

Power Exhaust on JET: An Overview of Dedicated Experiments

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5) See annex to J. Pamela, Fus. Energy 2002 (Proc. 19th Int. Conf. Lyon, 2002), IAEA, Vienna



followed by

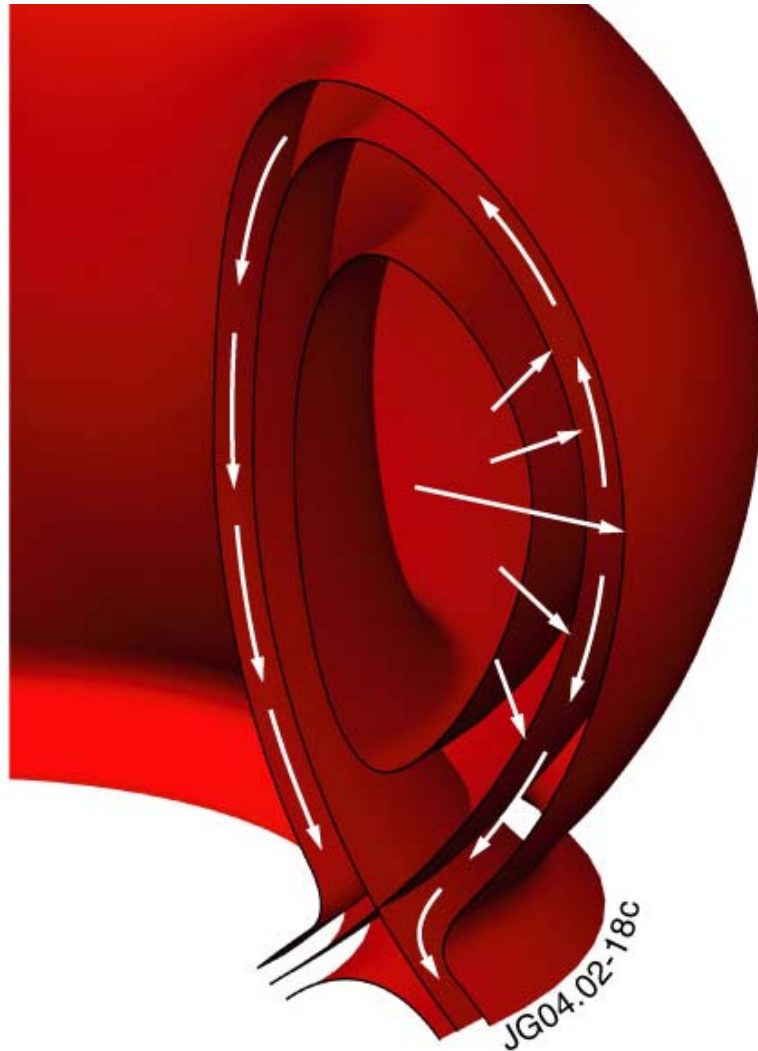
Wall and Divertor Load during ELMy H-mode and Disruptions in ASDEX Upgrade



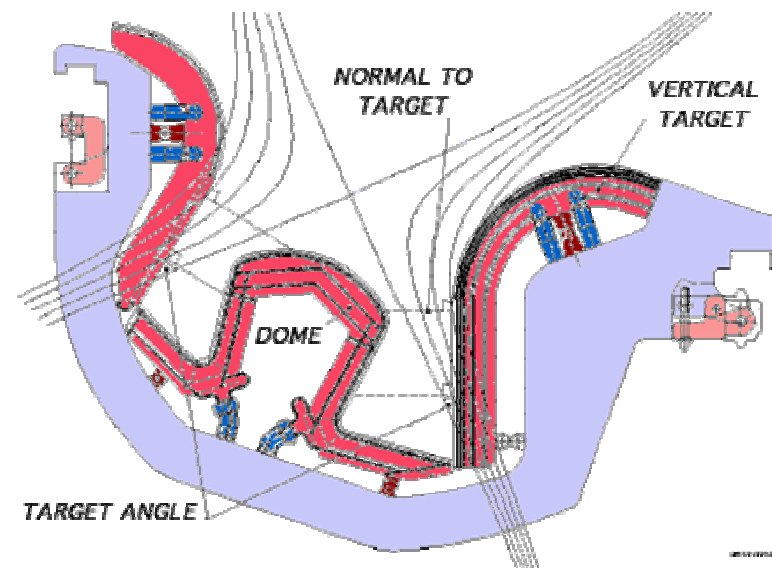
A. Herrmann, J. Neuhauser, G. Pautasso, V. Bobkov, R. Dux, T. Eich, C.J. Fuchs, O. Gruber,
C. Maggi, H.W. Müller, V. Rohde, M. Y. Ye, ASDEX Upgrade team¹

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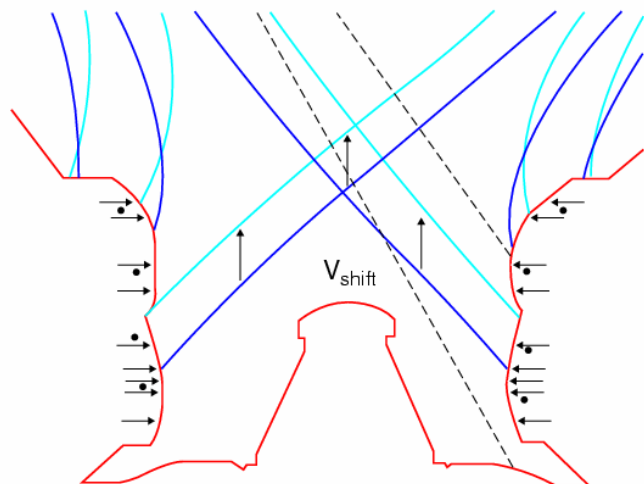
Power Exhaust: Outline



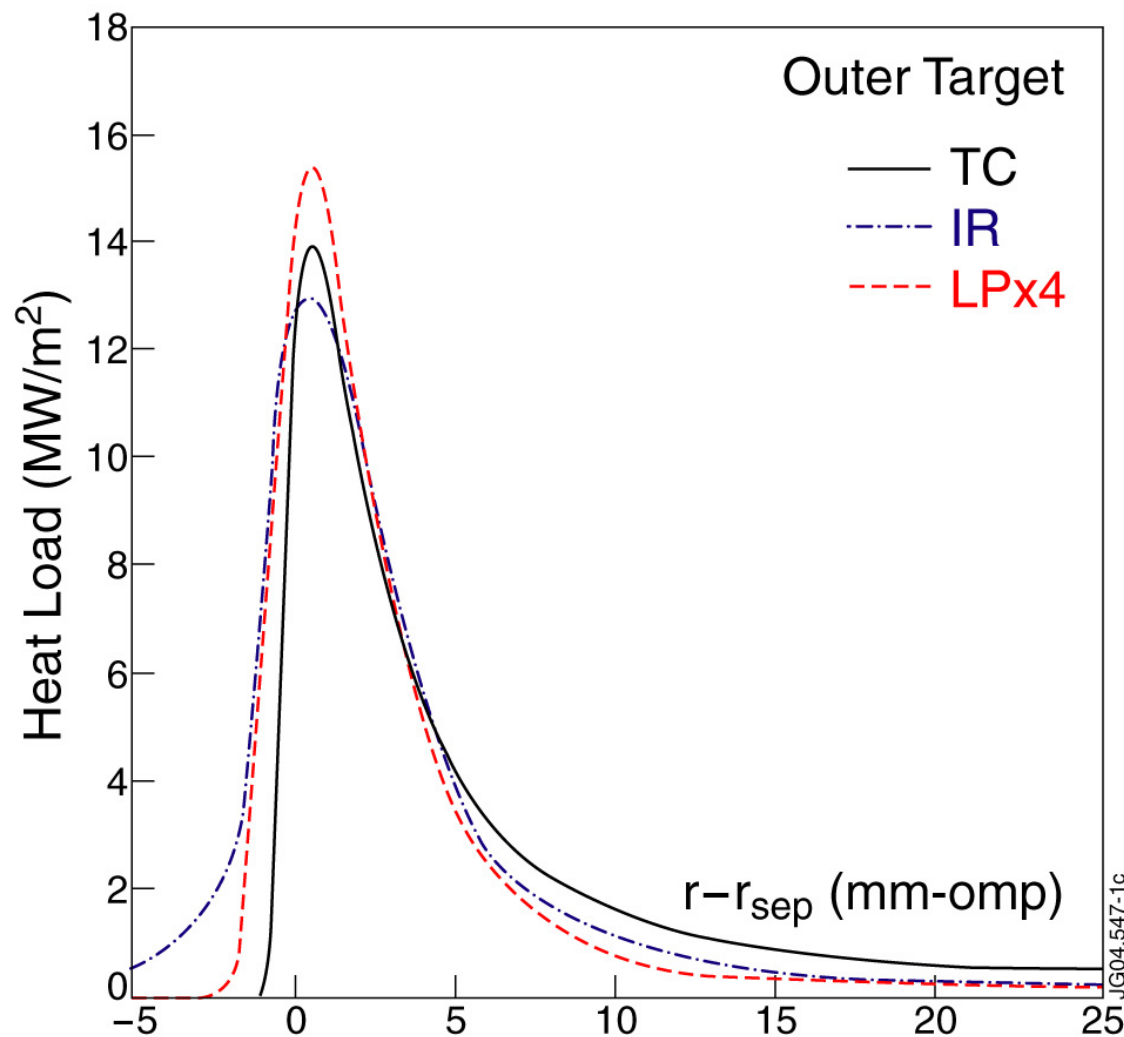
- **Steady-state (inter-ELM)**
 - fwd-B
 - rev-B
- **Transient (ELMs)**
 - JET
 - AUG



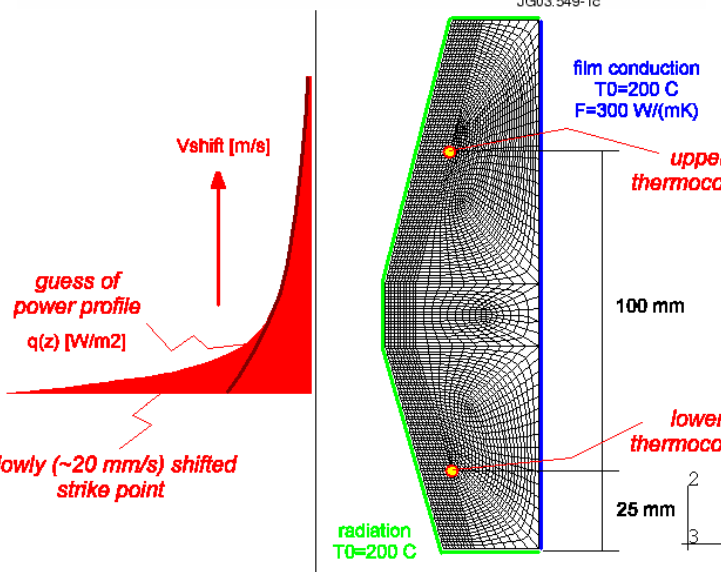
Divertor Target Power Deposition: IR, TC, LP



