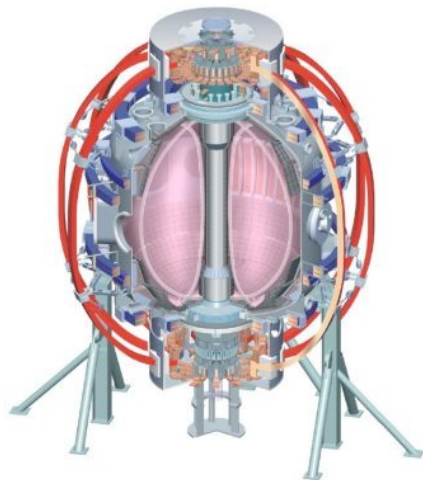


# RFA Suppression With Different Sensors and Time Scales in NSTX

**S. P. Gerhardt, J. E. Menard,  
S. A. Sabbagh**

**MHD TSG Group Review  
Feb. 12<sup>th</sup>, 2010**

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# Overview

- Background:
  - RFA is the amplification of “error fields” by a stable RWM
  - The resulting rotation damping can destabilize the RWM.
  - In 2007, JEM utilized RFA to develop a DEFC scheme.
    - XP-701 used  $B_p$  sensors only.
  - New compensations have been implemented in real-time, allowing better mode identification using  $B_R$  sensors.
- Goals of proposed XP:
  - Determine  $B_R$  sensor compensations and FB parameters which are optimal for error field correction.
    - Examine system response to applied  $n=1$  fields.
    - Examine system response to the intrinsic time-varying error field.
    - Attempt to minimize rotation damping and pulse length using  $B_R$  feedback.
  - Compare results to DEFC with  $B_p$  sensors.
    - Filtering from the PPPs slows the  $B_R$  response (filters noise), which can be beneficial for DEFC.
  - Note: Fast feedback is out of scope.
- Contributes to:
  - MDC-2: Joint experiments on resistive wall mode physics
  - MS Milestone R(10-1): Assess sustainable beta and disruptivity near and above the ideal no-wall limit.

## Outline

- New sensor compensations
- Results from previous XPs
- Considerations and shot list for this XP

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# New Realtime Sensor Compensations For Improved Mode Identification

- Sensors should measure the n=1 field from the plasma only.
  - Need to “compensate” the  $i^{\text{th}}$  sensor  $B_i$  for other sources of field
  - With proper compensations, vacuum shots produce no signal
- Three compensations now in realtime system

**Static**  
**Present From Beginning**

$$C_{i,static} = \sum_{j=0}^{NumCoils-1} p_j I_j$$

**816 Coefficients**

**OHxTF**  
**New For 2010**

$$f_i = LPF(I_{OH} \times I_{TF}; \tau_{OHxTF,i})$$

$$f_i = \frac{f_i}{1 + \beta_i f_i}$$

**if  $f_i > 0$  then  $C_{OHxTF,i} = r_{p,i} f_i$**

**if  $f_i < 0$  then  $C_{OHxTF,i} = r_{n,i} f_i$**

**96 Coefficients**

**AC Compensation For**  
**Fluctuating RWM Coil Currents**  
**New For 2010**

$$C_{AC,i}(t) = \sum_{j=0}^5 \sum_{k=0}^{k_{max}} p_{i,j,k} LPF\left(\frac{dI_{RWM,j}(t)}{dt}; \tau_{AC,i,k}\right)$$

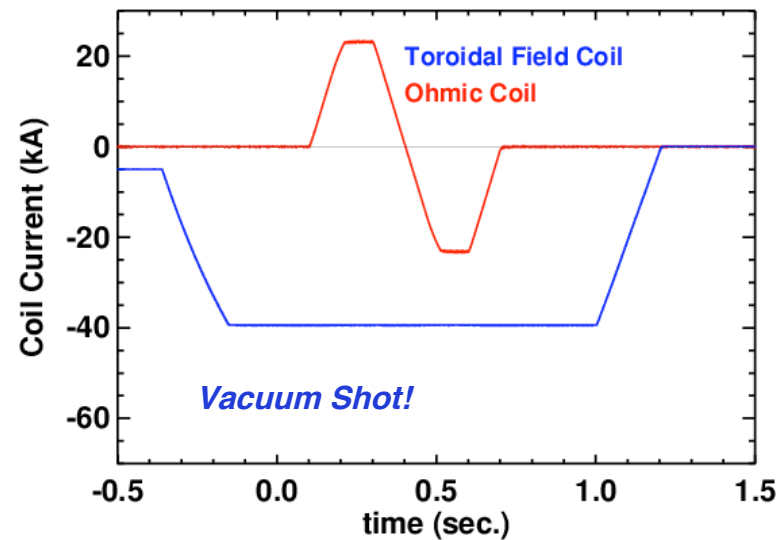
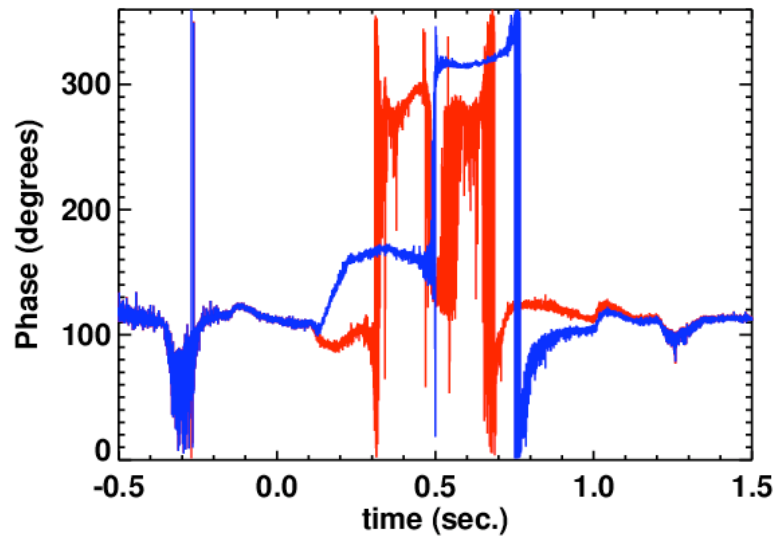
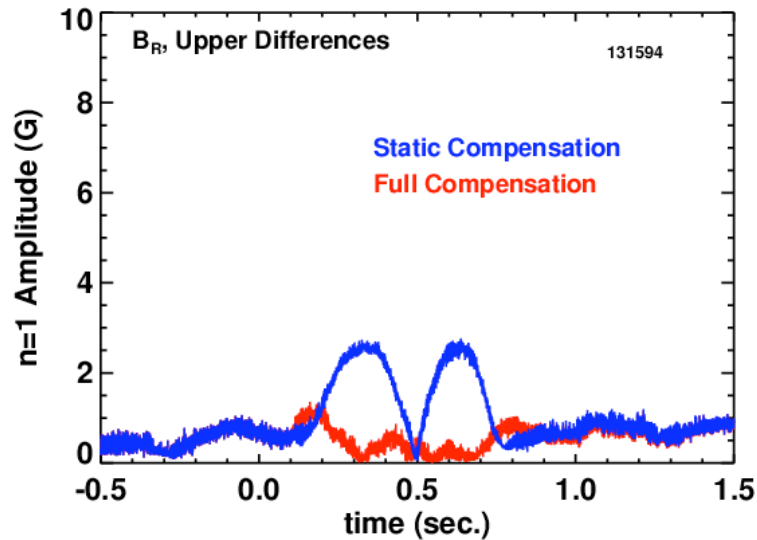
**504 Coefficients**

