

TF Joint Operations Review

Introduction

- ✓ Scope and Outline of Review
- ✓ Summary of Findings from 2004 Run
- ✓ Review of Joint Force, Pressure and Moment Concepts
- ✓ Improvements made on Rebuilt Coil
- ✓ Overview of New Analysis
- ✓ New Operating Envelope

C Neumeyer

2/10/05

Committee Members

P Anderson (GA)

L Dudek (PPPL) - Chair

J Irby (MIT)

B Nelson (ORNL)

A Von Halle (PPPL)

Chit forms have been forwarded to off-site members

Scope of Review

- ✓ Declare targeted operating scenarios/envelope
- ✓ Provide justification for operating envelope
- ✓ Describe protection method to enforce operating envelope
- ✓ Describe commissioning plan

Outline of Review

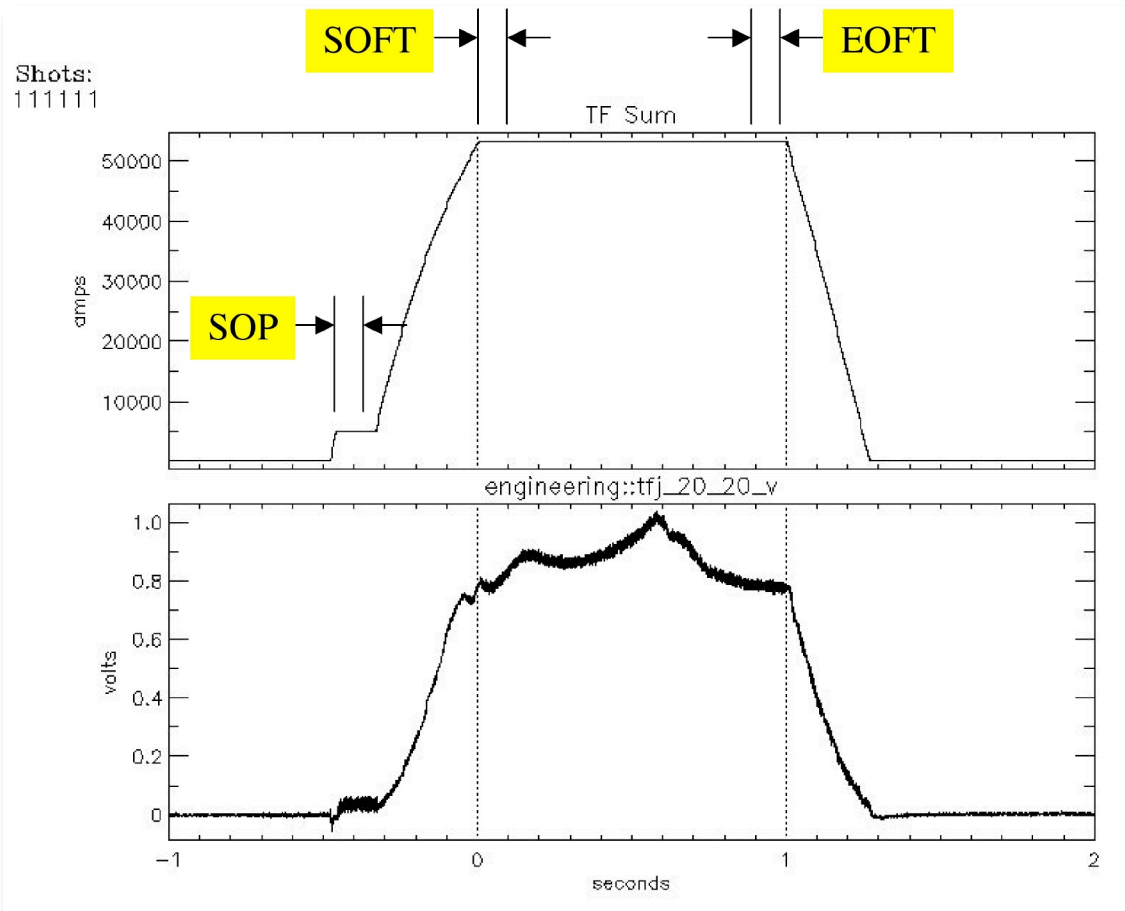
- ✓ Introduction (40 min)
- ✓ Description of New Potting Process (30 min)
- ✓ Simplified Modeling and Protection (30 minutes)
- ✓ Commissioning Plan (20 minutes)
- ✓ Summary (15 minutes)

2+ hours

Results from 2004 Operations

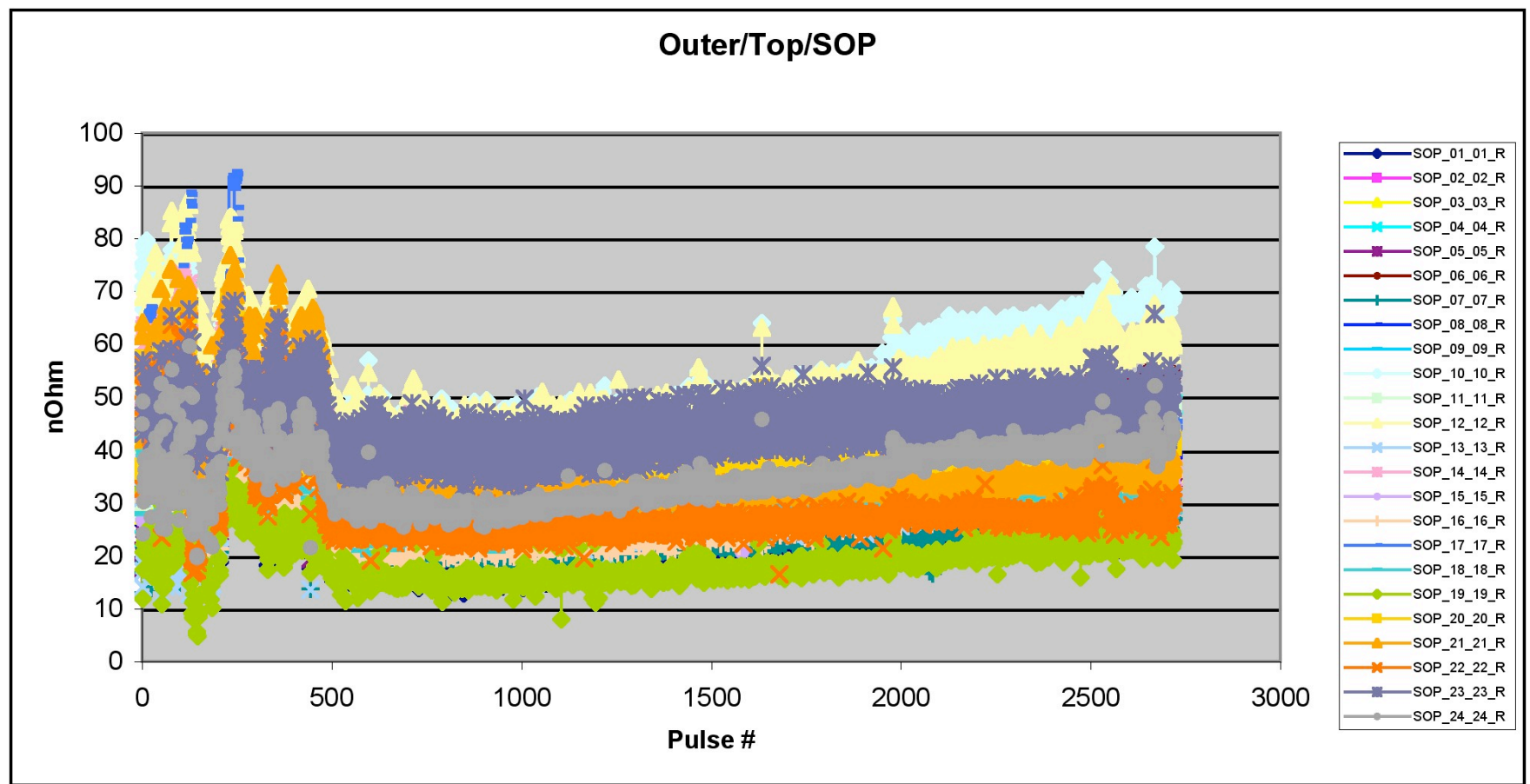
- Approximately 2800 pulses were executed with $Bt \leq 4.5\text{kG}$ (January - July)
- Measurements from initial commissioning results were not well understood and did not benchmark well with design basis (January- February)
- Efforts were initiated to develop refined analytic models and tools to promote better understand of behavior and interpretation of measurement data (February)
- Deeper understanding and tool development, along with upward trending of resistance data, led to concern that structural support system was not functioning properly (June)
- Additional measurements were made which confirmed excess motion of flags and excess moment being applied to joint (July)
- Operating level was reduced to $Bt \leq 3.0\text{kG}$ after ~ 2200 shots (July)
- Disassembly revealed defects in potting of flags in boxes, along with pitting on the contact surfaces (August)

Trending Measurements



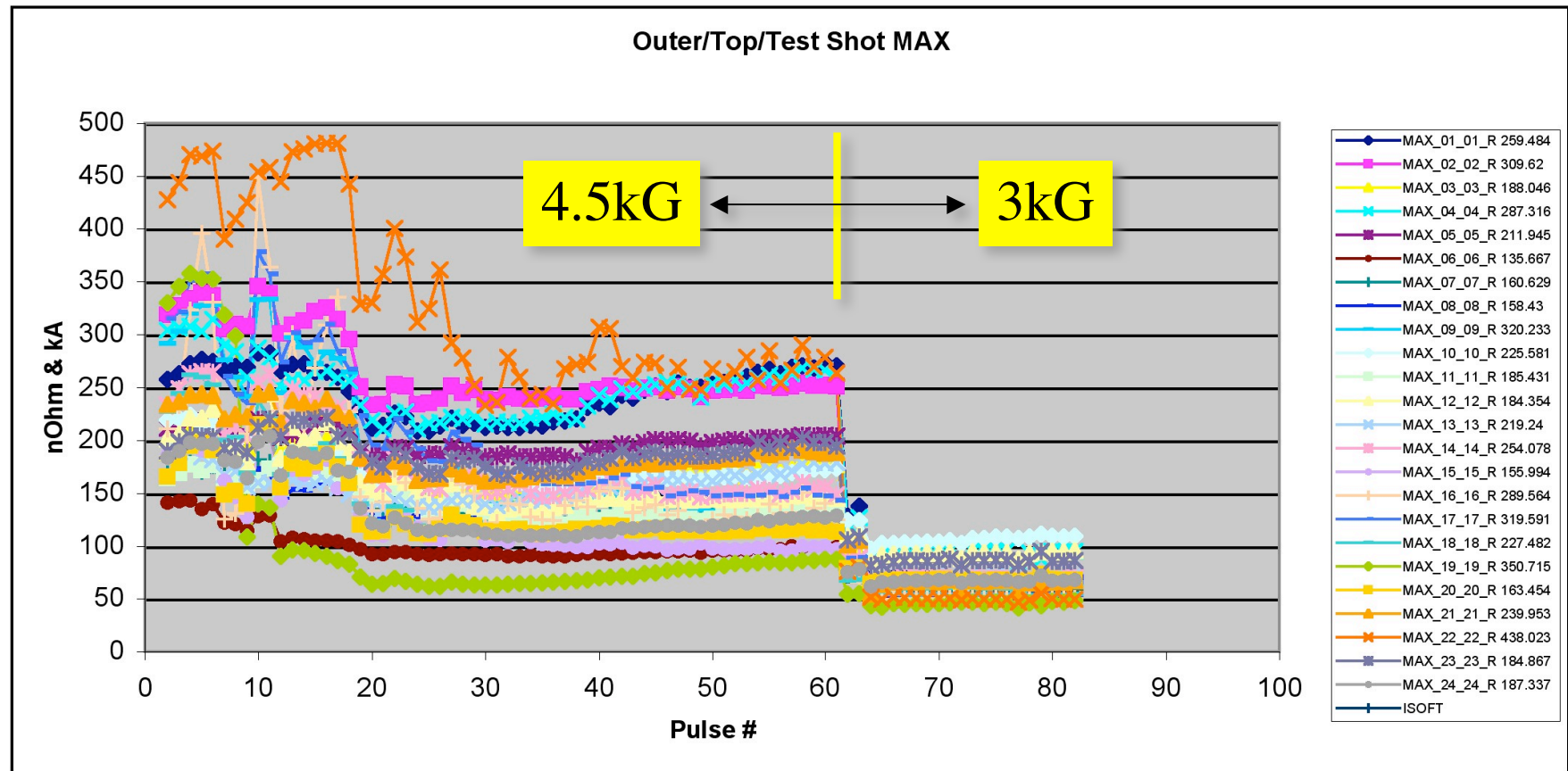
- Resistance Measured At 5kA At Start of Pulse (SOP) And At Other Times (SOFT, EOFT) During Pulse
- Maximum (MAX) Also Recorded Each Pulse

