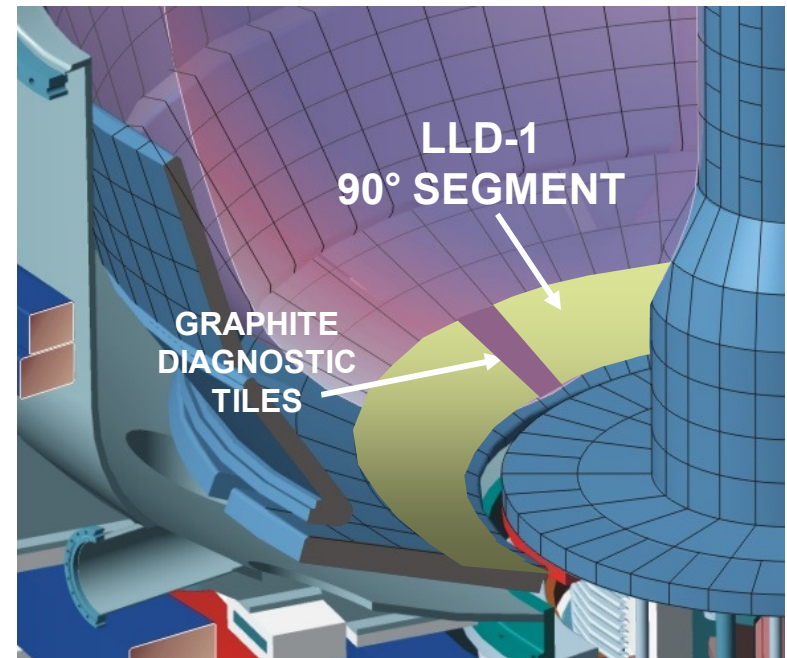


## Abstract

*A small prototype sample of the NSTX Liquid Lithium Divertor (LLD) was exposed to a MSE-LIF diagnostic neutral beam at a power of  $\sim 10$  MW/m<sup>2</sup> for 1-3 seconds. Calibrated IR measurements of front face temperature and thermocouple measurements of bulk sample temperature were obtained. Predictions of temperature evolution were derived from a simple 1D heat flux model and compared with experimental data. These results demonstrated the effective heat load handling of a thin stainless steel liner with porous Mo coating on a copper heat sink, suggesting usefulness as NSTX-Upgrade PFCs. A novel method of measuring the resistance of the lithium films inside NSTX was also developed, the initial results of which will be presented.*

# Lithium experiments are ongoing on NSTX

- Three-phase approach:
  1. Lithium pellet injection (LPI)
  2. Lithium evaporation (LITER)
  3. Liquid lithium divertor (LLD)
    - Located on lower OD in four 82.5° segments
    - 152  $\mu\text{m}$  porous Mo plasma-sprayed on 254  $\mu\text{m}$  SS bonded to 1.9 cm Cu
    - “Filled” via evaporation from LITER probes
- Experiments with LITER probes have produced evidence of reduced edge density



*H. Kugel.*

## LLD also provides greater power handling capabilities

- Mo has advantages over C
  - Higher thermal conductivity -> expanded distribution of heat
  - Higher Z -> lower sputtering yields
- **Additional offline testing of porous Mo required**
  - Determine extent of physical damage to the substrate
    - Will the LLD melt or suffer significant erosion?
  - Measure spatial & temporal thermal evolution of front face
    - How is thermal conductivity affected by the porosity?
  - Quantify the effects of solid/liquid Li
    - What are the erosion and sputtering yields vs. temperature?
    - Does Li protect the Mo?

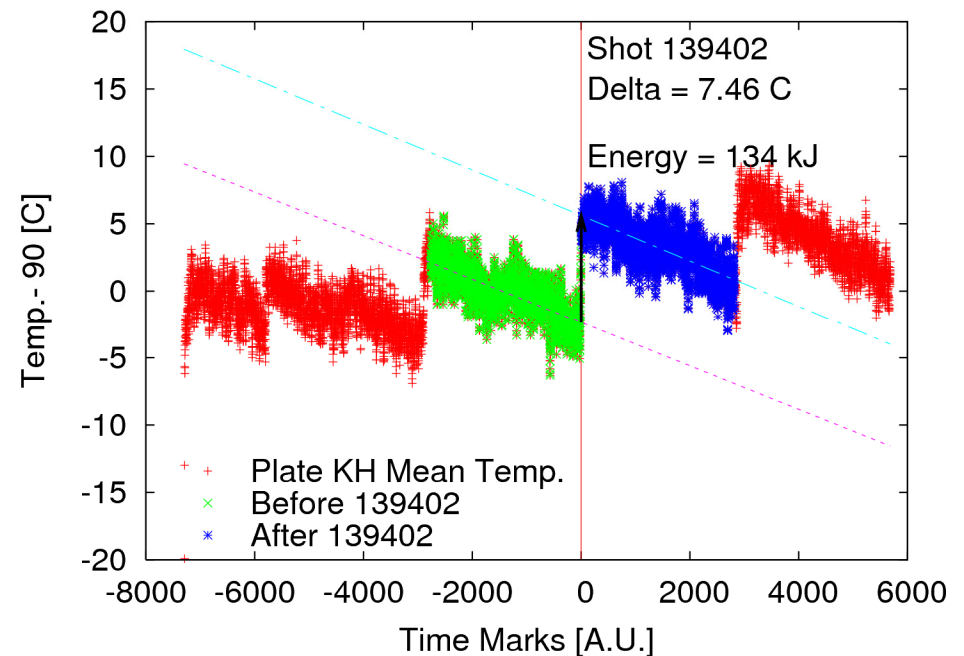
# Heat flux constrained by thermocouple measurements

- Thermocouples measure LLD plate temperatures
- Treat LLD plate as a 90lb. calorimeter
- Rise in mean temperature yields energy deposited
- Energy into KH for shot 139402 is 134 kJ
  - Geometric conversion to 360 degrees yields ~590 kJ
  - NBI input into tank is ~4 MJ
  - Mean plate power for 1.1s discharge is 530 kW

$$E = V_{plate} \rho_{Cu} C_{p,Cu} \Delta T$$

$$E = 5222 \text{ cm}^3 \cdot 8.94 \text{ g/cm}^3 \cdot 0.384 \text{ J/(gm K)} \cdot \Delta T$$

$$E = \Delta T \cdot 17.9 \text{ kJ/K}$$



M.A. Jaworski.

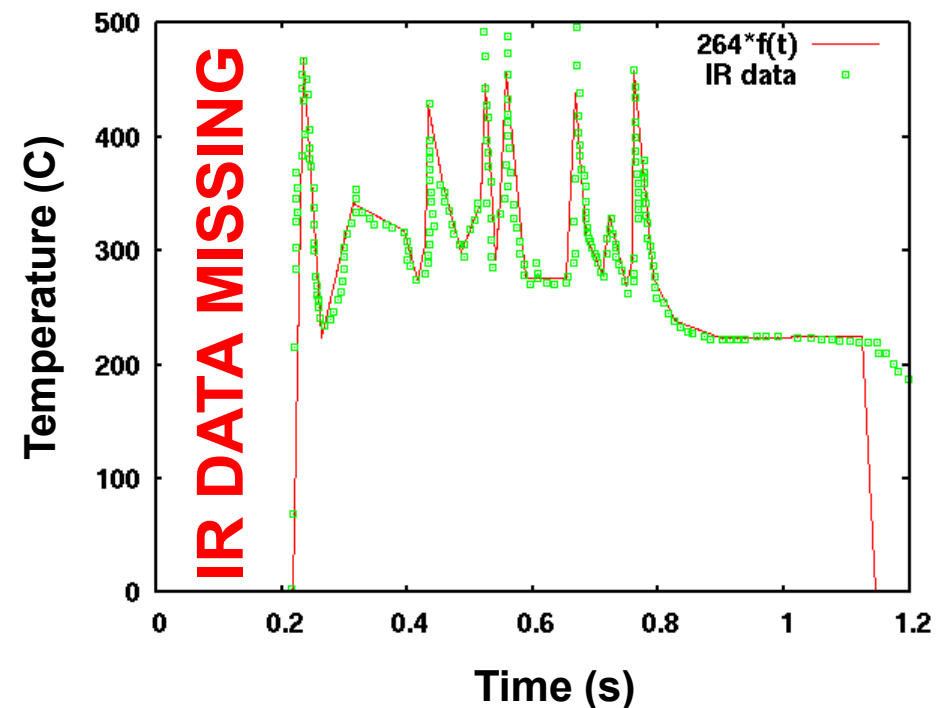
# Integral heat flux obtained from two-color IR data

