

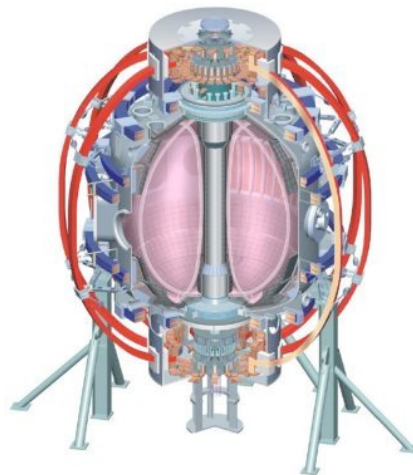
# Control Development for NSTX and the Effects of Strong Shaping

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**EGEMEN KOLEMEN, PPPL**

*D.A. GATES, S. P. GERHARDT, D.A. HUMPHREYS, D. MUELLER, V. SOUKHANOVSKII, M.L. WALKER*

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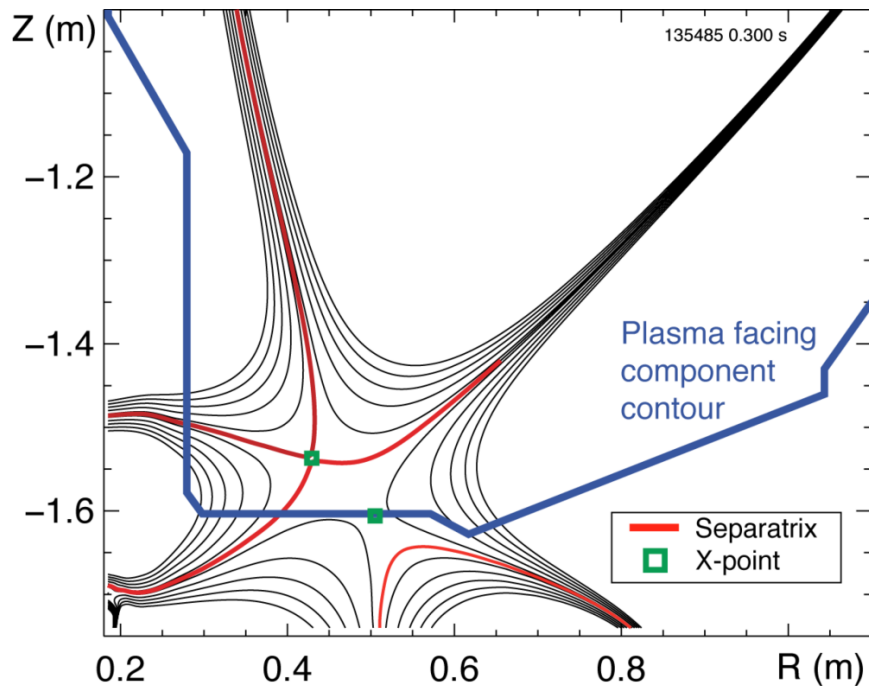


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## Summary

- Real-time snowflake divertor configuration tracking
- Development of snowflake control
- Independent control of squareness ( $\zeta$ )
- Effect of  $\zeta$  on performance
- Effect of  $\zeta$  on stability

# Snow Flake Divertor

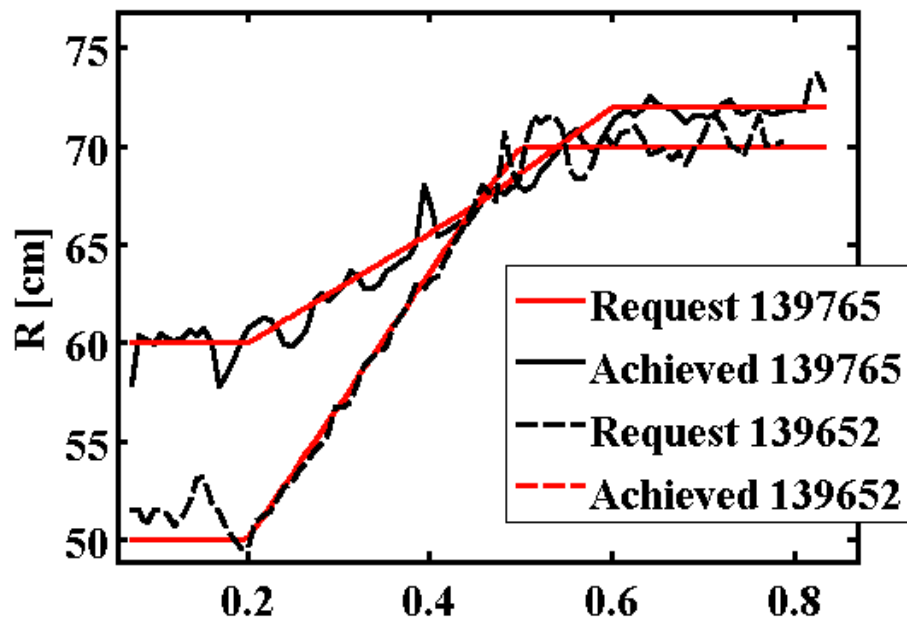


- “Snowflake” divertor configuration, a second-order null is created in the divertor region by placing two X-points in close proximity to each other.
- This configuration has higher divertor flux expansion and different edge turbulence and magnetic shear properties, beneficial for divertor heat flux reduction, and possible “control” of turbulence and ELMs.
- Implemented and used inner/outer strike point control to test the “snowflake” configuration.

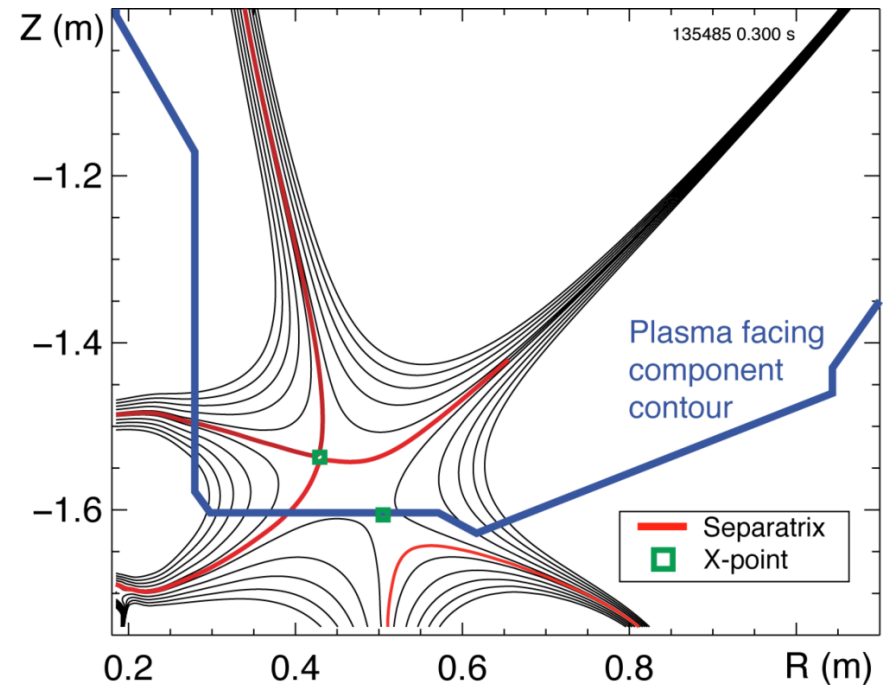
*Example "snowflake" divertor configuration in NSTX.*

## Combined Upper/Lower-Inner/Outer Strike Point (SP) Control

- PID control for U/L-I/O SP to enable “snowflake”, LLD operation
- 8 PF coils in Single-input-single-output control (Outer gap, vertical position and 4 SP are controlled).