JG03.549-1c



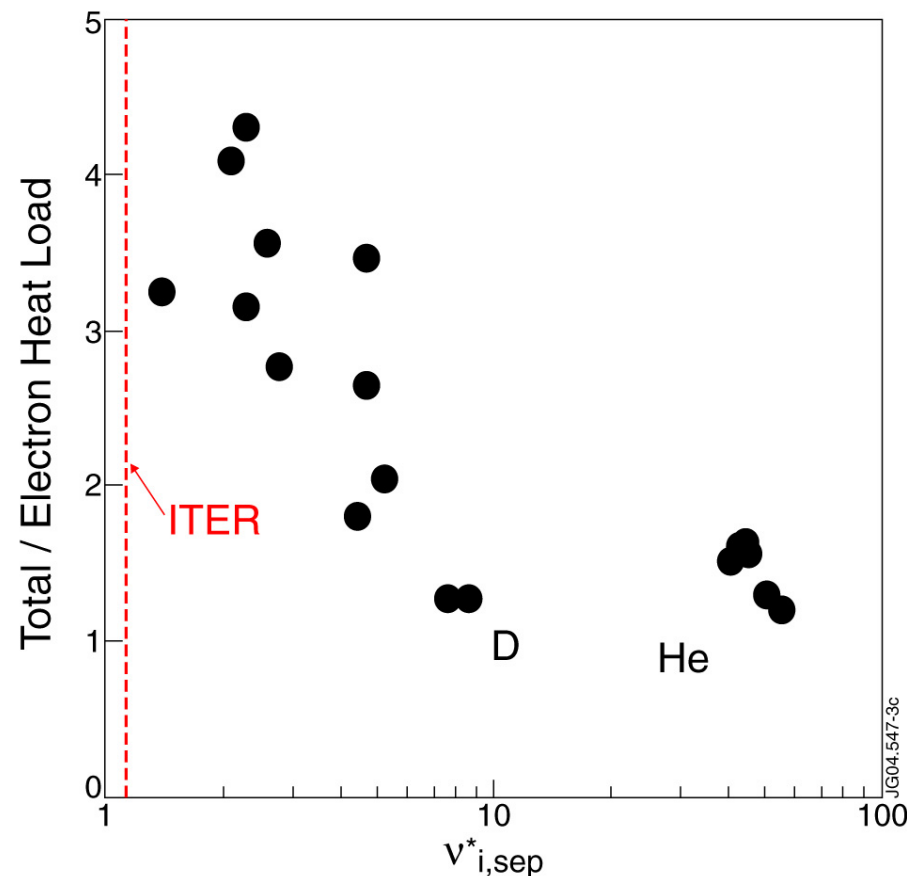
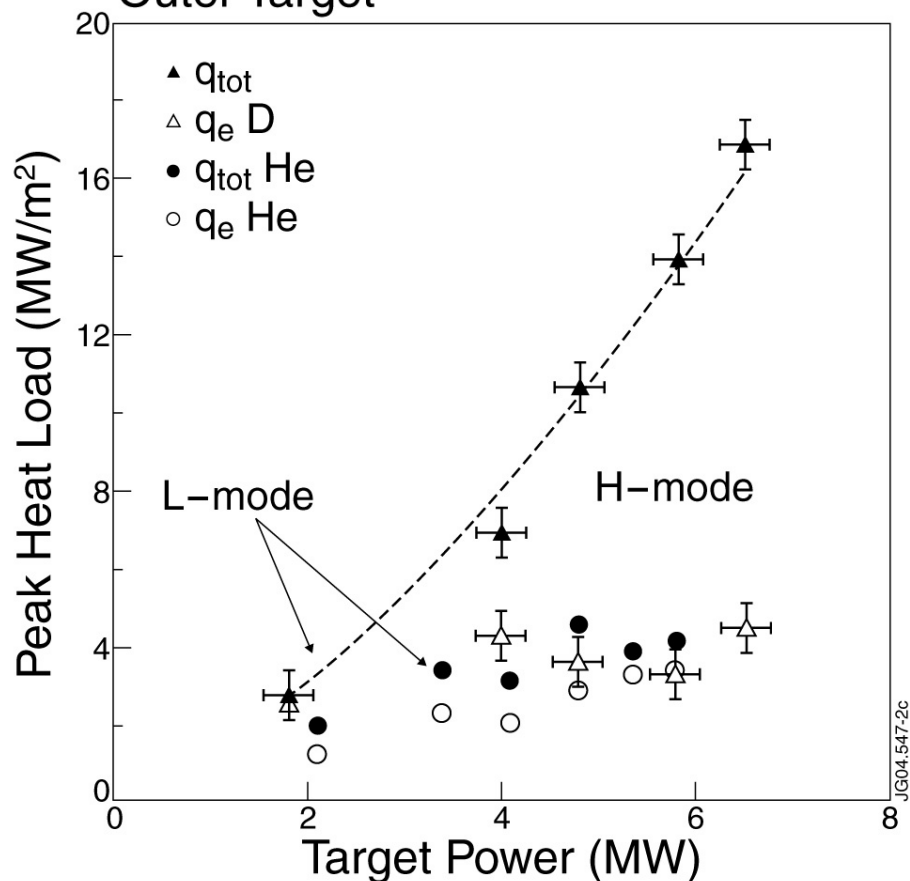
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Forward field (fwd-B) ELMy H-modes: $B \times \nabla B \downarrow$

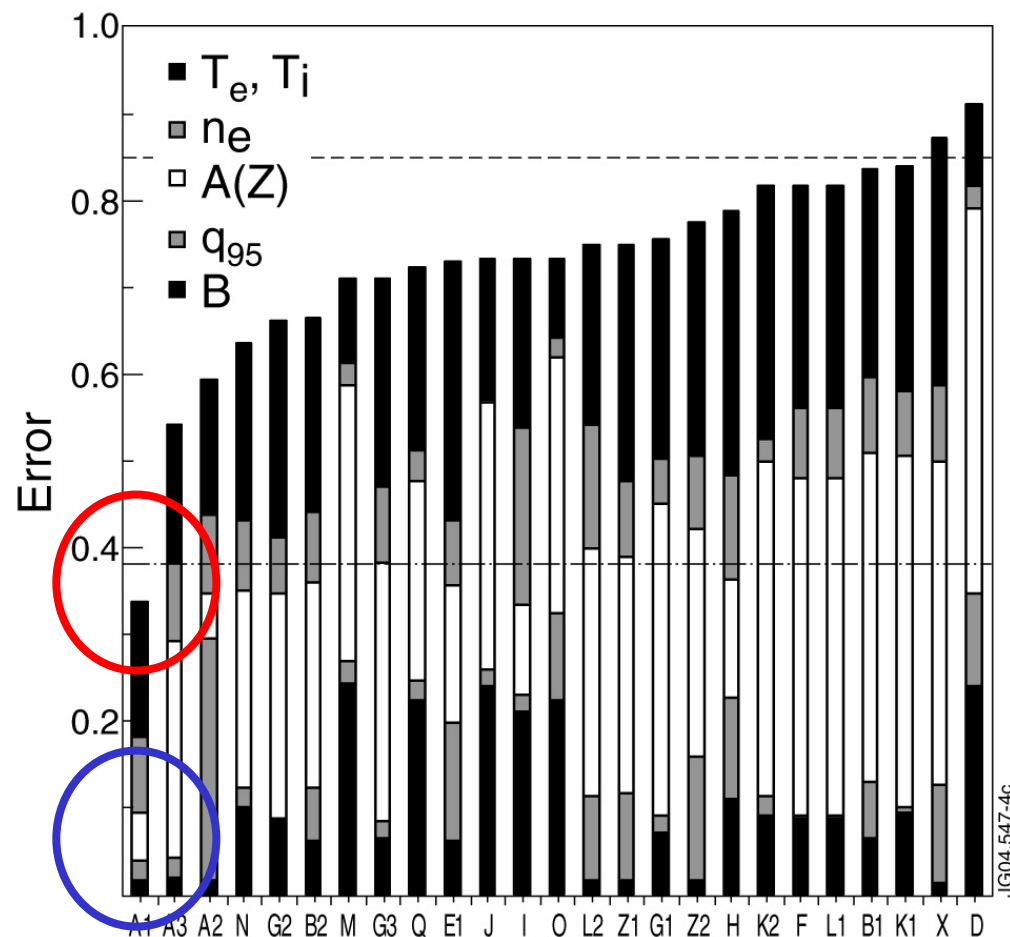
$$\lambda_q^H \propto A(Z)^{1.1 \pm 0.12} B_\phi^{-0.93 \pm 0.2} q_{95}^{0.41 \pm 0.27} P_{\text{div}}^{-0.48 \pm 0.09} n_e^{0.15 \pm 0.13}$$

Outer Target



Comparison with theories of \perp SOL energy transport

$$\lambda_q^H \propto A(Z)^{1.1 \pm 0.12} B_\phi^{-0.93 \pm 0.2} q_{95}^{0.41 \pm 0.27} P_{\text{div}}^{-0.48 \pm 0.09} n_e^{0.15 \pm 0.13}$$



