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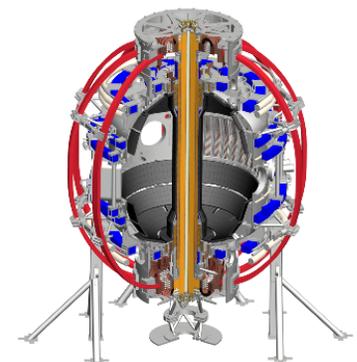


# Impact of the Digital Coil Protection System and Plasma Shutdown Handler on NSTX-U Operations

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58<sup>th</sup> Annual Meeting of the APS Division of Plasma Physics  
San Jose, CA, 11/2/16



# DCPS Overview

- NSTX-U power supplies can produce combinations of currents which result in forces that exceed limits on coils and their supports.
- DCPS = Digital Coil Protection System
- System → hardware, realtime software, parameter determination and archiving, testing, ops. procedures.
- Realtime software runs simultaneously in two independent locations:
  - Dedicated computer in the “junction area” adjacent to the power supply room.
  - Same computer as the plasma control system, in the FCC adjacent to the control room.
- DCPS can take only a single action...power supply crowbar that ends the shot.

# DCPS Computes Four “Types” of Algorithms

- Post-Disruption Current Analysis on Current Vector I:
  - $I_{\text{post-dis}} = I - I_P P$
  - P is a vector derived from all coil-plasma mutual inductance.
  - Force algorithm evaluated on I &  $I_{\text{post-dis}}$
- “Action” Integrals:
  - $A_i = \text{integral}(I_i^2 dt)$
  - $A_{i,\text{full}} = A_i + I_i^2 \tau_i / 2 \leftarrow \tau_i$  accounts for a potential power supply crowbar
- Simple Forces:
  - $F_i = I_i \sum \alpha_{i,j} I_j$
  - Radial and vertical forces, internal stresses and moments
- Complex Forces:
  - $C_i = \sum \beta_i F_{Z,i} + \sum \chi_i \beta_i F_{R,i} + \sum \delta_i A_i + \sum \epsilon_i A_{i,\text{full}} + \sum \phi_i I_i$
  - Used for combining vertical forces, bolt stresses, OH-TF interaction

Action, Simple Forces, and Complex Forces are All Compared to Positive and Negative Limits

