

Recent progress in EM GTS*

E.A. Startsev, W.W. Lee, W.X. Wang

Plasma Physics Laboratory, Princeton University
Princeton, NJ, USA

September 22, 2015

*Research supported by the U.S. Department of Energy.

Recent EM developments in GTS

- In the past year we have been working on implementation of recently developed perturbative particle simulation double-split-weight scheme for simulation of gyrokinetic finite- plasmas in the gyrokinetic tokamak code GTS.
- The scheme uses two delta-f weights carried by each particle to represent particles density and pressure.
- Use of separate weight to represent particle pressure allows to alleviate so called "cancelation" problem in finite- gyrokinetic simulations with fully kinetic electrons.
- We have successfully used this scheme for simulation of linear tearing and drift-tearing modes, in both collisionless and semi-collisional regimes in sheared slab and high-aspect ratio cylindrical cross-section tokamak geometries.
- In the last several month this scheme has been extended to includes key toroidal effects for the simulation of linear semi-collisional micro-tearing (MTM) and kinetic ballooning (KBM) modes in realistic aspect ratio cylindrical cross-section tokamak.
- The initial simulations tests of KBM modes using the modified turbulence code GTS has been successful.

Double-weight EM Perturbative Scheme

- Introducing particle weights $\delta f_e = w_e F_{0e}$, the Vlasov equation for electrons becomes ($\partial_y = (1/r)\partial_\theta$):

$$\frac{\partial w_e}{\partial t} + v_{\parallel} \partial_{\parallel} w_e + v_{dr} \partial_z w_e = -\partial_y (\phi - v_{\parallel} A) \kappa_e - v_{\parallel} E_{\parallel} + v_{dr} \partial_z \phi + C[w_e].$$

- Next, we introduce $\bar{w}_e = \partial_{\parallel} w_e - \kappa_e \partial_y A$ the equation for \bar{w} becomes:

$$\frac{d\bar{w}_e}{dt} = \partial_y (\kappa_e E_{\parallel} - \nu \kappa_e^I A) - v_{\parallel} \partial_{\parallel} E_{\parallel} + (v_{dr} \partial_z) [\partial_{\parallel} \phi - \kappa_e \partial_y A] + C[\bar{w}_e].$$

- We also introduce second weight $\hat{w}_e = w_e + \kappa_e \partial_y \int dt \phi$ which satisfies the equation:

$$\frac{d\hat{w}_e}{dt} = -\partial_y \int dt (v_{\parallel} \kappa_e E_{\parallel} - \nu \kappa_e^I \phi) - v_{\parallel} E_{\parallel} + (v_{dr} \partial_z) [\phi + \kappa_e \partial_y \int dt \phi] + C[\hat{w}_e].$$

where in the first term κ_e^I includes only current gradient part of κ_e :

$$\kappa_e \equiv -(\partial F_{0e} / \partial \mathbf{x}) / F_{0e} = \kappa_n - \frac{3}{2} \kappa_{Te} + \frac{1}{2} \kappa_{Te} \frac{v_{\parallel}^2 + v_{\perp}^2}{v_{te}^2} + \frac{U'(r)}{\beta} \frac{v_{\parallel}}{v_{te}^2}$$

- Here the background current gradient is related to $q(r)$ profile by Ampere's law:

$$U'(r) = r \left(\frac{d}{r dr} \right)^2 \left(\frac{r^2}{Rq} \right)$$

Field Equations

- With introduction of new weights \bar{w}_e and \hat{w}_e , the field equations become

$$\nabla_{\perp}^2 \phi = \hat{S}_0 + (\kappa_n + \kappa_{Ti})(\hat{\Gamma}_0 - 1)\partial_y \phi + \kappa_{Ti}\hat{\Gamma}_1\partial_y \phi, \quad (1)$$

