



Quiescence of Magnetic Braking and Non-resonant Field Control in KSTAR

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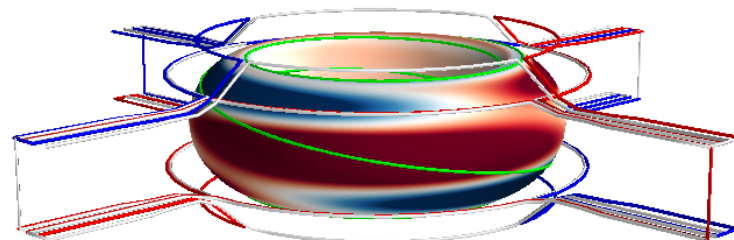
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Motivation to quiescent magnetic braking

- 3D field in tokamaks can provide various utilities depending on field spectrum
- Resonant vs. Non-resonant Magnetic Perturbation (RMP vs. NRMP)
 - RMP can control ELMs by particle and heat transport
 - NRMP can modify rotation by momentum transport (NTV or magnetic braking)
- Reality is mixture, due to limited coils
 - Many poloidal modes, strongly coupled
- Excluding one for the other is important
 - To minimize unwanted effects
 - To isolate and understand mechanism
- Quiescent magnetic braking – NRMP applications without RMP effects, to control local rotation/shear without disturbing particle or heat transport channel

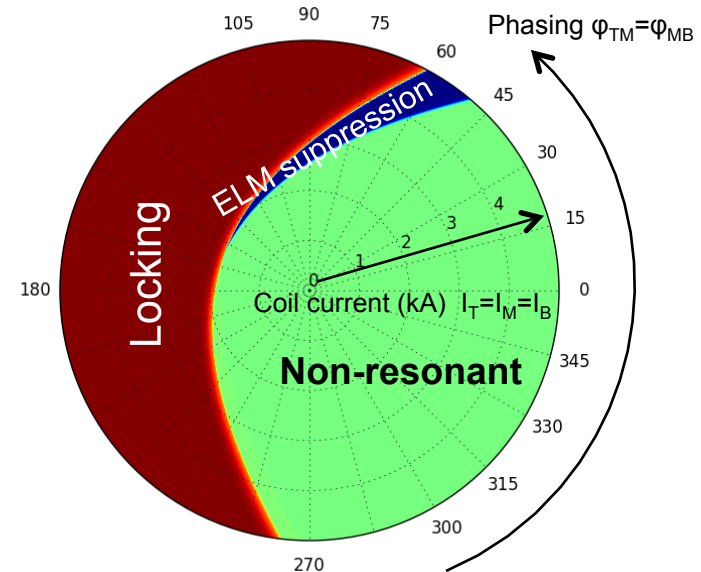


KSTAR IVCC -90p to #15433.08000

KSTAR provides great opportunity to nail down resonant effects in magnetic braking

- KSTAR IVCC consists of 3 rows of internal coils like ITER: Top, Middle, Bottom coils
- Spectral diversity for $n=1$ is greater than any other devices, enabling $n=1$ RMP ELM control
 - In magic window of coil configuration space
 - By isolating edge resonant coupling from core
- NRMP is even more diversified, giving great chance to study remnant RMP effects

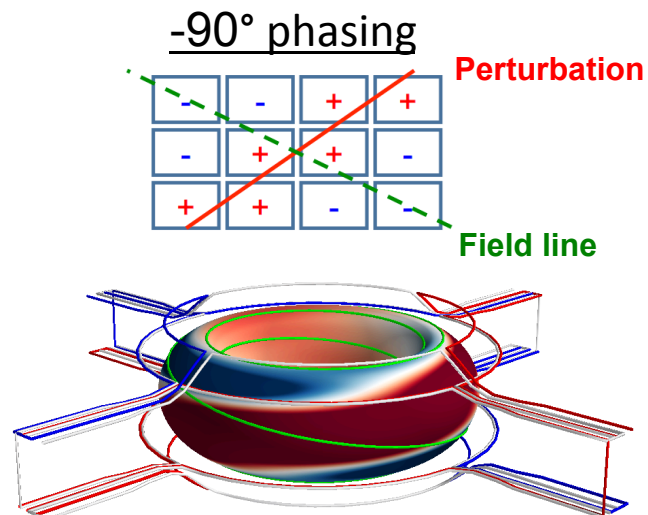
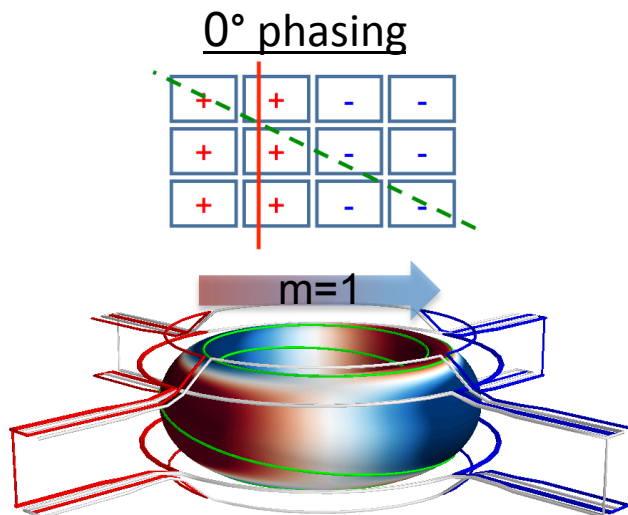
Primary effects induced by KSTAR $n=1$ vs. (I, ϕ) – subset of coil configuration