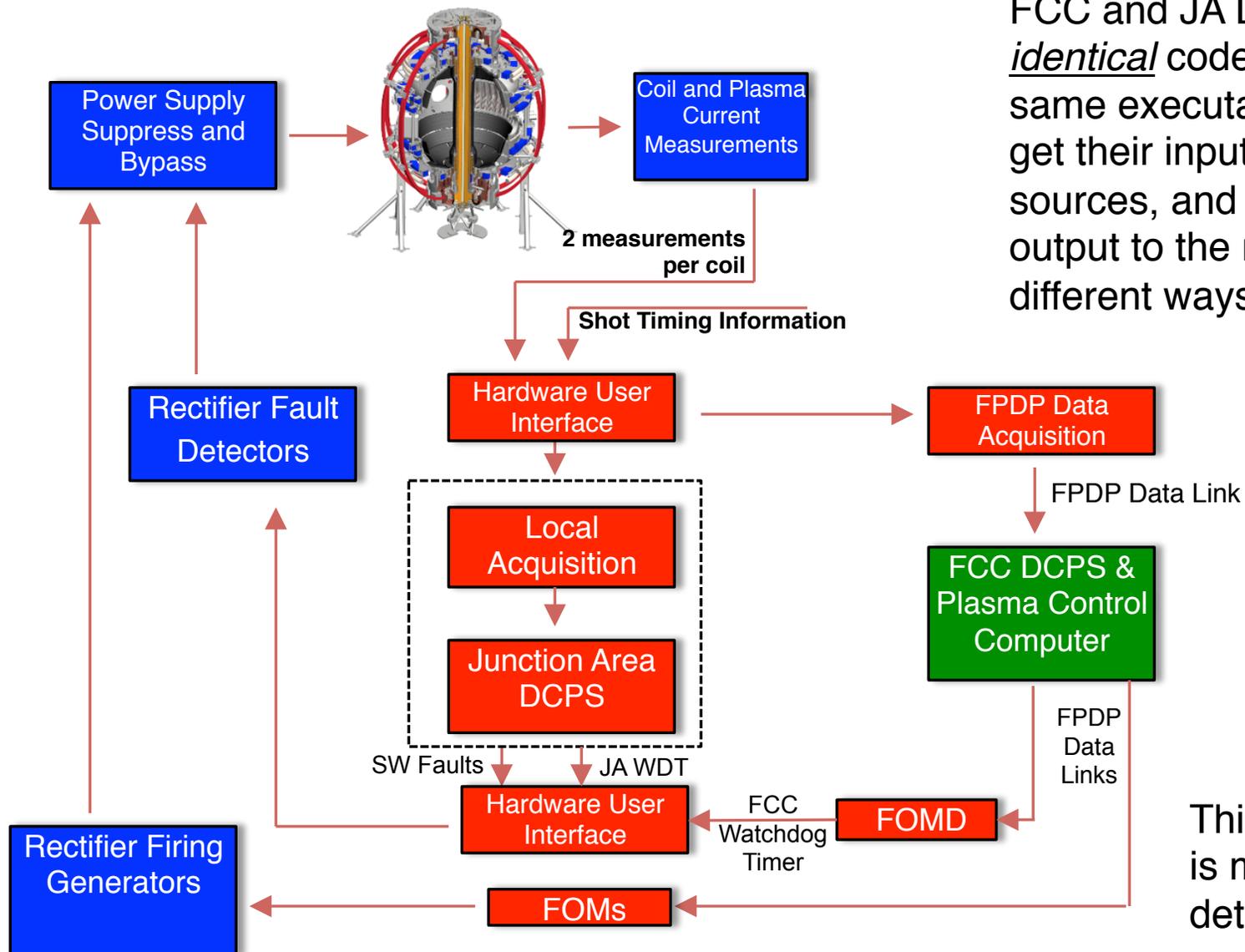
# List of DCPS Component Protection

- Overcurrent
  - $I^2t$  integrals
  - $T_{TF} - T_{OH}$ 
    - Must limit this due to OH-TF Frictional Interaction!
- Including the heating after a suppress and bypass

- Vertical and radial forces on coils
- Combinations of vertical forces
- PF Clamp Bolt Stresses
- Local stresses in OH, PF-4, PF-5
- Torsional Shear Stress
- TF Outer Leg Moments

Including calculations of the forces following a disruption with a simple model for the post-disruption currents.

# DCPS Uses Two Realtime Computer, With a Distributed System

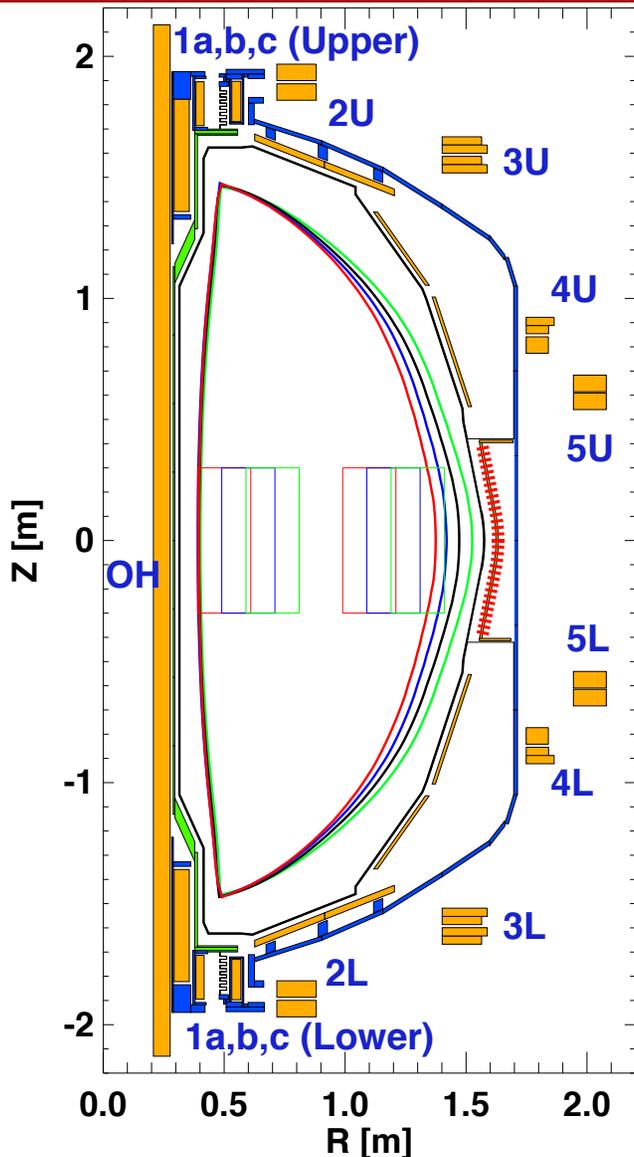


FCC and JA DCPS have *identical* code, and are the same executable file, but i) get their input from different sources, and ii) send their output to the rectifiers different ways

**Red for Junction Area (i.e. Next to FCPC)**  
**Green for FCC (i.e. Next to Control Room)**  
**Blue for FCPC (i.e. Power Supply Room)**

This block diagram is missing A LOT of details!