- Time varying function  $f(t)$  taken from IR data waveform
  - $f(t)$  is normalized and assumed proportional to heat flux  $q(r,t)$
  - 2cm decay length  $\lambda$  taken from shot 120755 (similar shape as original plasma)
- Resulting heat flux integral set equal to energy
  - 3.7 MW/m<sup>2</sup> mean heat flux obtained
  - “true” mean flux is lower (missing IR data)

$$q(r,t) = q_0 f(t) \exp\left[\frac{-(r-r_{sep})^2}{\lambda^2}\right]$$

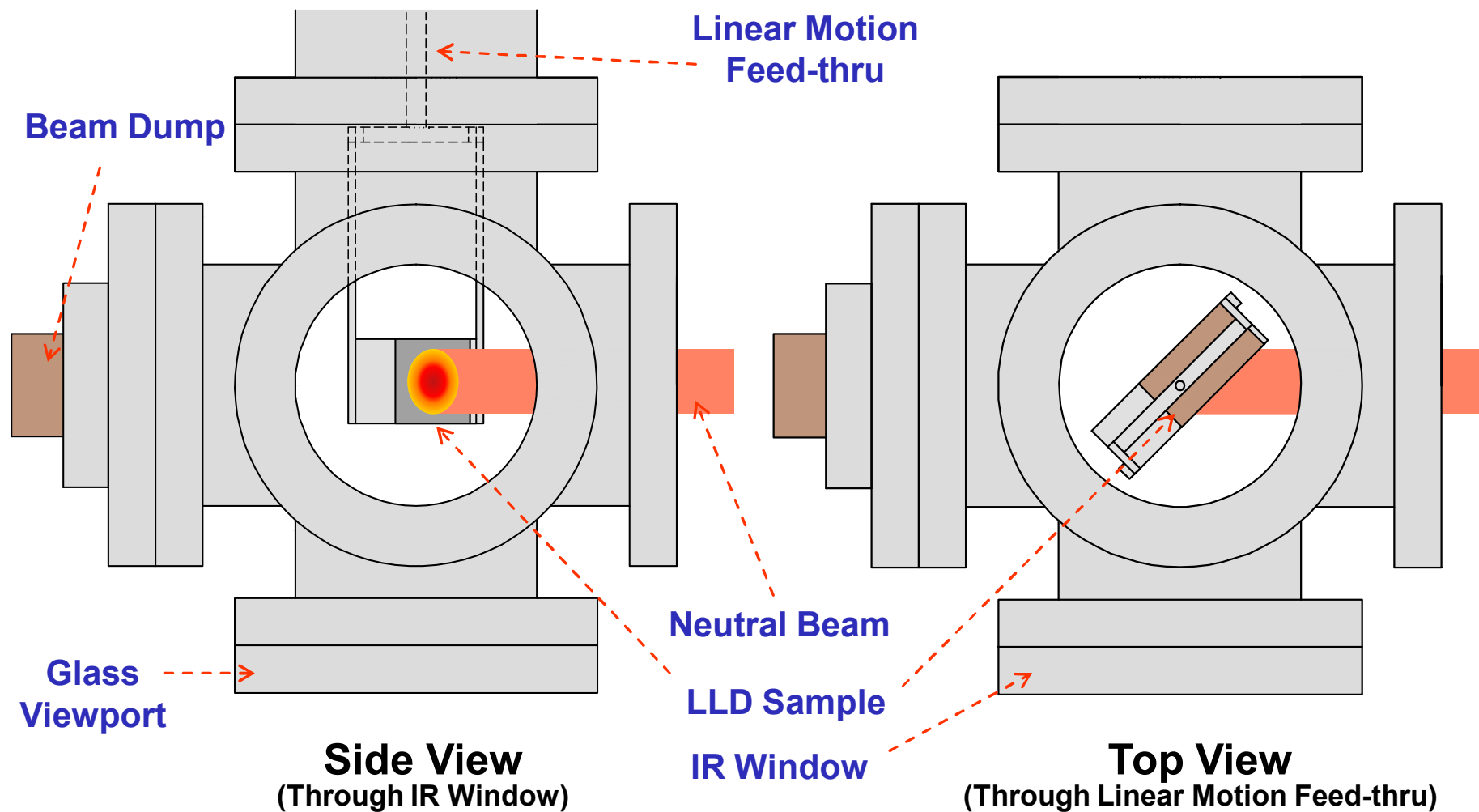
$$E = \iiint q(r,t) r d\theta dr dt$$

$$q_0 = \frac{E}{2\pi 0.025 m^2} = 3.73 MW / m^2$$



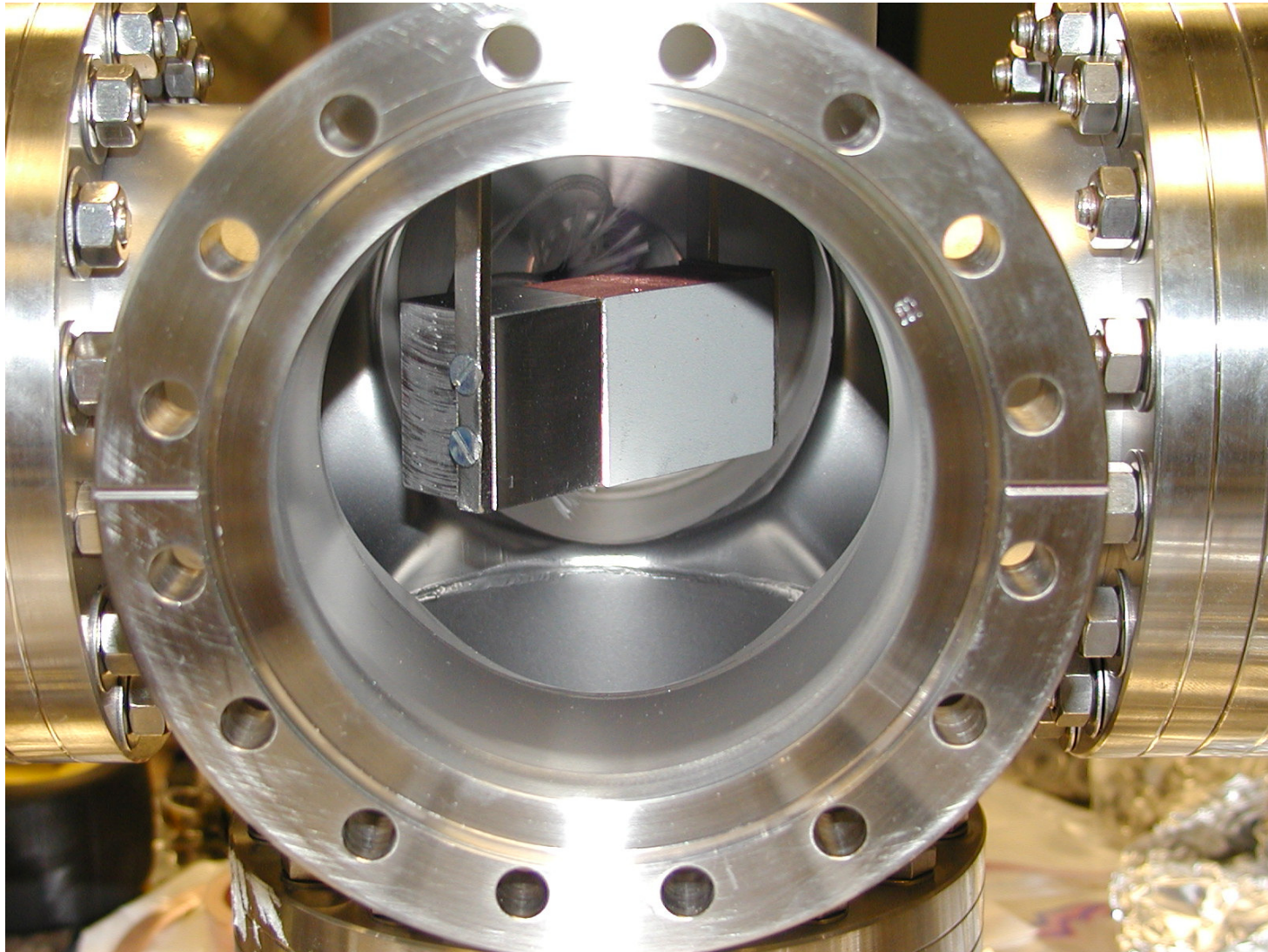
*M.A. Jaworski.*

# Diagram of Experimental Setup



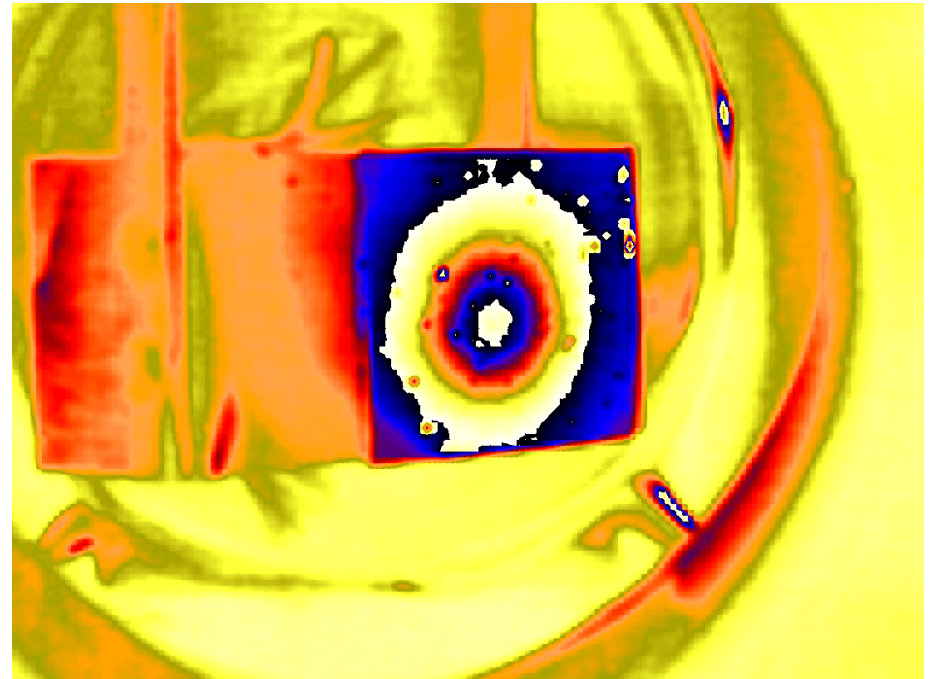