* This is $n=1$ study, but remnant RMP effects other than locking is also important for $n>1$

Geometrics for non-resonance

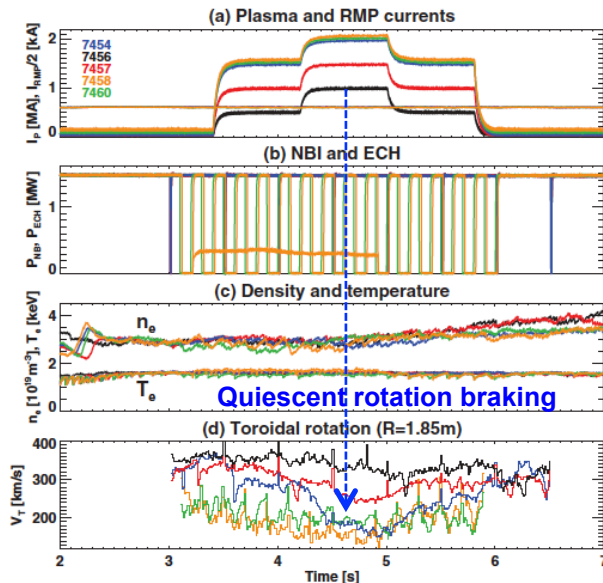
- Two most intuitive ways to generate non-resonant field:
 - Make long poloidal wavelength in perturbation : 0° phasing: $m=1$ dominant field
 - Place perturbation pattern across field lines : $-90^\circ(270^\circ)$ phasing: RMP-orthogonal field
 - * Phasing: Toroidal phase shift from top to middle (identically from middle to bottom)



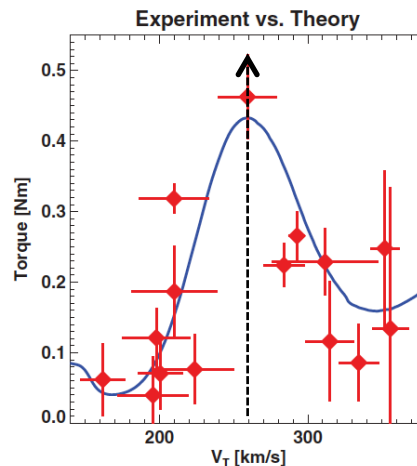
RMP-orthogonal field can be highly quiescent in magnetic braking as demonstrated in BH resonance studies

- RMP-orthogonal field (-90° phasing)
 - Unique in KSTAR as 3 rows of coils are needed
 - Successfully produced quiescent magnetic braking for low $q_{95} \approx 4$, weakly shaping ($\kappa \approx 1.4$)
 - Used to study 'pure' NTV effects and bounce-harmonic rotation resonance in NTV