# NSTX-U Coils



## PF-5,4 Coils:

- Provide the vertical field,
- Upper and lower coils in series.

## PF-3 Coils:

- Control the plasma vertical position by applying a radial field (up-down asymmetric currents).
- Also help in controlling the elongation, squareness, and dr-sep
- Upper and lower coils independently controlled

## PF-1a,1b,1c,2 Coils:

- Control the divertor geometry, X-point and strike point locations.
- Upper and lower coils are independently controlled.

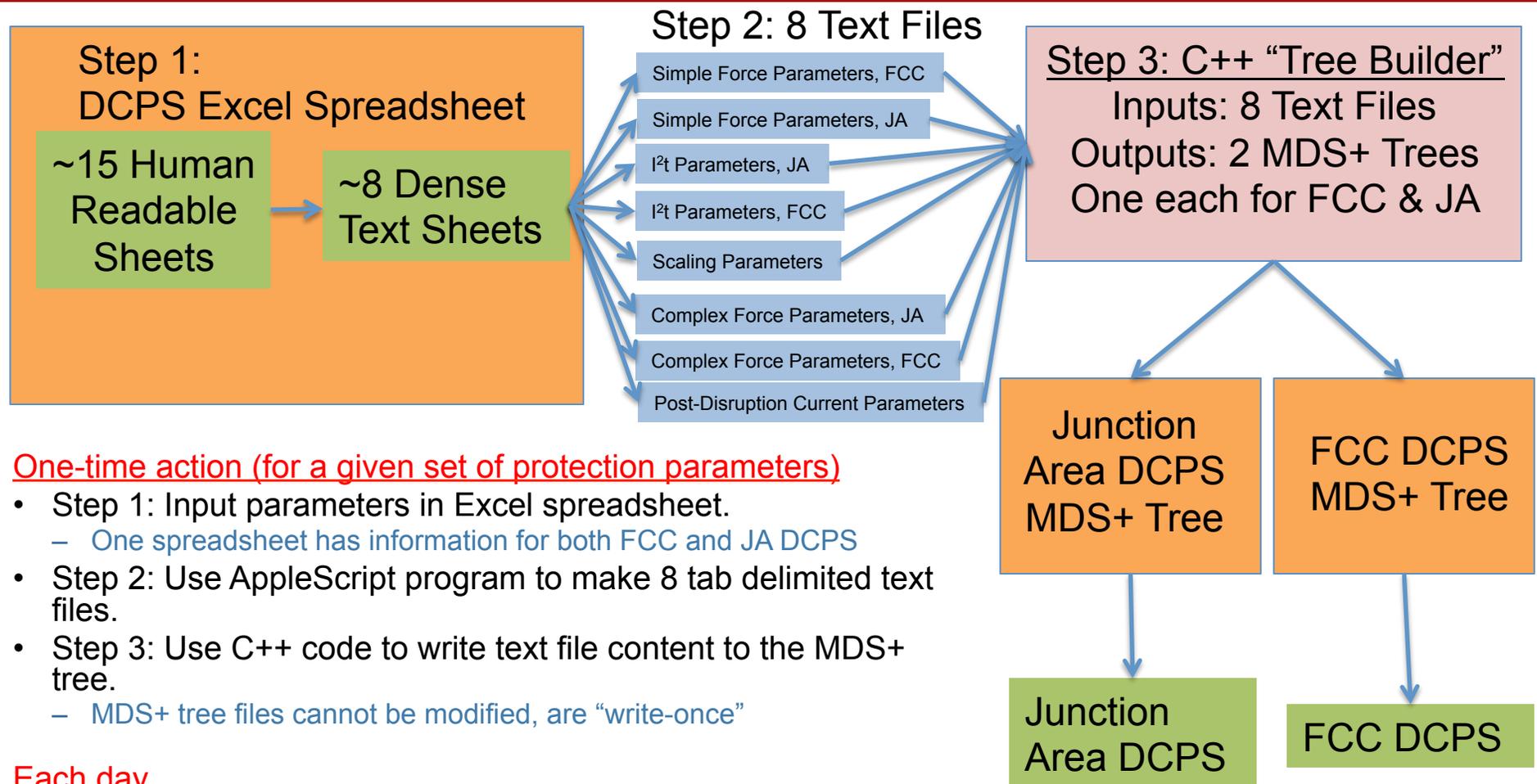
## OH Coil:

- Single coil provides loop voltage to the plasma.