**Final Field For Plasma Mode Identification**

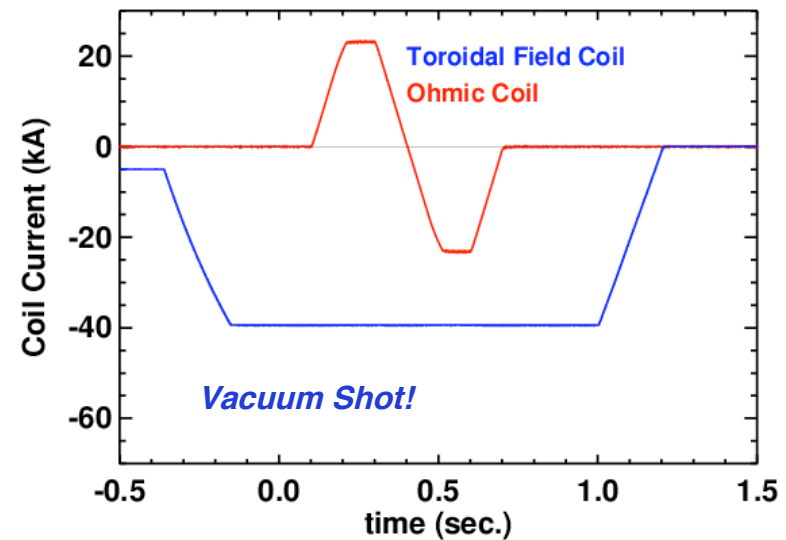
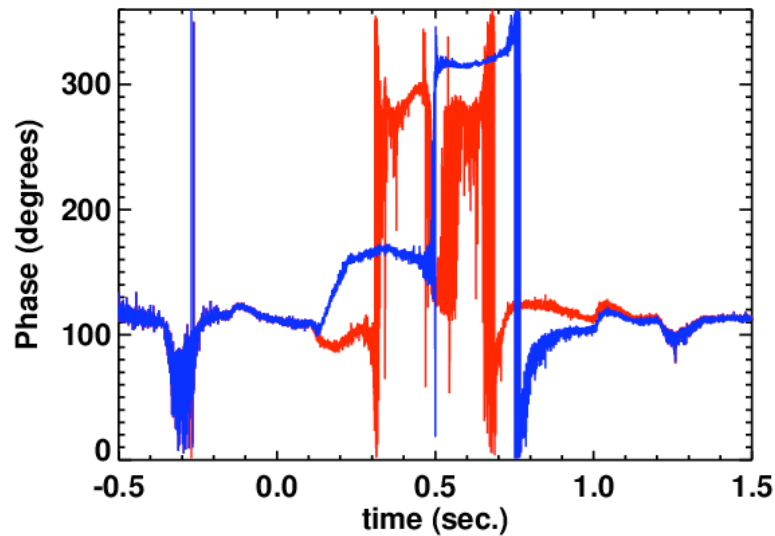
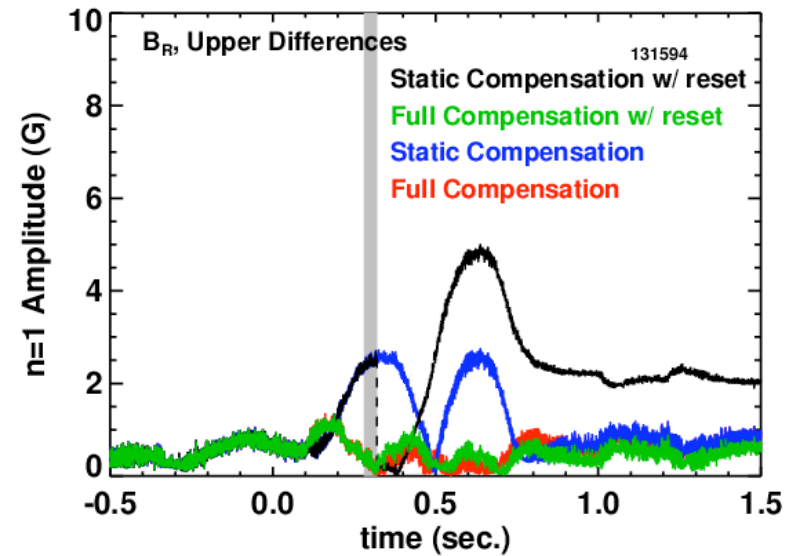
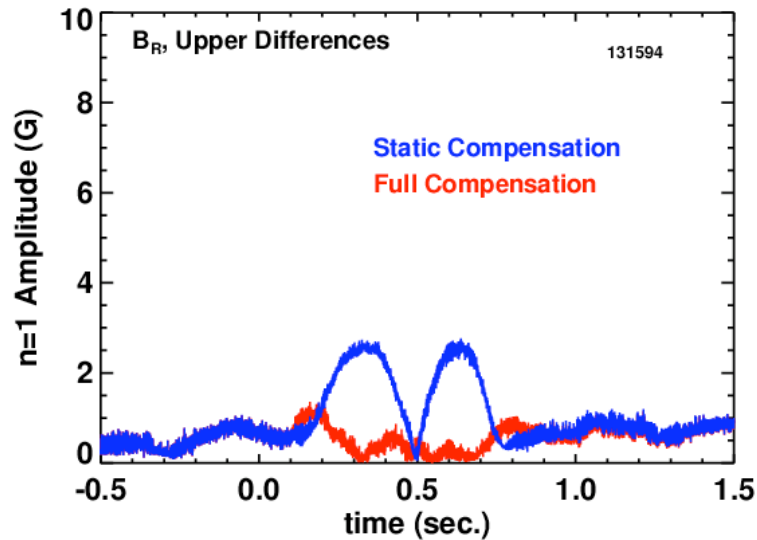
$$B_{i,plasma} = B_i - C_{i,static} - C_{i,OHxTF} - C_{i,AC}$$

*remaining compensation: vessel eddy currents via loop voltages*

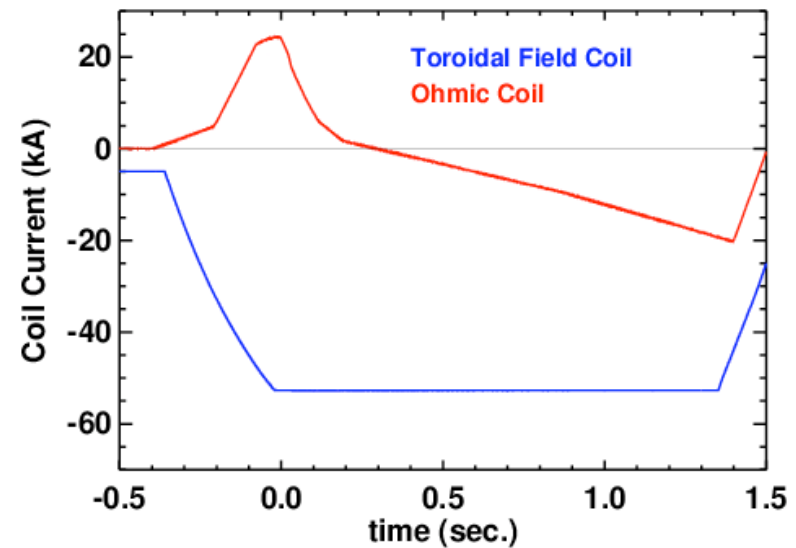
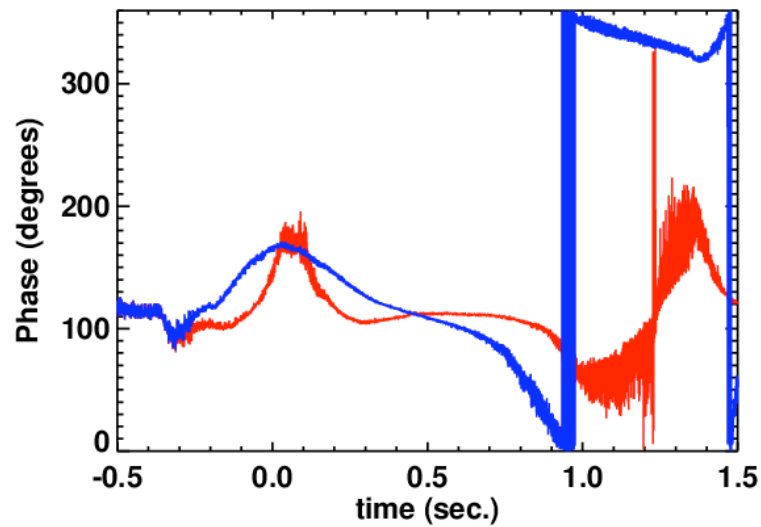
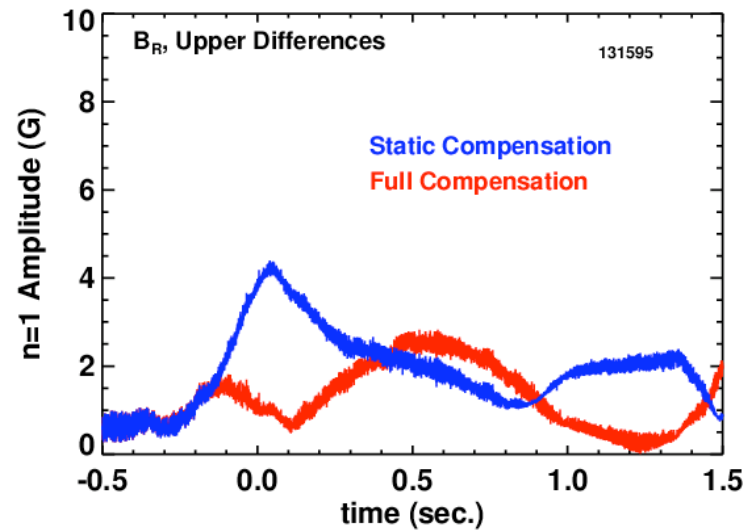
# OH x TF Compensations Important For The $B_R$ Sensors (I)