J.-K. Park et al.,
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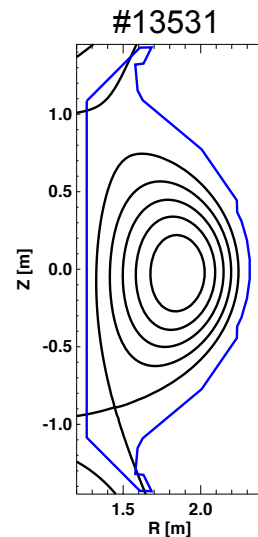
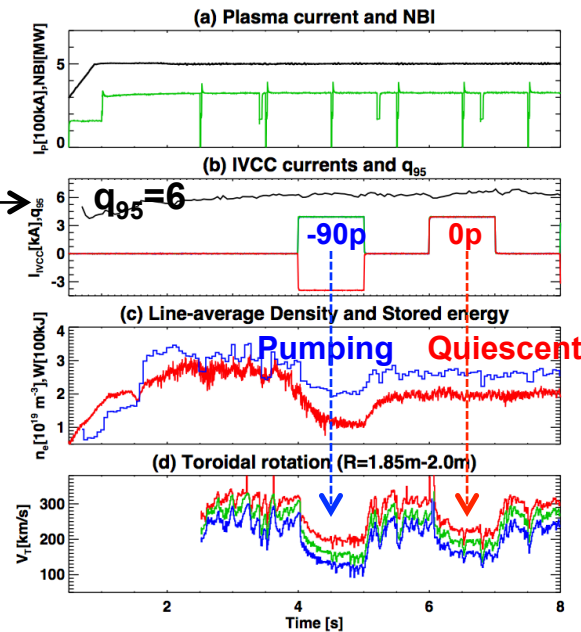
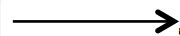
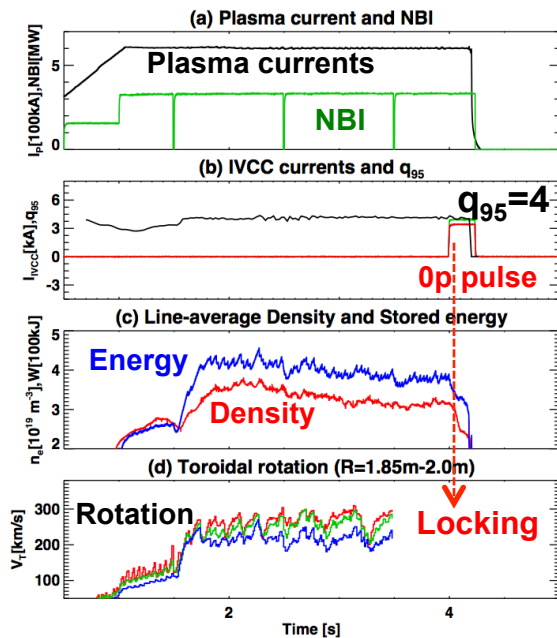
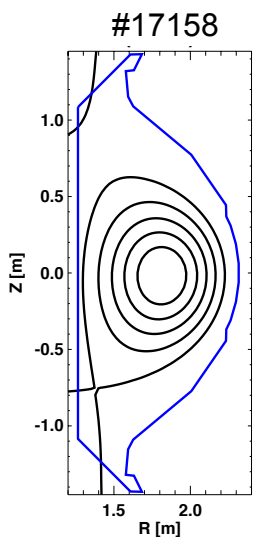


1st Bounce-Harmonic resonance Shown in both



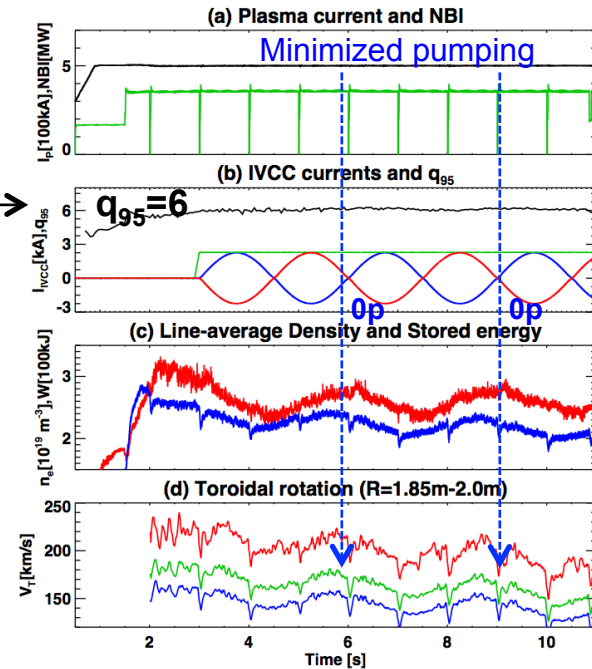
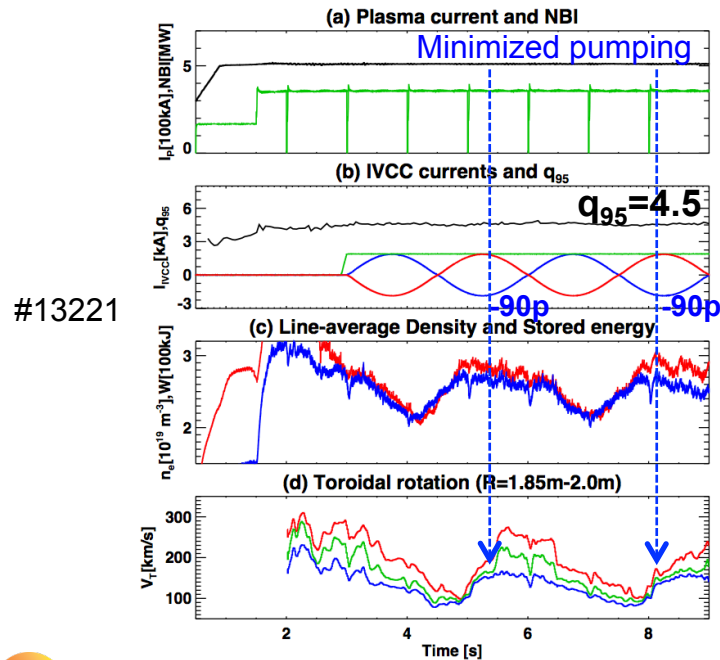
Further evidences show quiescence of magnetic braking requires fine matching between phasing and target