Scaling and Magnitude consistent with classical ion conduction

$$\lambda_q \sim 2.25 \lambda_q^{A1} \sim 0.27 \lambda_q^{A2}$$

$$\chi_\perp^{\text{SOL}} \sim (1-5) \chi_\perp^{A1}$$

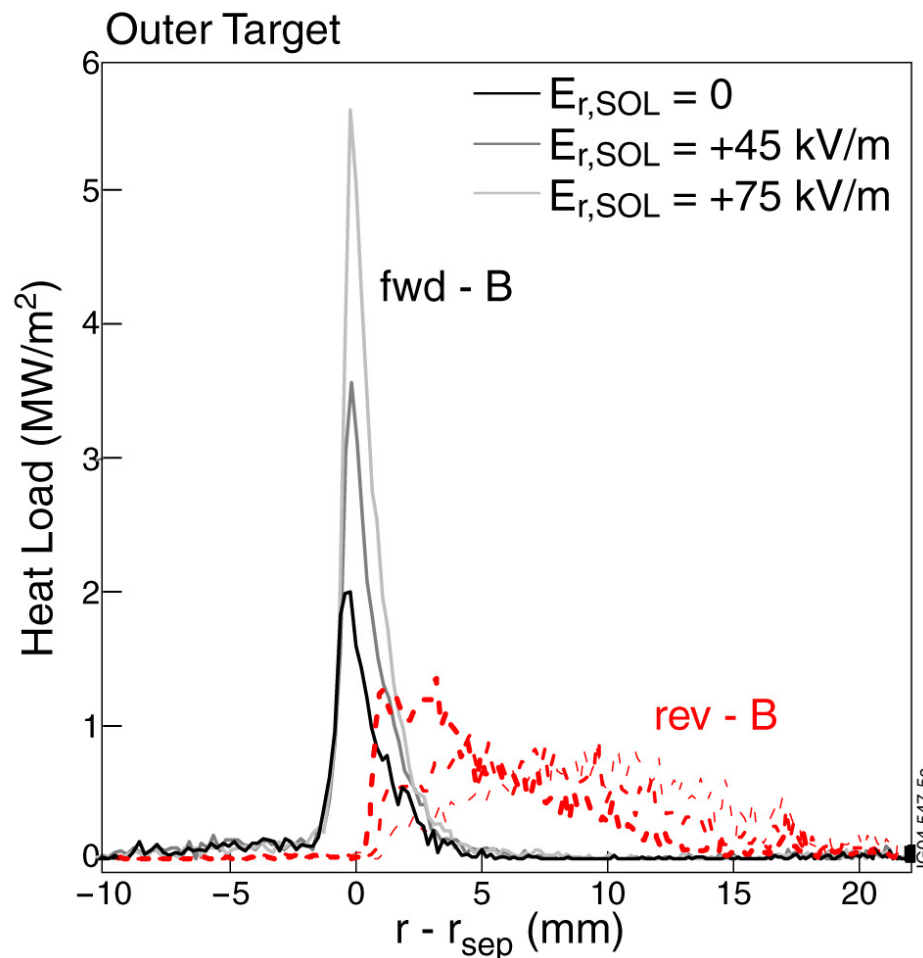
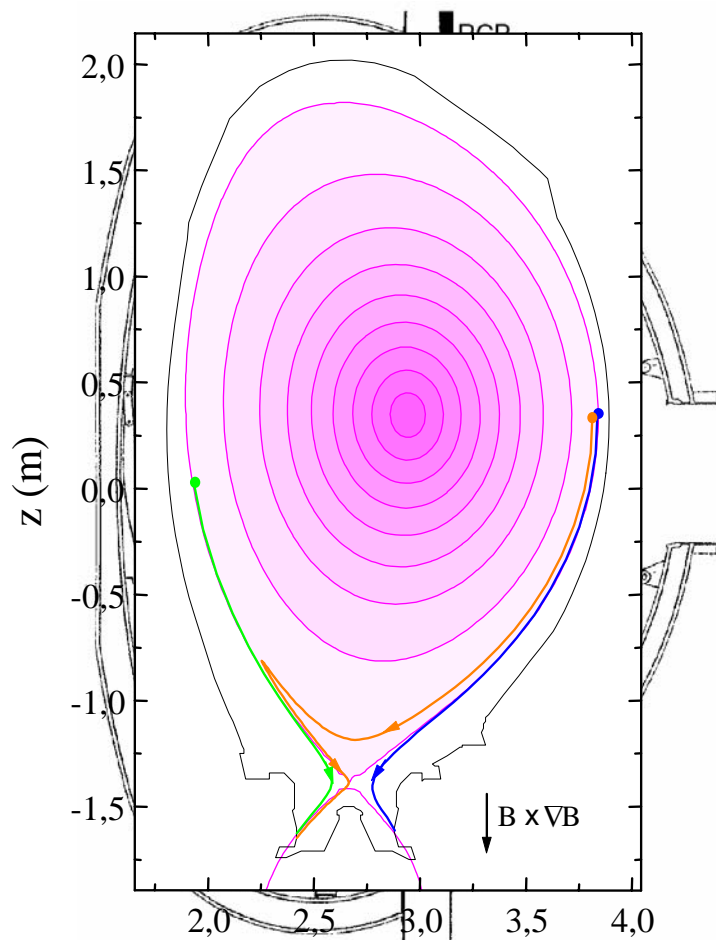
as well as collisionally modified ion orbit loss

$$\lambda_q \sim 2.4\zeta\lambda_q^{A1} + (1-\zeta)\lambda_q^{\text{IOL}},$$

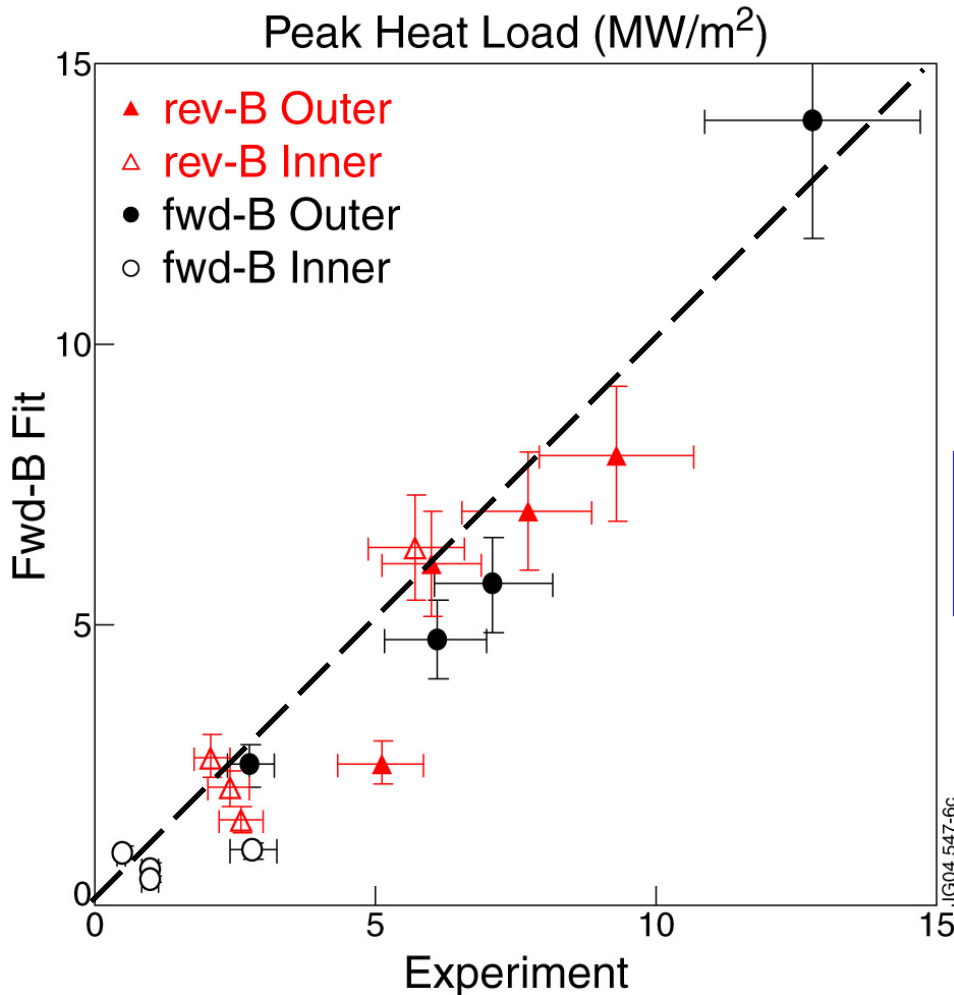
$$\zeta = v_i^* / (1 + v_i^*)$$

Ion orbit loss (ASCOT) profiles: fwd-B vs. rev-B

Very sensitive to field reversal; outer profile broadened



Reversed field (**rev-B**) ELMy H-modes: $B \times \nabla B \uparrow$



Rev-B peak heat flux well matched by **fwd-B** scaling

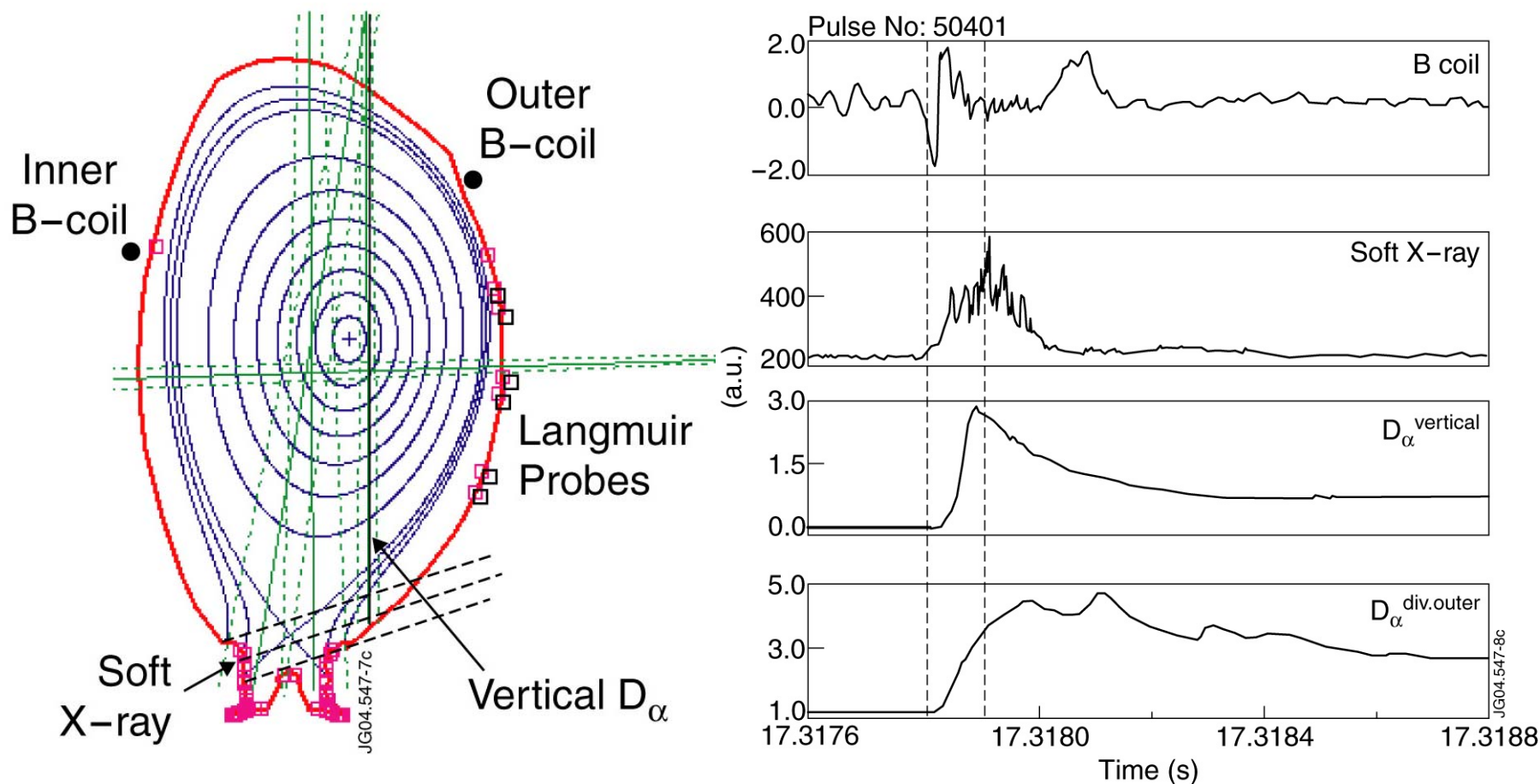
∴ Radial profiles and transport, insensitive to $B \times \nabla B$ direction !

