\alpha$
- (c) Electron inventory N_e , fueling efficiency
- (d) SGI thermocouples, Langmuir probe I_{sat}
- (e) and (f) - various SGI magnetic field and magnetic fluctuation sensors

Fueling efficiency is a function of SGI plenum pressure and distance to plasma



- Experiments in ohmic plasmas were conducted at reduced $\Gamma_{\text{SGI}} = 2.8 \times 10^{21} \text{ s}^{-1}$
- Calculated instantaneous fuelling efficiency $(dN_e/dt) * \Gamma_{\text{SGI}}$, then averaged over Γ_{SGI}
- Plasma density and fueling efficiency is a weak function of SGI-separatrix distance
- Need to run SGI at highest plenum pressure (presently 2500 Torr) and as close as possible to plasma

Fueling efficiency higher in inner-wall limited plasmas



- Example of NBI-heated inner wall limited L-mode plasma
- Pulsed SGI fueling
- Fueling efficiency 0.1 - 0.4
- Result important for using SGI during start-up when plasma is limited
- Instantaneous fueling efficiency is calculated using plasma volume $Vol(t)$ and dn_e/dt from FReTIP interferometer
- SGI at $\Gamma \sim 4.2 \times 10^{21} \text{ s}^{-1}$

NSTX reference data

NSTX fueling

- Gas injection: low field side (LFS, top + side), high field side (HFS, midplane + shoulder), private flux region. D_2 , He, injected at $S = 20 - 120$ Torr l / s.
- Neutral beam injection system: three beams, 40 - 100 keV, 6 MW, fueling rate: $S < 6$ Torr l / s
- Supersonic gas injection: $S < 65$ Torr l / s

NSTX wall conditioning

- Between shots He GDC
- He conditioning plasmas
- TMB and Plasma TMB

NSTX pumping

- Turbomolecular pump (3400 l / s)
- NBI cryopump (50000 l / s)
- Conditioned walls

PFC

- ATJ graphite tiles on divertor and passive plates
- ATJ and CFC tiles on center stack
- Tile thickness 1" and 2"