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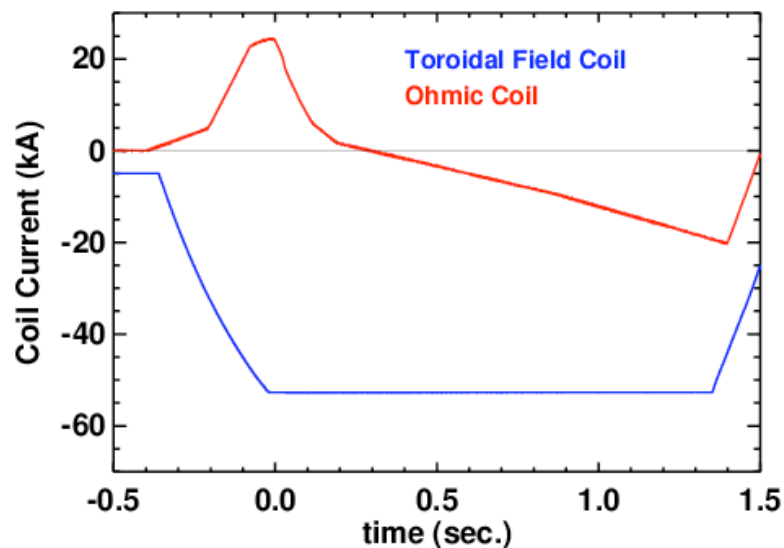
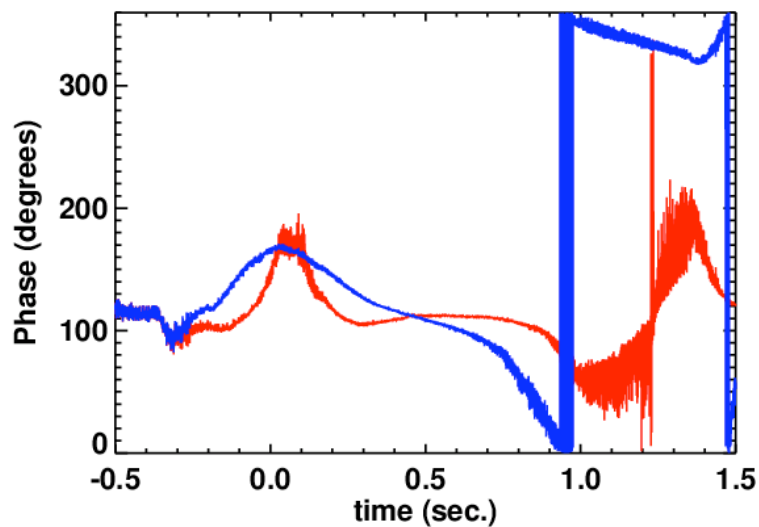
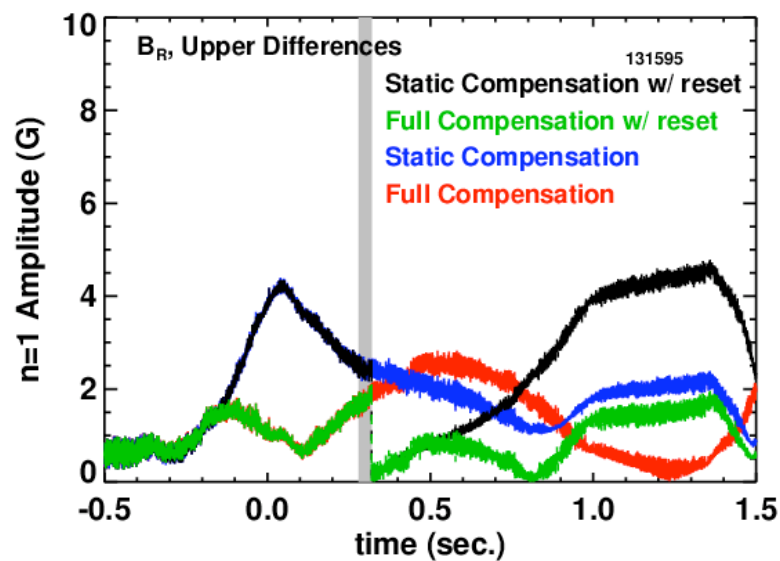
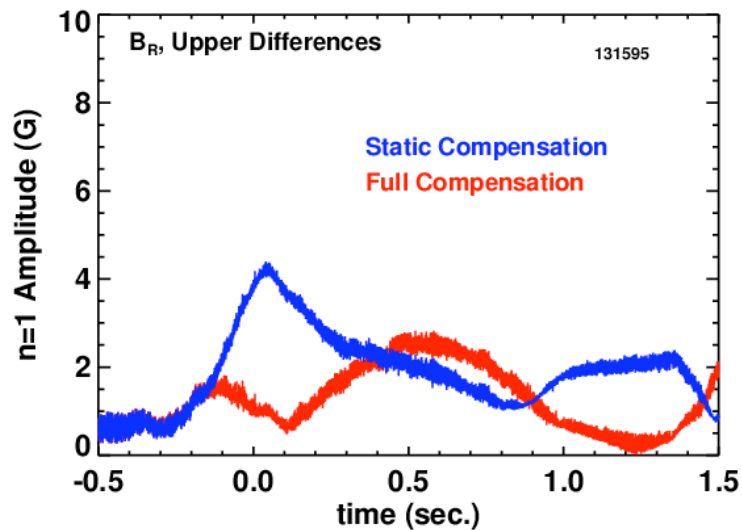