## Side View of Experimental Setup



# IR Camera provides Time-Resolved 2D Temperature Data

- Camera resolution:
  - ~1mm spatial
  - 33.3 ms temporal
- LLD sample “plunged” in front of DNB for 1-3 s
- Front face temperature recorded by IR camera
  - Absolute temperatures determined via calibration
  - Performed with replicated experimental conditions, matches TC data to within 10° C
- Back face temperature recorded by TCs



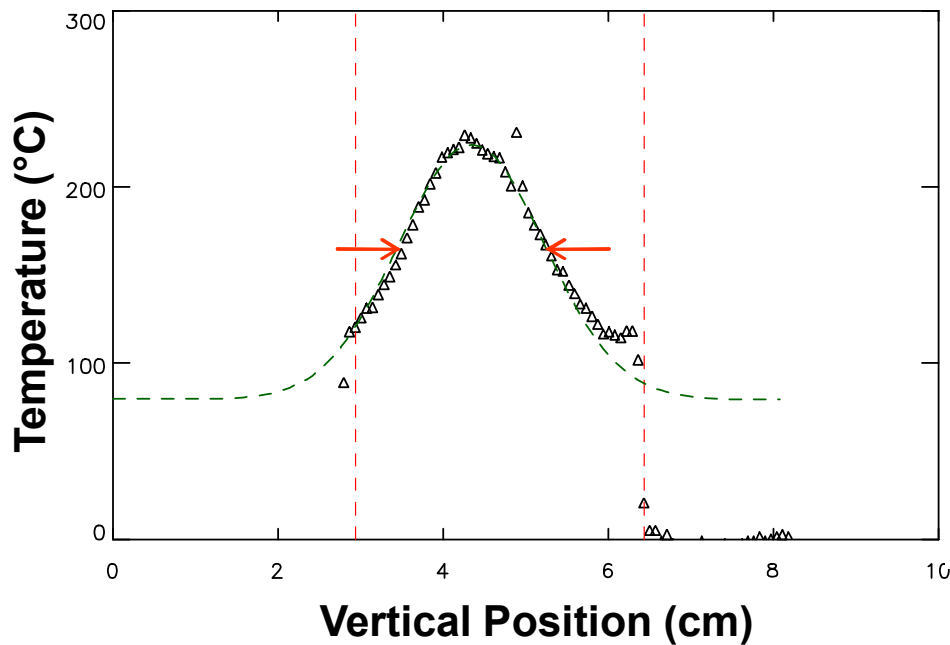
*False color image of LLD sample during neutral beam exposure*



# Beam profile determined from Temperature data

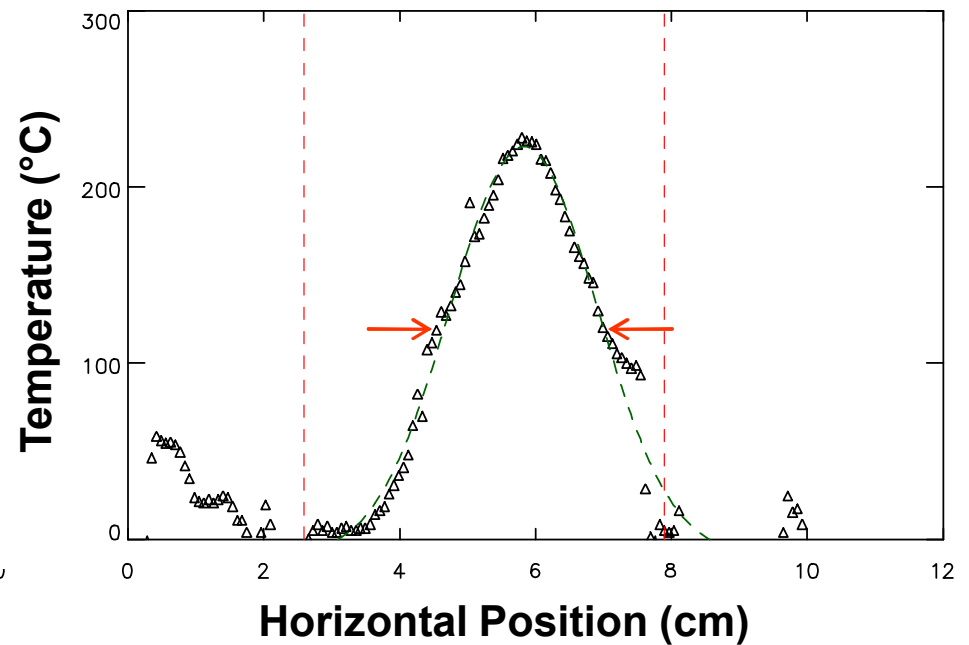
- Beam profile assumed Gaussian
- Again assume  $q$  proportional to  $T$

