

NSTX-U is sponsored by the U.S. Department of Energy Office of Science Fusion Energy Sciences

NSTX-U Milestone R18-2: Develop simulation framework for ST breakdown and current ramp-up

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R18-2: Develop simulation framework for ST breakdown and current ramp-up

- Inductive startup calculations using LRDFIT
 - Develop predictive vacuum field simulation capability for NSTX-U and MAST-U
 - Establish metrics for comparing and optimizing startup scenarios
- Control modeling focusing on IWL \rightarrow DN transition
 - Establish framework for closed-loop simulations with PCS code and "mirrored" control algorithms in SIMULINK
 - Develop power supply, conductor and plasma models suitable for time-dependent NSTX-U rampup calculations
- TRANSP calculations for heating and current drive
 - Evaluate models within TRANSP for NSTX and NSTX-U ramp-up
 - Demonstrate the capability for predictive time-dependent calculations for the ramp-up period

Developed 1-D metrics for startup calculations (LRDFIT)

- Assume fixed boundary shape, zero-beta and force-free (J ~ B_{ϕ} ~ 1/R)
 - Breakdown: E $B_{\phi}/B_{\theta} \sim E/(RB_{\theta})$
 - Cross-section averaged EB_{ϕ}/B_{θ}
 - Assume 10G NA field
 - Radial force balance: $I^2/R_0 \sim JB_Z$
 - I_p ramp rate: d(I_p)/dt ~ d(B_ZR₀/R)/dt
 - Cross-section averaged
 - Heating: JE ~ E/R
 - Cross-section averaged V_{loop}/R²
 - Vertical stability: dF/dZ ~ d(JRB_R)/dZ
 - Boundary averaged dB_R/dZ
 - Positive is stable



Startup modeling efforts in Q4

- Calculations supporting MAST-U operating procedures
- Size of null (breakdown) versus vertical stability
 - Use divertor coils to increase null size at the expense of vertical stability
- Limits to B_Z/dt after breakdown
 - Power supply voltage, current drive (heating) and vertical stability





- Connect PCS for a "flight simulator" or test control algorithms in SIMULINK environment
- Plasma model could be
 - TOKSYS
 - Reduced models for fast calculations
 - Different models for computing plasma equilibrium
 - TRANSP
 - More complete physics

Update on closed-loop calculations with PCS



- [Q2-3] PCS feed-forward demonstration
 - Archived data provides input to PCS
 - Power supply commands communicated to SIMULINK
 - PCS commands converted to coil voltage to drive plasma model
- [Q4] Format SIMULINK output for input into PCS to complete closed-loop framework

Closed-loop simulation between PCS and Simulink connects previously developed and validated models





- [Q3-4] Demonstrated closed-loop SIMULINK framework with TRANSP and TOKSYS
 - Reproduce shape & beta feedback algorithms in SIMULINK
 - Includes inner gap, drsep and strikepoint control algorithms
 - Supports PFC working group
 - Currently adding algorithm transitions to control algorithms



- [Q3-4] Demonstrated closed-loop SIMULINK framework with TRANSP and TOKSYS
 - Reproduce I_p , shape, beta feedback algorithms in SIMULINK
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- Linear "conductor model" computes induced wall current
- Options for computing diagnostic signals including plasma response
 - Linear models use a constant plasma response (~1 minute)
 - Derived from existing equilibrium, assumes boundary is fixed, or rigid
 - Linear model must change as equilibrium evolves
 - Nonlinear model solves the free-boundary GS equation (~1 hour)
 - Inputs: Coil and vessel currents, target values for I_p , β_p , and I_i .
 - Output: Flux on grid and updated plasma boundary.

Treatment of the passive plate currents was improved in the conductor model

- [Q3] Induced current in PPs modeled as two circuits
 - Eddy current loop + winding toroidal path through mounting brackets



Evaluate VDE growth rate at different times in a discharge as a function of the passive plate mounting bracket resistance

Smaller vertical growth rate is better

Capability added to interpolate linear models for ramp-up simulations

- [Q3] Demonstrated linearized models changing in time
 - Important for ramp-up where equilibrium has considerable differences
 - L-H transition, limited to diverting transition, etc.
 - Reworked parts of SIMULINK model for matrix interpolation
 - Provides more realistic simulation capability
 - For example, evolving vertical growth rate, coil effectiveness



Closed-loop simulator with free-boundary solution was used to develop new snowflake control algorithm

- Nonlinear simulation <u>required</u> for some control development such as snowflake divertor
- Time-independent control algorithm performs well with simulations using a linear equilibrium model
 - However, this control fails in a simulation using free-boundary solution
- Motivated development of time-varying snowflake controller algorithm
- Equilibrium models of different fidelity now available for NSTX-U simulations
 - Linear reduced models (including NN)
 - Non-linear equilibrium
 - Transport driven models (TRANSP)



Neural net development for NUBEAM, to be used for scenario optimization and control