Example SP control



Snowflake high-flux expansion divertor obtained via SP control at NSTX

## Snowflake Control: Finding the 2<sup>nd</sup> X-point

- Locate snowflake centroid & 2<sup>nd</sup> X-point
- Locally expand of the Grad-Shafranov equation in toroidal coordinates:

$$(R + x) \frac{\partial}{\partial x} \left( \frac{1}{R + x} \frac{\partial \Psi}{\partial x} \right) + \frac{\partial^2 \Psi}{\partial z^2} = 0$$

- Keep the 3<sup>rd</sup> order terms and find the magnetic nulls

$$\Psi_{00} = \Psi_f - \Psi(\rho_f, \xi_f)$$

$$= \Psi_f - \left[ l_2 \xi_f + q_3 \xi_f^2 + c_4 \xi_f^3 + l_1 \rho_f + 2q_2 \rho_f \xi_f \right. \\ \left. + (-3c_1 - q_3) \rho_f \xi_f^2 + \frac{1}{2} (1_1 - 2q_3) \rho_f^2 + (-3c_4 + q_2) \rho_f^2 \xi_f + c_1 \rho_f^3 \right]$$

$$\Psi_1 = \Psi(\rho_1, \xi_1) + \Psi_{00}$$

$$\Psi_2 = \Psi(\rho_2, \xi_2) + \Psi_{00}$$

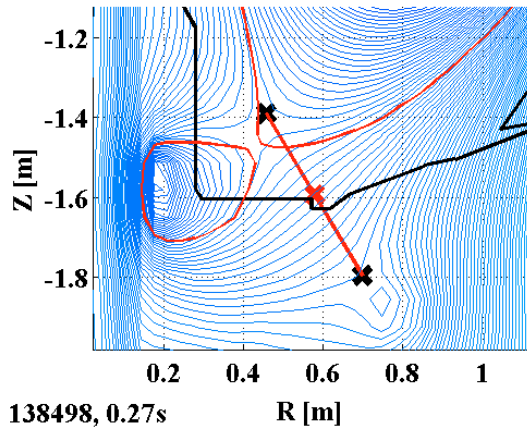
- Find coefficients from sample points
- No iteration, one step fast algorithm with reasonable accuracy.

Ref. M.A. Makowski & D. Ryutov, "X-Point Tracking Algorithm for the Snowflake Divertor"

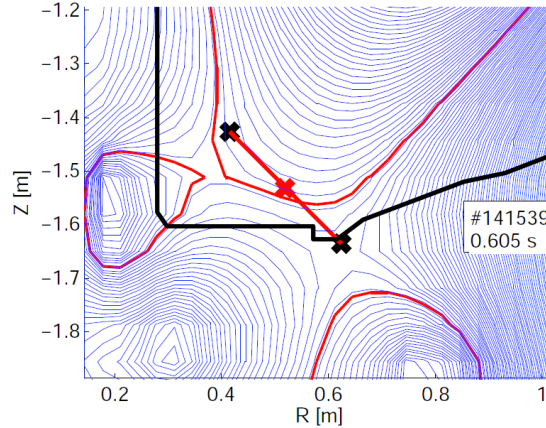
M.V. Umansky et al.. "Analysis of geometric variations in high-power tokamak divertors." LLNL-JRNL-410565.

# Tracking Works for Snowflake -/+ and Non-Snowflake

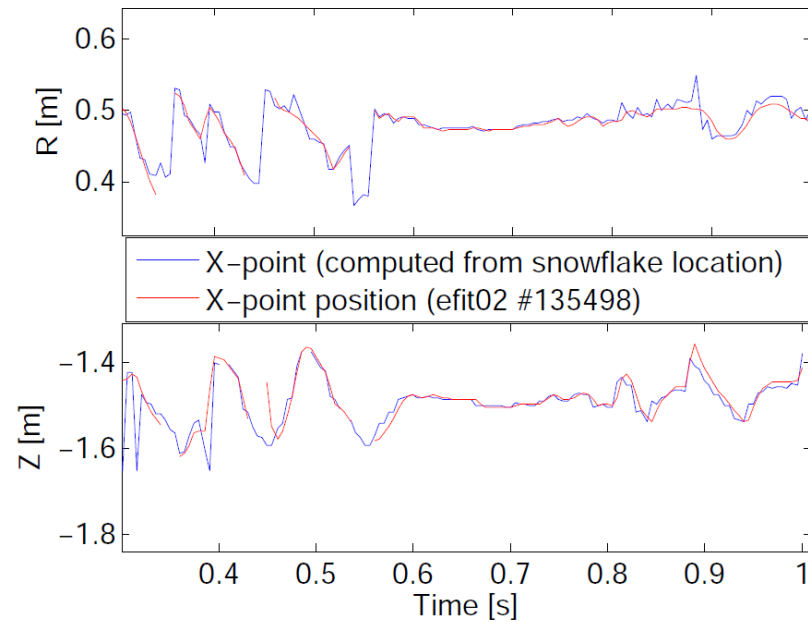
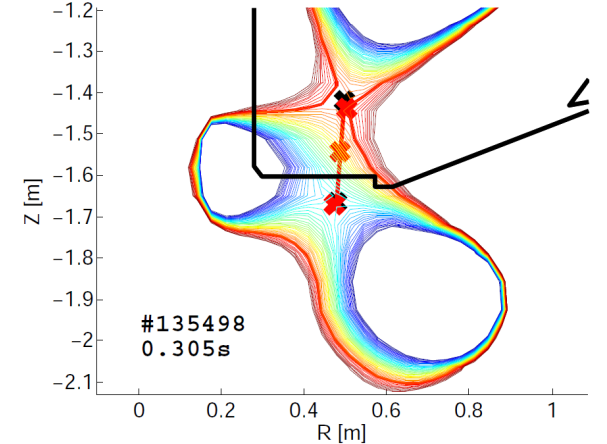
**Snowflake tracking & extrapolated X-points**