- Optimal phasing for quiescent braking varies sensitively (-90° vs. 0° issue)
 - -90° phasing $\rightarrow 0^\circ$ phasing when $q_{95}=4 \rightarrow 6$, and shaping becomes stronger



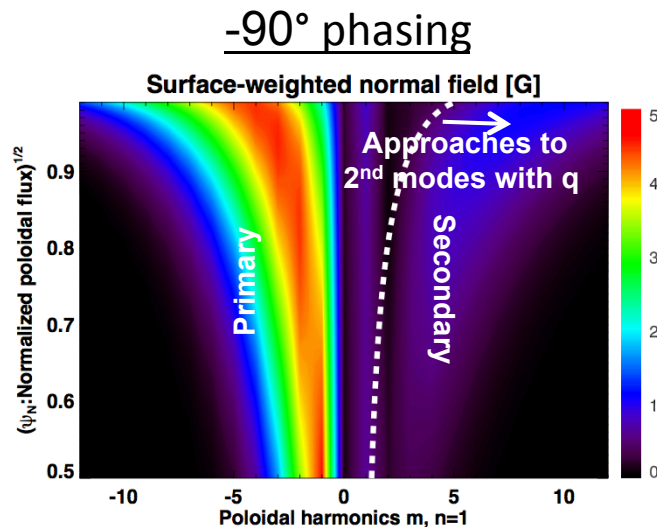
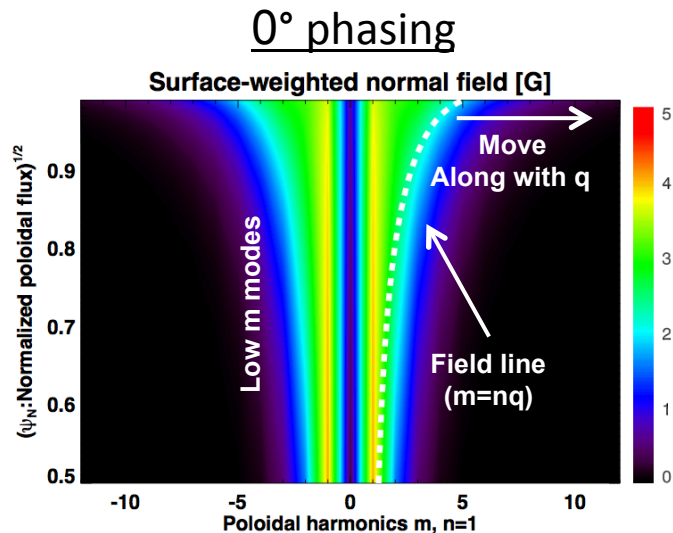
Similar trend found in continuous phasing scan

- Continuous phasing scan using 3 rows of coils also shows
 - -90° phasing $\rightarrow 0^\circ$ phasing when $q_{95}=4 \rightarrow 6$