Typ. Resistance Trends at 5kA Pedestal



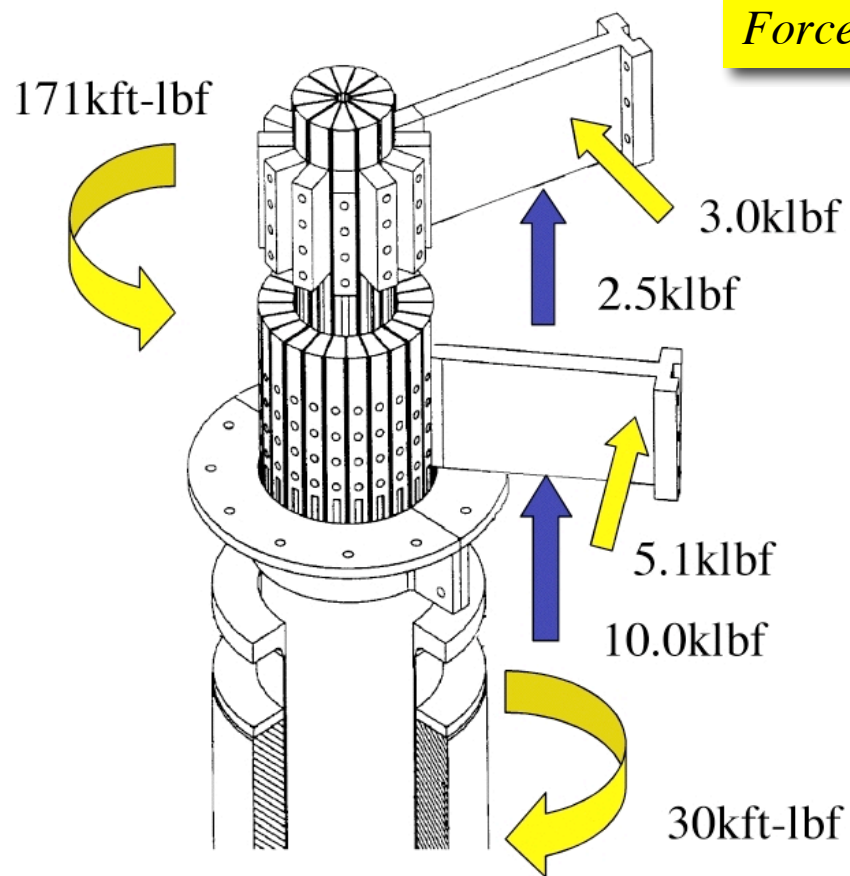
Includes all test shots and plasma shots

Typ. Max Resistance During Test Shots



Includes test shots only

JxB Forces on Flags and Bundle

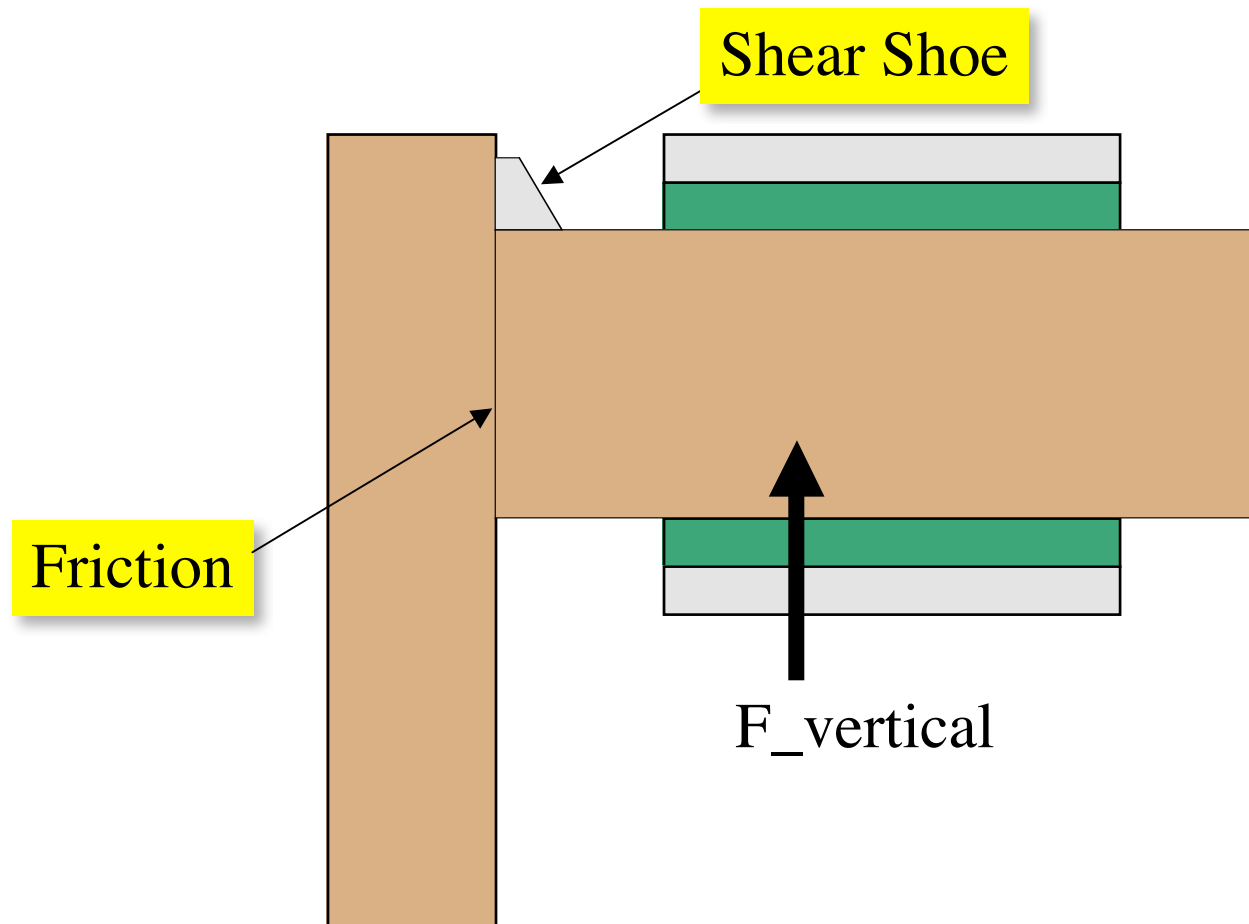


- **In-Plane** ■
 - vertical load and moment due to magnetic pressure from self-field
- **Out-of-Plane** ■
 - lateral due to $I_{tf} \times B_{z(oh\&pf)}$
 - torsional due to $I_{tf} \times B_{r(oh\&pf)}$

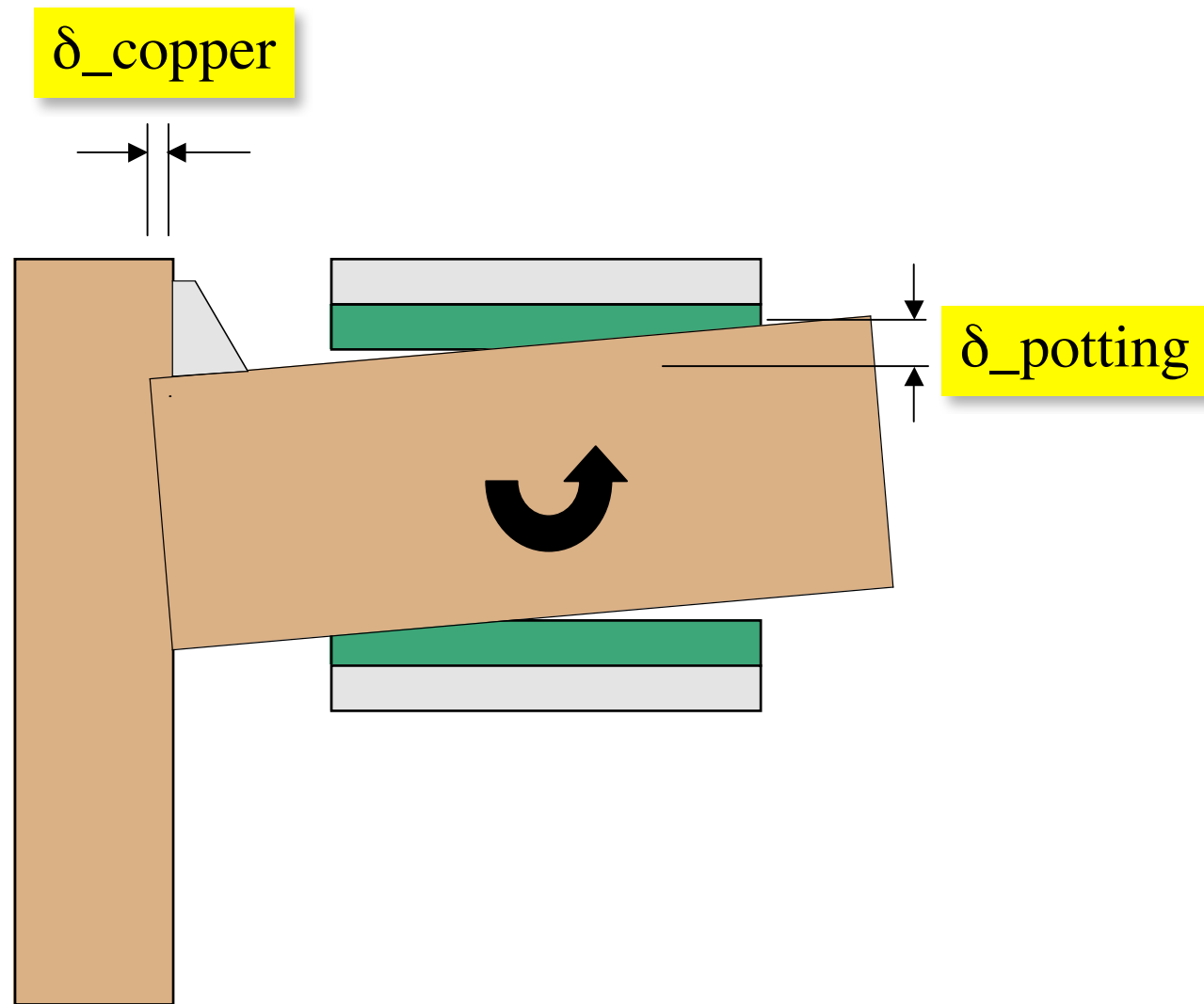
Notes:

- 1) All coils assumed at full current, worst case polarity (conservative)
- 2) Forces equal and opposite on two ends of bundle

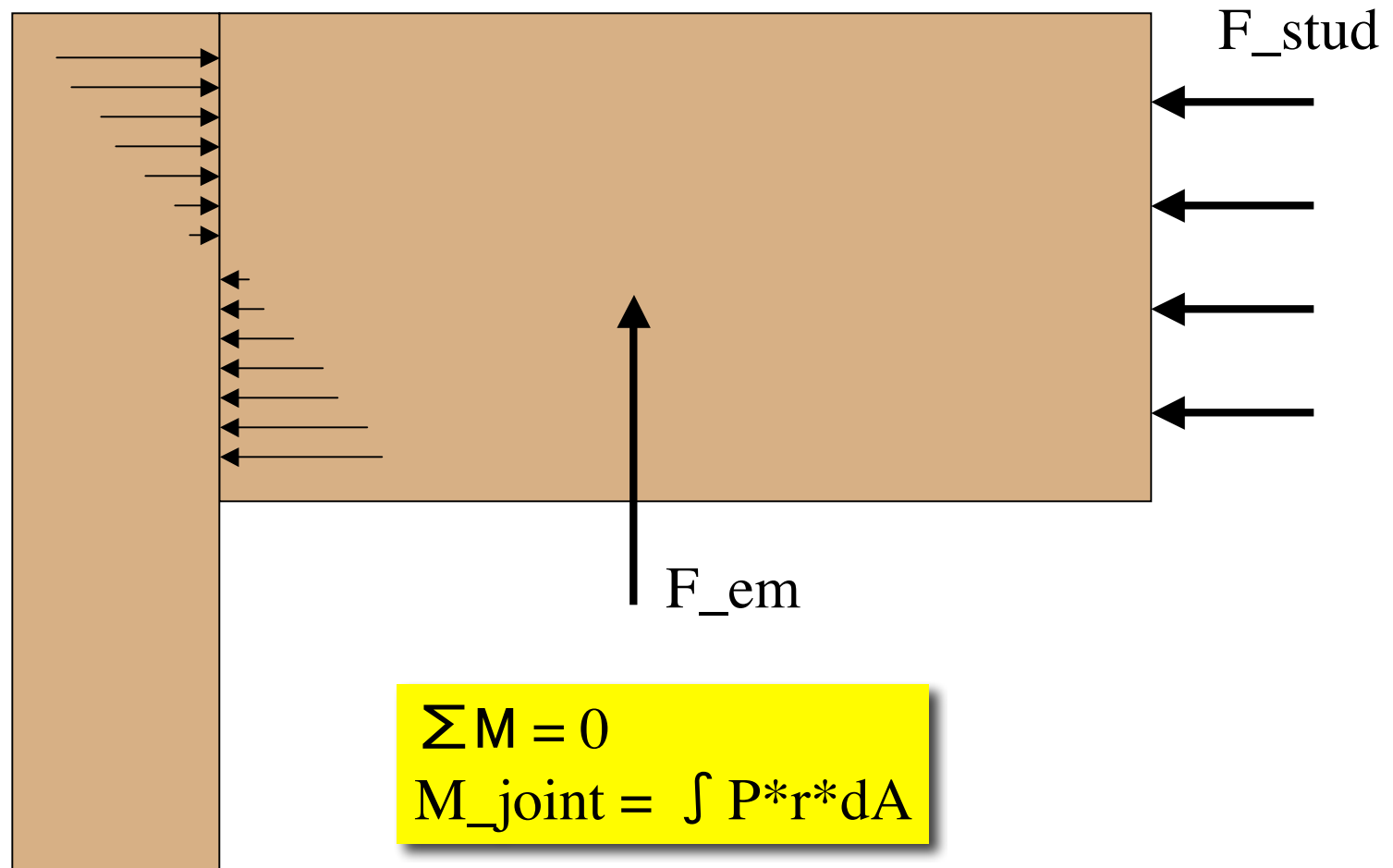
Vertical Loads Taken By Friction and Shear Shoe



Moments Shared by Structure and Joint



Moment Reacted at Joint Related to Pressure Distribution



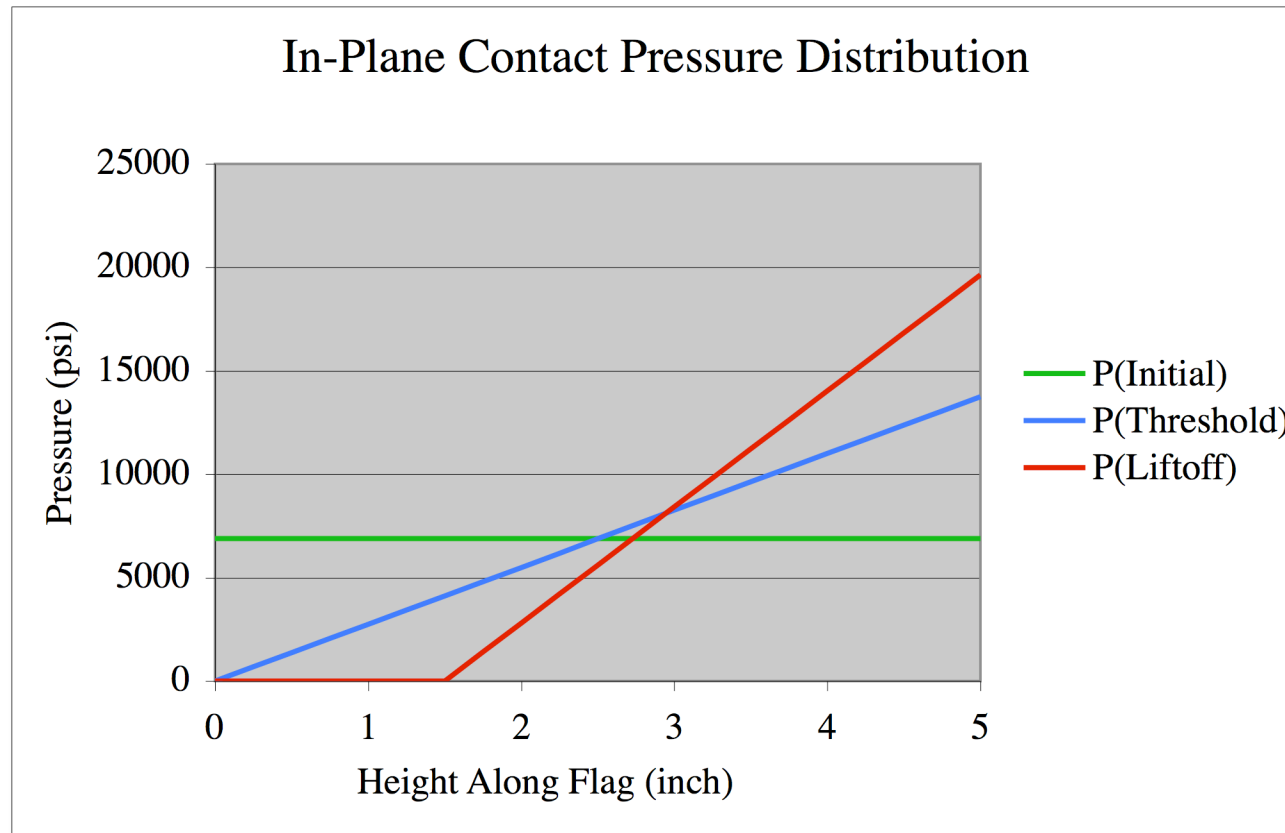
Reaction of Moment By Potting Is Key Factor in Joint Behavior

Excess moment leads to skewed pressure distribution and...

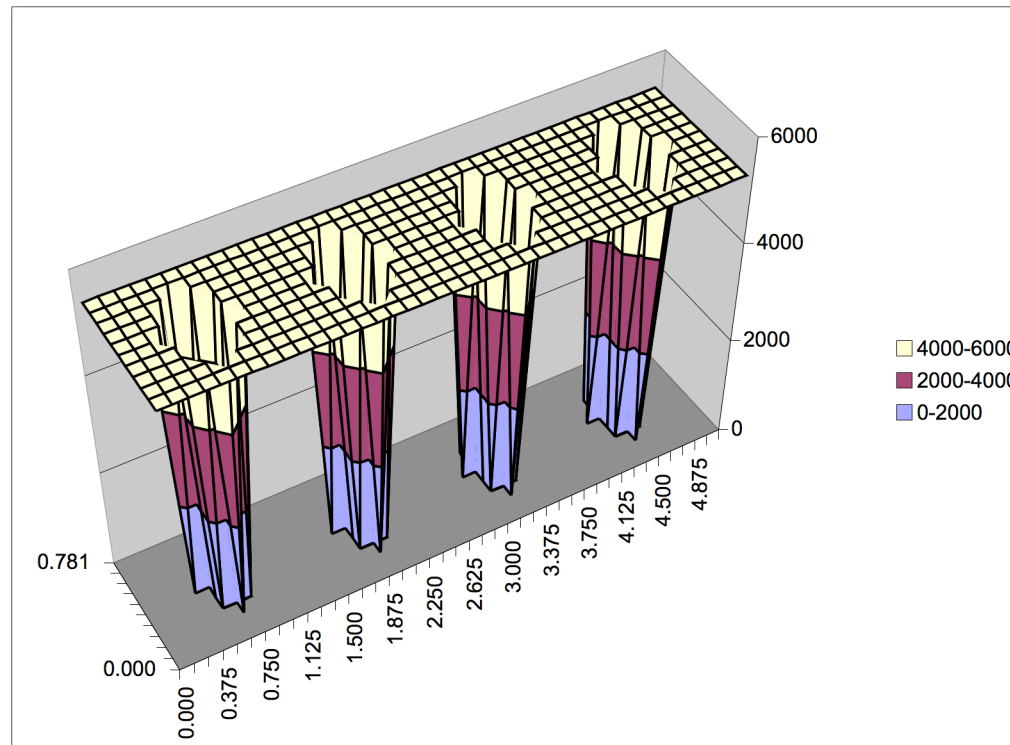
- shift in current pattern
- liftoff during pulse
- excess copper stress

Contact Pressure Distribution is Key Factor

2D Concept of Contact Pressure and “Liftoff”