### Vertical Temperature Profile



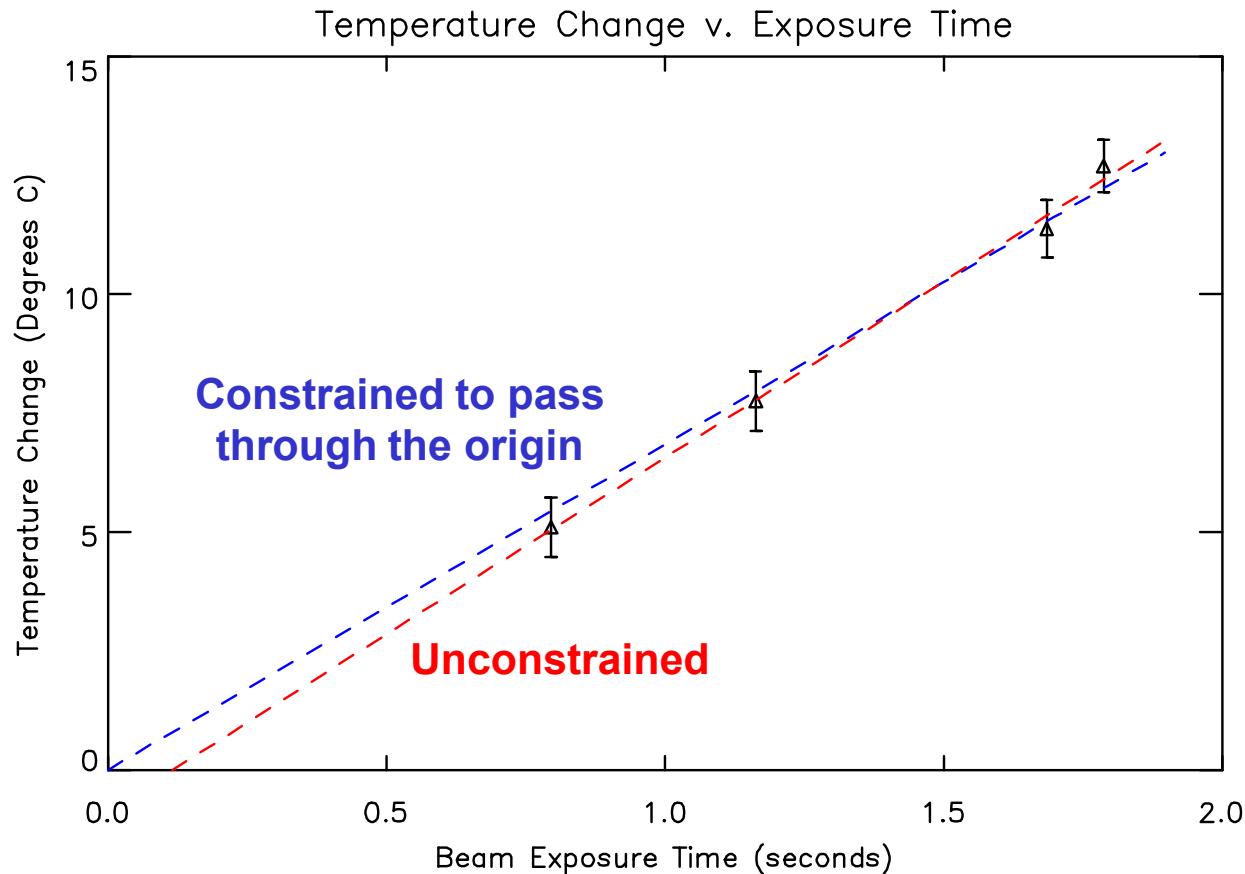
$$\sigma_y = \sigma_V = 0.89 \text{ cm}$$

### Horizontal Temperature Profile



$$\sigma_x = \sqrt{\sigma_v^2 + \sigma_h^2} = 1.40 \text{ cm}$$

# Copper Sample can be used as Calorimeter



$$\Delta E = mC_p\Delta T = \langle J \rangle \cdot t + E_0$$

$$q(x, y) = \frac{\langle J \rangle}{2\pi\sigma_x\sigma_y} \exp\left[\frac{-x^2}{2\sigma_x^2} + \frac{-y^2}{2\sigma_y^2}\right]$$

$$q_{\max} = q(0,0) = \frac{\langle J \rangle}{2\pi\sigma_x\sigma_y}$$

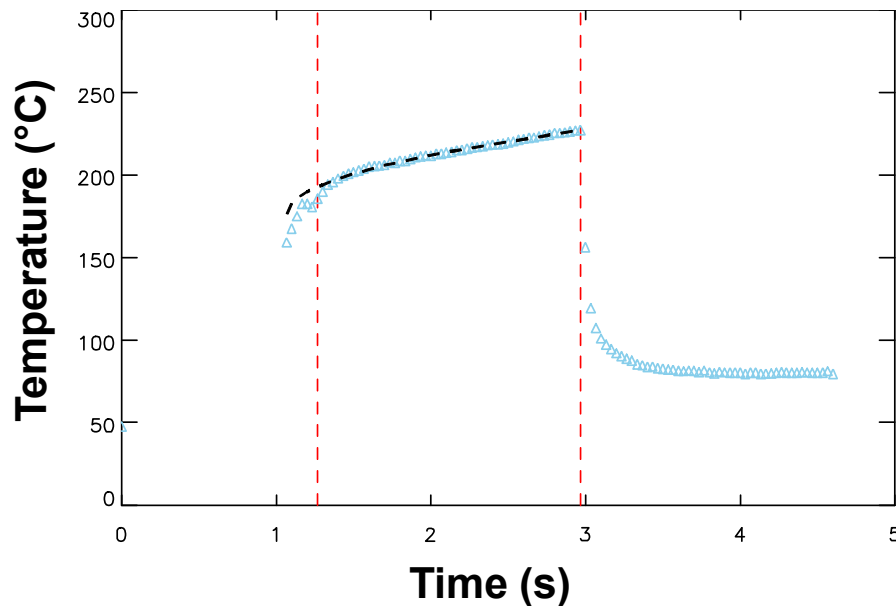
- Temperature change varies linearly with exposure time
- Corresponds to peak heat flux of:
  - $1.13 \pm 0.03$  MW/m<sup>2</sup> (blue),  $1.22 \pm 0.07$  MW/m<sup>2</sup> (red)

# IR Data can be fit analytically, but with arbitrary $T_0$

- Assume 1D problem, constant heat flux  $q_s$
- Using  $\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}$  and  $q_s = -k \frac{\partial T}{\partial x} \Big|_{x=0}$  one obtains:

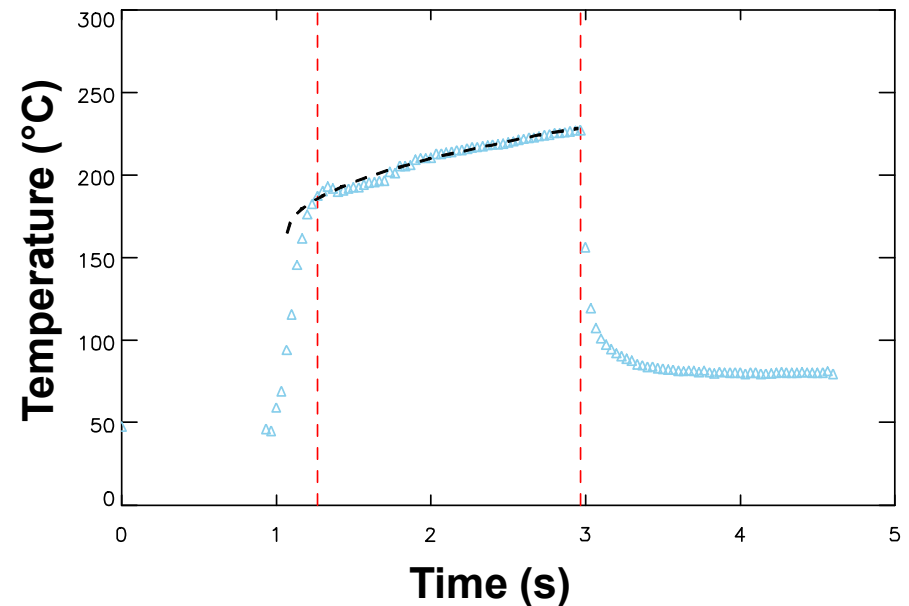
$$T(x, t) \Big|_{x=0} = q_s \left[ \left( \frac{4\alpha_{Cu} t}{\pi k_{Cu}^2} \right)^{1/2} + \frac{\Delta x_{Mo}}{k_{Mo}} + \frac{\Delta x_{SS}}{k_{SS}} \right] + T_0$$