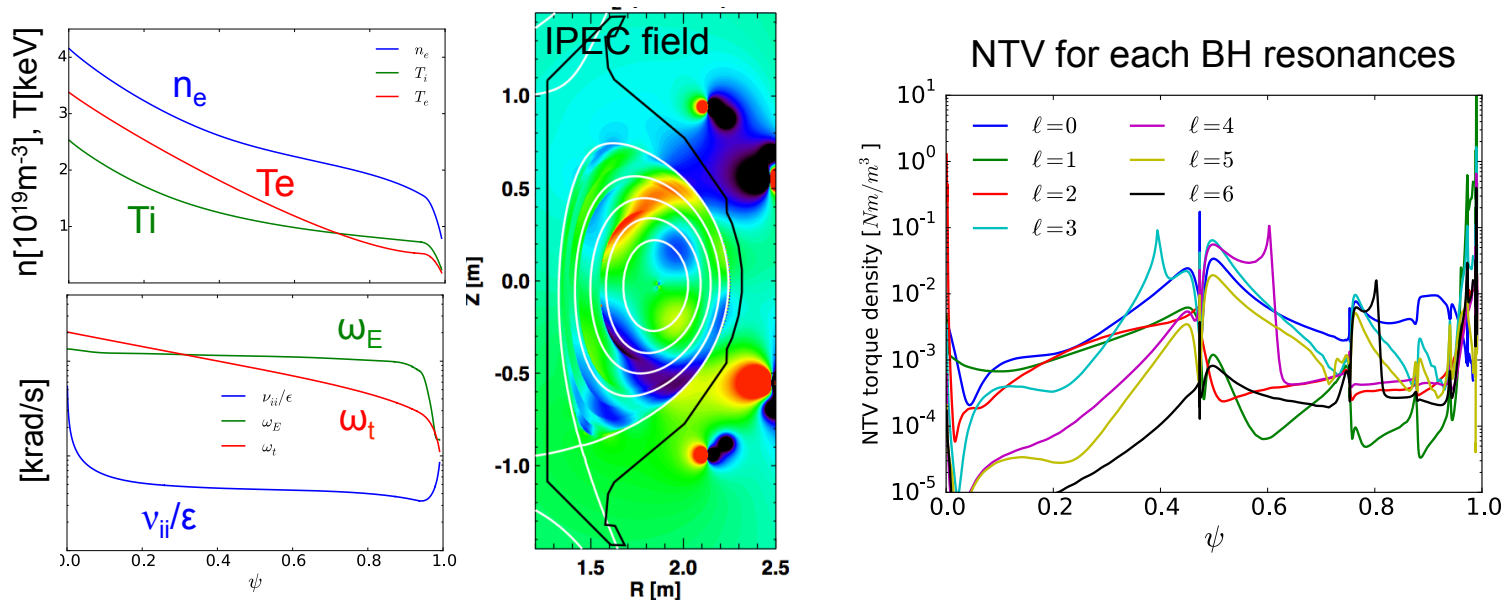
External kink coupling gives qualitative explanation, implying importance of small remnant RMP control for NRMP

- Resonant amplification is driven by well-known external kink coupling ($m > nq$)
- If q in the edge increases
 - Low m modes in 0° phasing move away from kink, becomes more non-resonant
 - $m < 0$ modes in -90° phasing also move away, but small secondary $m > 0$ modes approach



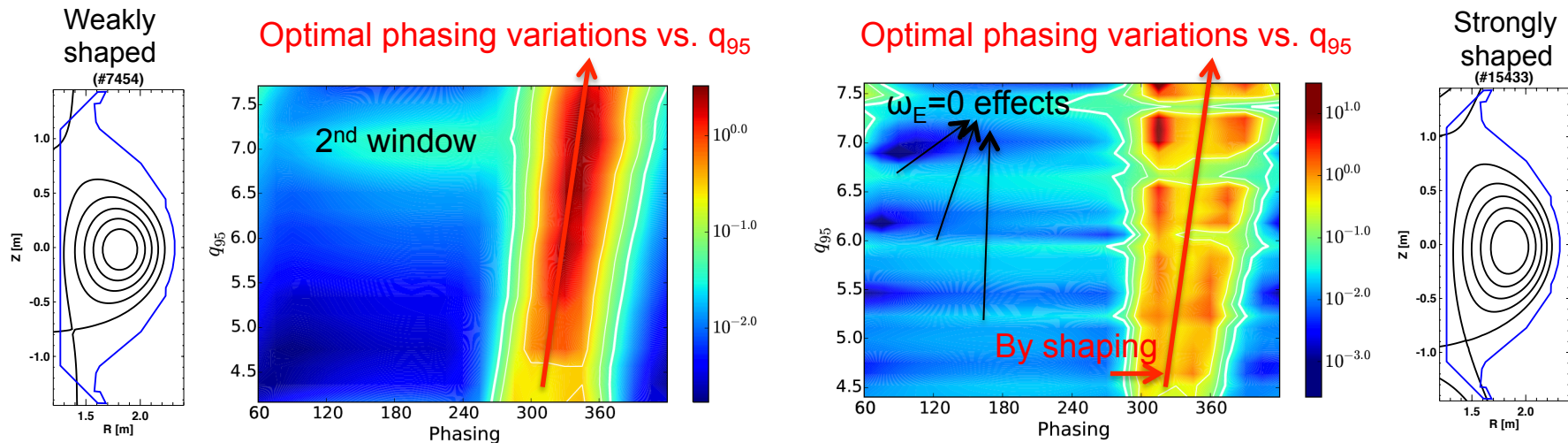
IPEC and PENTRC modeling used to evaluate resonant field and NTV, and figure of merit for quiescent NTV braking