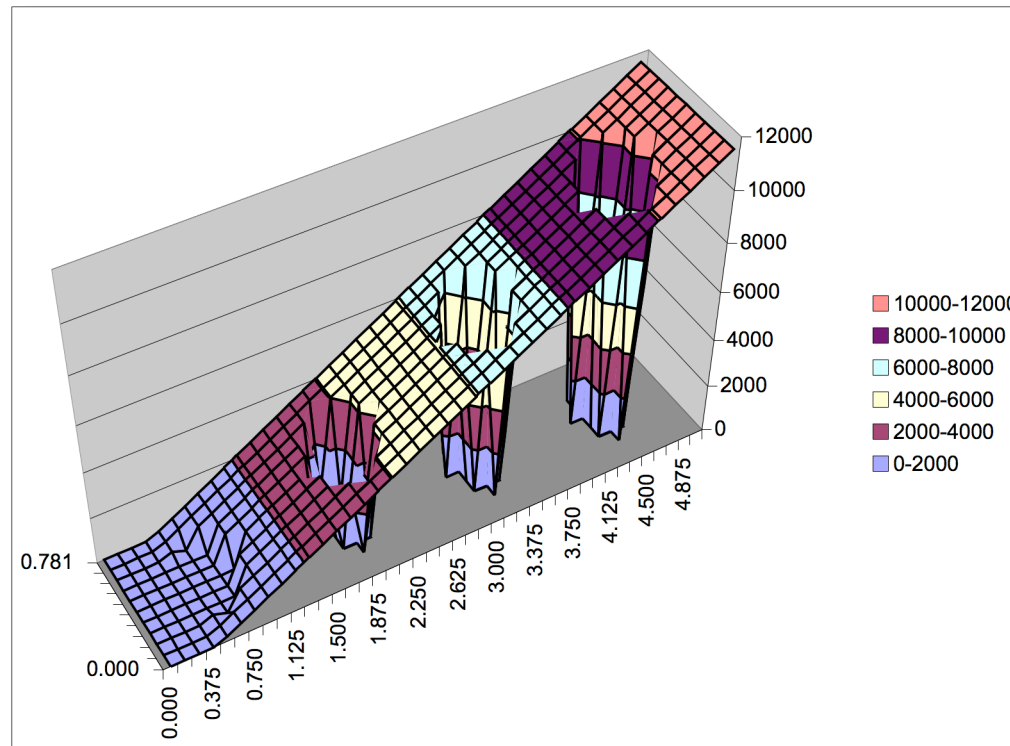


3D Pressure Distribution at Joint - Initial



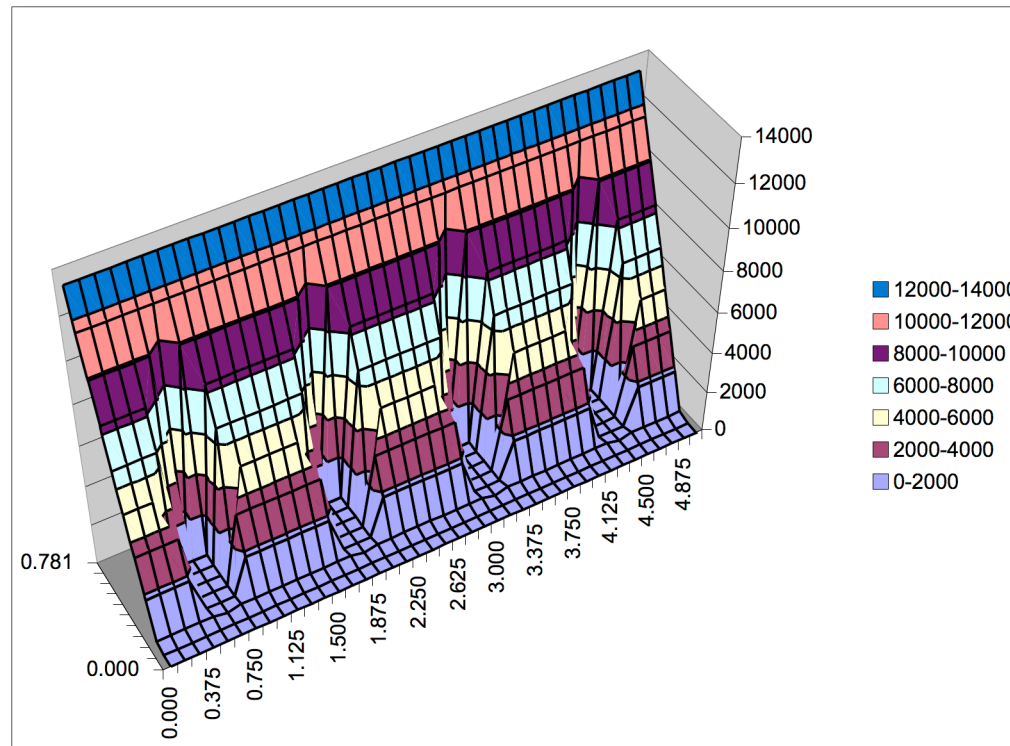
Initial Pressure ~ 5ksi

3D Pressure Distribution at Joint: In-Plane Only



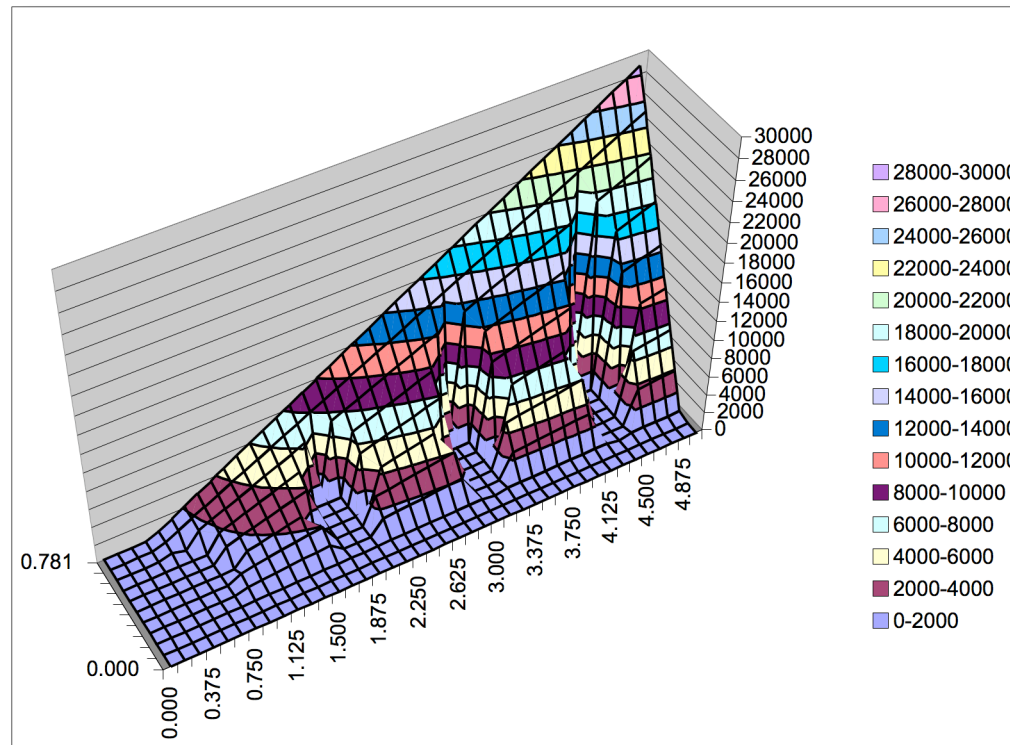
In-Plane Effect

3D Pressure Distribution at Joint: Out-of-Plane Only



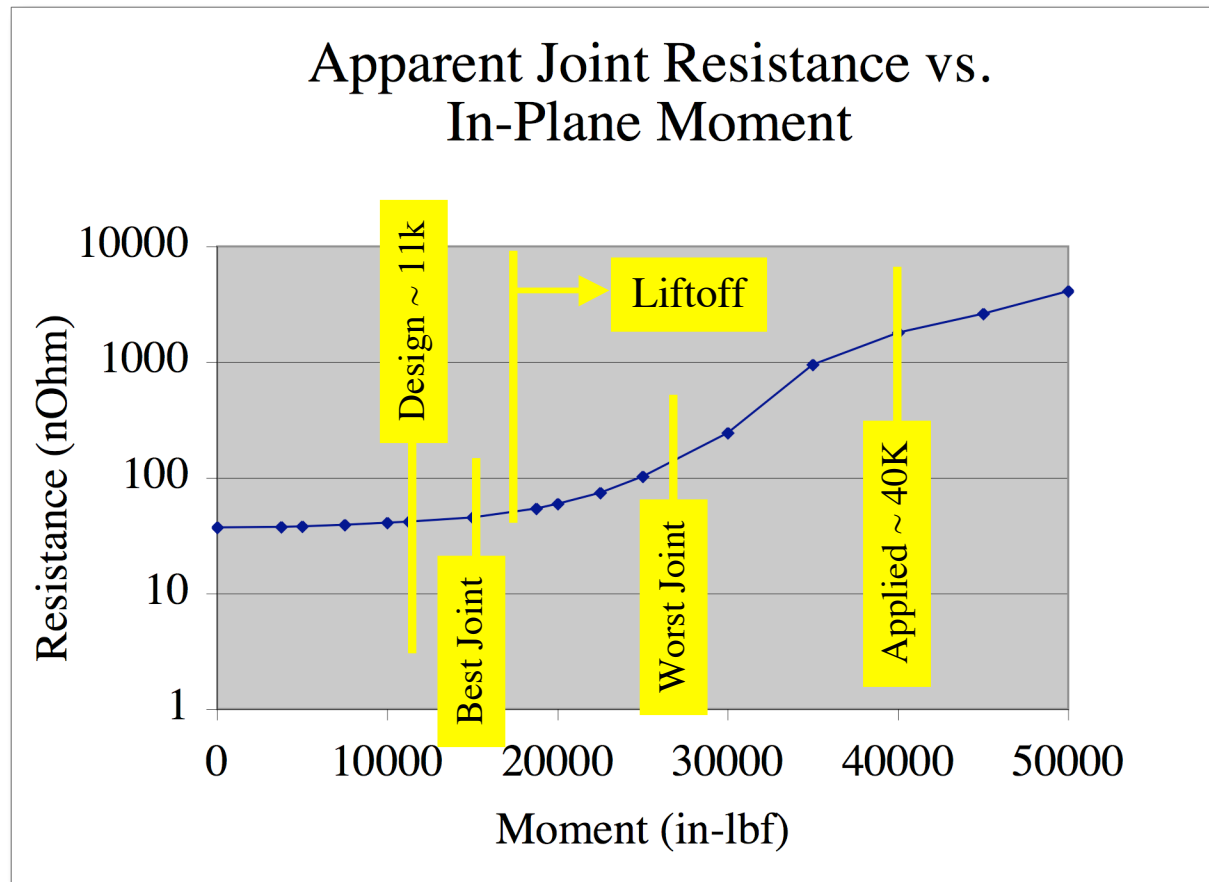
Out-of-Plane Effect

3D Pressure Distribution at Joint: Combined Loading

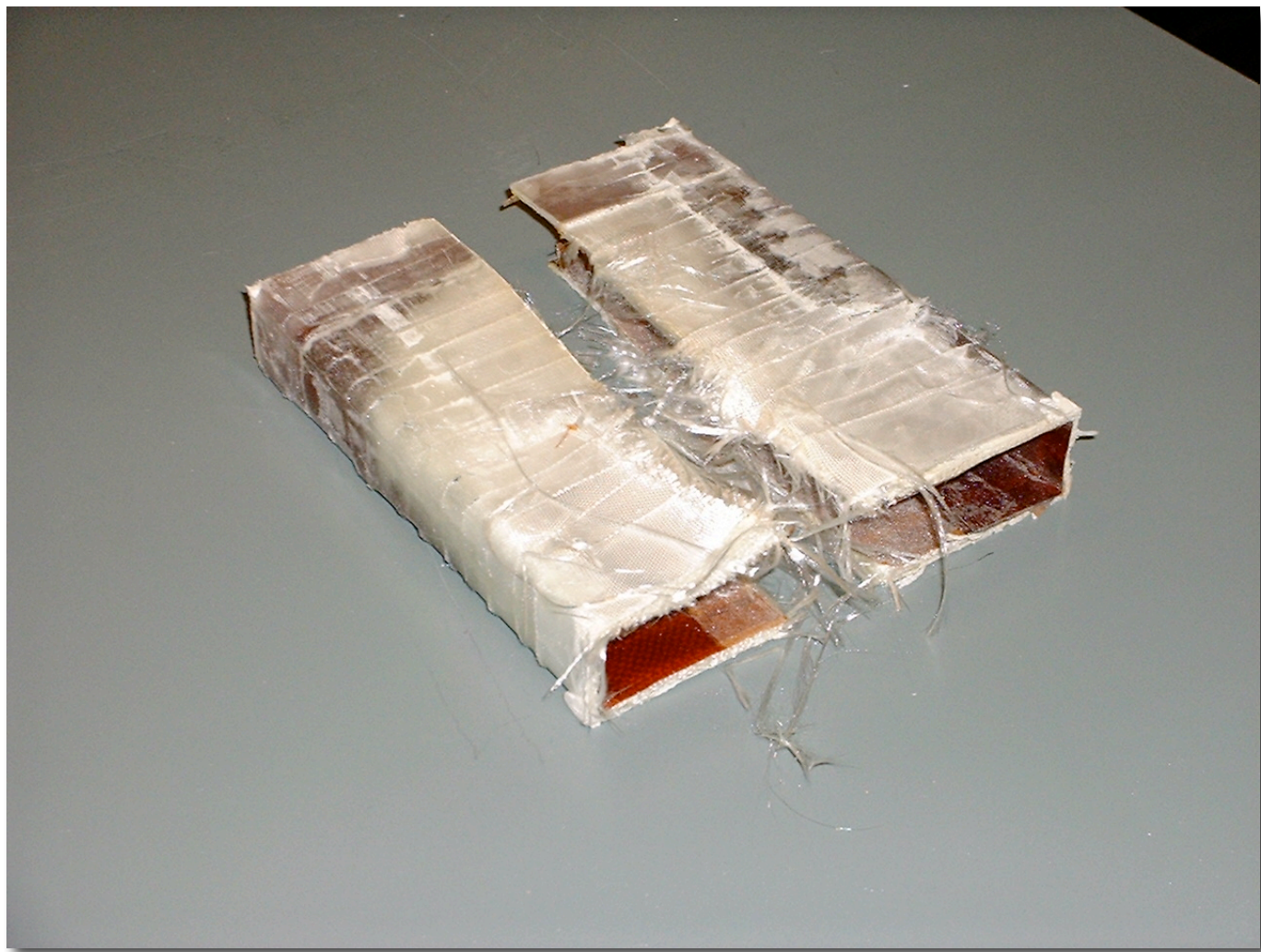


Combined Effect

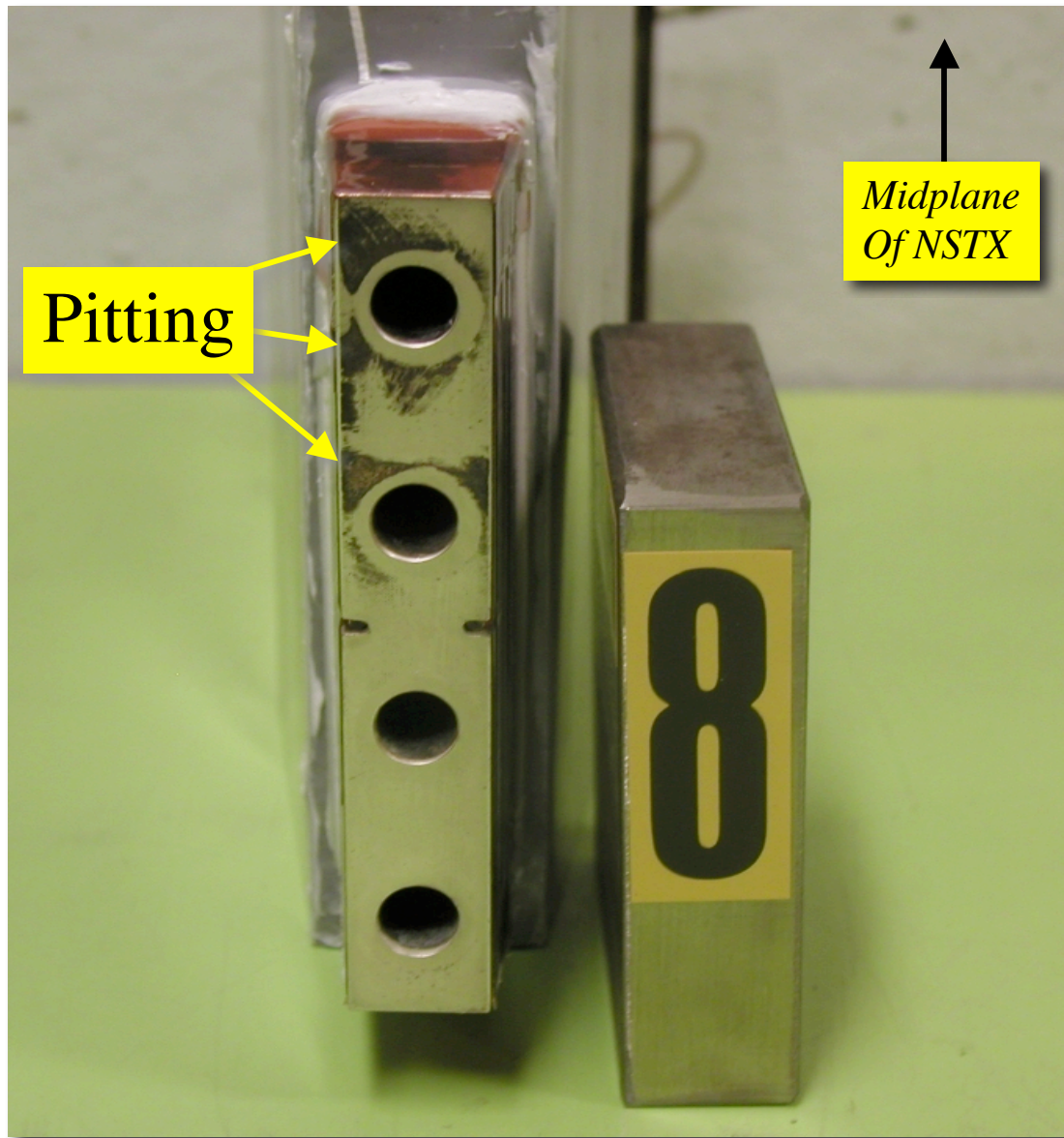
Analysis During Last Run Showed That Structure Was Not Reacting the Moment As Intended



Potting Was Found to be Defective



Liftoff of Joint Led to Pitting Damage



- There was a wide range in degree of pitting damage
- This joint is one of the worst examples
- This is not a new phenomenon

Effect of Liftoff and Pitting

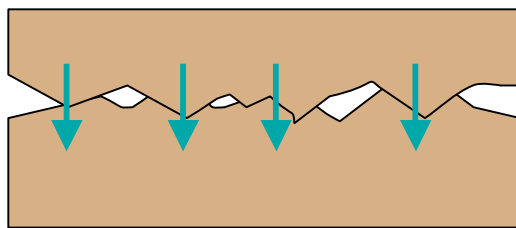
- Based on prior run, we do expect pitting phenomenon to occur with liftoff

- Pitting should occur to a much lesser degree with potting improvements