# OH x TF Compensations Important For The $B_R$ Sensors (II)



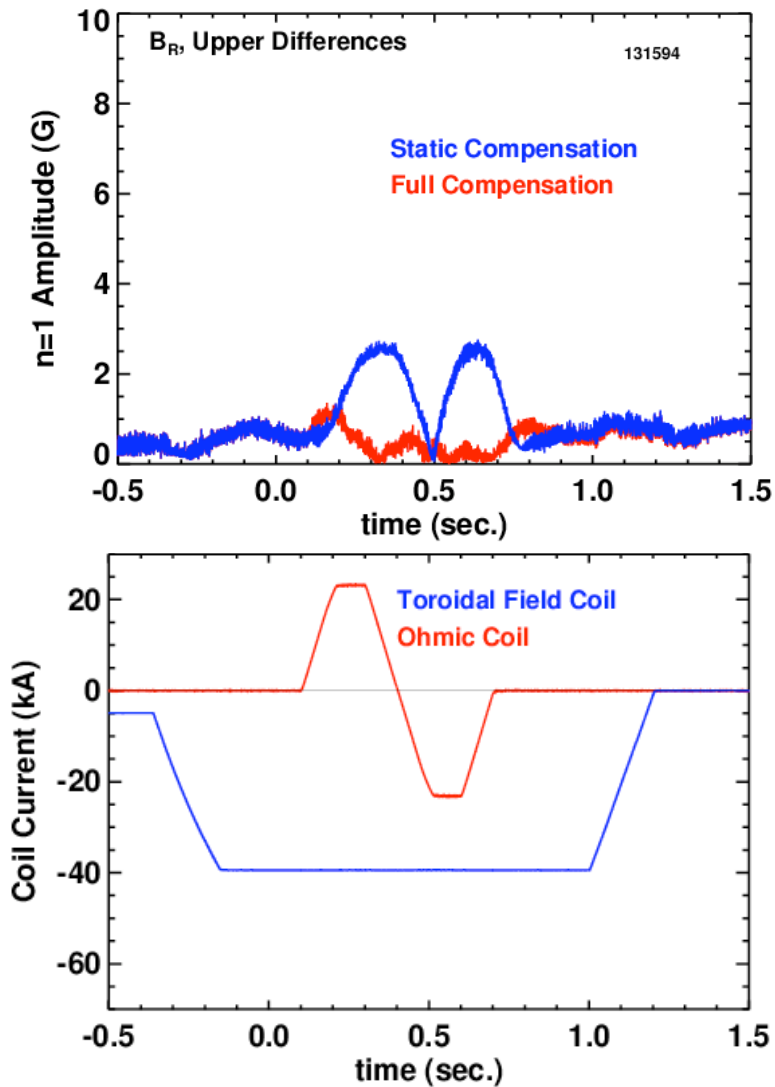


# OH x TF Compensations Important For The $B_R$ Sensors (II)

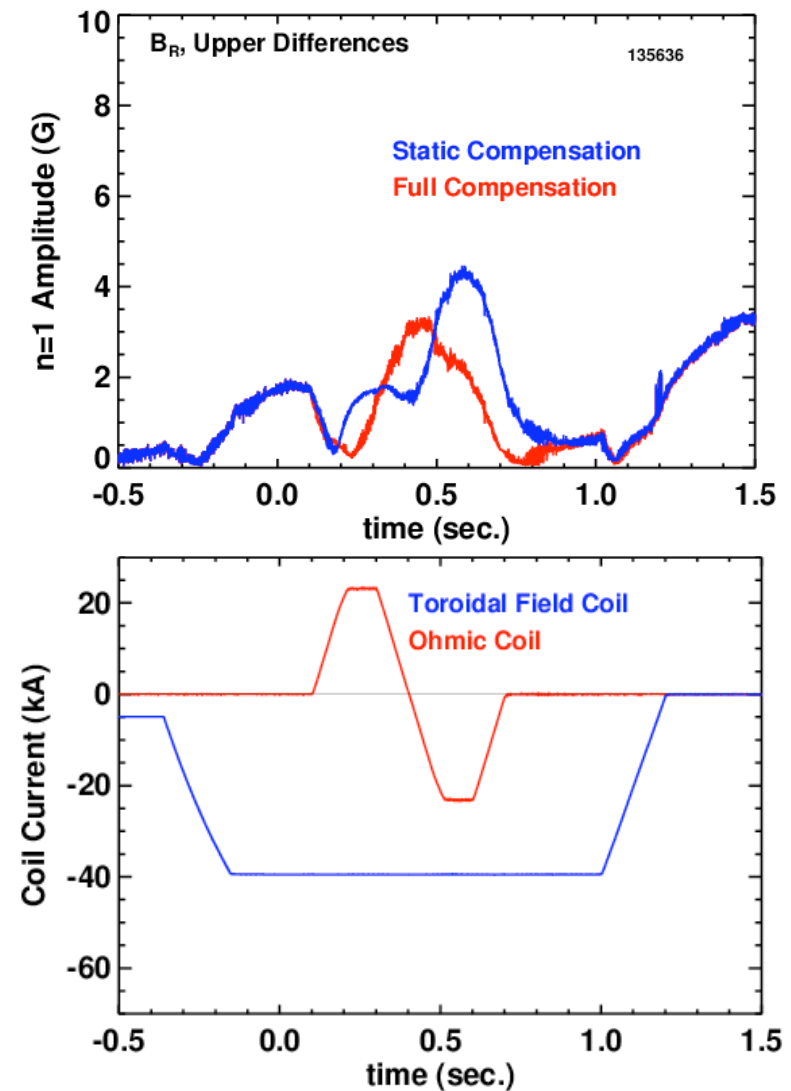


# Need to Keep a Careful Eye on Compensations Through the Run

*Beginning of Run*



*End of Run*

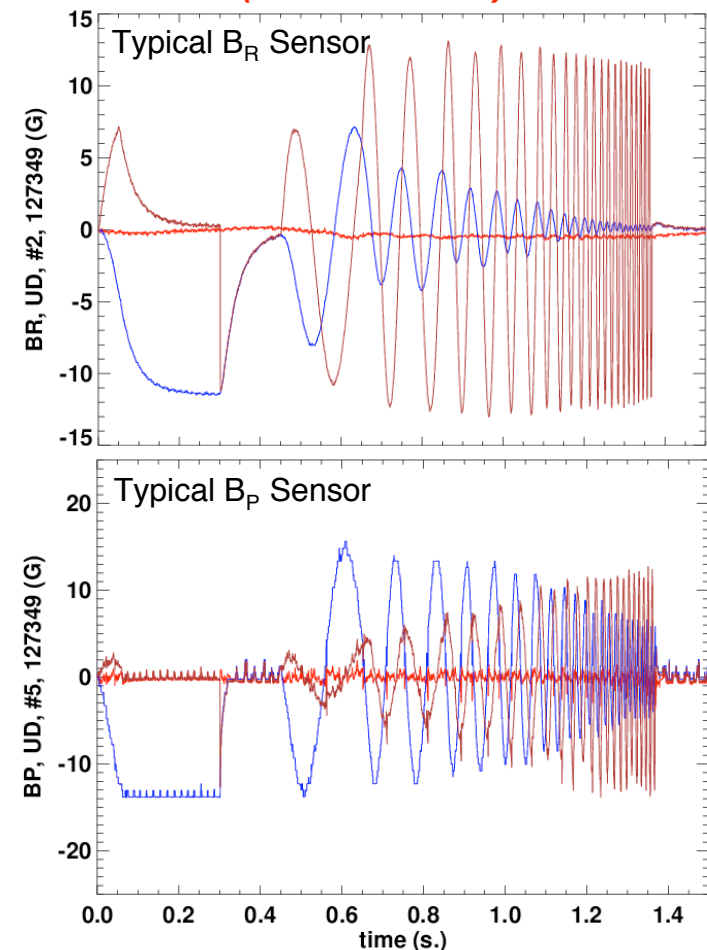


# AC Compensations Remove $dI_{RWM}/dt$ Driven Eddy-Current Pickup

$$C_{AC,i}(t) = \sum_j^{NumRWMCoils} \sum_{k=0}^{k_{max}} p_{i,j,k} LPF\left(\frac{dI_{RWM,j}(t)}{dt}; \tau_k\right)$$

- Sensors should measure the n=1 field from the plasma only.
  - Direct mutual coupling of RWM coil to sensors has always been subtracted off in PCS.
  - Eddy currents due to  $dI_{RWM}/dt$  leads to pickup without plasma.
    - *Eddy currents are out of phase with the coil currents.*
- Realtime AC compensations may be useful for:
  - Mode identification during fast feedback.
    - *SAS proposal on fast feedback.*
  - Mode identification with rapidly changing preprogrammed currents.
    - *ELM triggering experiments.*
  - Future realtime RFA measurements.