- Figure-of-merit (FOM) for braking: Non-resonant vs. resonant torque $F_{QM} = \frac{T_{NTV}}{T_{j \times B}} \propto \frac{T_{NTV}}{\Sigma \delta B_{mn}^2}$
- IPEC-PENTRC is used for NTV simulation including bounce and transit resonant effects



Modeled F_{QM} shows optimal phasing variations for quiescent braking consistent with observations

- Optimal F_{QM} moves to higher phasing (e. g. $-90^\circ \rightarrow 0^\circ$) as q_{95} increases
- Optimal F_{QM} is also shifted to higher phasing when shaping increases
- F_{QM} model gives prediction consistent with observation
 - with new details, e.g. 2nd window for $q_{95} > 7.0$, variation due to $\omega_E = 0$ at q surfaces



F_{QM} modeled by IPEC-PENTRC

Experimental validation for F_{QM} towards non-resonant field control for quiescent magnetic braking

- Empirically F_{QM} is about momentum vs. particle/heat level changes at the saturation level

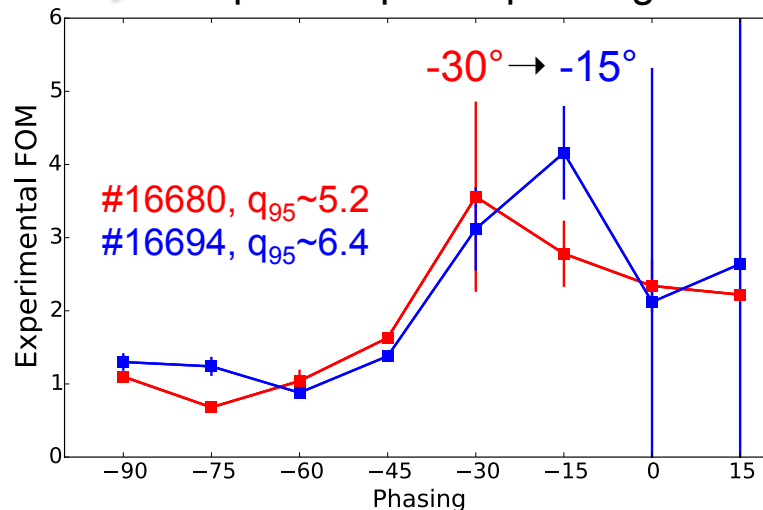
$$F_{QM}^{Exp} = \frac{\Delta(nV)/nV}{\Delta(\Sigma nT)/\Sigma nT}$$

→ Empirical optimal phasing

- Modeled F_{QM} is however based on torque at the onset, which will drive rotation and energy degradation non-linearly

$$F_{QM}^{Exp} = \frac{\Delta(nV)/nV}{\Delta(\Sigma nT)/\Sigma nT} = \alpha \left(F_{QM}^{Model} \right)^\beta ?$$

- Quantitative comparisons with fine tuning for non-resonant coil configurations are important for physics validation and prediction for F_{QM}



Summary and Conclusion

- Versatile 3-rows of coils in KSTAR provide various $n=1$ NRMPs with fine tuning capability on field spectrum
- Optimal $n=1$ phasing for quiescent braking varies with q_{95} and shaping
- $F_{QM} = T_{NTV} / T_{JXB}$ modeling with IPEC-PENTRC explained empirical trends very well, including -90° vs 0° phasing issue, and predicted new details
- This study shows importance of remnant RMP control in NRMP applications, and modeled and validated F_{QM} can be used to predict quiescence in magnetic braking of rotation/shear