- We anticipate that this type of phenomenon will stabilize after some erosion takes place, and that current will find alternate pathways in regions not subject to liftoff ($z_{\text{flag}} \gg \text{liftoff length}$)

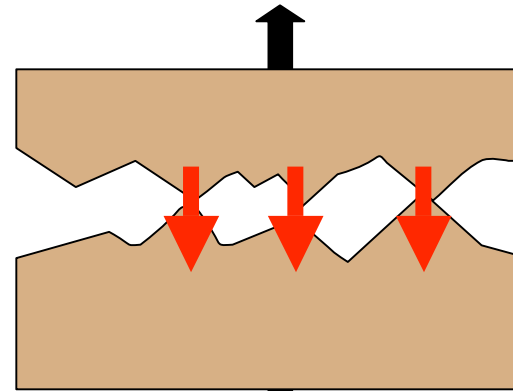
- Exact mechanism is not known but two theories have been hypothesized
 - microscopic pinching off of current pathways
 - macroscopic instability due to high current density

Theories to Explain Pitting

- Surface peaks (asperities) at microscopic level become disconnected leading to current pinching and small melt regions

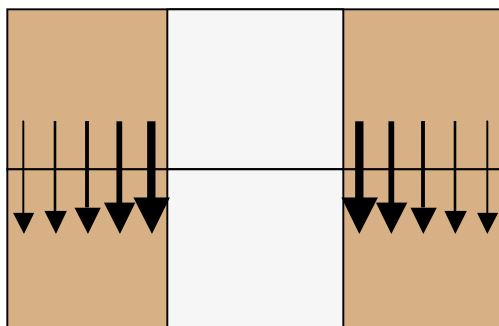


Before Liftoff, low current density

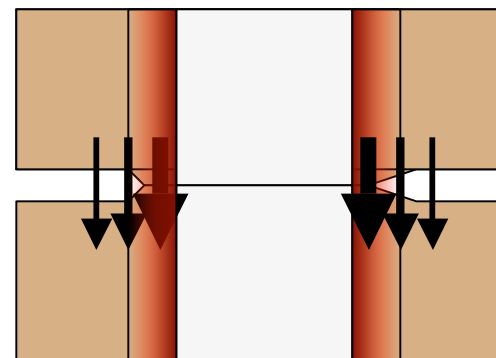


During Liftoff, high current density and circuit breaking, local melting

- Small localized regions with high current density swell up as they heat more than surrounding areas, increasing local contact pressure, increasing local current density, and so on, in an unstable fashion