Temperature at Center of Beam



- Heat flux:  $1.22 \pm 0.02$  MW/m<sup>2</sup>

Temperature at Center of Block



- Heat flux:  $1.53 \pm 0.03$  MW/m<sup>2</sup>

## IR Data can also be fit numerically

- Again in 1D, but variable  $q$
- Finite difference the diffusion equation:

$$\frac{T_j^{n+1} - T_j^n}{\Delta t} = \alpha \left[ \frac{T_{j+1}^n - 2T_j^n + T_{j-1}^n}{(\Delta x)^2} \right]$$

- Boundary Conditions:

$$q^n = -k \frac{T_1^n - T_0^n}{\Delta x} \quad T_J^n = T_{J-1}^n$$

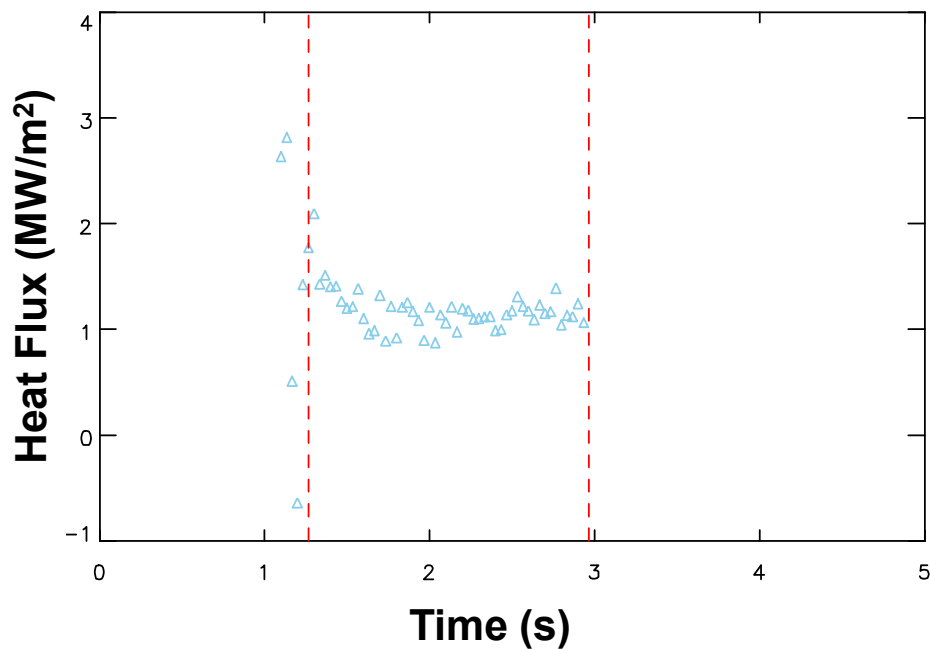
- $T_1^n, T_j^0$  known for all  $n, j$  respectively. Solve for  $q$ :

$$q^n = \frac{k}{\Delta x} \left\{ \left[ \frac{T_1^{n+1} - T_1^n}{\Delta t} \right] \frac{(\Delta x)^2}{\alpha} - T_2^n + T_1^n \right\}$$

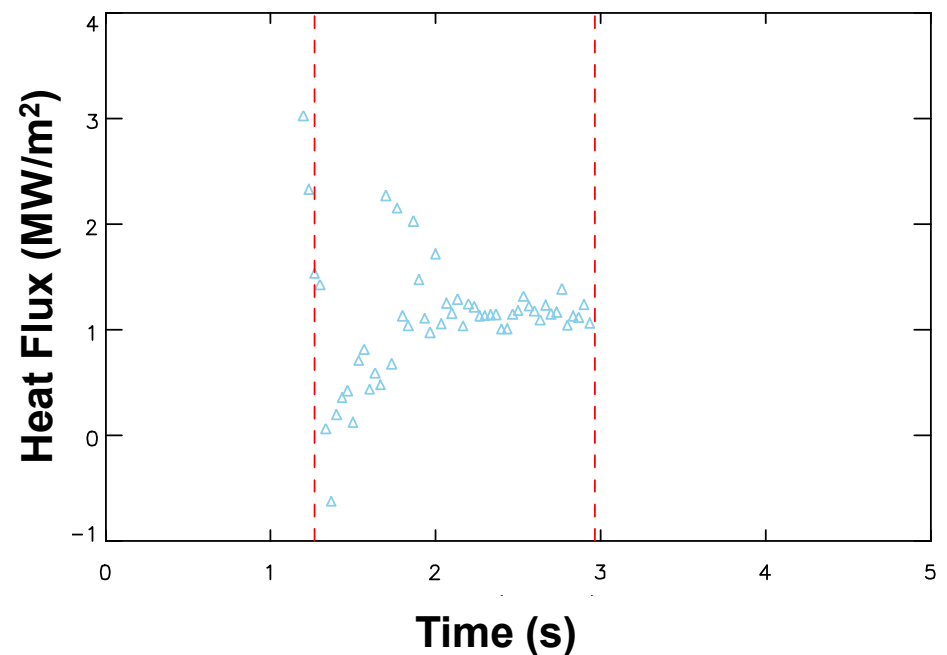
## IR Data can also be fit numerically

- $T_1^n, T_j^0$  known for all  $n, j$  respectively. For each  $n$ :
  1. Calculate temperatures other than at boundaries
  2. Determine the heat flux
  3. Find temperatures at boundaries using BCs

