



3D magnetic response modeling and synthetic diagnostics with GPEC/MARS

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GPEC/MARS can be used to address capability of 3D magnetic sensors for multi-modes and field penetration

- Multi-modes and bifurcation in 3D magnetic response are important topics in error field, NTV, RMP ELM control
 - DIII-D highlighted the importance of optimal sensor locations to resolve subdominant modes and/or response bifurcation by field penetration
- GPEC can address sensor capability for linear/static response, by synthetic diagnostics and systematic mode decomposition
 - Synthetic diagnostics: PYPEC
 - Mode decomposition: SVD of matrix between sensors and reluctance
 - Bifurcation by layer penetration: RPEC
- MARS can address dynamic sensor capability and response change by field penetration in linear regime
 - Frequency characteristics and Nyquist contour for multi-modes
 - Linear resistive response by MARS-F

Synthetic diagnostics in IPEC (N. Logan) allow direct comparison with experiment for static 3D response

- IPEC diagnostics have been successfully used to validate 3D response codes, and to identify multi-mode characteristics in DIII-D
- Recent study shows that the modes can be decomposed best by reluctance matrix, which can be possibly coupled to sensors and coils for multi-mode response measurement and control



DIII-D n=2 response to I-coil (Logan, APS 2015)

In the courtesy of Logan



Extensive magnetic synthetics have been developed for DIII-D



Arbitrary accuracy "diagnostic" at the wall

Synthetics include toroidal arrays of sensors for both the radial and poloidal field

Field projected to true length, tilt to calculate average flux

Full vessel wall provides arbitrarily fine diagnostic

- Shows structures averaged over by finite sensor lengths
- Upgrade used this to project to previously un-diagnosed regions (HFS)



In the courtesy of Logan



IPEC synthetics played a major role in guiding the DIII-D 3D magnetics upgrade

- Scale lengths were used to determine necessary sensor size/ spacing
- Geometry variations estimated positioning sensitivity/errors
- Reconstructions using discrete sensor distributions were tested for robustness in constraining multiple types of plasma response
- IPEC synthetics can be readily implemented for NSTX-U (with sensor geometry/locations) and can be utilized as done for DIII-D



In the courtesy of Logan



GPEC can also be used to improve synthetic diagnostics and address kinetic response in NSTX-U

- GPEC can be used with NSTX-U synthetic magnetics
- NSTX-U can be very different from DIII-D due to large difference in HFS vs. LFS, requiring careful exercise with sensors and different modeling



NSTX-U

MARS can be used to address sensor capability of dynamic multi-mode responses



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MARS Nyquist contour can be tested with different design of NSTX-U sensors to validate physics model and multi-modes

- MARS shows clear separation of Nyquist contour in frequency response depending on physics model
- With validated model, MARS can be used to test capability of designed sensors to discriminate secondary or higher order mode responses



MARS can be used to address sensor capability for ideal vs. resistive response for NSTX-U, as shown in DIII-D

- In recent DIII-D experiments, 90 deg phase change at HFS has been observed at the transition of ELM suppression in the presence of n=2 external perturbation (Nazikian)
- MARS resistive simulation shows a quantitative agreement with experimental observation
 - Resistive response show ~90 deg phase difference compared to ideal response at HFS
- For NSTX-U, MARS can be used to locate sensors to amplify difference of resistive response vs. ideal response



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