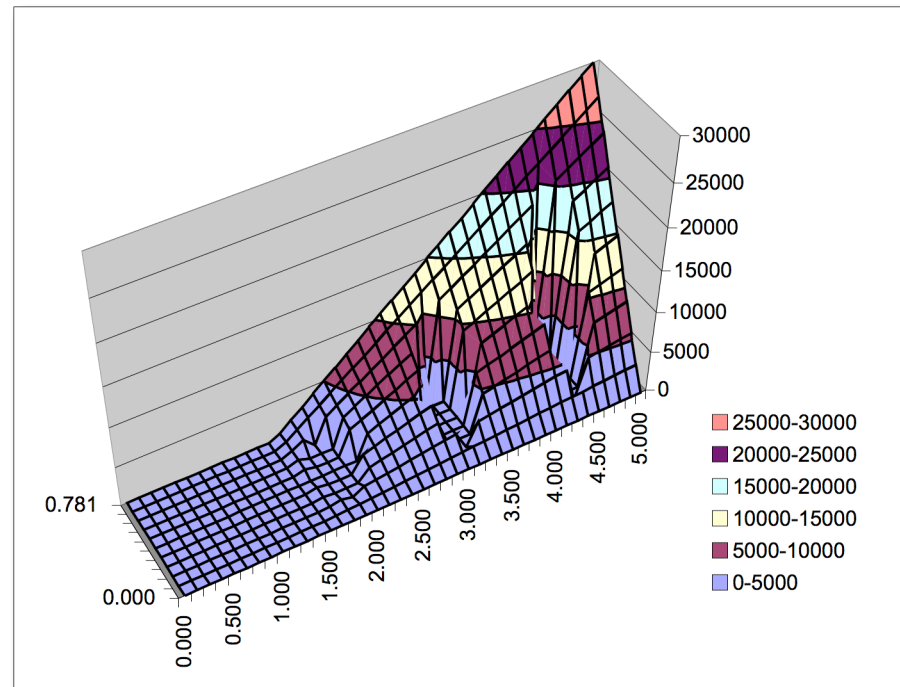
High current density, e.g. near holes



Swelling, increased pressure and conductivity,

These are hypotheses, not proven

Models would Predict Local Yielding on Some Joints, However, No Visible Evidence



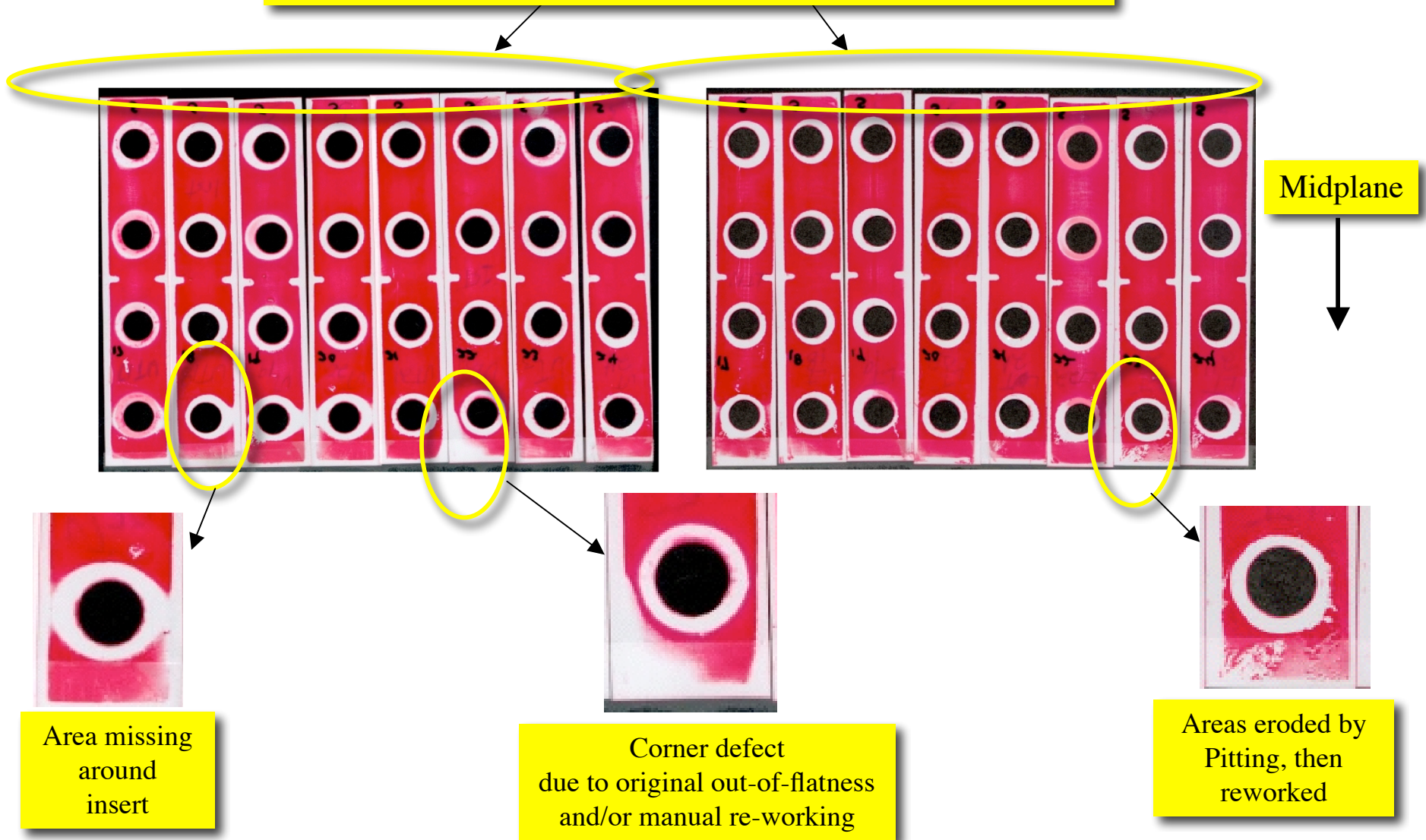
Worst case joint IP moment $\sim 27\text{kin-lbf}$
(67% of IP moment to joint instead of 29% expected)
Local Pressure $> 30\text{ksi}$ assuming 2.7kin-lbf OOP moment

Repair of Contact Surfaces

- Pitted contact surfaces on flags were re-machined
- Pitted surfaces of bundle conductors were manually honed (high spots removed)
- All flags were measured, and the worst case out-of flatness measurement on the flag surfaces after machining was 1.1 mil
- Two of the bundle contact surfaces were measured for flatness down the center and were within 2 mils
- This slightly exceeds original drawing spec of 1 mil
- Pressure sensitive paper was used to assess all joint fit-ups after re-work

Condition of Repaired Surfaces

No obvious indication of deformation at corners



Effect of Surface Irregularities

- We anticipate that contact regions lost to surface irregularities are tolerable since current will find alternate pathways in regions further up the flag
 - We anticipate that pitting will stabilize because current will eventually avoid eroded areas and find alternate pathways in regions further up the flag
 - Structural integrity of joint is not significantly effected by surface irregularities
-
- Area lost around inserts is probably most critical, will cause higher local temperatures than predicted in analysis
 - Analysis of joints with missing contact area has not been performed

Flag Stud and Insert Stresses

• Although more moment was transmitted to joints than intended, axial loads on flag studs and inserts did not exceed design value

- Moment induced load on flag and stud in parallel (\sim equal strain) reduces compression on flag and increases tension on stud
- Most of load reaction comes from flag due to lower elasticity of flag vs. stud/belleville washer stack
- Design basis (NASTRAN) $\Delta F \sim 200\text{lbf}$ over 5klbf preload
- Fatigue (design and test to 100kcycles) based on $\Delta F = 1\text{klbf}$
- NASTRAN (run 64N) for no-potting case at 4.5kG is $\Delta F = 850\text{lbf}$

Potting Improvements

Extensive development program was conducted to optimize potting process

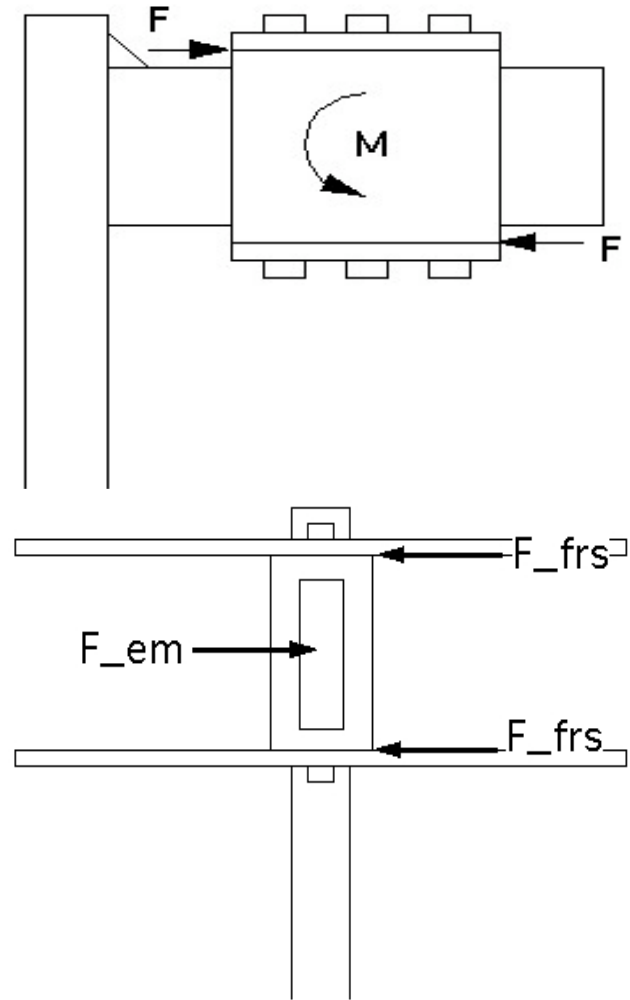
- improved vacuum seals
- improved electrical insulation
- different resin (long pot life)
- improved process
- all potted flags will be tested for mechanical properties



Hub Disk Improvements

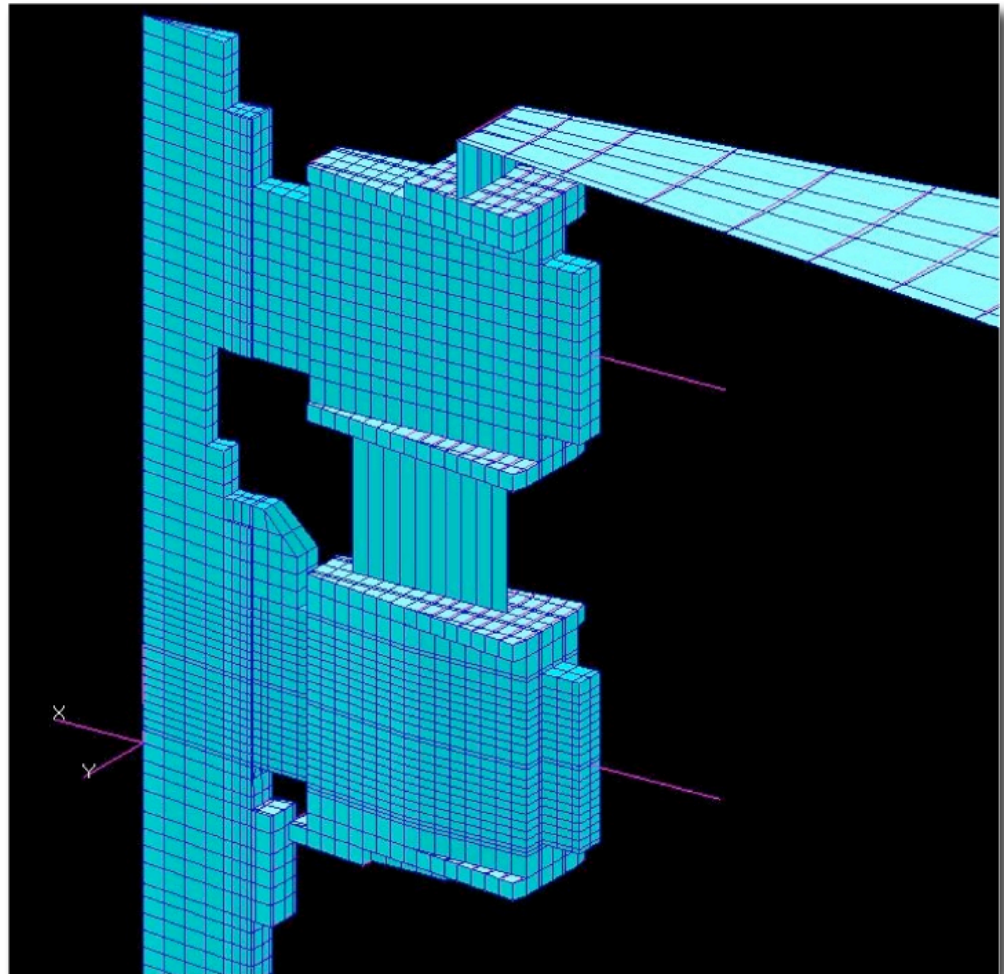
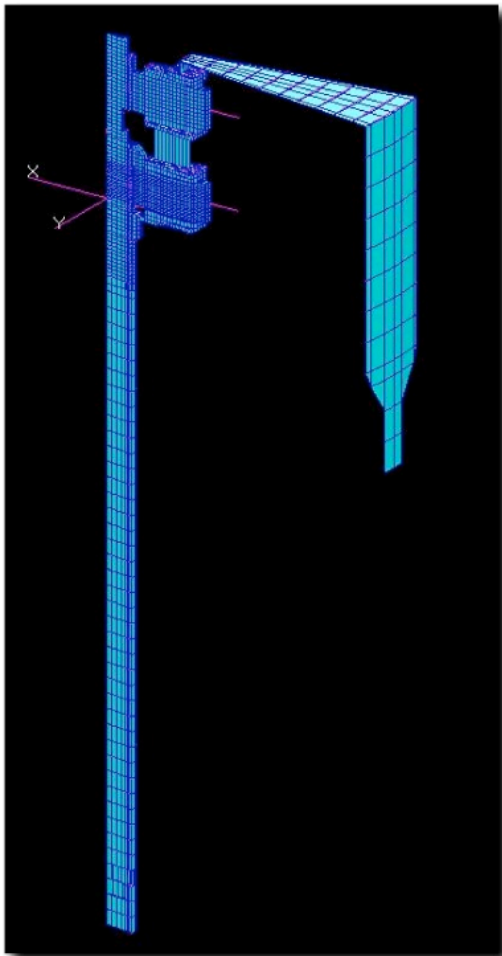
High friction coating developed to enhance friction shear interface between hub disks and flag boxes