**Snowflake tracking and the extrapolated X-point locations**



**Snowflake tracking: Centroid, Calculated and Efit02 X-points**



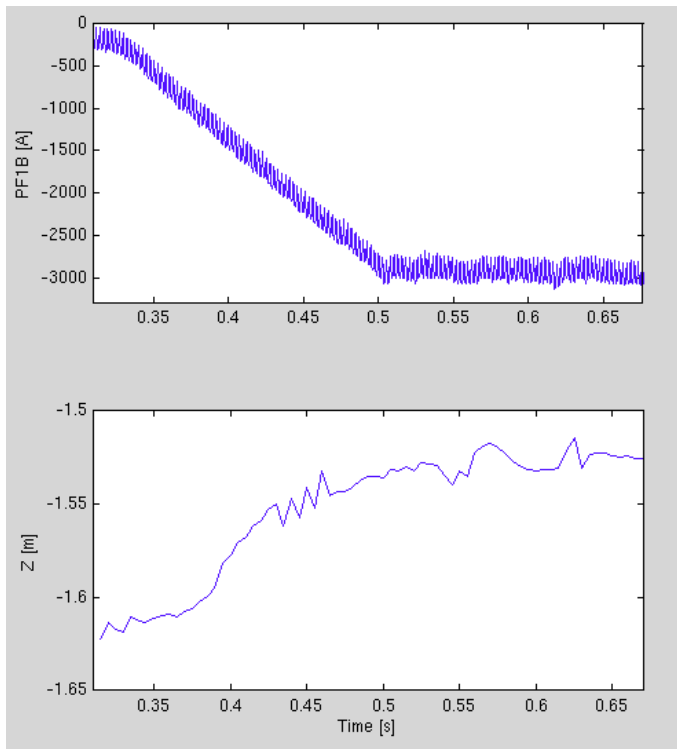
**Above: Snowflake tracking for NSTX:**

**1.Red cross is the tracked snowflake centroid**

**2.Black crosses are the calculated X-points locations by the snowflake tracking algorithm**

**Left: X-point position computed from the radius and angle obtained from the snowflake tracking and position of the 2<sup>nd</sup> X-point.**

## Actuators to Control 2<sup>nd</sup> X-point



**Example: Effect of PF1B on 2<sup>nd</sup> X-point Height**

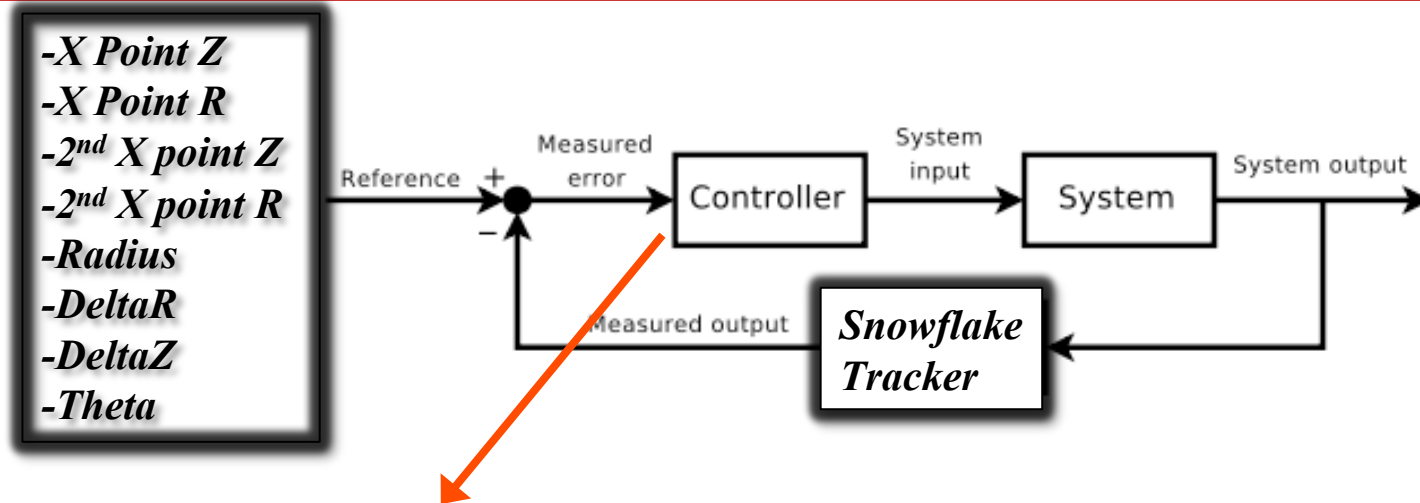
- Control both the location of the X-points with PF coils.
  - Need 4 independent actuators for full control
  - Optimal use of the capability we have 3 PF coils (PF1AL, PF2L and PF1B)
  - Control the best combination of properties of interest (Relative distance/angle between the X-points)
- After lower snowflake divertor, extend this algorithm to control the upper snowflake configuration as well.

# Snowflake Control

- Locations of the X-points → feedback-control
- The aim of the control:
  - Primary aim is the distance between the two X-points.
  - Secondary aim relative angle between the X-points.
- Actuator: PF1B as the primary controller, PF1A/2 secondary
  - PF1B is a very effective coil in moving the secondary X-point
  - Not used in any other control loop
  - MIMO using PF1A, PF1B and PF2L will be probably be obtain control objective.



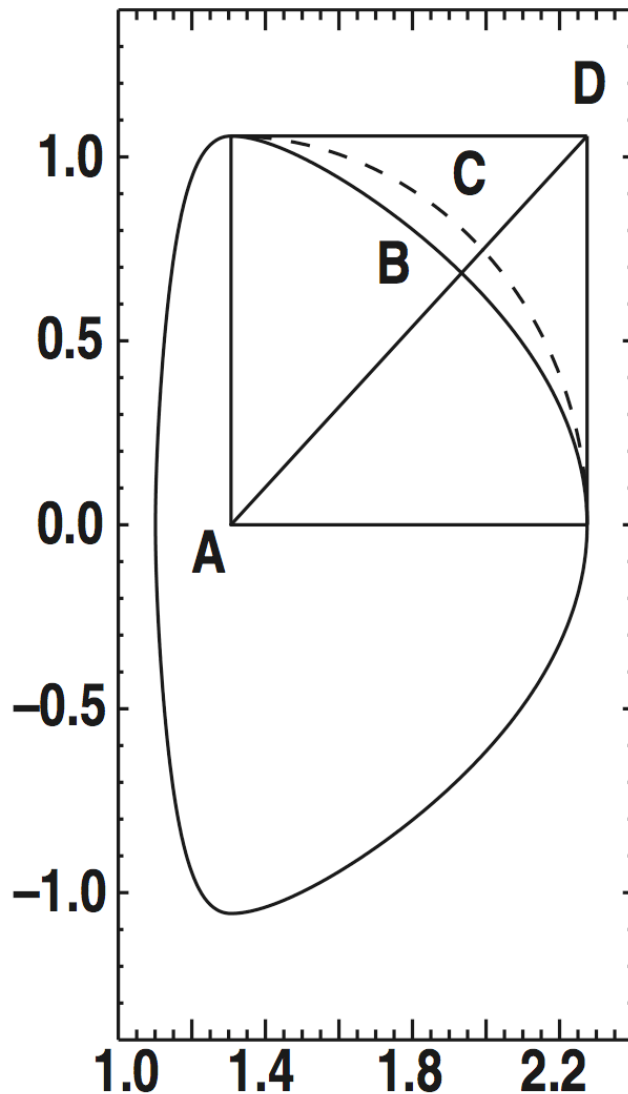
# Snowflake Control Algorithm



$$V_{PF} = X_{mat}PID(Err_{snow}) + M_{mat}PID(Err_{seg})$$

- For convenience leave all the possible references.
- Define X Matrix similar to the M matrix.
- For unused references set X row to zero.
- Add the segment PID and snowflake PID.