## TF Coil (not shown)

- Makes toroidal field.

# Configuration Parameters Handled Via Excel and MDS+



## One-time action (for a given set of protection parameters)

- Step 1: Input parameters in Excel spreadsheet.
  - One spreadsheet has information for both FCC and JA DCPS
- Step 2: Use AppleScript program to make 8 tab delimited text files.
- Step 3: Use C++ code to write text file content to the MDS+ tree.
  - MDS+ tree files cannot be modified, are "write-once"

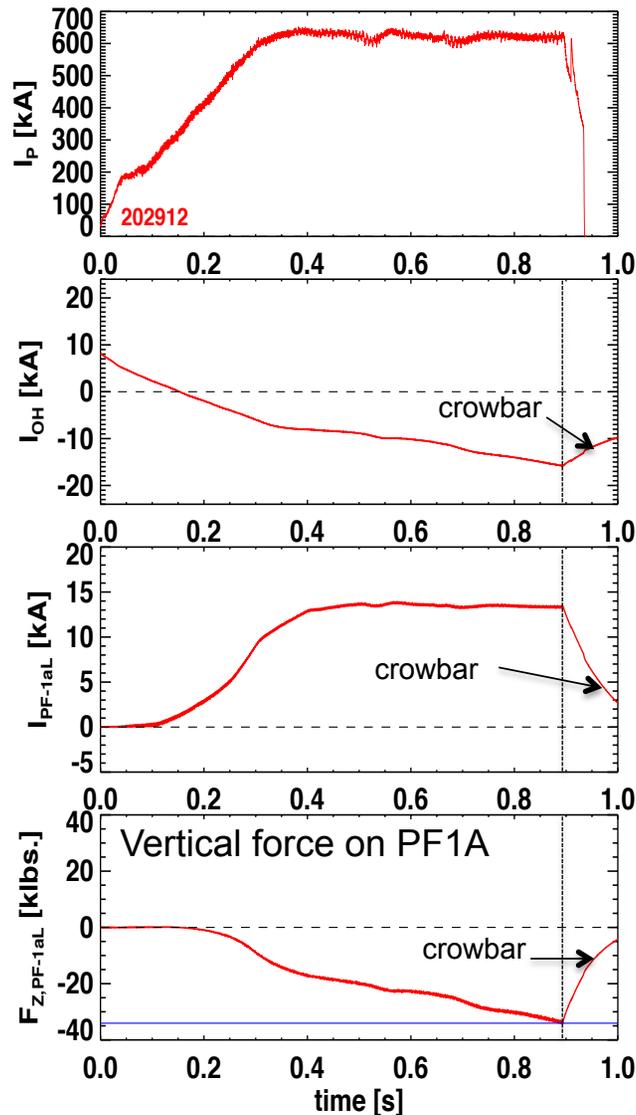
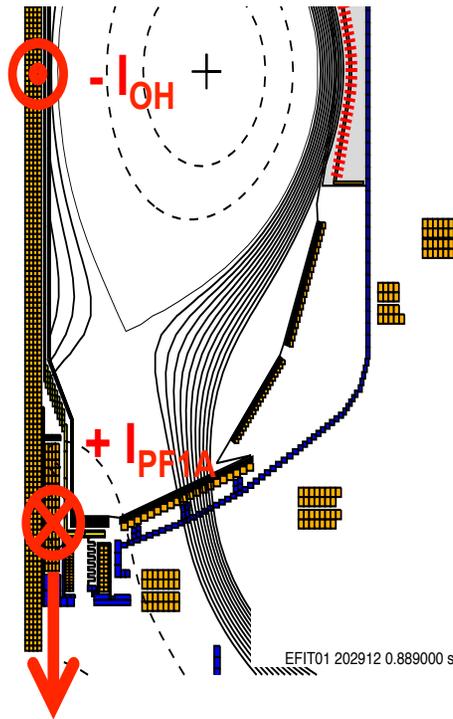
## Each day

- MDS+ tree files used to provide all input parameters to DCPS

## To change the protection parameters

- Make a new spreadsheet and use it to generate new trees

# Example of DCPS Terminating a Shot



Positive Plasma Current

OH Swinging Negative

PF-1aL Holds a Steady Positive Value

Growing negative vertical force on the PF-1aL.  
Trips at ~-34 klbs.