- diamond grit coating
- full scale mock-ups tested at PPPL
- COF > 0.5 (~ 2x base SS COF)
- design review held on 10/27/04

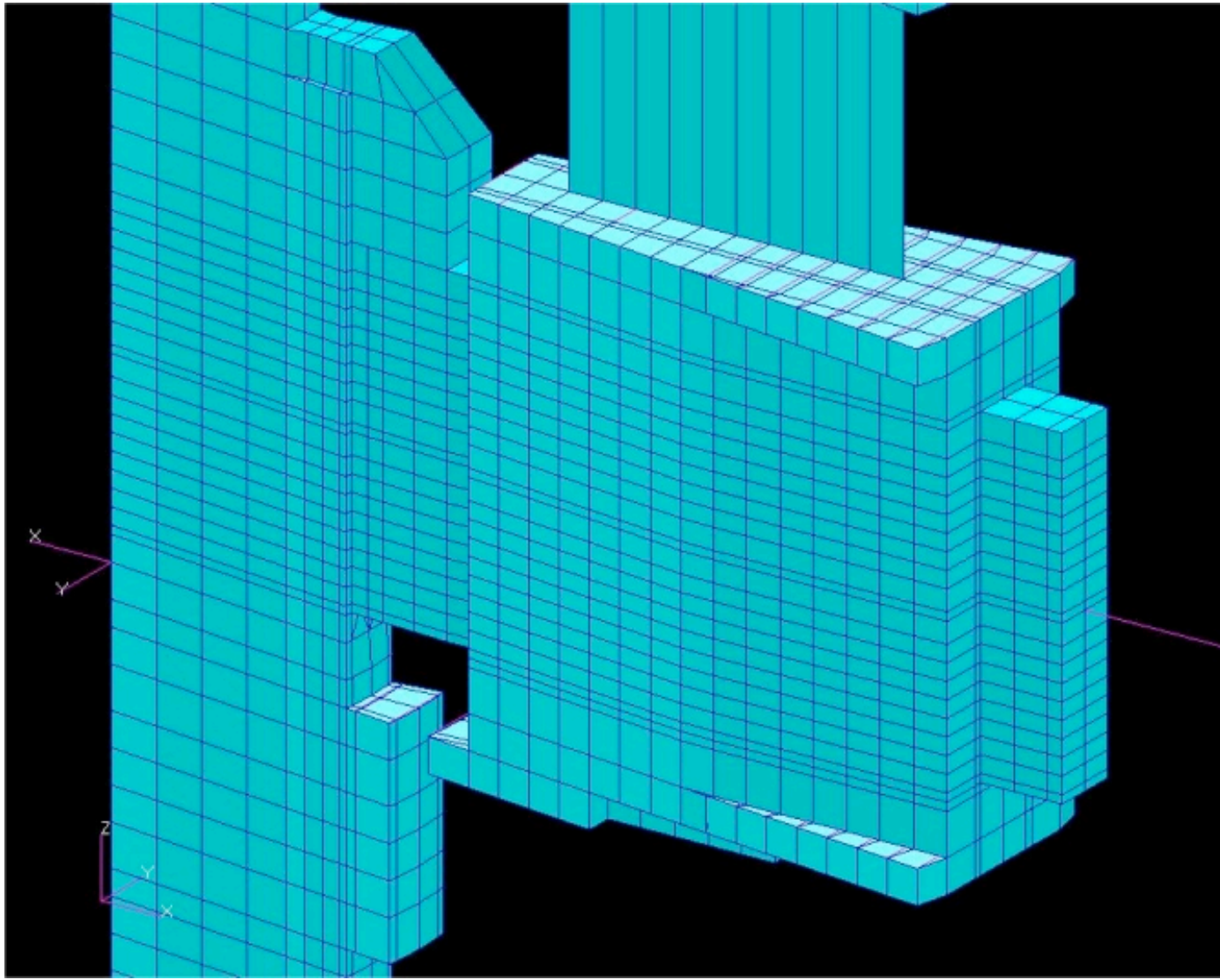


New Analysis - Structural

- NASTRAN (I Zatz)
 - ✓ increased mesh density at joint
 - ✓ included additional length of flex link in force calculation
 - ✓ incorporated revised PF1a coil in force calculation



New Analysis - Structural



New Analysis - Structural

- No significant differences from findings reported at August '04 FDR
- More cases run and more data extracted
- Developed influence matrix for in-plane and out-of-plane moments at joint

RUN CASE	OUTER FLAG IN-PLANE MOMENT (in-lbs)	OUTER FLAG O-O-P MOMENT (in-lbs)
4.5 kG – SOFT – No PF – Run 47NA	11490	-
4.5 kG – SOFT – 100% PF – Run 70N	10920	2667
4.5 kG – OHSS – 100% PF – Run 71N	10430	2827
4.5 kG – EOFT – 100% = No PF – Run 48N	10340	13
4.5 kG – SOFT – 24 kA OH, only – Run 72N	10810	2542
4.5 kG – SOFT – 5 kA PF3, only – Run 73N	11461	179
4.5 kG – SOFT – 5 kA PF1A, only – Run 74N	11460	33
4.5 kG – SOFT – 10 kA PF2, only – Run 77N	11390	461
4.5 kG – SOFT – 20 kA PF5, only – Run 78N	11360	336
6.0 kG – SOFT – 100% PF – Run 75N	17770	3390
6.0 kG – OHSS/EOFT – 100% PF – Run 76N	10340	3424

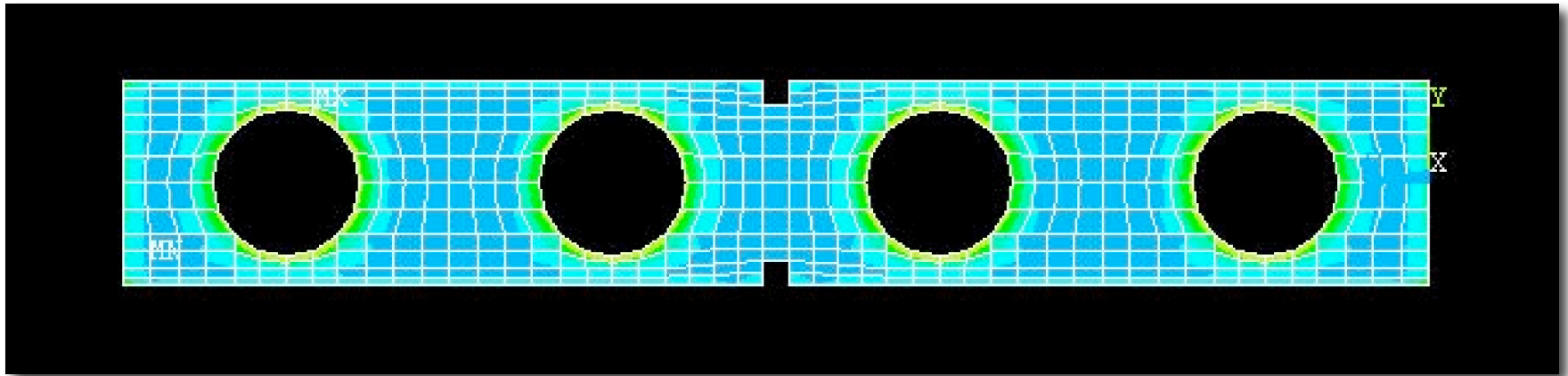
New Analysis - Joint Behavior

- ANSYS

- ✓ Developed fine mesh 3d ANSYS model of joint

- Captures nuances of pressure distribution and conductivity near inserts and at corners

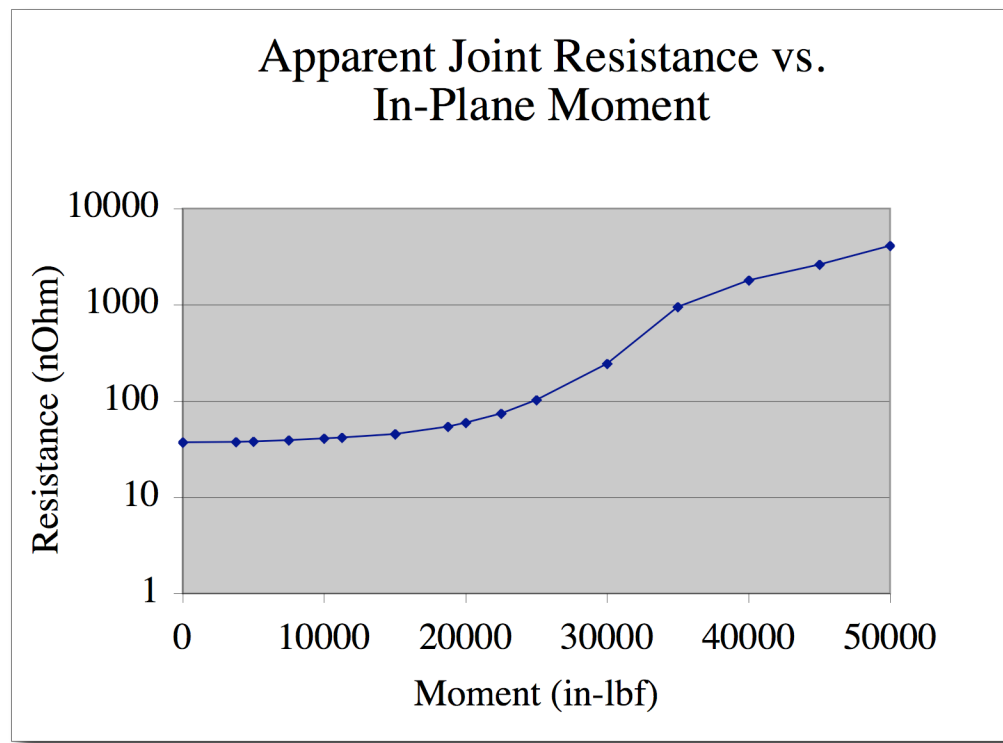
- Used to develop “Rosetta Stone” translation data base of apparent resistance measured by voltage probe vs. in-plane and out-of-plane moments at joint



New Analysis - Joint Behavior

- MATLAB

✓ Developing tools for “data mining” of MDS+ voltage probe measurements so actual in-plane and out-of-plane moments at joint can be extracted from voltage data and performance of structure can be assessed.