Heat Flux at Center of Beam

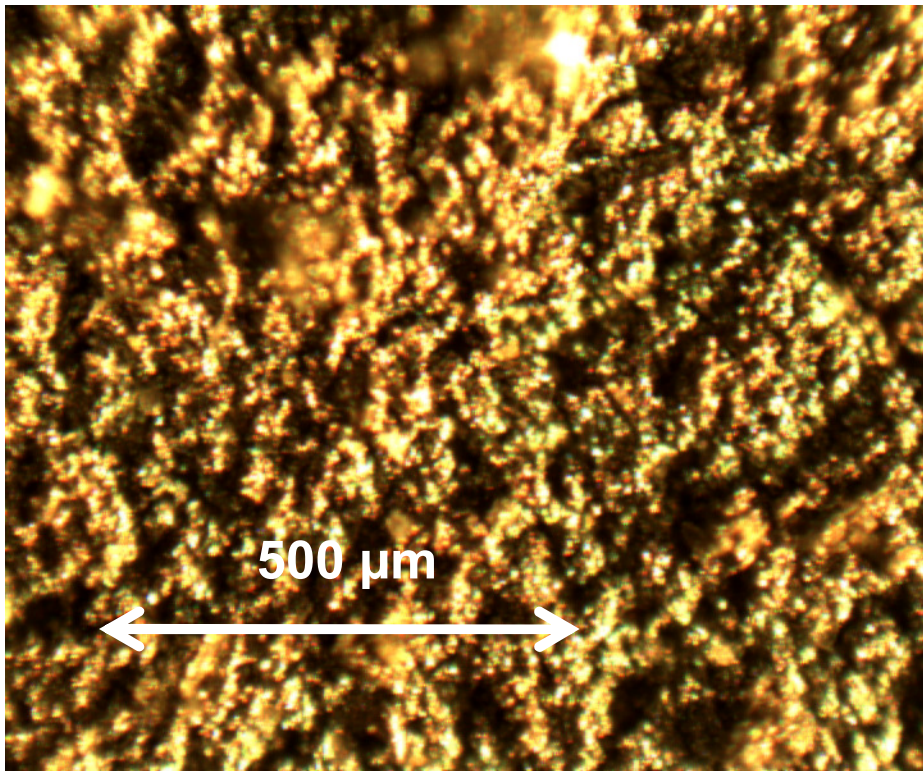


Heat Flux at Center of Block

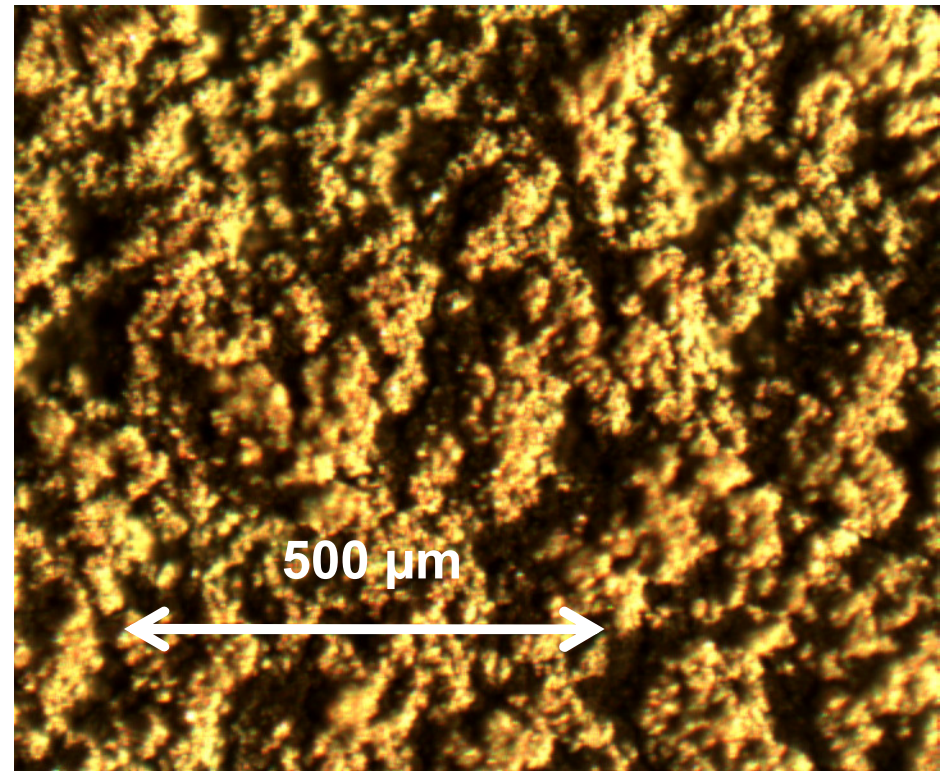




# Optical Microscope provides micron-level spatial resolution



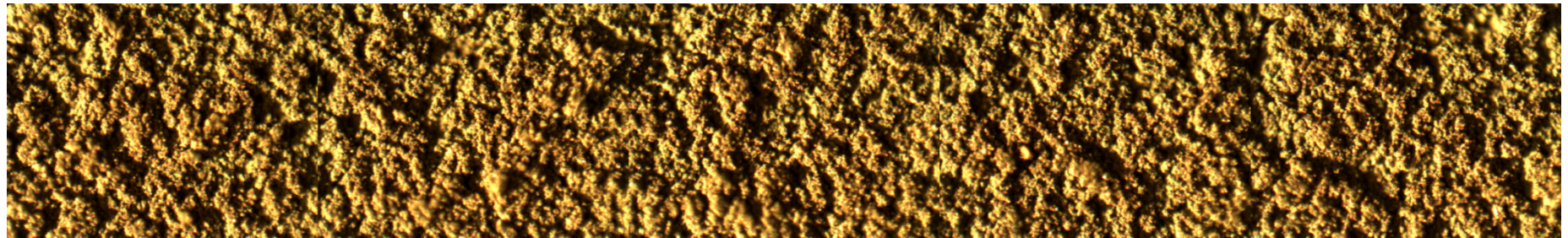
**No Beam Exposure**



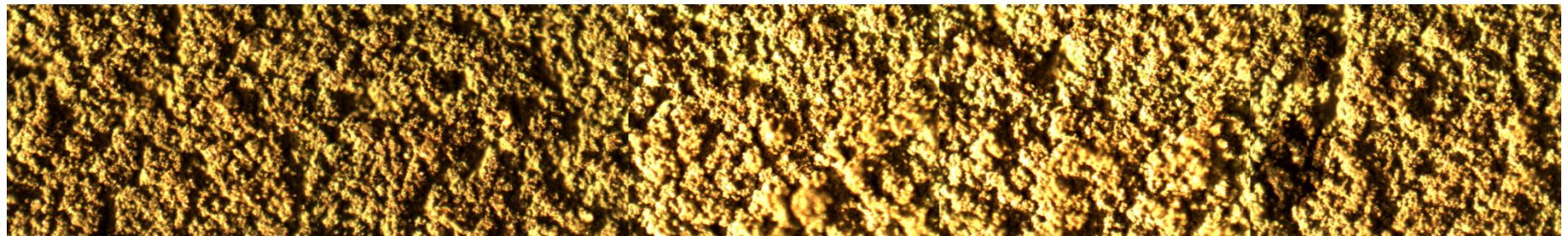
**With Beam Exposure**



# No Apparent Spatial Dependence of Damage



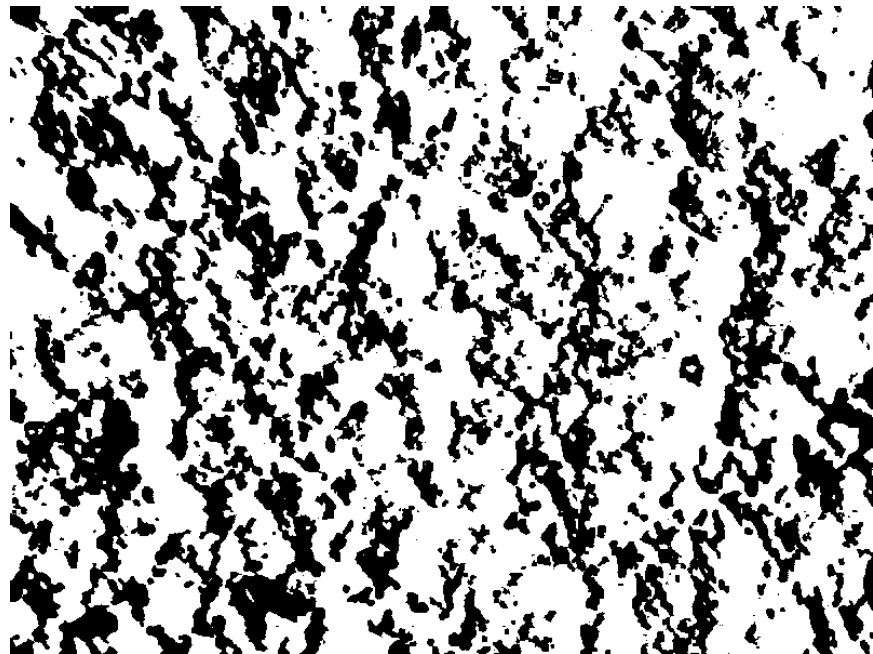
-9.0 mm      -8.0 mm      -7.0 mm      -6.0 mm      -5.0 mm