This sort of trip only in L-mode, which requires more divertor coil (PF-1a, PF-2) current for a given  $I_p$ .

# DCPS Prevents OH-TF Frictional Interaction

- As OH coil is wound directly on the TF, must avoid the TF becoming hotter than the OH.
  - If it does, the thermal axial growth of the TF will, via friction, put an axial force on the OH coil that could damage it.
- DCPS uses the “Complex Force” algorithm to protect against this:

- Assume the temperature rise is proportion to the  $I^2t$  integral
- Temperature difference between coils

$$T_{TF} - T_{OH} = T_{TF,0} + \delta_{TF} A_{TF} - T_{OH,0} - \delta_{OH} A_{OH}$$

- This fits the “complex force” algorithm template

DCPS Enforces These Quantities  $< 1$  C

Bond is broken, Aquapour is not Removed, OH Lorentz Forces Off , OH at 20C TF Ramped to 100C

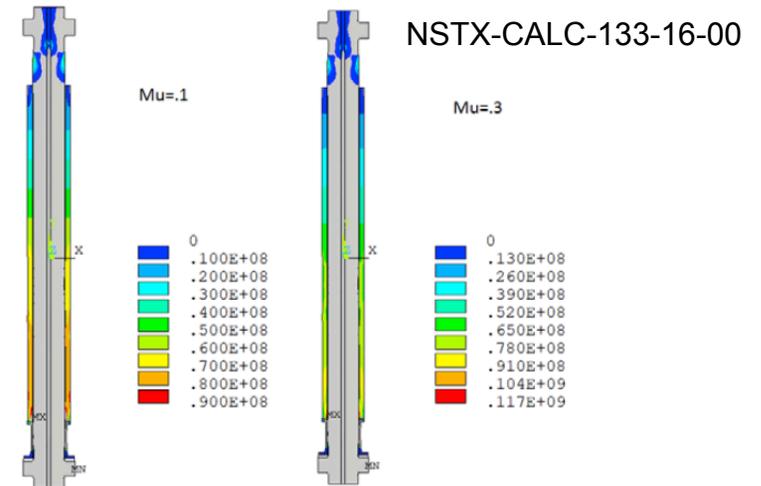
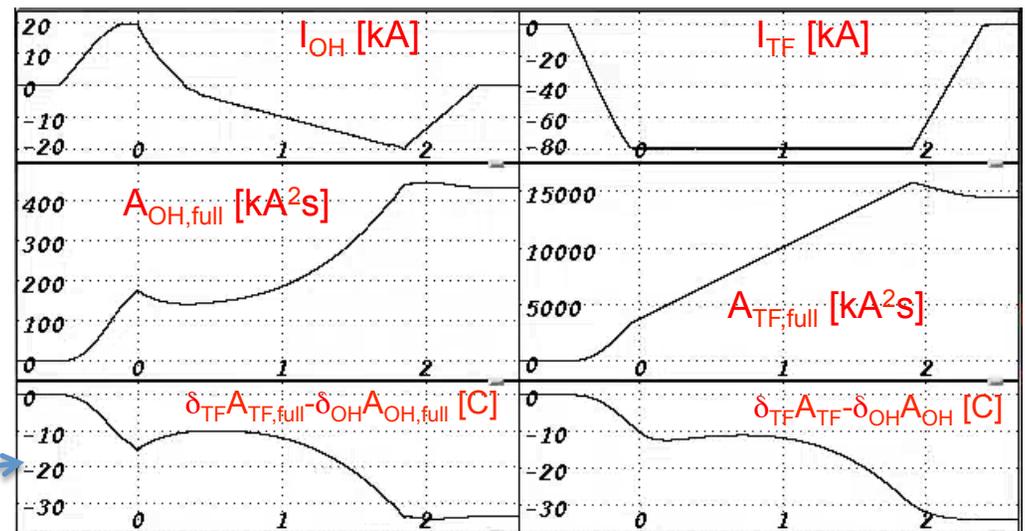