**Blue: Full Pickup**  
**Brown: Direct Pickup Only Subtracted (Previously in PCS)**  
**Red: Fully Compensated (Now in PCS)**

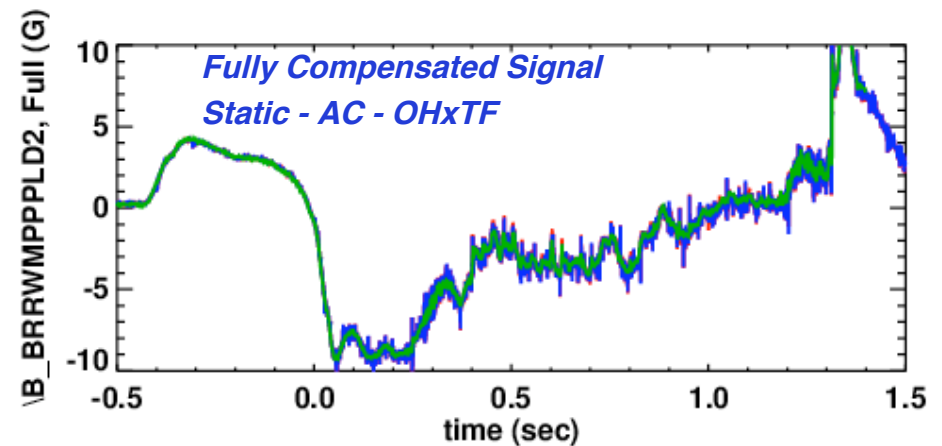
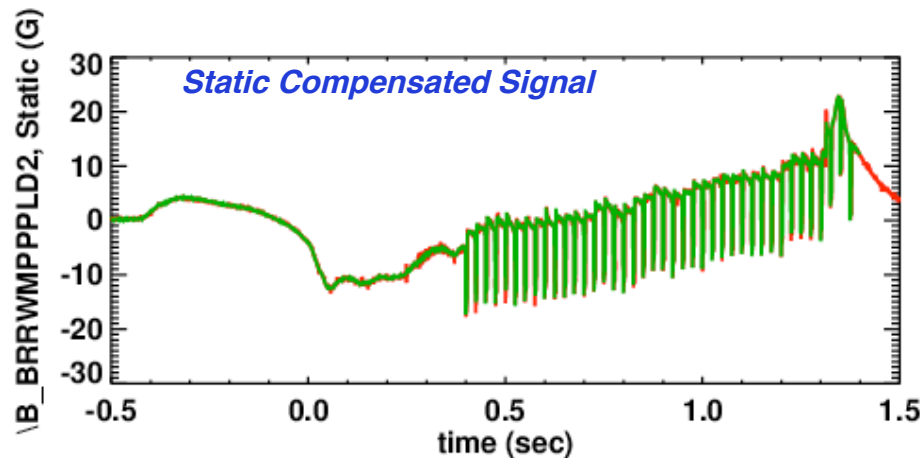
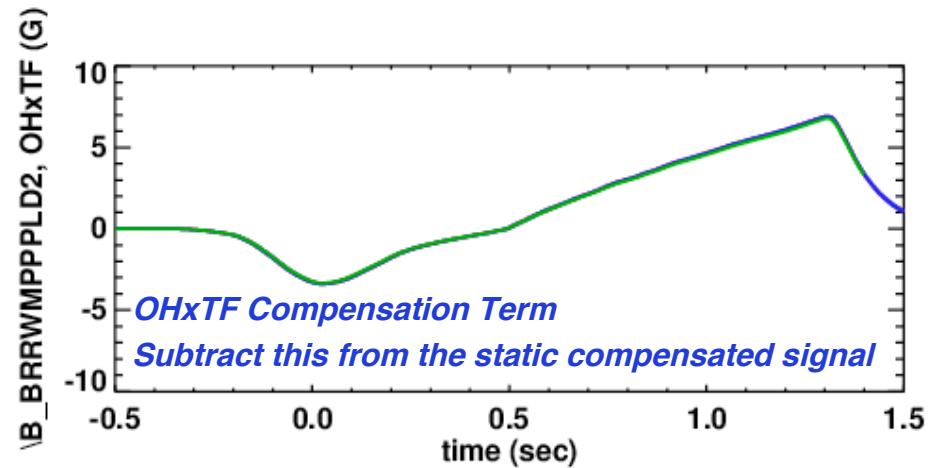
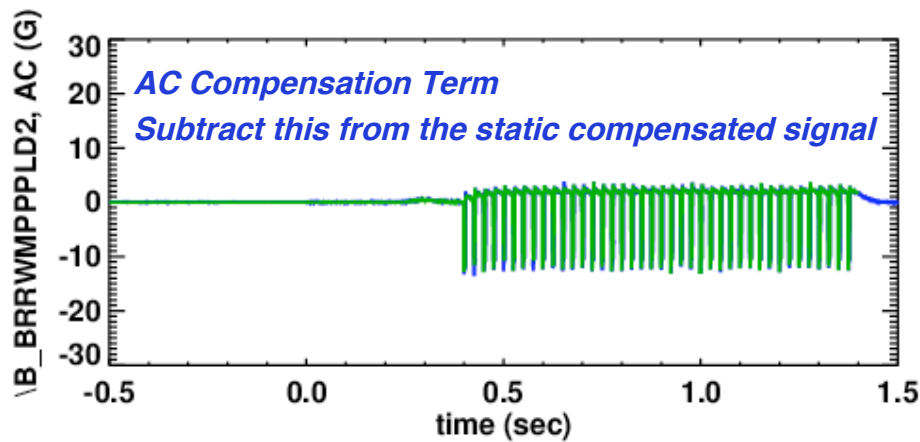


