## Using the frequency domain for the real-time detection of the n=1 plasma response

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# Potential of active MHD spectroscopy as a real-time stability measurement

From H. Reimerdes, et al., 49th Annual Meeting of the Division of Plasma Physics Orlando, 2007

Including corrected formulas



49th DPP Meeting, November 12-16, 2007

## Fourier analysis of perturbation measurements yields plasma response at applied frequency

- Fourier analysis in time-domain
  - Signal of magnetic probe s

$$B_{\rm s}(t) = \Re \left( \boldsymbol{B}_{\rm s}^{\omega} \cdot \boldsymbol{e}^{i \omega t} \right)$$

- Current in coil c
  - $I_{\rm c}(t) = \Re \left( I_{\rm c}^{\omega} \cdot \boldsymbol{e}^{i\omega t} \right)$
- Fourier coefficients yield the transfer function

$$\boldsymbol{b}_{\mathrm{SC}}^{\mathrm{co}} = \frac{\boldsymbol{B}_{\mathrm{S}}^{\mathrm{co}}}{\boldsymbol{I}_{\mathrm{C}}^{\mathrm{co}}}$$

 Use vacuum coupling to extract plasma response from signals

$$\boldsymbol{b}_{\mathrm{SC}}^{\mathrm{\omega},\mathrm{plas}} = \boldsymbol{b}_{\mathrm{SC}}^{\mathrm{\omega}} - \boldsymbol{b}_{\mathrm{SC}}^{\mathrm{\omega},\mathrm{vac}}$$

 Frequency-dependent vacuum coupling is well documented





## Fourier analysis and toroidal mode decomposition yields *n*=1 plasma response at applied frequency

Fourier analysis of sensor signals



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Toroidal mode analysis of Fourier

### Calculation of *n*=1 plasma response from discretely sampled magnetic probe signals

Discrete time steps: Probe plasma with currents in coils C: Measure magnetic field with probes S:

$$\begin{aligned} \dot{t}_{k} &= k \cdot \Delta \\ c_{c}(t_{k}) &= l_{C} \mathbf{cos}(\omega_{ext} t_{k} + \phi_{c,0}) \\ B_{s}(t_{k}) \end{aligned}$$

Calculate Fourier series for each probe s and time  $t_{k}$  over L preceding periods of applied field corresponding to N = L·  $2\pi/(\omega_{ext}\Delta)$  previous samples:  $a_{s,k} = \sum_{k'=K-N}^{K} B_{s}(t_{k'}) \cos(\omega_{ext}t_{k'})$  and  $b_{s,k} = \sum_{k'=K-N}^{K} B_{s}(t_{k'}) \sin(\omega_{ext}t_{k'})$ Subtract known vacuum coupling at  $\omega_{ext}$ using  $b_{sc}^{\omega_{ext},vac} = a_{sc}^{vac} + ib_{sc}^{vac}$ :  $b_{s,k}^{plas} = a_{s,k} - I_{C} \sum_{c'=c}^{C} \left(a_{sc'}^{vac} \cos(\phi_{c',0}) - b_{sc'}^{vac} \sin(\phi_{c',0})\right)$  $b_{s,k}^{plas} = b_{s,k} - I_{C} \sum_{c'=c}^{C} \left(a_{sc'}^{vac} \sin(\phi_{c',0}) + b_{sc'}^{vac} \cos(\phi_{c',0})\right)$  $b_{s,k}^{plas} = 0.5 \sum_{s'=s} \left(c_{s'}^{r}a_{s',k}^{plas} - c_{s'}^{i}b_{s',k}^{plas}\right)$  $B_{S,k}^{plas} = 0.5 \sum_{s'=s} \left(c_{s'}^{r}b_{s',k}^{plas} + c_{s'}^{i}a_{s',k}^{plas}\right)$ 



## Real-time algorithm is equivalent to offline analysis on DIII-D





 Discrepancy possibly due to difference between I-coil current target (real-time algorithm) and actual current (offline analysis)

#### Additional slides

H. Reimerdes, NSTX MS TSG Meeting, April 7, 2009

#### Calculation of toroidal mode component increases signal-to-noise ratio

- General least square fit of toroidal mode components
  - Solution by normal equations yields coefficients C<sup>n</sup>

$$\boldsymbol{B}^{n}(t) = \sum_{s} \boldsymbol{C}^{n}_{s} B_{s}(t)$$
 with  $B_{s}(t) = \Re \left( \boldsymbol{B}^{n}(t) \cdot \boldsymbol{e}^{-in\varphi_{s}} \right)$ 

240 Deg I-coil phasing Generalize to obtain toroidal -Phase b<sub>SC</sub>mode component at  $\omega = \omega_{ext}$ 90 Upper I-coil ·R+1  $\boldsymbol{B}_{S}^{n,\omega} = 0.5 \sum \boldsymbol{C}_{S}^{n} \boldsymbol{B}_{S}^{\omega}$ Pol. angle ⊖ (Deg.) Midplane • Coupling of coils to sensors **B**<sub>p</sub> sensors for a mode number n at a Lower I-coil frequency  $\omega$ R-1  $\boldsymbol{b}_{SC}^{n,\omega} = \frac{\boldsymbol{B}_{S}^{n,\omega}}{\boldsymbol{I}_{S}^{n,\omega}}$ -90 360 (left handed 90 180 270 0



Tor. angle  $\phi$  (Deg.)

**Field line** 

helicity)

## Plasma response increases at the (*n*=1) ideal MHD no-wall beta limit

- No or very weak plasma response at low β<sub>N</sub> (≤1.5)
- Significant amplification above a β-threshold
- Threshold is close to or coincides with the ideal MHD no-wall β-limit
  - Limit set by n=1 kink mode
  - Typically (in this type of plasma)scales as β<sub>N,nw</sub>~2.4 ℓ<sub>i</sub>
- In the wall stabilized regime the RFA continuously increases with  $\boldsymbol{\beta}$





## Frequency response well described by a single weakly damped mode

 Frequency response of stable high β plasma is well described by a single mode model

$$\tau_{\rm w} \, \frac{dB_{\rm s}}{dt} - \tau_{\rm w} \gamma_0 B_{\rm s} = M_{\rm sc}^* \, I_{\rm c}$$

with  $\gamma_0 = \gamma_{RWM} + i\omega_{RWM}$ 

- Fit of measured spectrum yields
  - Damping rate $-\gamma_{RWM}$ Mode rotation frequency $\omega_{RWM}$ Effective mutual inductance $M_s^*$
- RFA spectrum has also been observed in NSTX [Sontag et al, NF (2007)] and JET [Gryaznevich et al, EPS (2007)]
- Consistent with MARS-F calculations showing that a rotationally stabilized plasma is well described by a single pole [Liu et al, PoP (2006)]