# What is Squareness, $\zeta$ ?



$$\zeta = \frac{AB-AC}{CD}$$

• Squareness is the second shape moment.



•  $\zeta = 1.0 \rightarrow$  rectangular plasma



•  $\zeta = 0.0 \rightarrow$  circular plasma



# Motivation and Study of $\zeta$

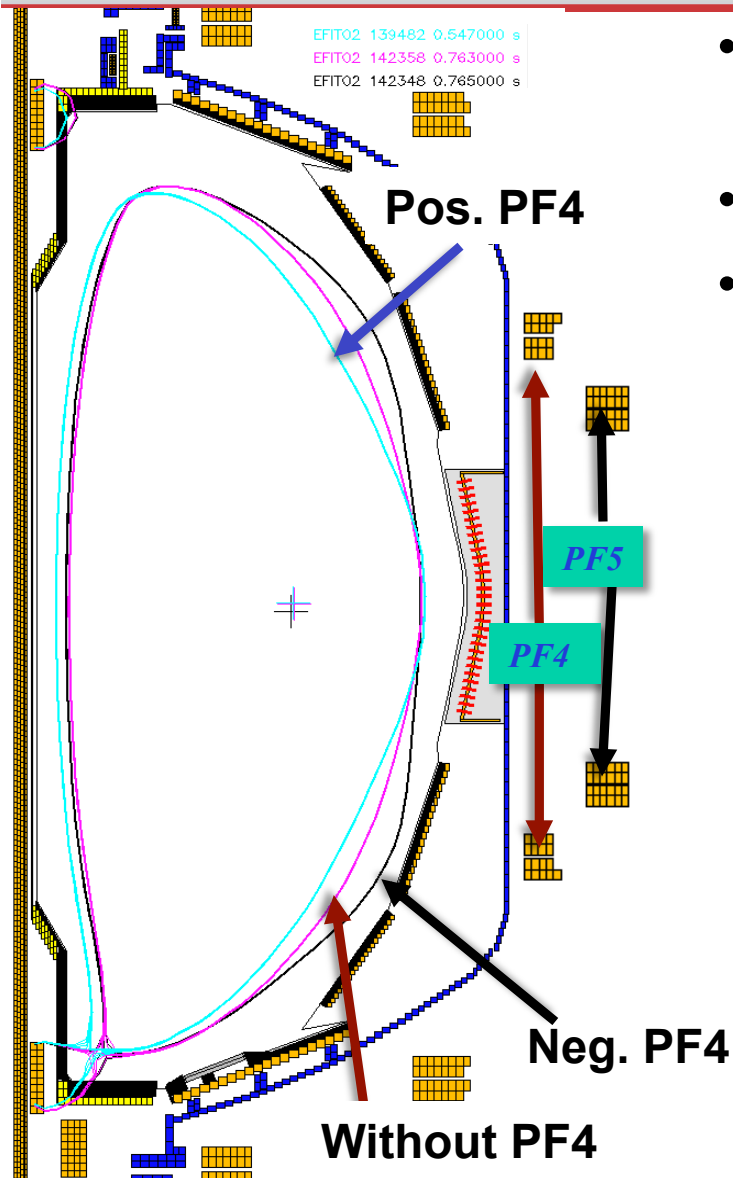
## Motivation:

- STs all operate at high  $\kappa$  in order to maximize the bootstrap fraction and  $q^*$ . In addition, the location of the outer strike point must often be fixed for effective divertor operation. As a result, neither the plasma  $\kappa$  nor the  $\delta$  can be modified greatly. An additional shape parameter that can help optimize plasma stability is  $\zeta$ .

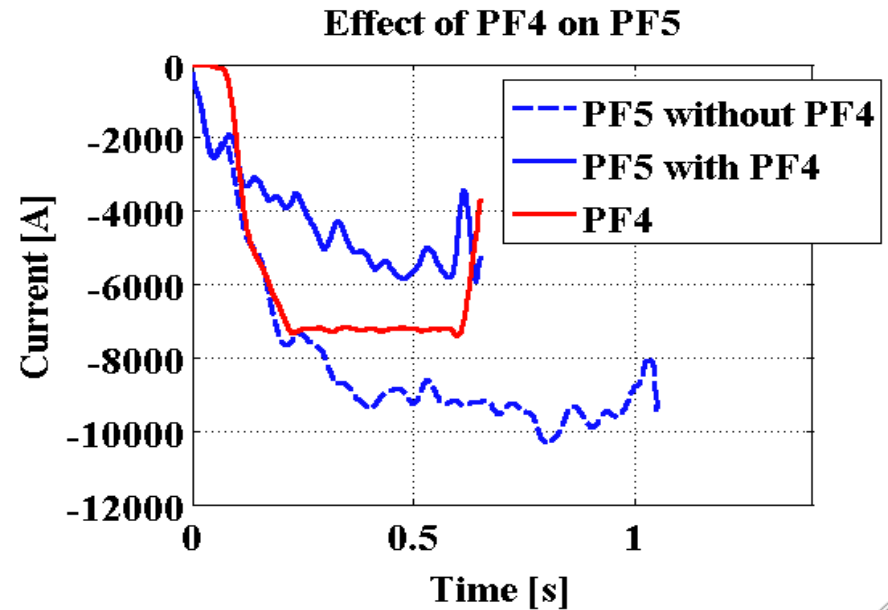
## Summary:

1. Can  $\zeta$  be varied without effecting the other important parameters?
2. Independent control of  $\zeta$
3. Study of the effect of  $\zeta$  on performance
4. Study of the effect of  $\zeta$  on stability