# New Sensor Compensation Fully Implemented in PCS “miu” Algorithm (I)

**Red:** Calculations in idl, from Jon’s routines

**Blue:** Calculations in idl, in a form appropriate for PCS (streamlining a bunch of loops)

**Green:** Archived PCS Calculations

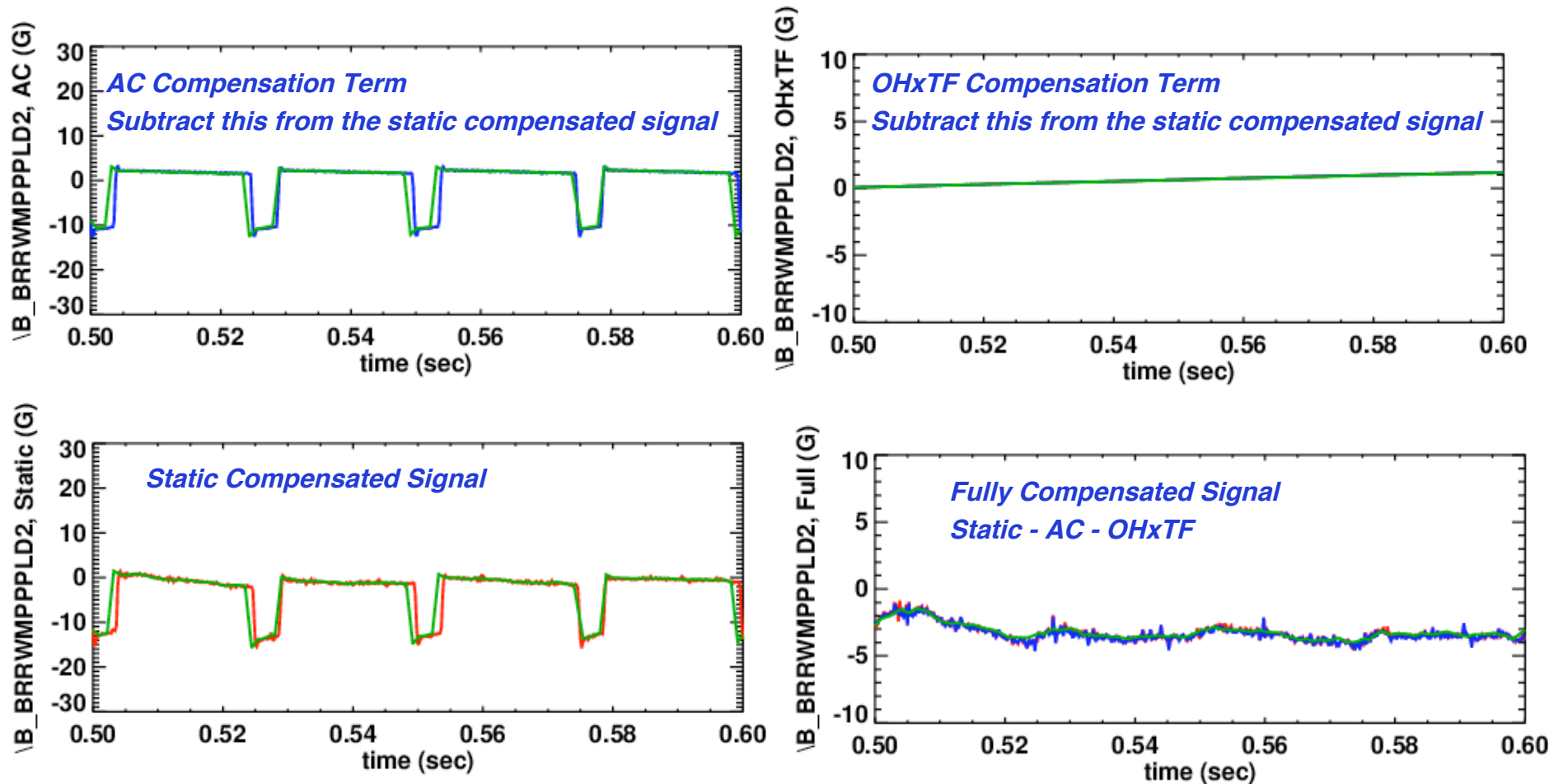


# New Sensor Compensation Fully Implemented in PCS “miu” Algorithm (II)

**Red:** Calculations in idl from Jon’s routines

**Blue:** Calculations in idl in a form appropriate for PCS (streamlining a bunch of loops)

**Green:** Archived PCS Calculations



## More About the New “miu” Algorithm

- Provides identical “outputs” as the present mid algorithm
  - Mode amplitude and phase from  $B_P$ ,  $B_R$ , &  $B_P+B_R$  sensors.
  - Fully interchangeable with the mid algorithm for RWM control.
- Allows separate re-zeroing times for  $B_R$  and  $B_P$  sensors.
  - Old mid algorithm had a single common re-zeroing time.
- Has switches to turn off the new compensations.
  - “static only”
  - “static +AC”
  - “static+OH×TF”
  - “static+AC+OH×TF”
- All compensation coefficients are read from the model tree.
  - Many new nodes open in the model tree in September.
- Archives many many internal calculations for comparison to off-line.
- Prepares sensor data for the state-space controller.

## Outline

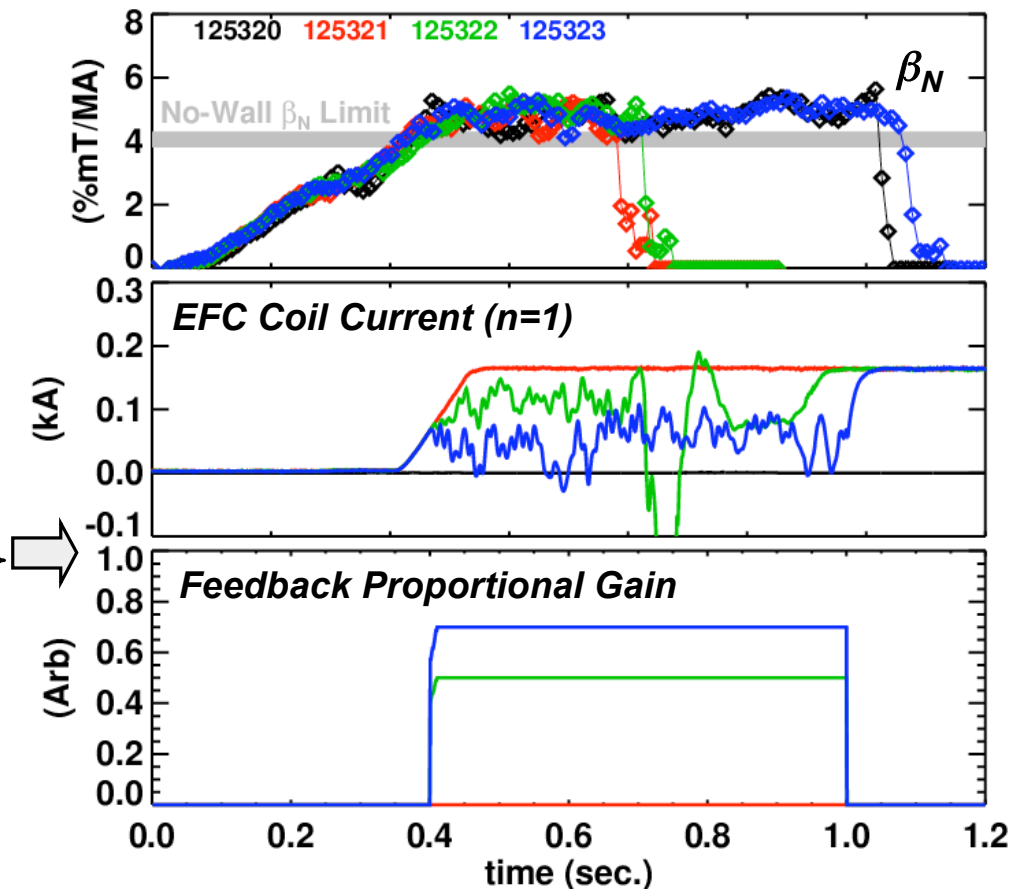
- New sensor compensations
- Results from previous XPs
- Considerations and shot list for this XP

## 2007 Experiment Had a Phase Scan... ...and a Gain Scan

- Pre-programmed n=1 EF correction requires a priori estimate of intrinsic EF
- Detect plasma response → EF correction using *only feedback on RFA*

### RFA Suppression Algorithm

- Use discharge with rotationally stabilized RWM.
- **Deliberately apply n=1 EF in order to reduce rotation, destabilize an RWM.**
- **Find feedback phase that reduces the applied n=1 currents ( $B_p$  sensors).**
  - Direct coil-sensor pickup is removed.
- Increase the gain until currents are nearly nulled and plasma stability is restored.

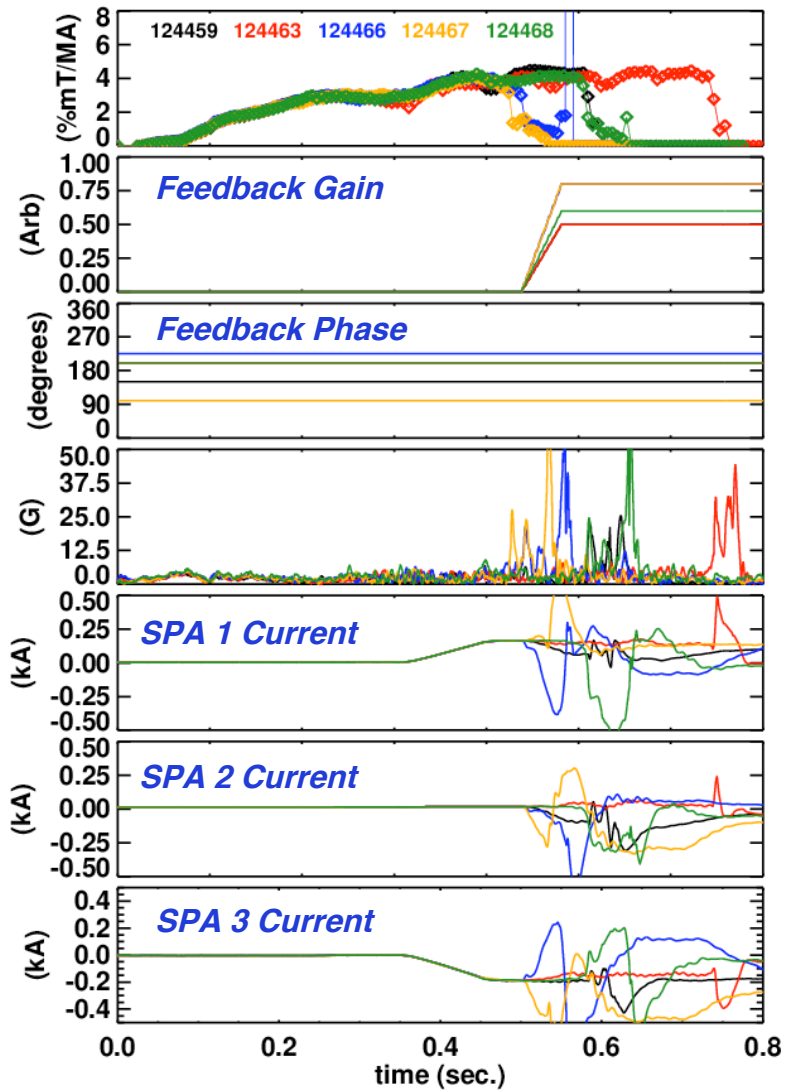


→ Use same gain/phase settings to suppress RFA from intrinsic EF **and** any unstable RWMs