and

$$\begin{aligned} [\nabla_{\perp}^2 - \beta(m + 1)]E_{\parallel} = & -[\nabla_{\perp}^2, \partial_{\parallel}]\phi - \bar{S}_0 + \beta(\bar{S}_2 + \hat{S}_{\nu}) + \beta\partial_y \hat{S}_{dr} \\ & + \beta(\hat{\Gamma}_0 - 1)E_{\parallel} + U'(r)\partial_y(\phi - \nu_0 \int dt \phi) - (\kappa_n + \kappa_{Ti})(\hat{\Gamma}_0 - 1)\partial_y A - \kappa_{Ti}\hat{\Gamma}_1\partial_y A, \end{aligned}$$

- Here $m = m_i/m_e$ and $\nu_0 = \int \nu(v)(v_{\parallel}/v_{the})^2 F_{0e}(v)d^3v$.

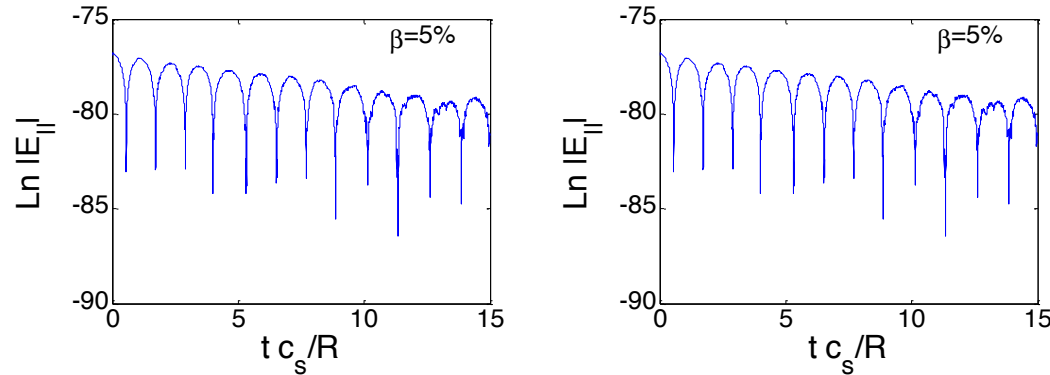
$$S_n = \int v_{\parallel}^n F_0(w_e - \langle w_i \rangle), \quad S_{\nu}^e = \int \nu(v)v_{\parallel} w_e F_{0e}, \quad S_{dr} = \int v_{dr} v_{\parallel} (w_e - \langle w_i \rangle) F_0$$

- where \hat{Q} quantities are now calculated by using new weight \hat{w} as for example $\hat{S}_{\nu}^e = \int \nu(v)v_{\parallel} \hat{w}_e F_{0e}$ and \bar{Q} quantities are calculated by using the weight \bar{w} .
- To find A we integrate in time