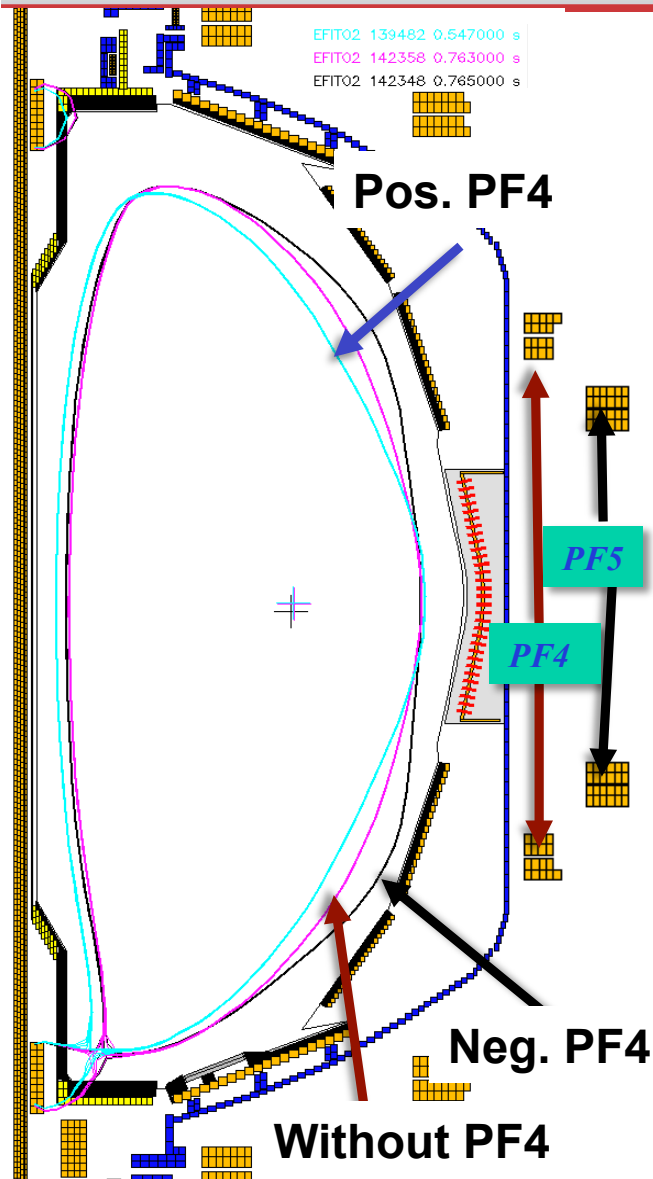
# PF4 can change $\zeta$ with minimal side effect



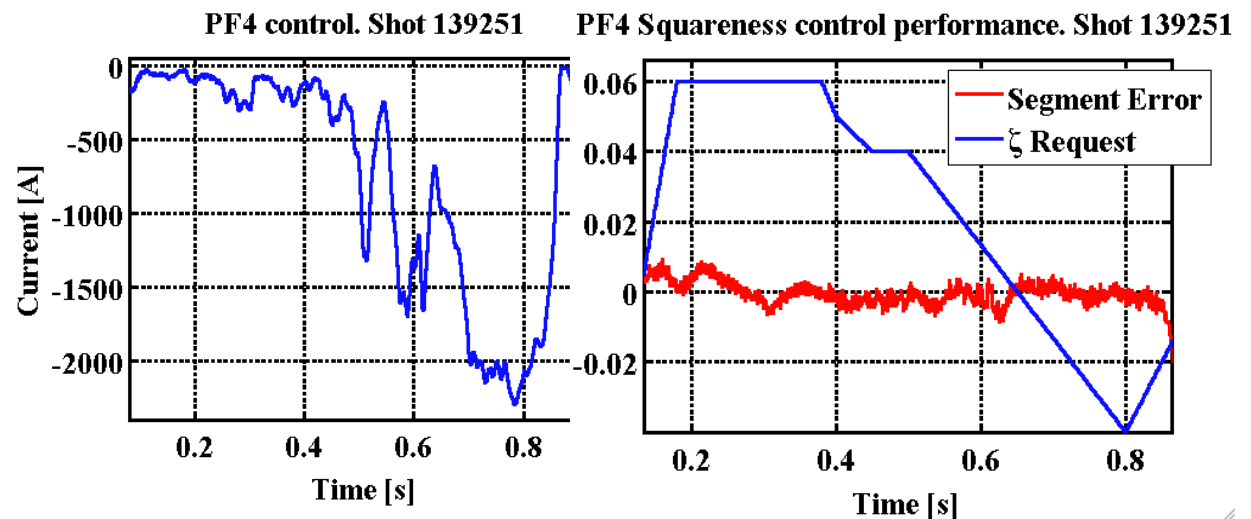
- Preprogram PF4 with PF5 for outer gap control
- Squareness varies with PF4.
- Keep other things the same.



## $\zeta$ Control with PF4

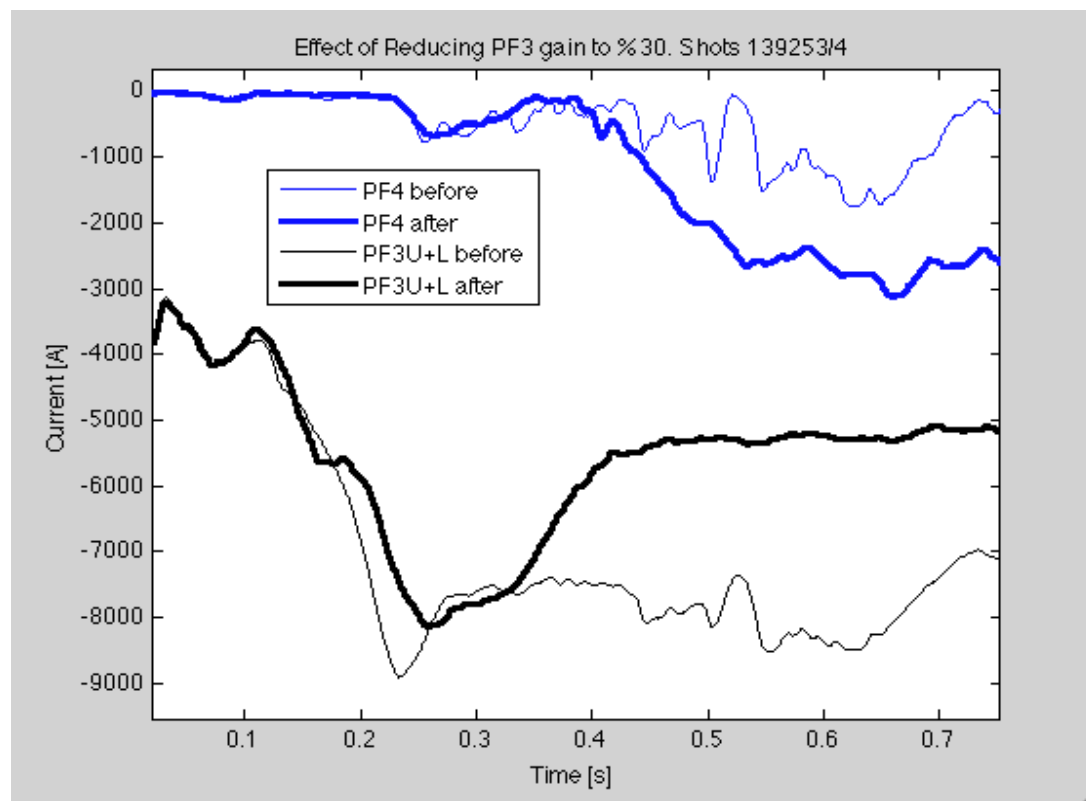


- Motivation: Assess the physics impact of squareness variation while other shape parameters are fixed.
- PF4 best  $\zeta$  control candidate. PF3/PF4 effect  $\zeta$  but PF3 used for vertical stability.
- Achieved stable  $\zeta$  tracking via PF4.
- Effect of  $\zeta$  on plasma is being studied.