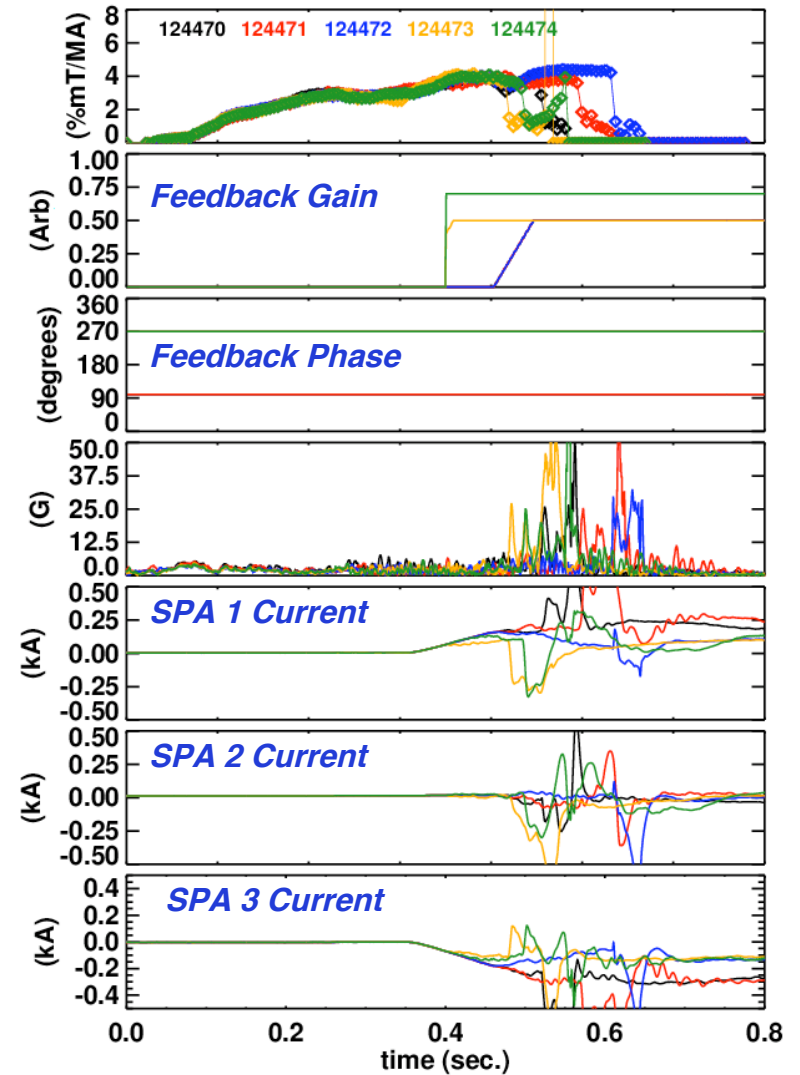


# 2007 Experiment Had a Phase Scan... ...and a Gain Scan

Upper  $B_p$  Sensors

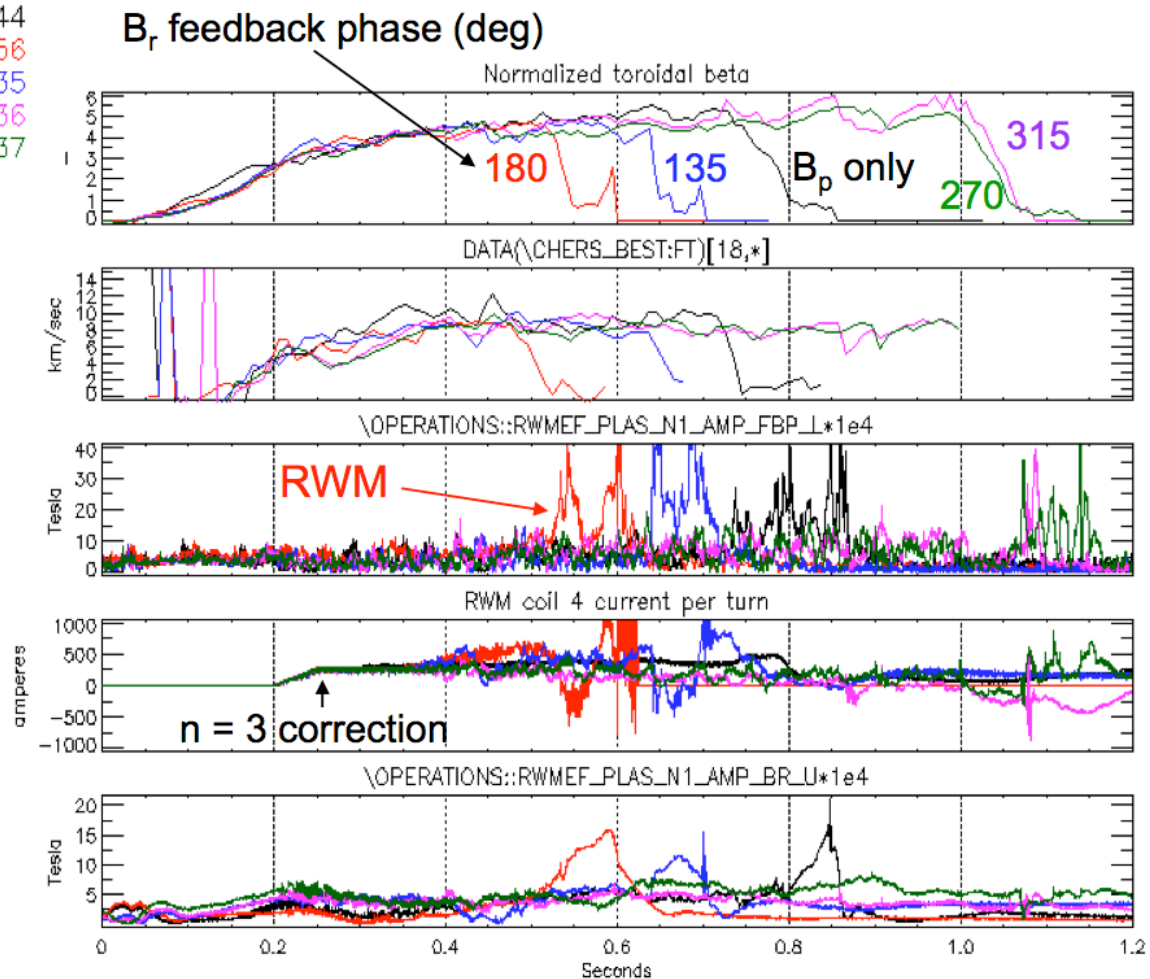


"Combined"  $B_p$  Sensors



# 2008 Also Had Feedback Attempt With $B_R$ Sensors

Shots:  
 130244  
 130256  
 130635  
 130636  
 130637



- Combined  $B_P + B_R$
- $B_R$  feedback phases around  $\sim 290$  appear to be useful.
- $B_R$  feedback gains of 0.7 appeared stable.
- Use these parameters as starting points for the XP.