$$A = - \int dt (\partial_{\parallel} \phi + E_{\parallel}).$$

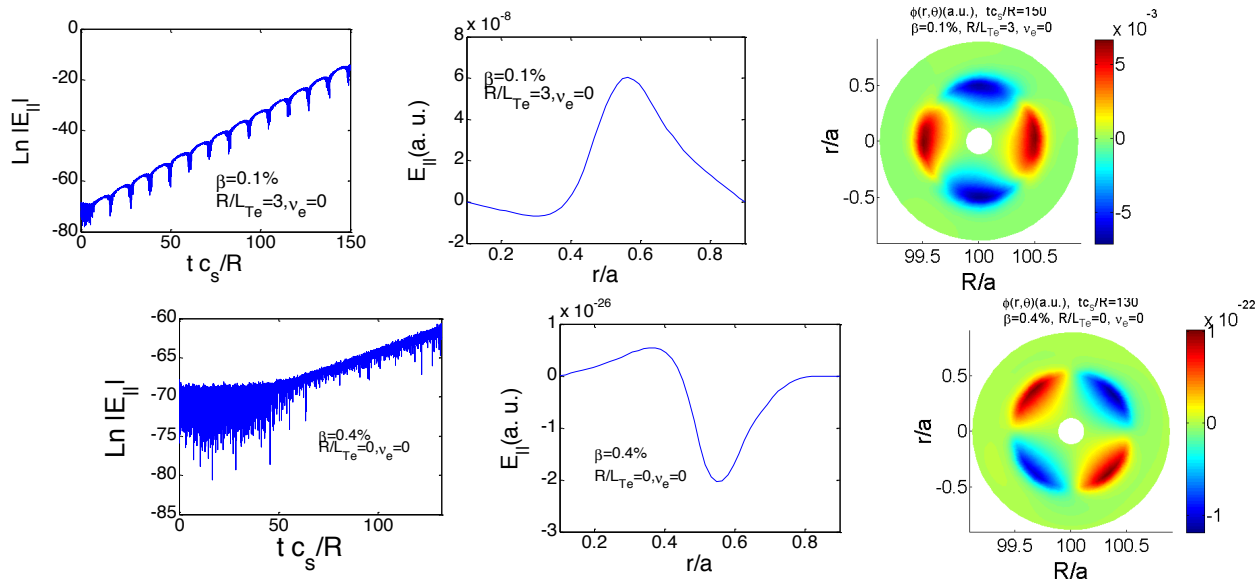
- The first term on the right in equation for E_{\parallel} involves commutator $[\nabla_{\perp}^2, \partial_{\parallel}]$ which requires only second derivative of potential and first derivative of q-profile and therefore can be neglected for modes with $k_{\perp} a \gg 1$.

Simulations of shear-Alfven wave



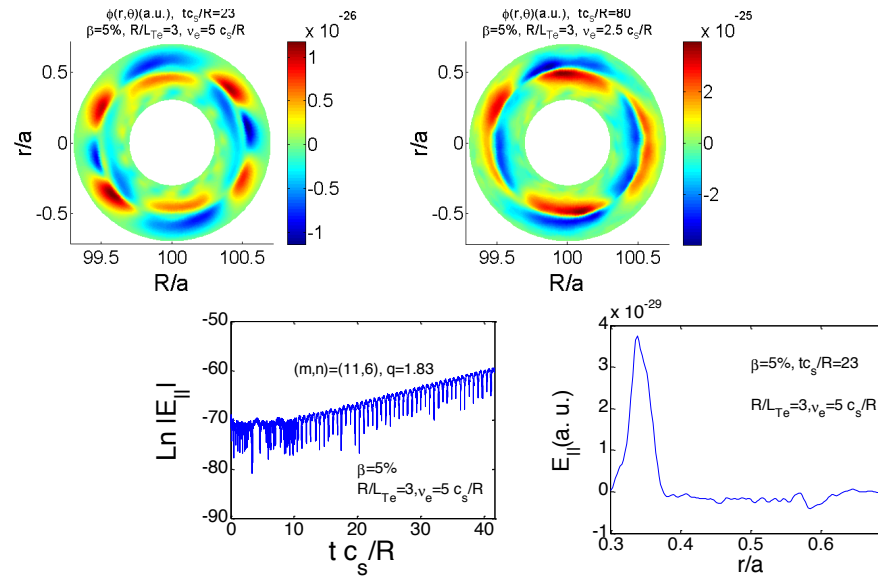
- Simulation of Shear Alfven wave with a minor radius similar to NSTX: $a/\rho_i = 165$.
- $dl_\theta = 1.65\rho_i$, $dr = 1.65\rho_i$, $dt(c_s/R) = 0.06$ with 32 poloidal planes, $N_p = 20$.
- $(m, n) = (1, 1)$ component of $\log|E_{||}|$ at $r/a = 0.56$ (corresponding to $q = 2$).
- The frequencies of the Alfven wave were $\omega = (2.7 + 0.15i)c_s/R$ for $\beta = 5\%$, and $\omega = (5.4 + 0.042i)c_s/R$ for $\beta = 1\%$.
- Approximate formula $\omega = (n - m/q)/\sqrt{\beta}(c_s/R)$ gives $\omega = 2.2c_s/R$ and $\omega = 5.0c_s/R$.