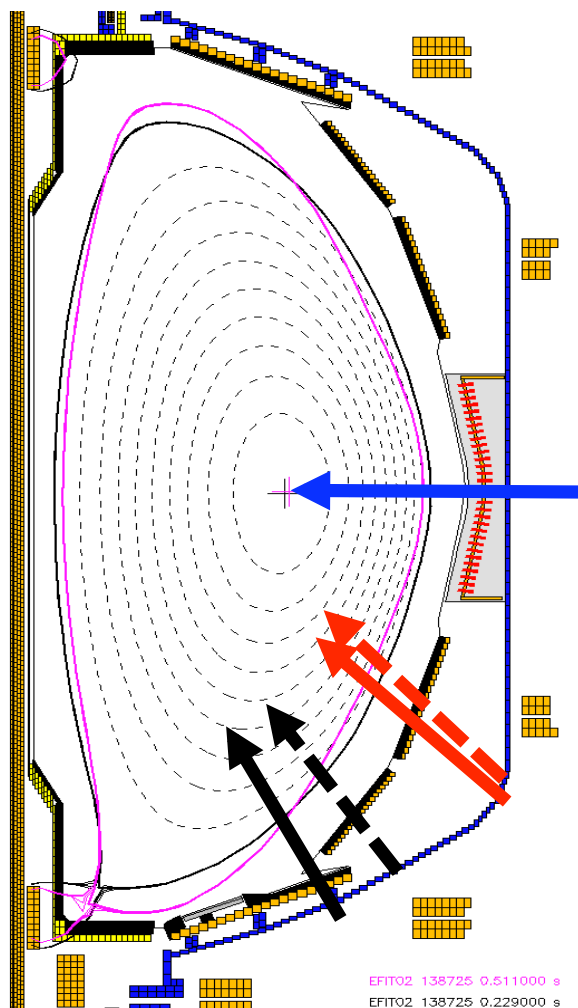


## Control Results: PF3-PF4 interaction

- With PF4 control on, we reduced the gain for PF3 %30 at 360 ms.
- PF4 compensated for the loss of inward pushing effect of PF3.
  - PF4 can offset both PF3 and PF5.

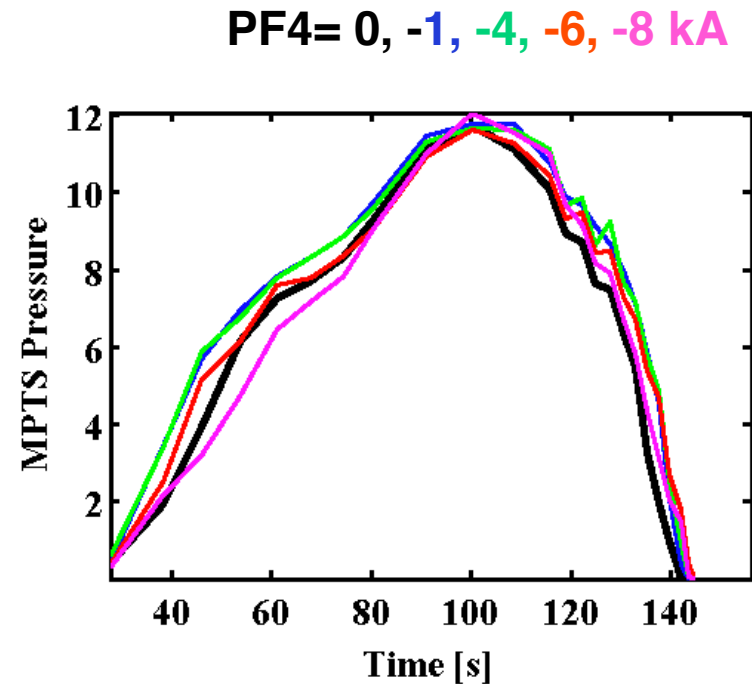
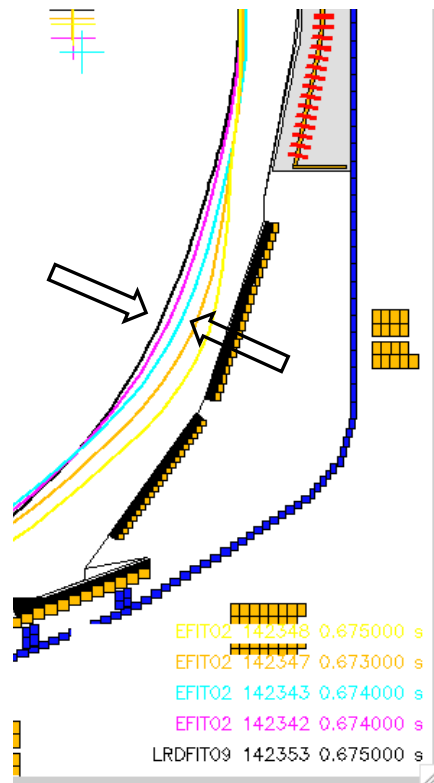


## Control Results: PF3-PF4 interaction



- Figure show the result of a ramp on PF4 from 0 to 2.6 kA.
- As PF4 increases, squareness change.
- In order to align, PF3/4/5 control points (shown in dashed black, dashed red and blue) X-point moves down.
- To solve this problem, move the PF3 and PF4 control segment. Shown in solid red, black.