- [Q3] Completed higher fidelity NUBEAM runs and added beam modulations to dataset
 - Helps reduce uncertainty when using beams that weren't used much in FY16 experiments
- [Q3] Implemented NUBEAM NN calculations on NSTX-U realtime computer
 - Demonstrated execution times well within 200us NSTX-U PCS control cycle time
 - Need to interface with diagnostics



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Additional neural network models for current diffusion

- [Q3-4] NN bootstrap current, resistivity, and geometric flux surface averages for current diffusion equation
 - SULI student Vaish
 Gajaraj
- Plans for developing NN for transport coefficients in FY19



Updates on evaluating TRANSP simulations of NSTX-U ramp-up

- [Q3] Fidelity of predictive models in TRANSP for current diffusion and thermal transport in ramp-up in NSTX and NSTX-U completed
 - Core electron thermal transport: MMM7.2 (no microtearing)
 - GLF23 has numerical problems at around 2/3 of the minor radius (not clear)
 - Core Ion thermal transport: neoclassical
 - Current diffusion: TEQ fixed boundary equilibrium



Good prediction of global parameters

- Good reproducibility of the stored energy and internal inductance when kick model is used.
- Overestimate of neutron rate after 0.40s to be investigated

204202 L-mode using only beamline 1



Summary of Q3-4 work

- Metrics established for evaluating breakdown scenario calculations
 - Applied to the development of the MAST-U startup procedures
- PCS feed-forward SIMULINK simulation completed

 Working to "close the loop" by feeding diagnostic signals from SIMULINK into PCS
- Closed-loop time-dependent simulations with control algorithms in SIMULINK completed
 - Developed ability to interpolate linear matrices
 - Demonstrated non-linear equilibrium GS solver for NSTX-U

Summary of Q3-4 work

- Improved PP model to assist in evaluating impact of bracket resistance on vertical stability
- Increased fidelity of NUBEAM NN and implemented NN model in PCS code

- NN for current drive under development

• Transport model options within TRANSP were evaluated for ramp-up phase on NSTX-U



R19-2: Demonstrate optimized ramp-up

- Extend linearized TOKSYS models to include current drive, heating and transport models
- Extend evaluation and development of transport models within TRANSP required for time-dependent ramp-up simulations
 - For example, neutral fueling model for density evolution
- Leverage models to evaluate stability (VDE, MHD, fast-ion) and resiliency of ramp-up scenarios aimed at low-l_i, high shaping
 - Accelerate the realization of high-performance discharges on NSTX-U and MAST-U

Backup



Implemented coil control algorithms in Simulink for testing and development



Implemented ISOFLUX in Simulink for testing and development





Status of TRANSP calculations

- [Q2-3] Validation of TRANSP model for ramp-up period (Doohyun, Francesca)
 - NSTX w/ MSE (139048)
 - See attached slides
 - NSTX-U w/ CHERs (204202)
 - See attached slides
 - NSTX-U early H-mode development (202946, 203679, 204112) using NBI #2
 - Underway
 - Evaluate ability of flux-driven transport models to capture evolution of discharge in L- and H-mode ramp-up
- [Q3-4] Free-boundary predictions for NSTX-U
 - Start with validated predictive model of an NSTX-U rampup
 - Examine impact of NBI, outer gap, density, dIp/dt, κ , and/or timing of L-H transition on I_i
 - Need to provide target shapes for NSTX-U cases
 - First try an NSTX-U ramp-up where everything happens earlier and faster

Te/Ti prediction initial test for NSTX/NSTX-U

- Transport
 - NSTX case (139048P61)
 - transport: turbulence (MMM), NC (NEOCH), ExB (TRANSPEXB)
 - MMM: Weiland (e/i), MTM (e), ETG (e)
 - NSTX-U case (204202P16)
 - Electron transport: turbulence (MMM), NC (NEOCH), ExB (TRANSPEXB)
 - MMM: Weiland, MTM, ETG
 - Ion transport: Neoclassical only (NEOCH)
 - Calculation boundary
 - Central (rho = 0 0.2), core (0.2 0.8), edge (0.8 1.0)
 - Te/Ti calculation in central and core regions
- Equilibrium / poloidal field diffusion
 - TEQ (fixed boundary)
 - Fixed total plasma current (ufile), calculated vloop
 - Default resistivity
- Anomalous Fast Ion Diffusion
 - Constant across minor radius (1e4)
- More test will be done for NSTX-U using 204202P16 setting

Te profiles - NSTX



NSTX-U

Ti profiles - NSTX



NSTX-U

Total current profiles - NSTX



q profiles - NSTX



0-D parameters - NSTX



Te profiles – NSTX-U



NSTX-U

Ti profiles – NSTX-U



Typical NSTX ramp-up



NSTX-U

LRDFIT modeling focus



TOKSYS modeling focus



Divert L-H transition

TRANSP modeling focus