Simulations of global drift-tearing mode



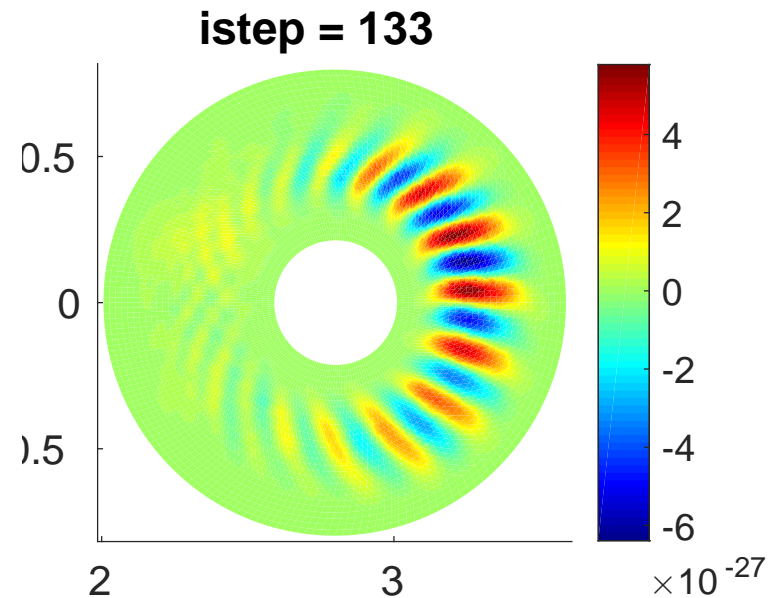
- $dl_{\theta} = 0.25\rho_i$, $dr = 0.15\rho_i$, $dt(c_s/R) = 0.06$, $N_p = 20$.
- $\log|E_{\parallel}|$ at $r/a = 0.56$ (corresponding to $q = 2$); radial profile of E_{\parallel} at $t(c_s/R) = 130$; $\phi(r, \theta)$ at $t(c_s/R) = 130$ for $a/\rho_i = 16$.
- $\gamma_{code} = 0.09(c_s/R)$, $\gamma_{eigen} = 0.1(c_s/R)$.
- $\log|E_{\parallel}|$ at $r/a = 0.56$ (corresponding to $q = 2$); radial profile of E_{\parallel} at $t(c_s/R) = 23$; $\phi(r, \theta)$ at $t(c_s/R) = 23$ for $a/\rho_i = 16$.
- $\omega_{code} = 0.28 + 0.38i(c_s/R)$, $\omega_{eigen} = 0.32 + 0.40i(c_s/R)$.

Simulations of micro-tearing mode with no curvature drifts



- $dl_{\theta} = 0.25\rho_i$, $dr = 0.055\rho_i$, $dt(c_s/R) = 0.06$, $N_p = 20$.
- $\phi(r, \theta)$ for runs with different values of electron collision frequency.
- $\log|E_{\parallel}|$ at $r/a = 0.35$ (corresponding to $q = 1.83 = 11/6$); radial profile of E_{\parallel} at $t(c_s/R) = 23$.

Simulations of Toroidal KBM mode for Cyclone-like parameters



- $\phi(r, \theta)$ in poloidal plane.
- $m_i/m_e = 3674$, $\beta_e = 3.3\%$, $R/L_{te} = R/L_{ti} = 6.92$, $R/L_n = 2.22$, $R/a = 2.8$, $a/\rho_i = 76$,
- $q(r) = 1.25 + 0.67(r/a)^2 + 2.38(r/a)^3 - 0.06(r/a)^4$.
- $dl_\theta = 0.7\rho_i$, $dr = 1.2\rho_i$, $dt(c_s/L_{ti}) = 0.01$, $N_p = 20$.