# Performance: Pressure Profile Change as $\zeta$ Increases

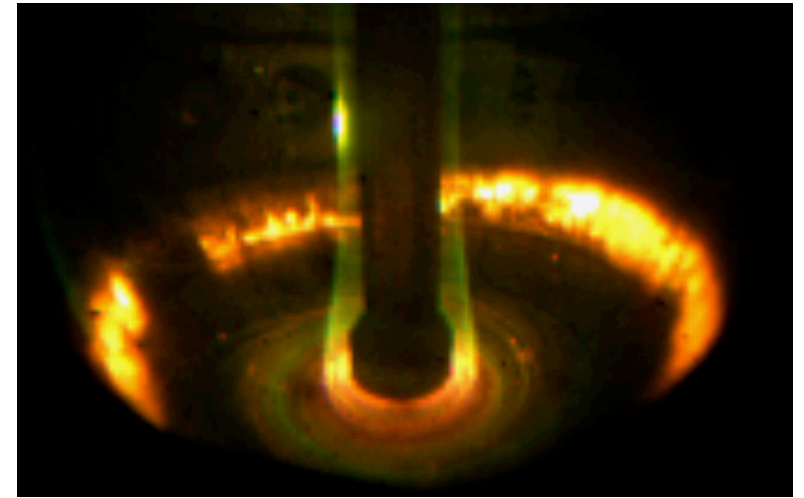
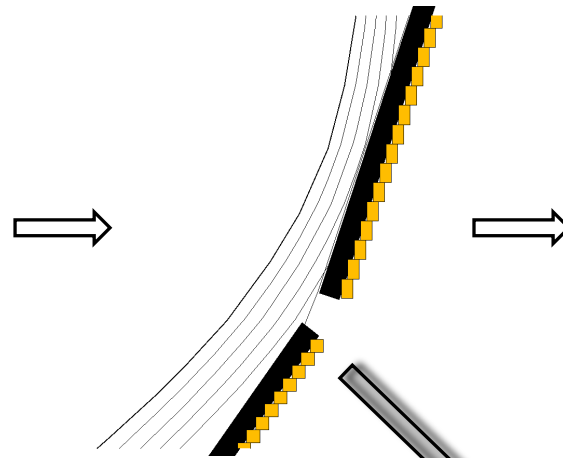
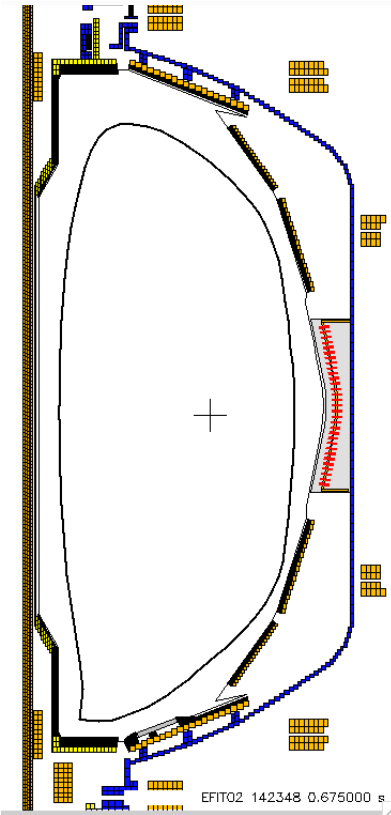


PF4 (opposing PF5) up to -5 kA (~2 inches in figure) increases pressure

Too high squareness interacts with the wall. Pressure drops.

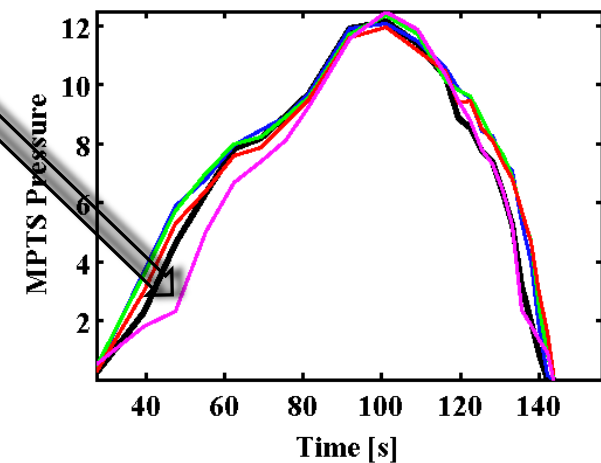


## Performance: High $\zeta$ Wall Interaction

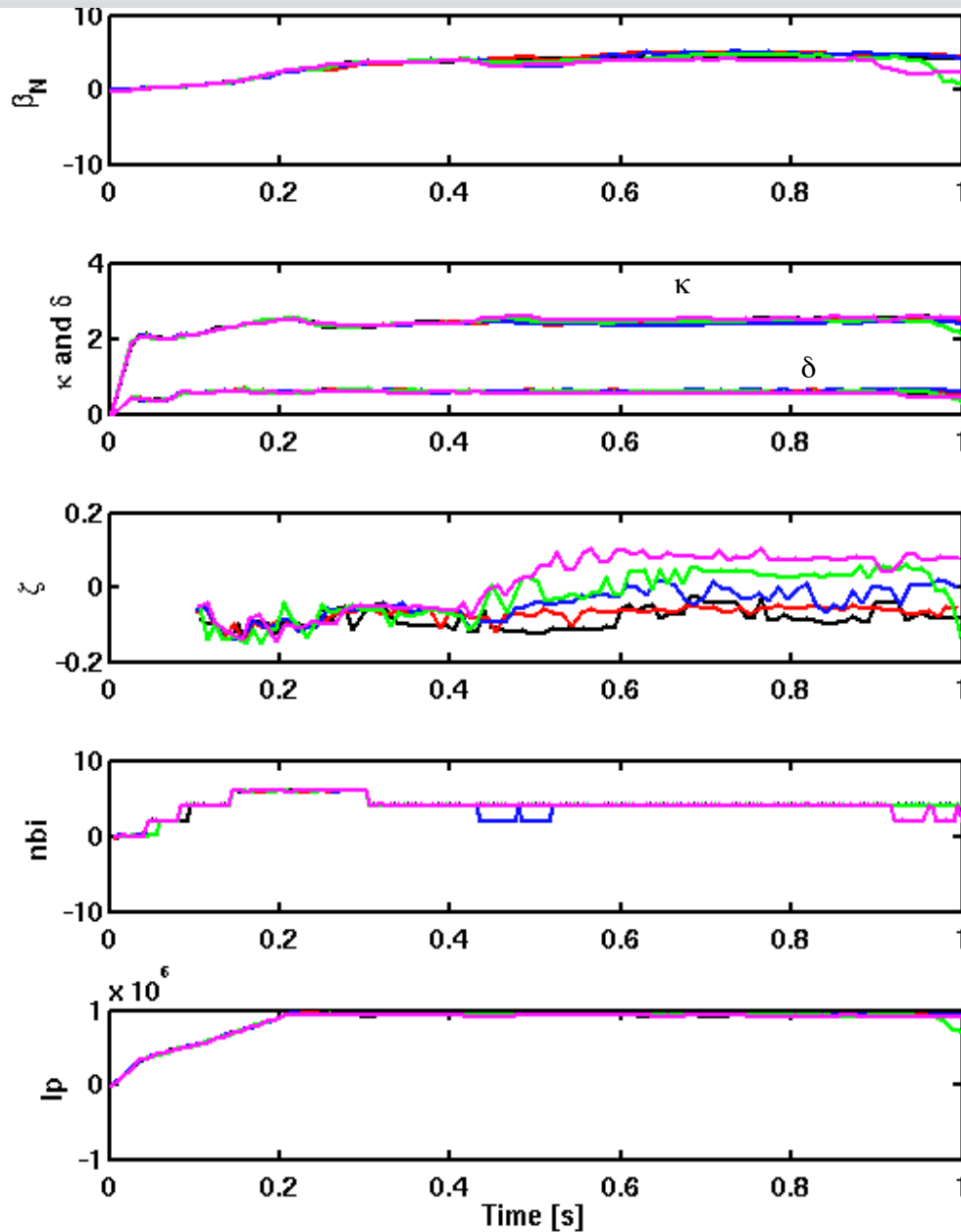


As PF4 gets close to -8 kA:  
Last closed flux surface gets 3-4 cm  
close to the wall.  
Pressure profile degrades