Consistent with neo-classical ion conduction, but **not** ion orbit loss!

ITER prediction: $\lambda_q^{\text{TC}} \sim 3.7 \pm 1.1 \text{ mm}$ at entrance to divertor volume

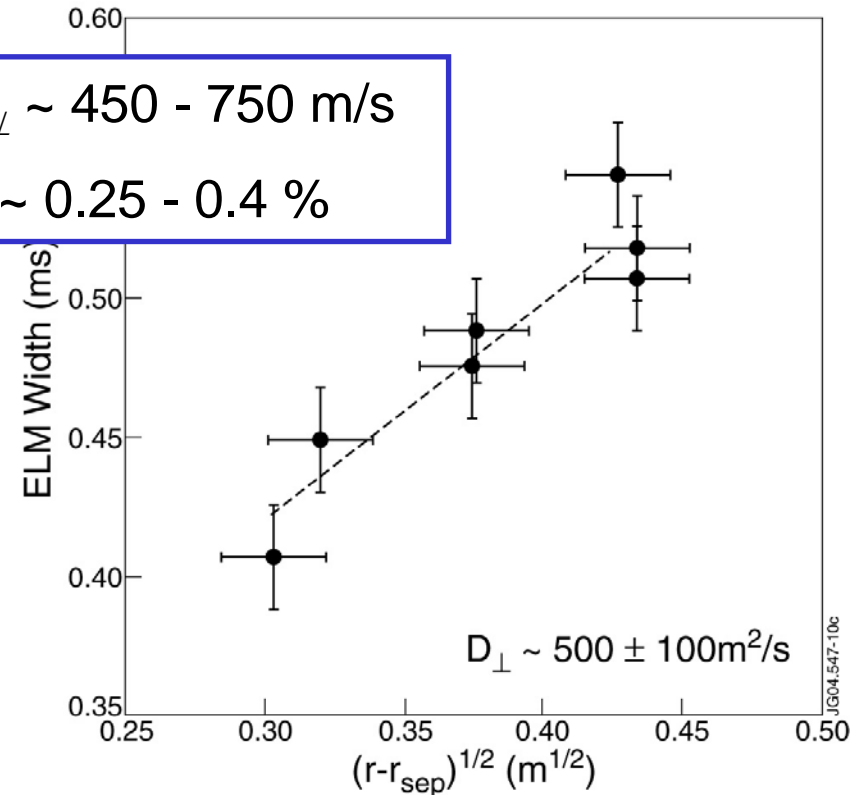
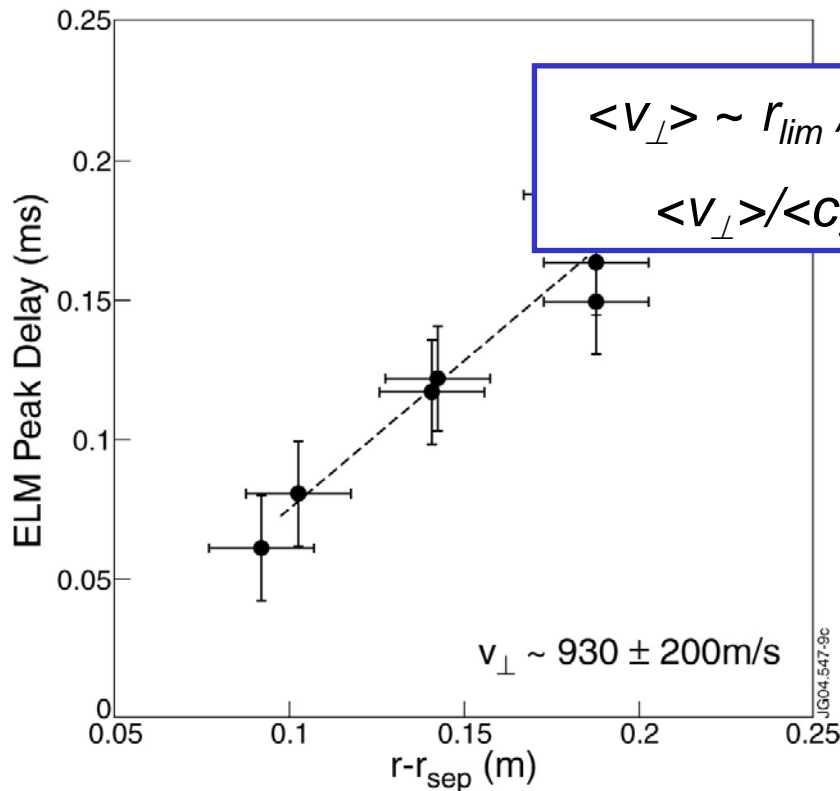
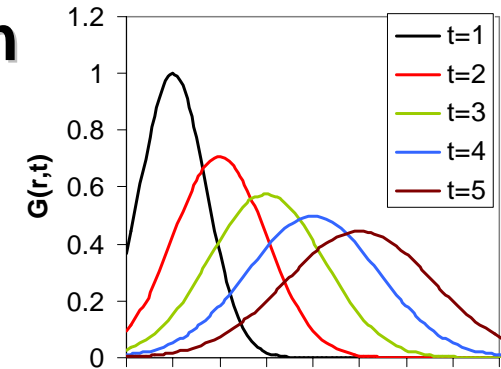
ELM power exhaust experiments

$$\Delta t_{\parallel} \sim 125 \pm 70 \mu\text{s} \sim \tau_{\parallel} \sim L_{\parallel} / c_{s,ped}$$



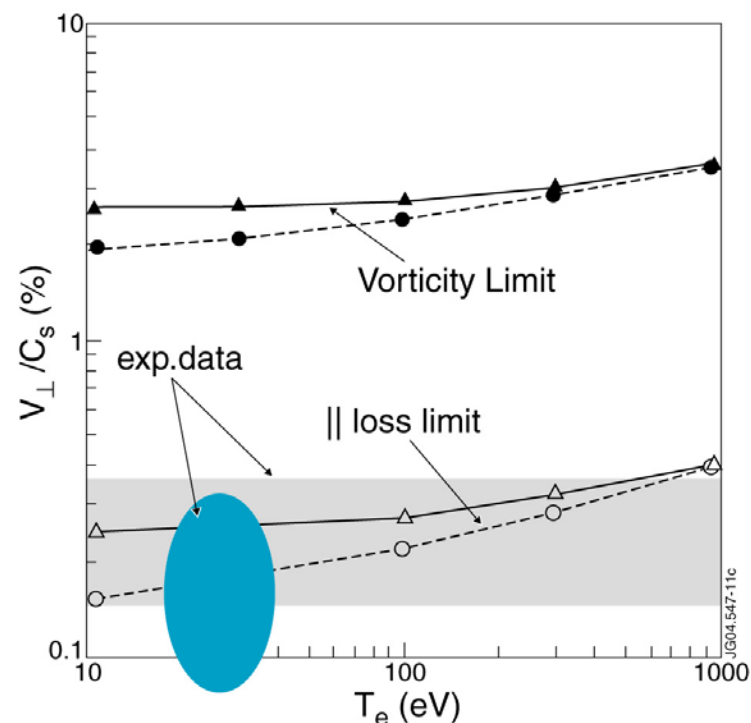
Advective-diffusive radial ELM propagation

$$G(t, r) = \frac{A}{\sqrt{D_{\perp} t}} \exp\left(-\frac{(r - v_{\perp} t)^2}{D_{\perp} t} - \frac{t}{\tau_{\parallel}}\right)$$



Comparison with theory: plasmoid propagation model

⊥ drive mechanism = sheath resistivity, curvature and $E \times B$ drifts



ELM values:

$$\delta_{\theta} \sim \delta_r < 10 \text{ cm}$$

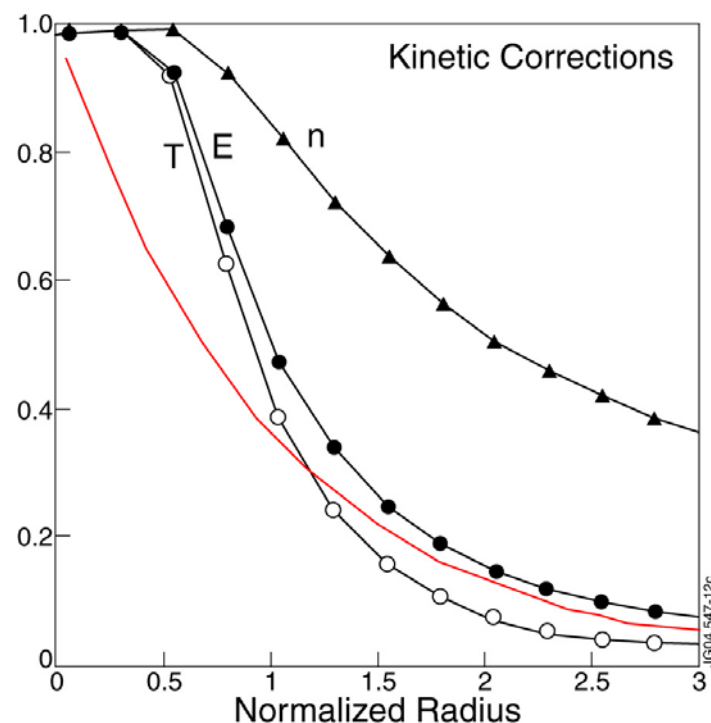
$$\lambda_n < 12 \text{ cm}$$

$$T_{e,\text{lim}} \sim 25 \text{ eV}$$

$$T_{i,\text{lim}} > 75 \text{ eV}$$

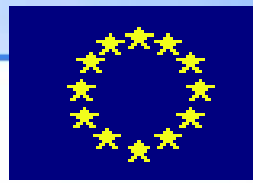
$$\lambda_{Te} < 3 \text{ cm}$$

$$\lambda_{Ti} < 8 \text{ cm}$$



ITER limiter load: $\lambda_{Te} < 3 \text{ cm}$, $\lambda_{Ti} < 6 \text{ cm}$ with $r_{\text{lim}} = 5 \text{ cm}$

$$n_e < 3.0 \times 10^{19} \text{ m}^{-3}, \quad T_i \sim 2.5 T_e < 1.0 \pm 0.2 \text{ keV}$$