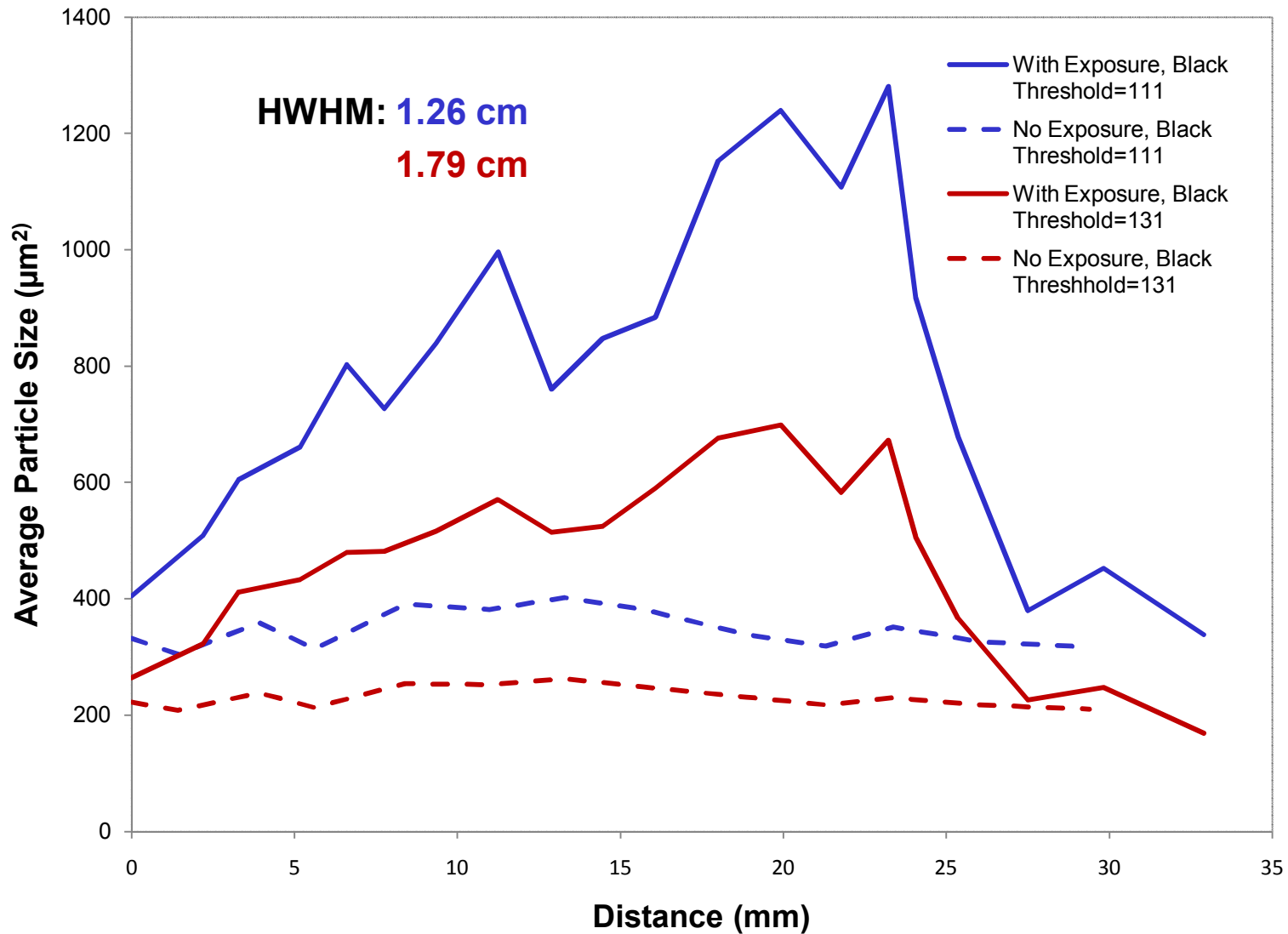
-4.0 mm      -3.0 mm      -2.0 mm      -1.0 mm      **Approximate  
Center of Sample**

# ImageJ software provides quantitative analysis methods

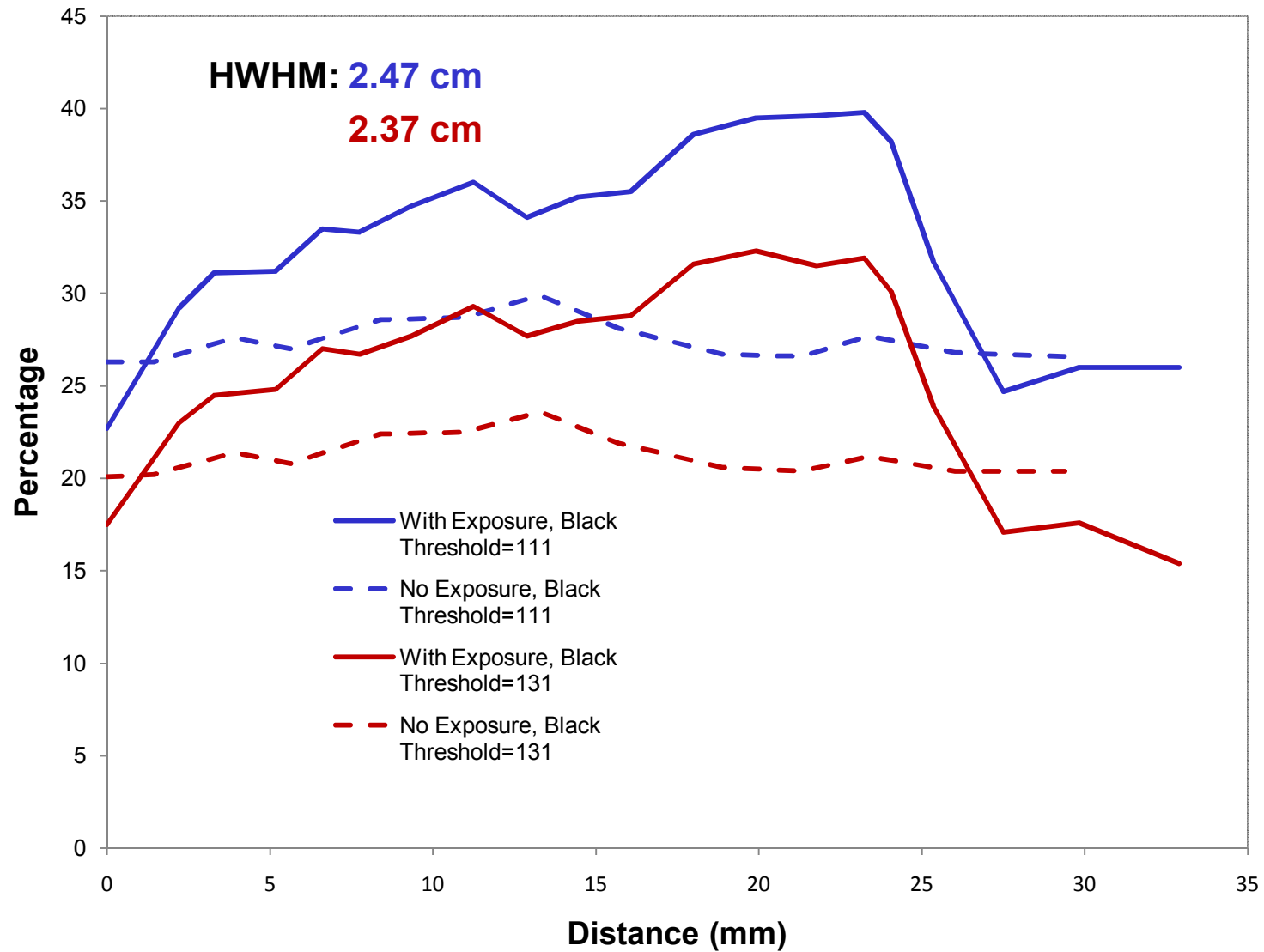
1. Start with full-color images
2. Convert to grayscale
3. Set black threshold (131 or 111) to convert to B&W
4. As a function of position, measure:
  - Fraction of black area
  - Number of “particles”
  - Average size of “particle”