XP-802, Sabbagh et al.

## Outline

- New sensor compensations
- Results from previous XPs
- Plan for this XP

# Experimental Plan (I)

- Background Testing
  - Algorithm tested already, but not as built into the present PCS.
  - Run some cases on the 2nd computer when the run starts, using shot data.
    - Compare to outputs of the “identical” idl code.
  - Introduce the miu algorithm as the primary mode-ID algorithm for standard RWM feedback.
  - Use 50% test shots to check for stability of OHxTF compensations.
- Qualify the reference discharge. (4 shots)
  - High- $\beta$  discharge with  $n=3$  correction, but no fast feedback.
    - 800 kA SAS and JB shots with high  $\beta_N$  from 2009 (like 133775)?
    - Lasted 1.15 seconds using only (-)10 kA of OH current.
  - Should suffer a rotation collapse and RWM
    - Induce with  $n=1$  applied field as necessary (as in XP-701).
    - Phase relationship with OHxTF field?

## Experimental Plan (II)

- Apply (only)  $B_R$   $n=1$  feedback with varying phases and gains. (10 shots)
  - Low-pass filter the feedback request in order to eliminate fast feedback.
  - Gain and phase optimization
    - Start with gain and phase from XP-802.
    - Scan both, starting with the phase, then optimizing the gain.
    - Try to achieve cancellation of the EF effect as in XP-701.
  - Repeat best test with OHxTF compensations turned off.
  - Particular emphasis on the edge rotation sustainment.
- Apply  $B_P$   $n=1$  feedback on the same situation. (6 shots)
  - Recreate phase scan in XP-701 for comparison.
  - Test FB noise level, rotation evolution in similar situations...can  $B_R$  cancel better?
- Repeat with intrinsic EF. (4 shots)
  - Raise  $I_p$  to  $\sim 1$ MA in order to get to larger OH currents.
  - Shots with both “optimal”  $B_R$  and  $B_P$  feedback separately, then combined.
- Test compensation of time varying error fields. (6 shots)
  - Choose “best” sensor polarity, phase and gain.
  - Apply  $n=1$  TWs with 10, 20, 30, 40 Hz.
  - Determine frequency above which the TW is not fully cancelled by FB.
  - Repeat without AC compensations

*Total: 30 Shots*

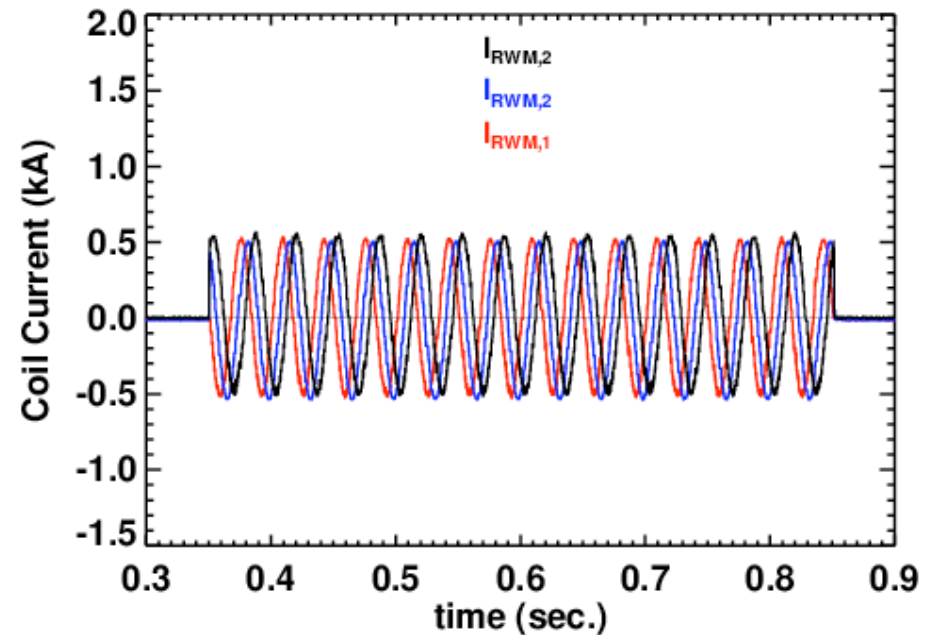
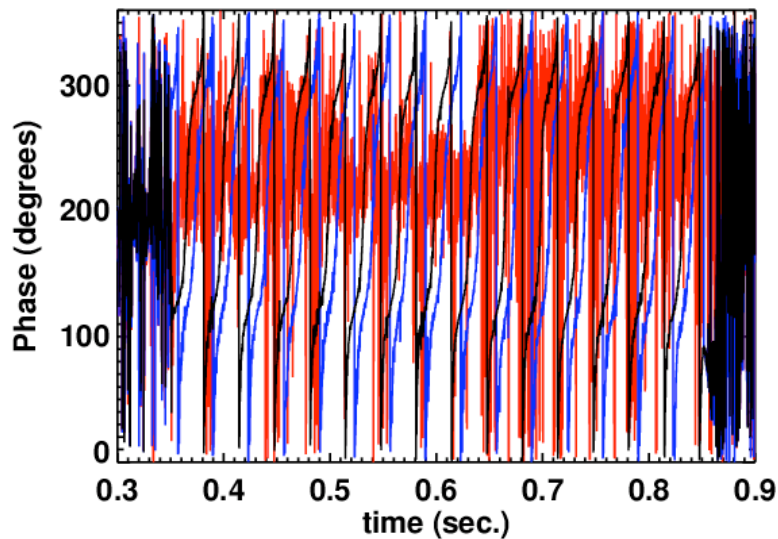
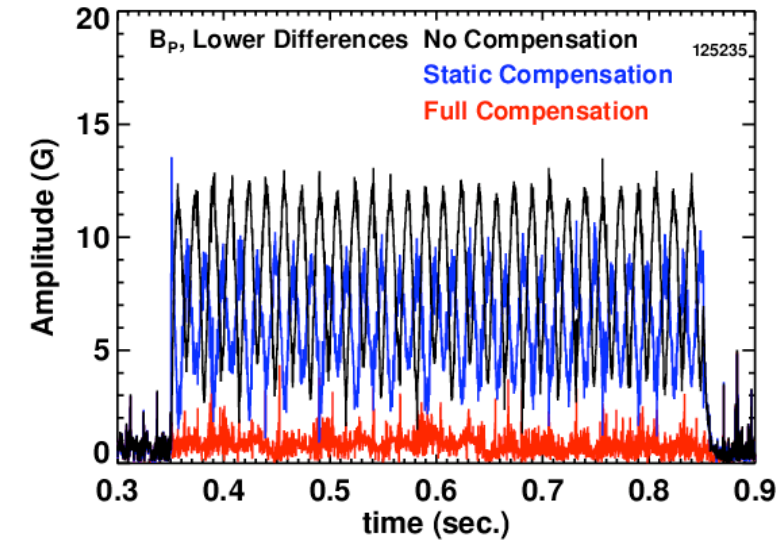
# Backup

# Goals For Proposed Experiment

- Qualify  $B_R$  sensors for error field correction.
  - Determine the optimal phase shift and gain for DEFC.
    - Can start with results from Steve's XP in 2008
  - Determine if OHxTF sensor compensation is necessary...or beneficial...or irrelevant.
  - Fast feedback is out of scope
- Determine if one or the other sensor type is better for correction:
  - Reduced fluctuations in the FB coil current?
  - Improved rotation sustainment?
  - Higher gain?
- Examine  $\beta$ -dependence of FB response.

# AC Compensations Can Be Important For

- Large amplitude modulation in signal with static compensation





## Other Stuff

- Lithium
  - LITER at ~200 mg/shot
  - No LLD
- Diagnostics
  - Profile diagnostics
  - RWM detection
- Analysis
  - MSE reconstructions.
  - DCON for proximity to ideal stability limits.
  - Intrinsic EF and detailed RWM sensor analysis.