Wall and Divertor Load during ELMy H-mode and Disruptions in ASDEX Upgrade

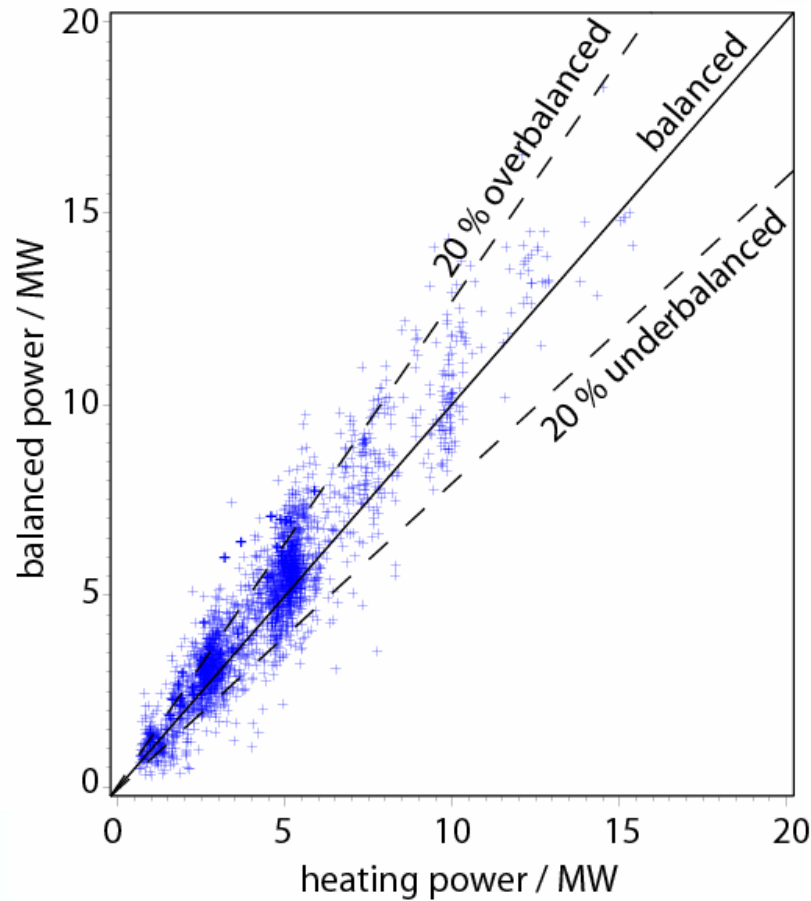
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Presented by W. Fundamenski

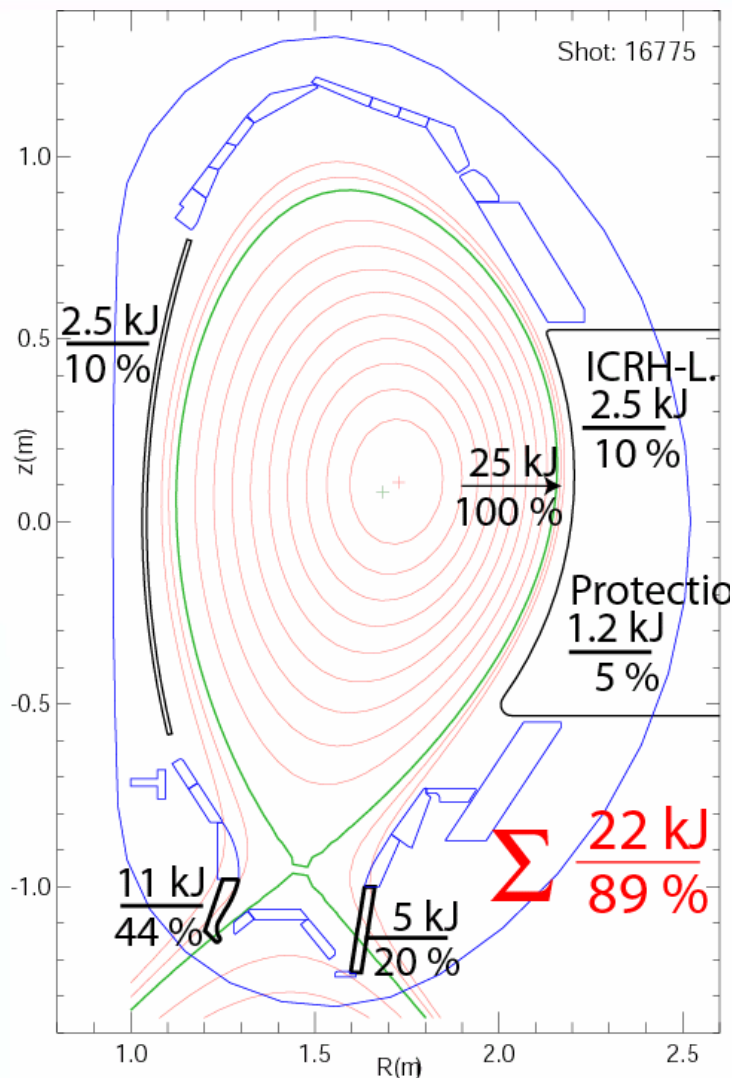


Global power balance within 20 %

but power on main chamber due to hot spots, ELMs and Disruptions



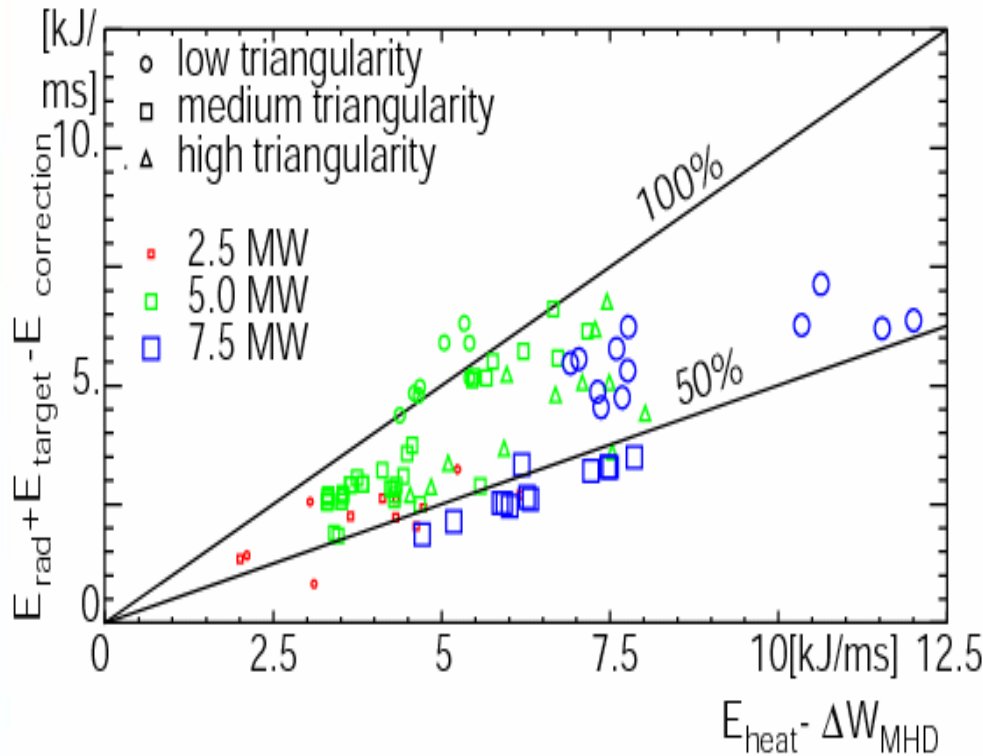
25% of ELM energy to main chamber wall



- fair power balance at $\sim 90\%$
- measured by IR
- calibrated by TC and calorimetry
- 10% of ELM energy to inner wall
- 15% of ELM energy to outer wall
- ELM radiation ?



10 to 40 % of ELM energy radiated

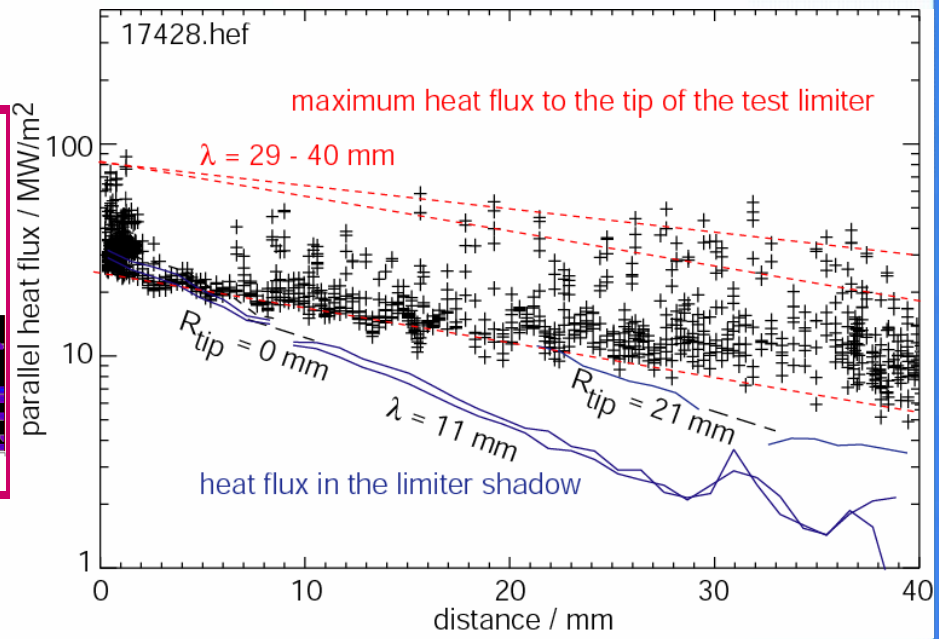
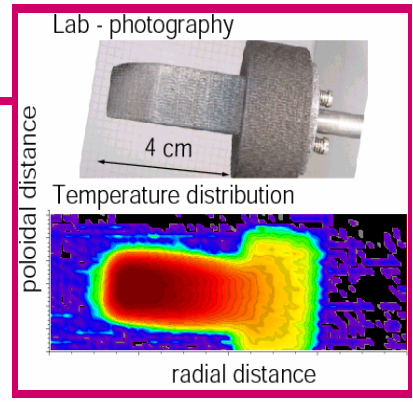
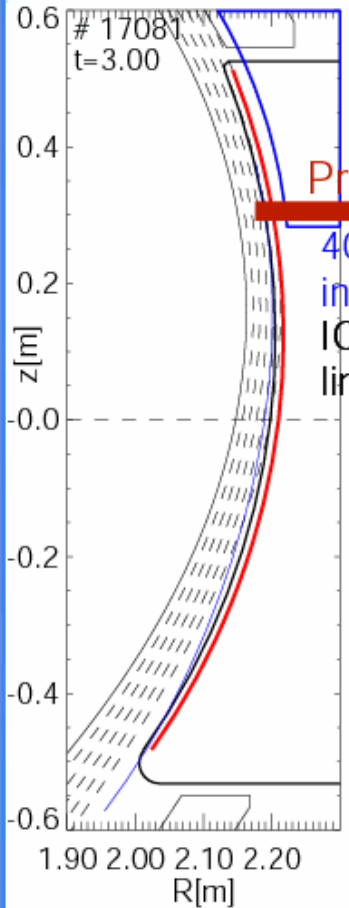