# Average Size of Particle per Image

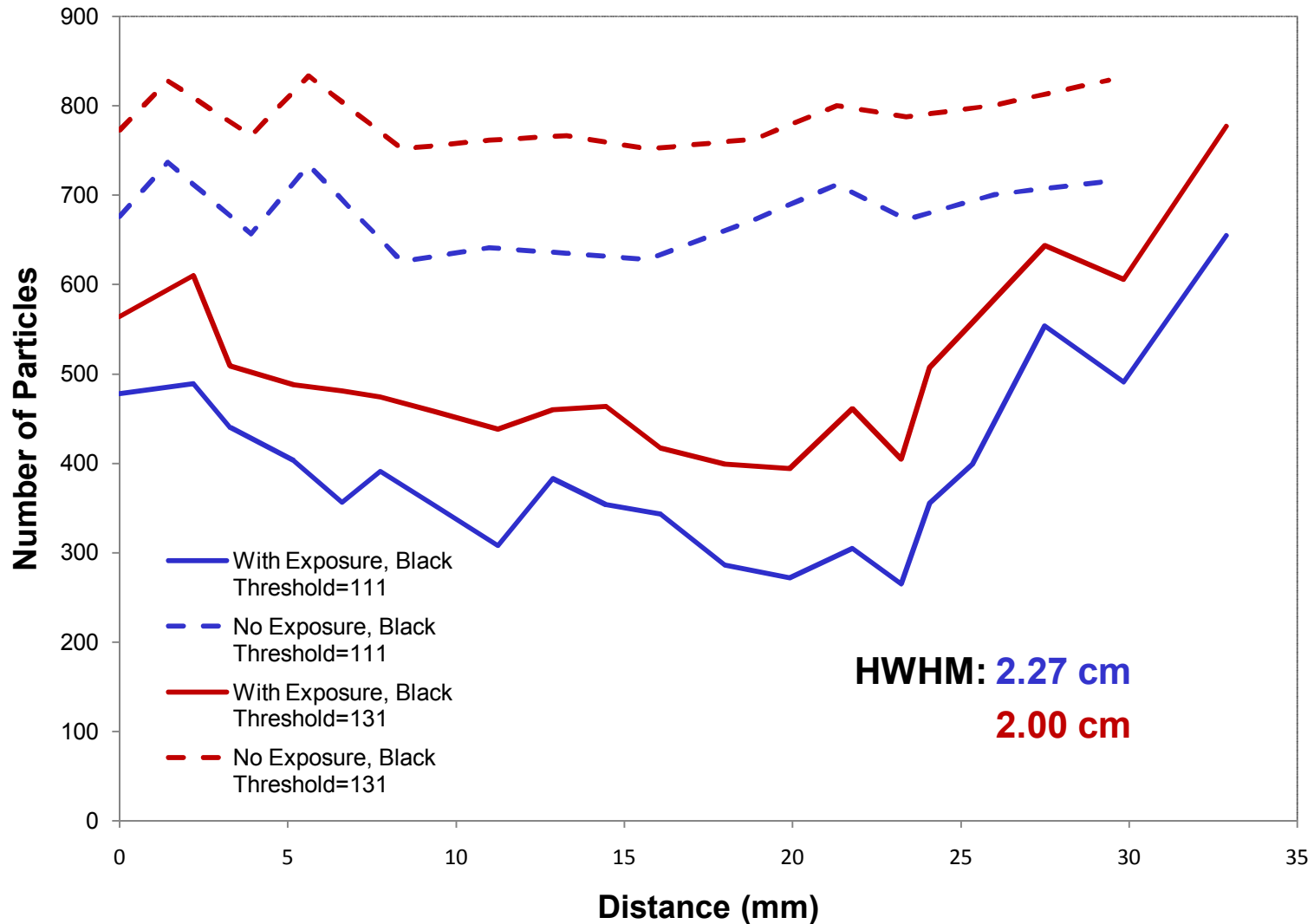


# Percentage of Black Area per Image





# Number of Particles per Image



## Discussion

- Heat flux confirmed to be on the order of strike-point fluxes
  - $\sim 1.5 \text{ MW/m}^2$  on sample,  $3 \text{ MW/m}^2$  for NSTX shot analyzed (139402)
- Outstanding issues:
  - Unknown error introduced by IR calibration
  - Arbitrary temperature offset in analytic heat flux determination
    - Needed correction to  $k_{Mo}$  would be a factor of  $\sim 20$
  - Finite “stroke time” results in non-uniform heat flux
    - Frame-by-frame “time weighting” introduces additional error

## Future Work

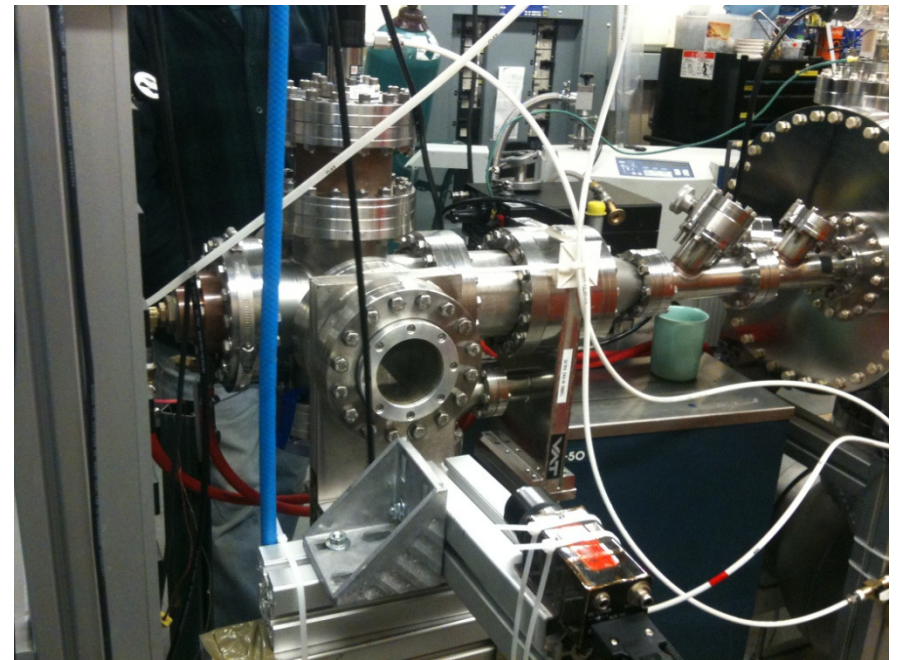
- Additional beam exposure tests:
  - Li-coated LLD sample
    - Strip heaters attached to sample
      - Enables in-situ (vacuum) calibration
      - Explore both solid & liquid Li regimes
    - Pneumatic feed-thru provides faster stroke time
      - Temporally uniform heat flux
      - MSE group also exploring “pulsed mode” beam operation
    - Longer pulse length
      - Test to failure!
  - Carbon sample (bare, Li-coated)
- 3-D Thermal Modeling (M. Jaworski)
- Possible collaboration with UIUC on surface modification by sputtering (VFTRIM)

## Tests with Li-Coated LLD Sample are Imminent

- Li has been loaded on to a new LLD sample that has not been exposed to the DNB



*New LLD sample coated with a fresh layer of Li*



*New experimental setup has been completed and Li sample will be installed as soon as next week*

## Summary/Conclusions

1. Will the LLD melt or suffer significant erosion?
  - No obvious macroscopic erosion or melting
  - Microscopic damage matches beam profile
    - HWHMs show sub-linear damage scaling with heat flux
    - Suggests “peaks” on LLD sample are eroded due to bombardment
2. How is thermal conductivity affected by the porosity?
  - Large correction needed (~20) suggests poor thermal contact between Mo and SS
  - Possible subject for future offline experiments
3. What are the Li erosion/sputtering yields? Does Li protect the Mo?
  - To be determined through further exposure tests.



# Acknowledgements

- Equipment:
  - Nova Photonics (E. Foley, F. Levinton) for use of DNB
  - Oak Ridge (T. Gray, R. Maingi) for use of IR camera
  - C. Skinner for use of optical microscope
  - LTX for various flanges and feed-throughs
- M. Jaworski, J. Kallman, R. Kaita (advisor) and the rest of the LLD team for constant advice/feedback
- Supported by US DOE contracts DE-AC02-09CH11466 and DE-FG02-01ER54616, and partially performed under appointment to the Fusion Energy Sciences Fellowship Program administered by Oak Ridge Institute for Science and Education.