New Analysis - Electrical/Thermal

- FEMLAB

- ✓ Developed 2d and 3d models of joint including transient electrical and thermal analysis with in-plane moments and TF current applied as a function of time

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- FEMLAB

- ✓ Developed 2d and 3d models of joint including transient electrical and thermal analysis with in-plane moments and TF current applied as a function of time

Target Operating Envelope - 4.5kG

- $B_t \leq 4.5\text{kG}$

- 1.0 second flat top

- full OH (-/+24kA)

- other PF's...

$$|I_{\text{pf1a}}| \leq 15\text{kA}$$

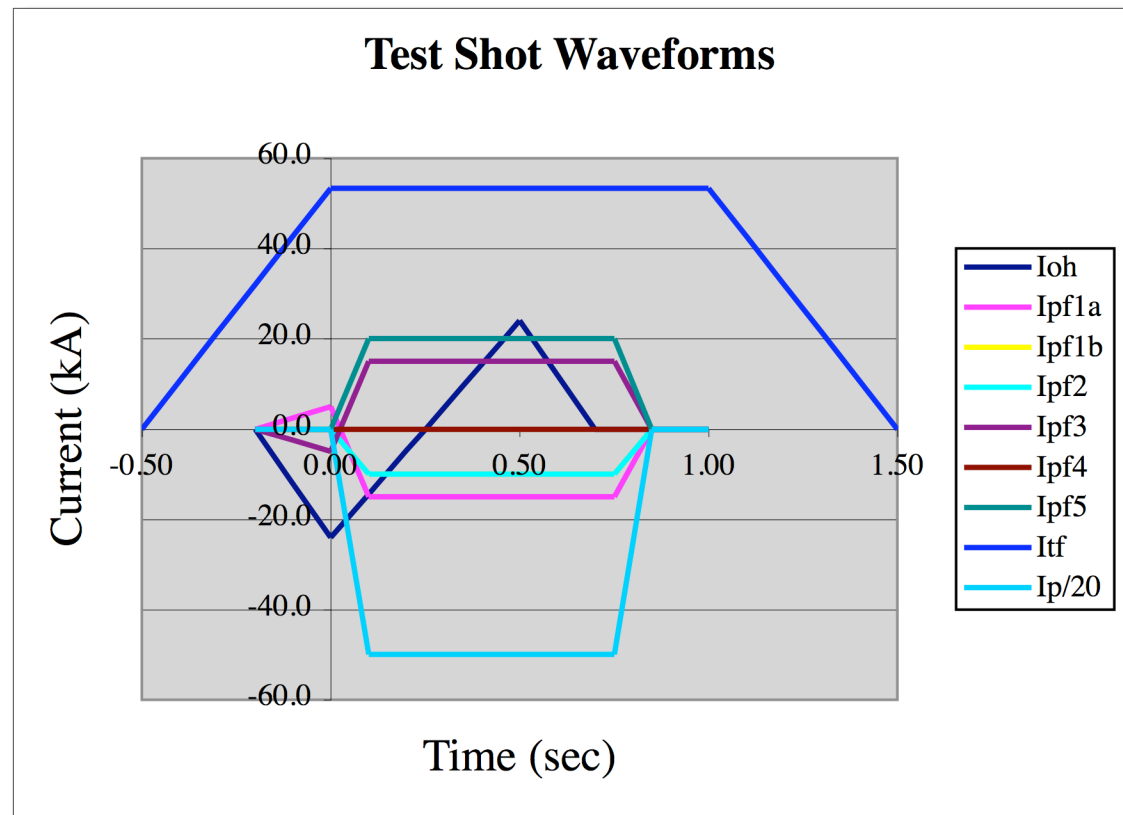
$$|I_{\text{pf1b}}| \leq 10\text{kA}$$

$$|I_{\text{pf2}}| \leq 10\text{kA}$$

$$|I_{\text{pf3}}| \leq 15\text{kA}$$

$$|I_{\text{pf5}}| \leq 20\text{kA}$$

- test shot waveform timing as indicated



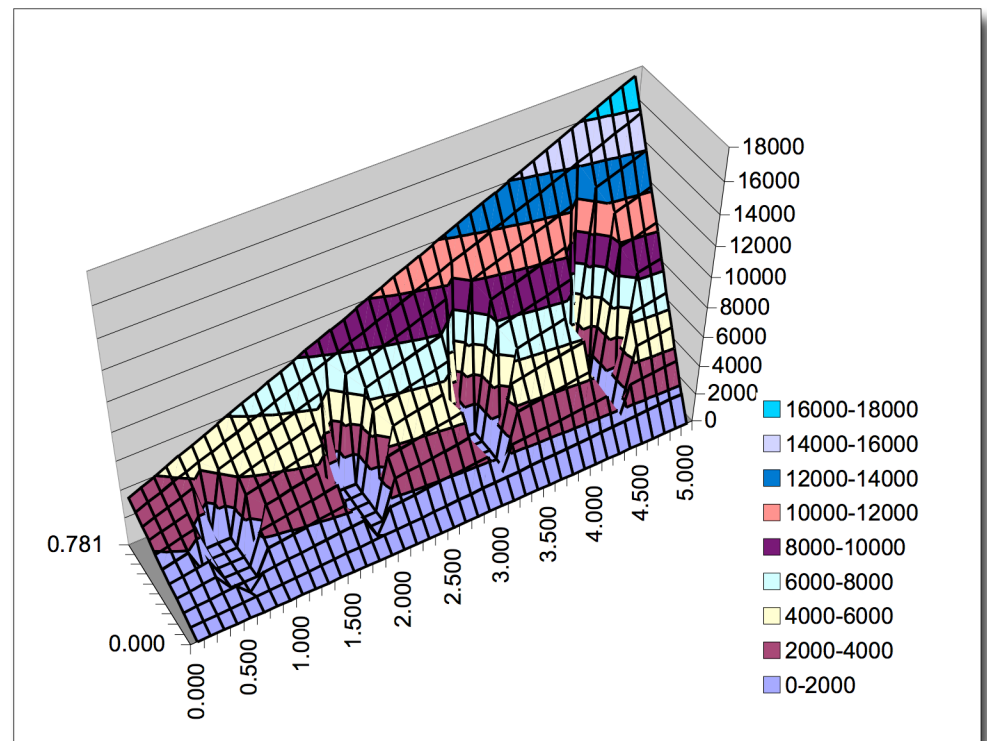
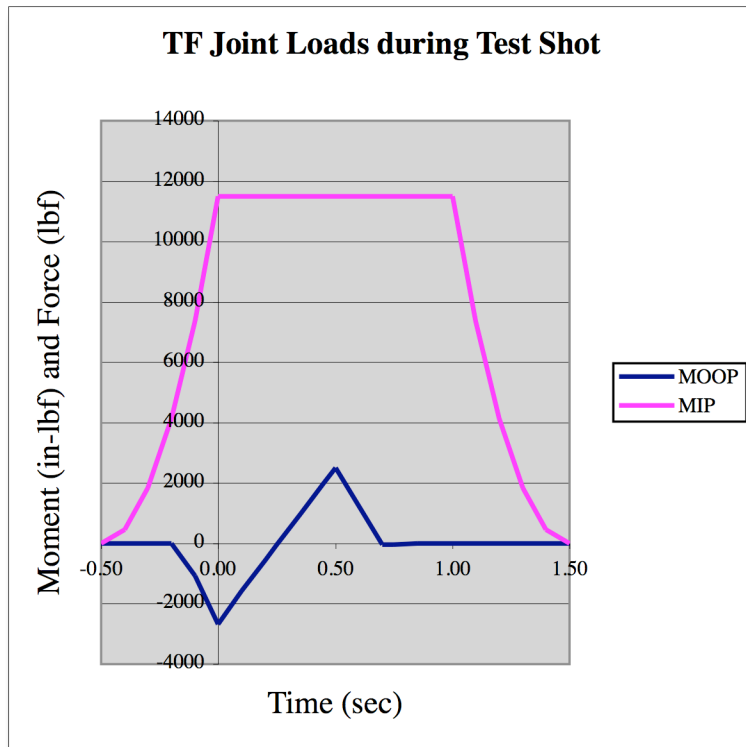
*PF Current Range Consistent with
Upcoming Plasma Operations*

Target Operating Envelope - 4.5kG

Predicted joint performance...

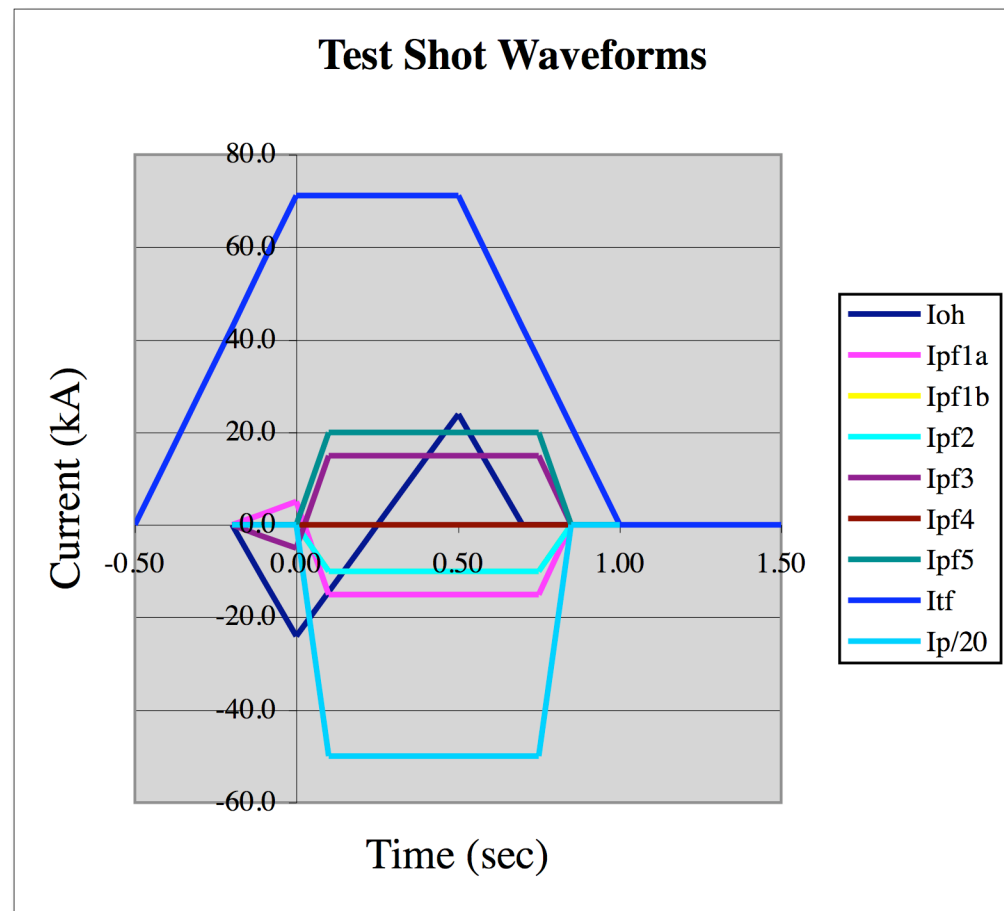
- ✓ $M_{ip} \sim 11\text{kin-lbf}$
- ✓ $M_{oop} \sim 2.7\text{kin-lbf}$
- ✓ minimal lift-off

- ✓ $P_{max} < 20\text{ksi}$ (excluding local peaks)
- ✓ Box stud friction $SF > 2$
- ✓ $T_{max} < 150\text{C}$



Target Operating Envelope - 6.0kG

- $B_t \leq 6.0\text{kG}$
- ✓ 0.5 second flat top
- ✓ full OH (-/+24kA)
- ✓ other PF's...
 - ✓ $|I_{\text{pf1a}}| \leq 15\text{kA}$
 - ✓ $|I_{\text{pf1b}}| \leq 10\text{kA}$
 - ✓ $|I_{\text{pf2}}| \leq 10\text{kA}$
 - ✓ $|I_{\text{pf3}}| \leq 15\text{kA}$
 - ✓ $|I_{\text{pf5}}| \leq 20\text{kA}$
- ✓ test shot waveform timing as indicated



*PF Current Range Consistent with
Upcoming Plasma Operations*

Target Operating Envelope - 6.0kG

Predicted joint performance...

- ✓ $M_{ip} \sim 20\text{kin-lbf}$
- ✓ $M_{oop} \sim 3.5\text{kin-lbf}$
- ✓ Liftoff to first bolt

- ✓ $P_{max} < 30\text{ksi}$ (excluding local peaks)
- ✓ Box stud friction $SF > 1.5$
- ✓ $T_{max} < 150\text{C}$