- Mostly in inner divertor
- Independent of ELM size and density
- reduction with triangularity
- tendency to be overbalanced



Test limiter probe measures ELM power profile

separatrix moved from 2.5 cm to 6.5 cm away from the limiter



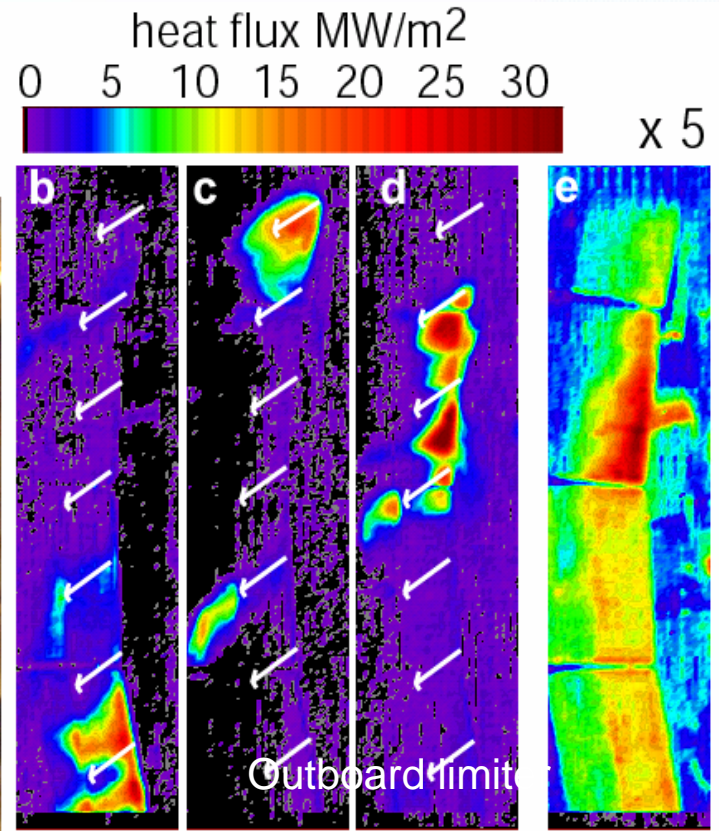
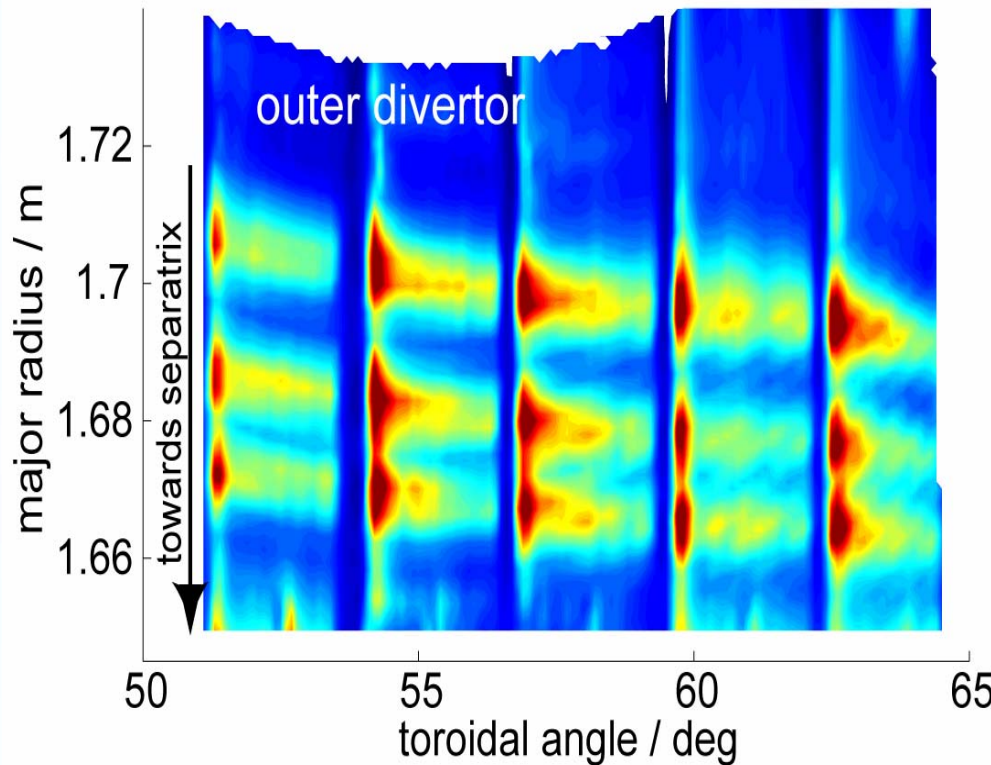
- inter-ELM and ELM power decay lengths in the SOL ~ 3-4 cm
- consistent with $v_{\perp}/c_s \sim \text{constant}$, for turbulent eddies and ELMs
- power decay lengths in the limiter shadow ~ 1-2 cm



Helical ELM filaments observed

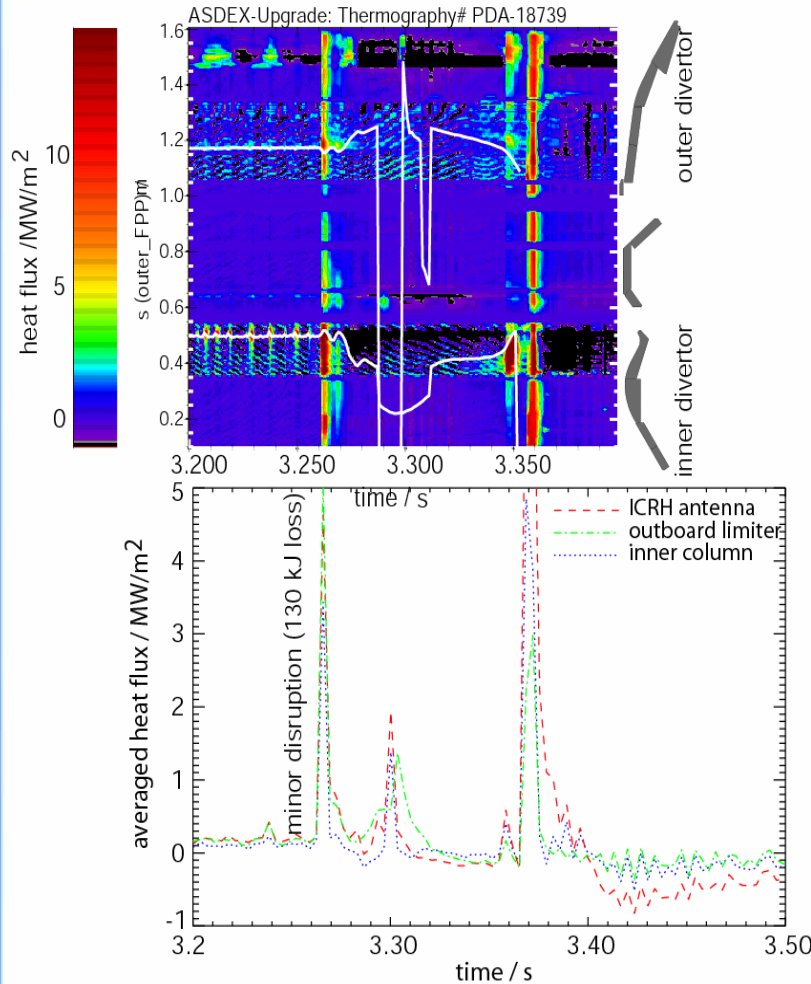
on upper outer divertor and outboard limiter

- Stripe energy content $\ll 1\%$ of total
- $v_{\text{tor}}^{\text{ELM}} \sim 350 \text{ Hz} \ll 3.5 \text{ kHz} \sim v_{\text{tor}}^{\text{inter-ELM}}$





Disruption heat load to main chamber wall



- density limit disruption
- ~ 90% lost in thermal quench phase
- heat deposition
 - fast rise: 0.1-0.5 ms
 - duration: few ms
- strong broadening on target
- significant power to non-divertor components.

See A. Loarte, this conference



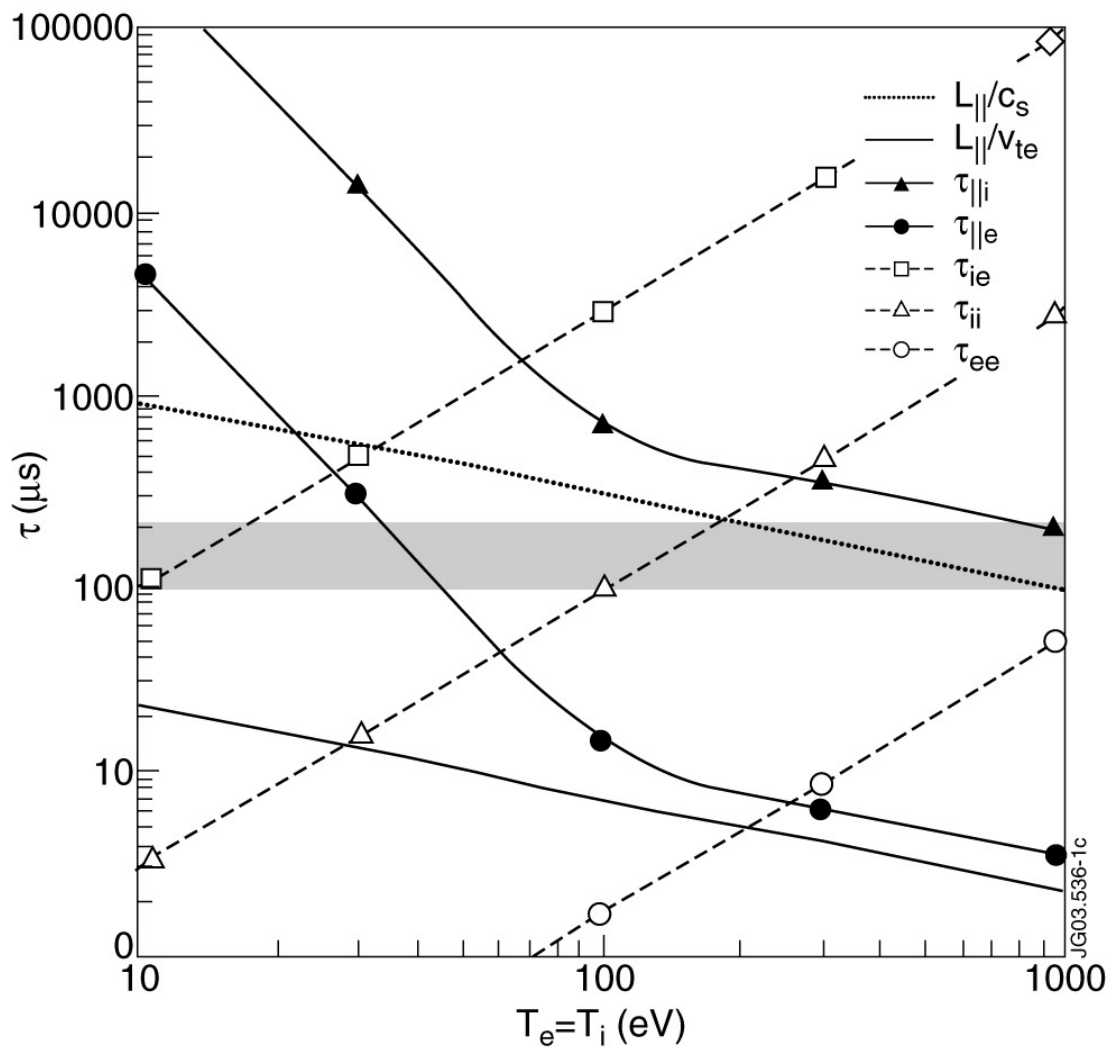
Conclusions (JET and AUG):