The EM algorithms generalized/reformulated for toroidal geometry; implementation into GTS is underway

Rigorously reformulate electron field-particle dynamics based on ideas developed/tested in simple cases, taking into account existing GTS framework

- Work on field quantity $E_{\parallel} = -\mathbf{b} \cdot \nabla\phi - (1/c)\partial A_{\parallel}/\partial t$ or $\int E_{\parallel} dt$ instead A_{\parallel}
 $A^h \equiv -c \int E_{\parallel} dt$; $A^s \equiv A_{\parallel}(t_0) - c \int \mathbf{b} \cdot \nabla\phi dt$
- Solve δf -equation for reformulated perturbed electron distribution δh_e
 $f_e \equiv \delta h_e + [1 - (e/cT_e)A^h(v - u_{\parallel})]f_{sm}$

$$\begin{aligned} \frac{\partial \delta h_e}{\partial t} + \frac{1}{B^*} \nabla_{\mathbf{z}} \cdot (\dot{\mathbf{z}} B^* \delta h_e) = & - \left[1 - \frac{e(v - u_{\parallel})}{cT_e} A^h \right] (\dot{\mathbf{z}} \cdot \nabla_{\mathbf{z}} f_{sm}) \\ & + \left\{ \frac{e(v - u_{\parallel})}{cT_e} \frac{\partial A^h}{\partial t} + \dot{\mathbf{z}} \cdot \nabla_{\mathbf{z}} \left[\frac{e(v - u_{\parallel})}{cT_e} A^h \right] \right\} f_{sm} + C^l \end{aligned}$$

note: on RHS, $\partial A^h/\partial t$ term can be canceled by a term in $v_{\parallel} \partial f_{sm}/\partial v_{\parallel}$

Associated weight equation:

$$\dot{w} = \frac{1 - w}{f_{sm}} (\text{RHS} - C^l) + \frac{w - \langle w \rangle}{f_{sm}} (\text{RHS} - C^l)$$

The EM algorithms generalized/reformulated for toroidal geometry; implementation into GTS is underway

- Field equations for A^h (generalized Amperes law), A^s and ϕ

$$(\nabla_{\perp}^2 - \frac{\omega_{pe}^2}{c^2})A^h = -\frac{4\pi e}{c} \int v_{\parallel} \delta h_e d^3v - \frac{4\pi e_i}{c} n_i \delta \bar{u}_{i,\parallel} - \nabla_{\perp}^2 A^s$$

$$\frac{\partial A^s}{\partial t} = -c\mathbf{b} \cdot \nabla \phi$$

$$-\nabla_{\perp} \cdot \frac{Z_i n_{i,0}}{B\Omega_i} \nabla_{\perp} \phi = \delta \bar{n}_i - \int \delta h_e d^3v$$

- Consistent Lagrangian equation of gyro-center motion using E_{\parallel}

$$\mathcal{L} = \frac{e_s}{c} [(\rho_{\parallel} + \frac{A_{\parallel}}{B})\mathbf{B} + \mathbf{A}] \cdot \mathbf{x} + \mu \dot{\xi} - \mathcal{H}$$

$$\mathcal{H} = \frac{1}{2} \frac{e_s^2}{m_s c^2} \rho_{\parallel}^2 B^2 + \mu B + e_s \phi$$

- We will focus on completion of implementing/testing/verifying generalized EM algorithms in GTS and initial applications, with a goal of bring this highly desirable capability to production for NSTX-U physics applications and other studies

Conclusions

- In the near future we will continue testing the double-split-weight EM scheme in GTS against available results for KBM and semi-collisional MTM eigenmodes in tokamaks with circular flux surfaces.
- Implementation of generalized, comprehensive EM algorithm into GTS is underway
- Apply GTS to current problems interest to NSTX-U.