PF4= 0, -1, -4, -6, -8 kA

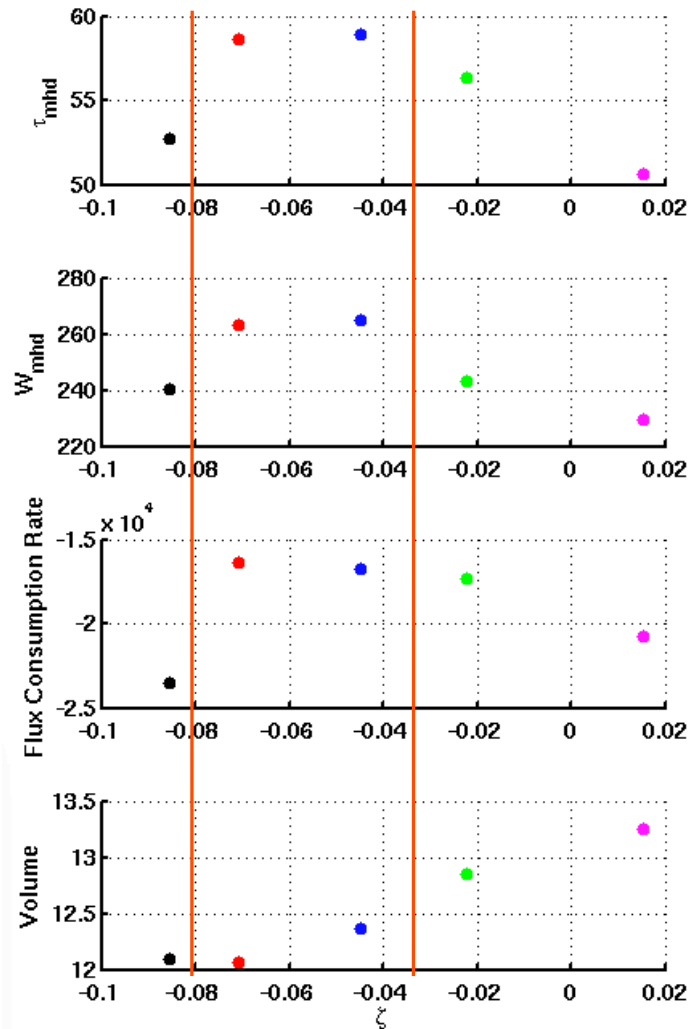


## Optimal Squareness for Performance



- Squareness scan
- IPF4: 0 to -8 kA
- Keep  $I_p$ , NBI,  $\beta_N$ ,  $\kappa$ ,  $\delta$  constant
- To compare the effect of  $\zeta$ , we average the results when the plasma is stable
- 600-900 ms average

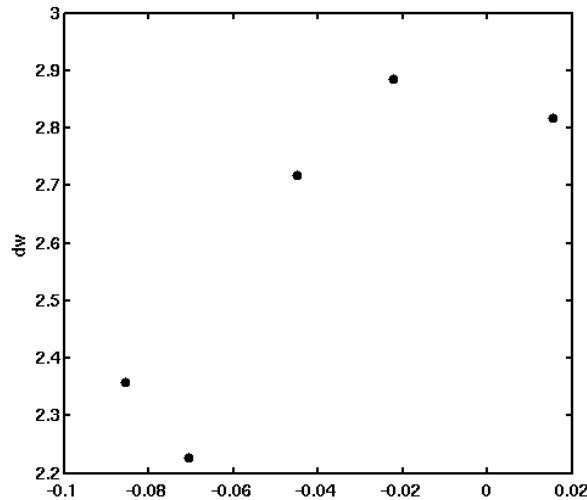
# Optimal Squareness for Performance



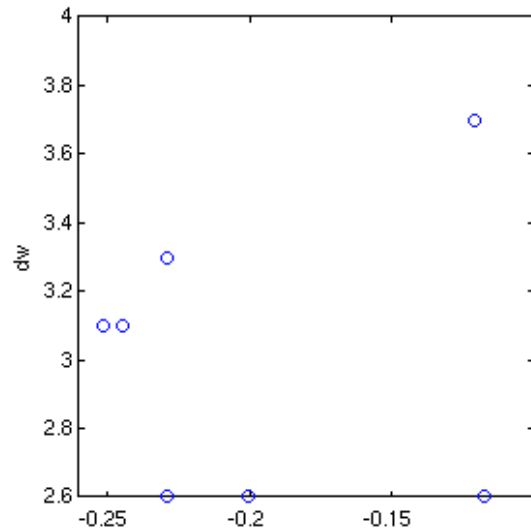
Averaged over 600ms to 900ms.  
[142353,142342,142343,142347,142348]

- Optimal  $\zeta \sim -0.06$
- Optimal PF4  $\sim -1$  to  $-3$  kA for performance.
- Confinement time increases
- Energy confinement increases
- Flux consumption reduces.
- Too high  $\zeta$  interacts with the wall and plasma is not as good.
- **Note for comparison:**
- $\zeta$  less than the fiducial (PF4=0) results are worse than the fiducial case.

## Stability Analysis: n=1 Stability



*Effect of squareness on n=1 stability between shots with same condition*



*Effect of  $\zeta$  on n=1 stability within 140689*

- We used DCON to look at the effect of squareness on vertical stability.
- The analysis did not show consistent correlation with squareness variation and n=1 stability.
- Neither when the squareness is ramped within a shot (140689) or under same conditions in different shots.
- Better LRDFIT reconstructions are needed to study the stability.
- Further analysis continuing.

## Stability Analysis: Vertical Stability

- We used Toksys to look at the effect of squareness on vertical stability.
- There seems to be no correlation with squareness and vertical stability.
- Further analysis will be conducted.

## Summary

- An effective real-time snowflake divertor configuration tracking is implemented at NSTX. Snowflake control algorithm based on the snowflake tracking is developed.
- An independent squareness control is on NSTX.
- As squareness increases, the pressure profile broadens and plasma performances increase. Then, performance degrades as further increase in squareness and finally starts interacting with the wall.
- The correlation between squareness and vertical and  $n=1$  stability is weak. We were not able to find clear correlations.
- Further analysis is needed to clarify the effects of squareness on stability but we expect the effects to be small.