- Steady state, Type-I ELMy H-mode radial power exhaust on JET dominated by weakly collisional ions
 - experimental data well matched by neo-classical ion conduction
 - predicts tolerable divertor heat loads for ITER
- Helical ELM structure observed on AUG
- Type-I ELM radial velocity agrees with sheath limited model (JET)
- ELM power decay length comparable to outer gap on JET and AUG
 - could pose problems for beryllium limiter on ITER
- Broad footprint (divertor and first wall) of heat flux deposition during disruption observed on AUG

Power Exhaust Summary:

		AUG	JET	ITER
Steady state (inter-ELM)	Electron	Interchange & drift wave turbulence		
	Total	–	(neo-)classical ion conduction	$\lambda_q \sim 4 \text{ mm}$
Transient (intermittent eddies, ELMs)	Electron	$\lambda_{qe}/R \sim 2 \%$	$\lambda_{qe}/R \sim 1 \%$	$\lambda_{qe} < 3 \text{ cm}$
	Total	Advection-diffusion $\lambda_q/R < 2 \%$		$\lambda_q < 6 \text{ cm}$

Characteristic times in the SOL



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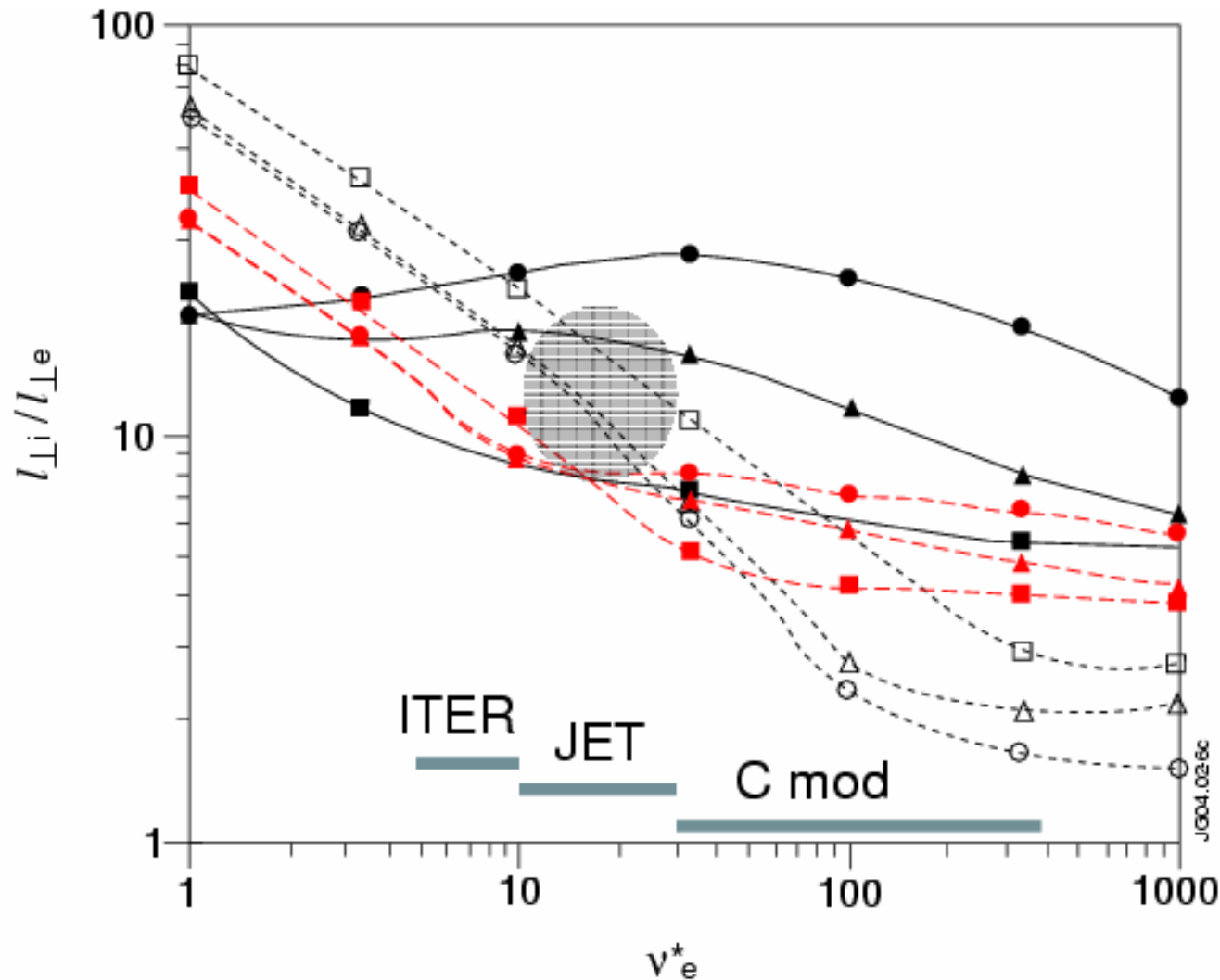
Kinetic estimates of \parallel losses

$$\frac{N(r)}{N(0)} = \frac{\int_0^{v_{cr}} e^{-\beta v^2} dv}{\int_0^{\infty} e^{-\beta v^2} dv} = \operatorname{erf}\left(\frac{\tau_{\parallel}}{\tau_{\perp}}\right) = \operatorname{erf}(\xi^{-1}), \quad 0 < \xi < 1$$

$$\frac{W(r)}{W(0)} = \frac{\int_0^{v_{cr}} v^2 e^{-\beta v^2} dv}{\int_0^{\infty} v^2 e^{-\beta v^2} dv} = \operatorname{erf}(\xi^{-1}) - \frac{2}{\sqrt{\pi}} \xi^{-1} \exp(-\xi^{-2}), \quad 0 < \xi < 1$$

$$\xi \sim \frac{\tau_{\perp}}{\tau_{\parallel}} \sim 1, \quad \xi_i \sim \frac{\tau_{\perp}}{\tau_{\parallel i}} \sim 1, \quad \xi_e \sim \frac{\tau_{\perp}}{\tau_{\parallel e}} \gg 1$$

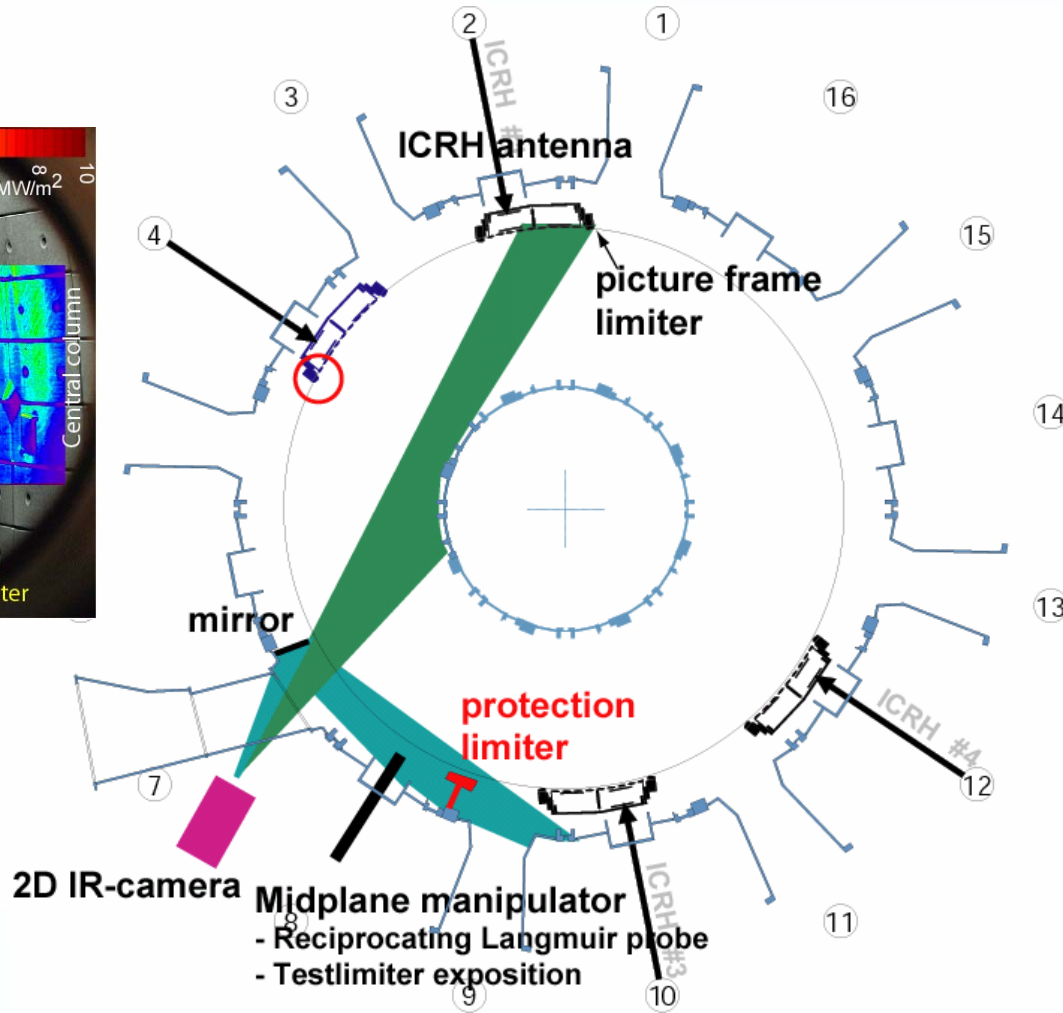
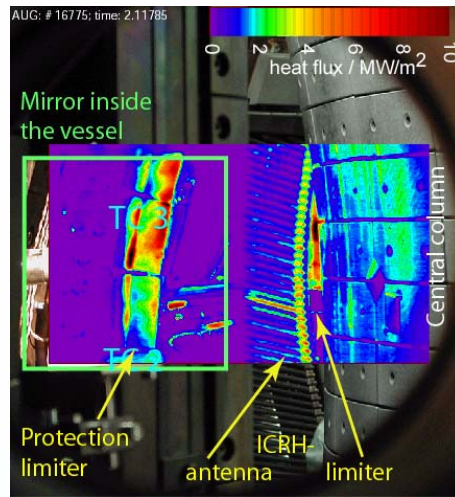
Ratio of ion and electron dissipative scales in the SOL



IR view into the vessel and the limiter positions

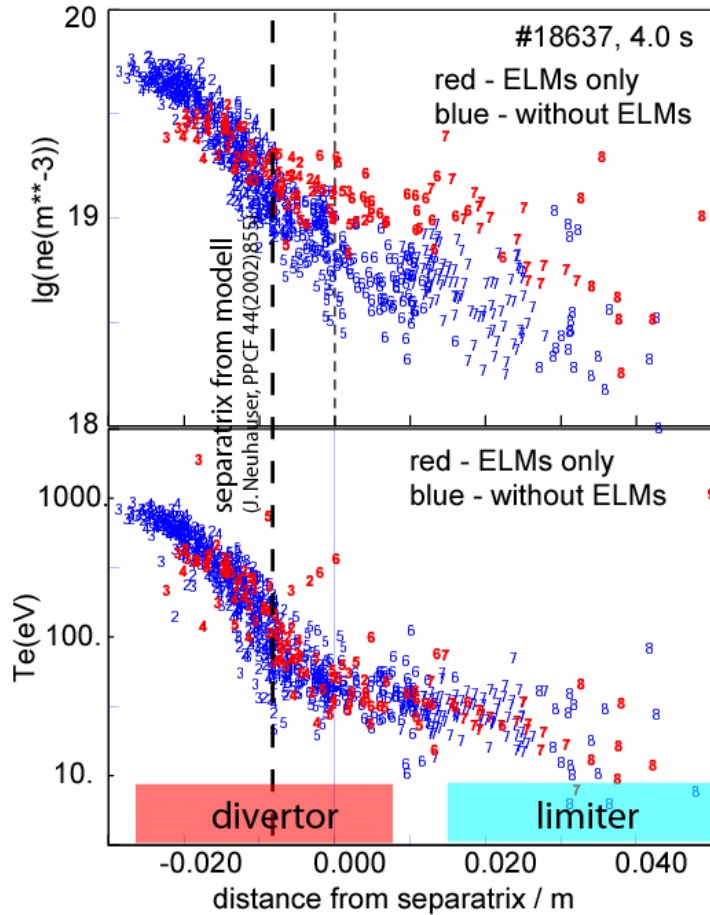


IR camera view





ELM ejected particles and energy partly deposited on limiters



$\lambda(R) \approx 3-8 \text{ mm} \approx 30-80 \text{ mm}$
(3-7 mm in the limiter shadow)

Large variation of ELM signature remote from the separatrix.

ELM structure measured at the upper divertor.

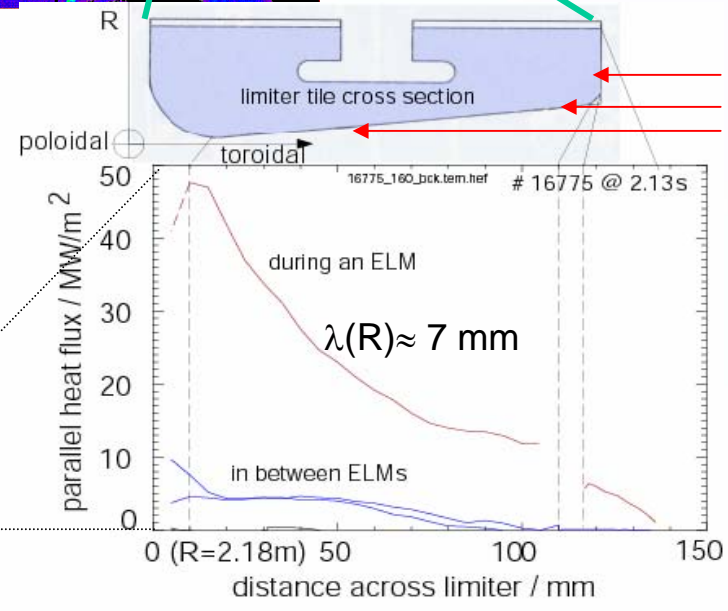
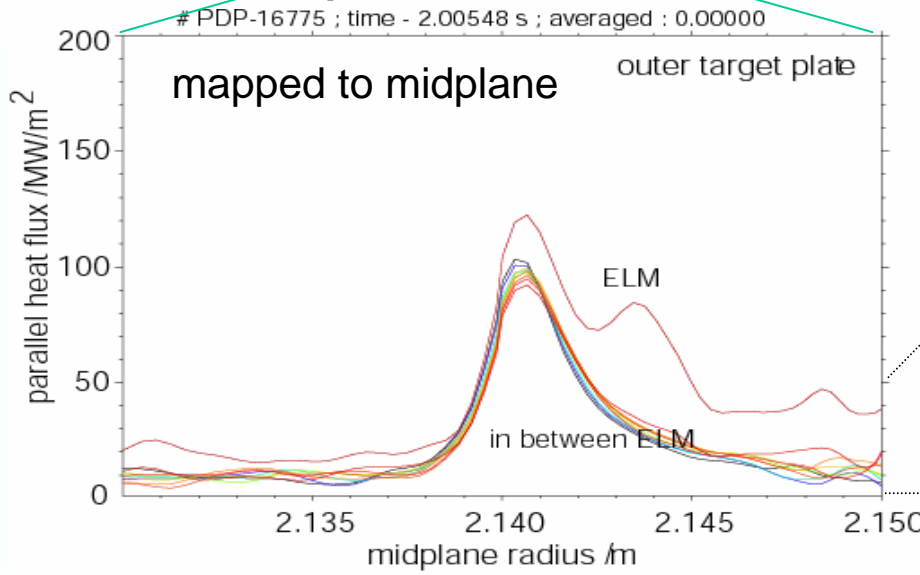
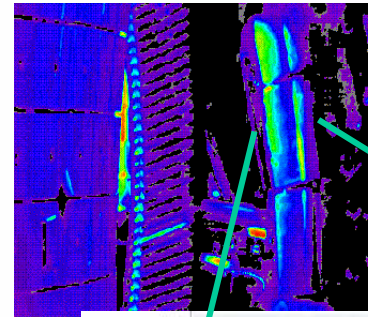
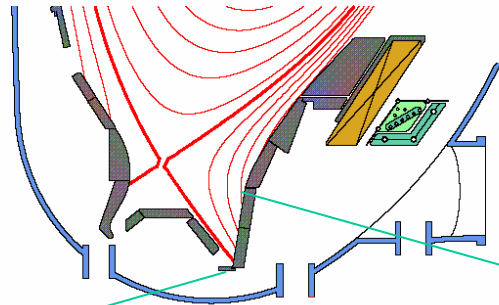
T. Eich, *Physical Review Letters*, 91 (2003)

ELM resolving diagnostics for non divertor heat load

- Thermography
- Langmuir probes
- Test limiters (M.Y. Ye, PSI 2004)

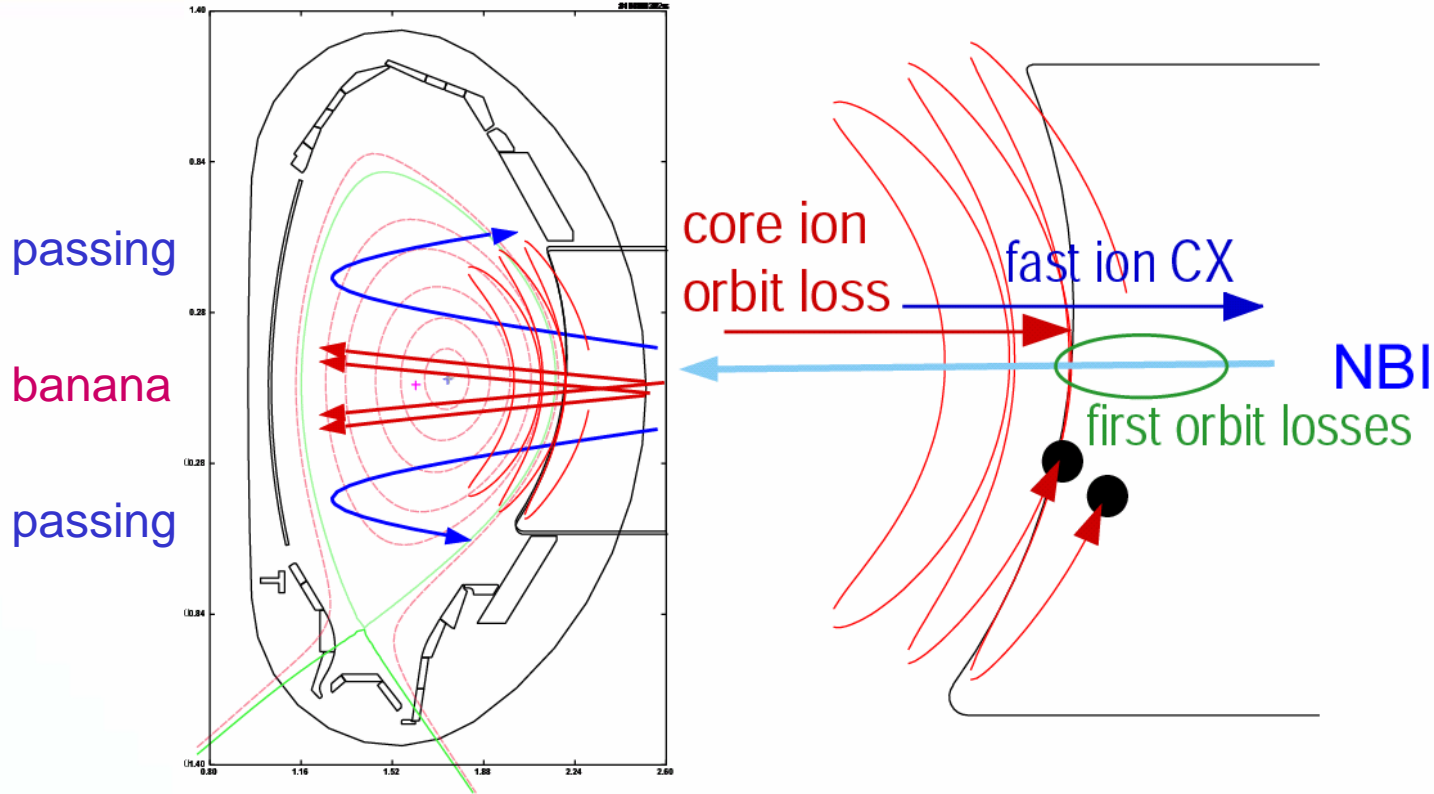


Heat flux values at the far edge of the divertor and the leading edge of the limiter are consistent





Experimental observation of local heat load is qualitatively understood



- Location of the intersection area depends on ionisation source location, magnetic field helicity, co/counter neutral injection and ...
- on non-axisymmetric first wall structure.