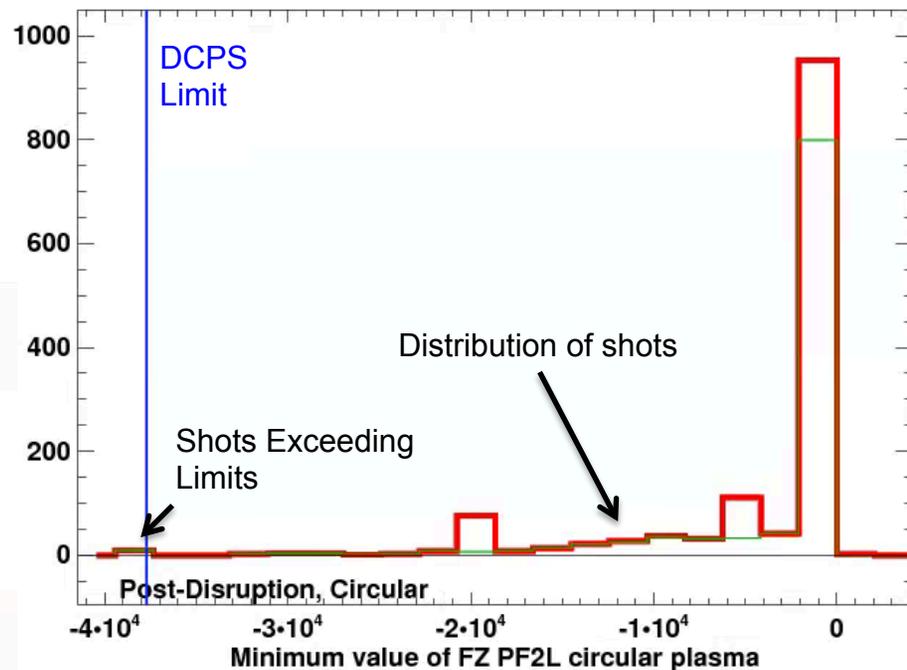
Figure 4.0-2 Showing a Worst Case Situation with the TF Hot and the OH Cold



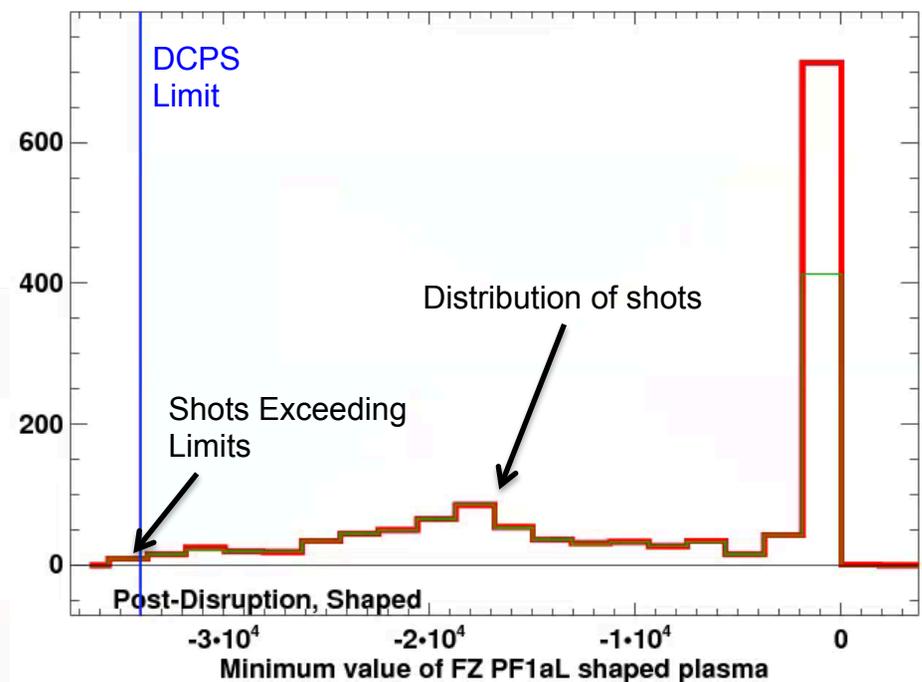
# Vertical Forces on Coils Were the Primary Sources of Trips (I)

Use database that archives maximum and minimum values for each algorithm

Vertical Force on the PF-2L Coil



Vertical Force on the PF-1aL Coil



This sort of trip only in L-mode, which requires more divertor coil (PF-1a, PF-2) current for a given  $I_p$ .

## Vertical Forces on Coils Were the Primary Sources of Trips (II)

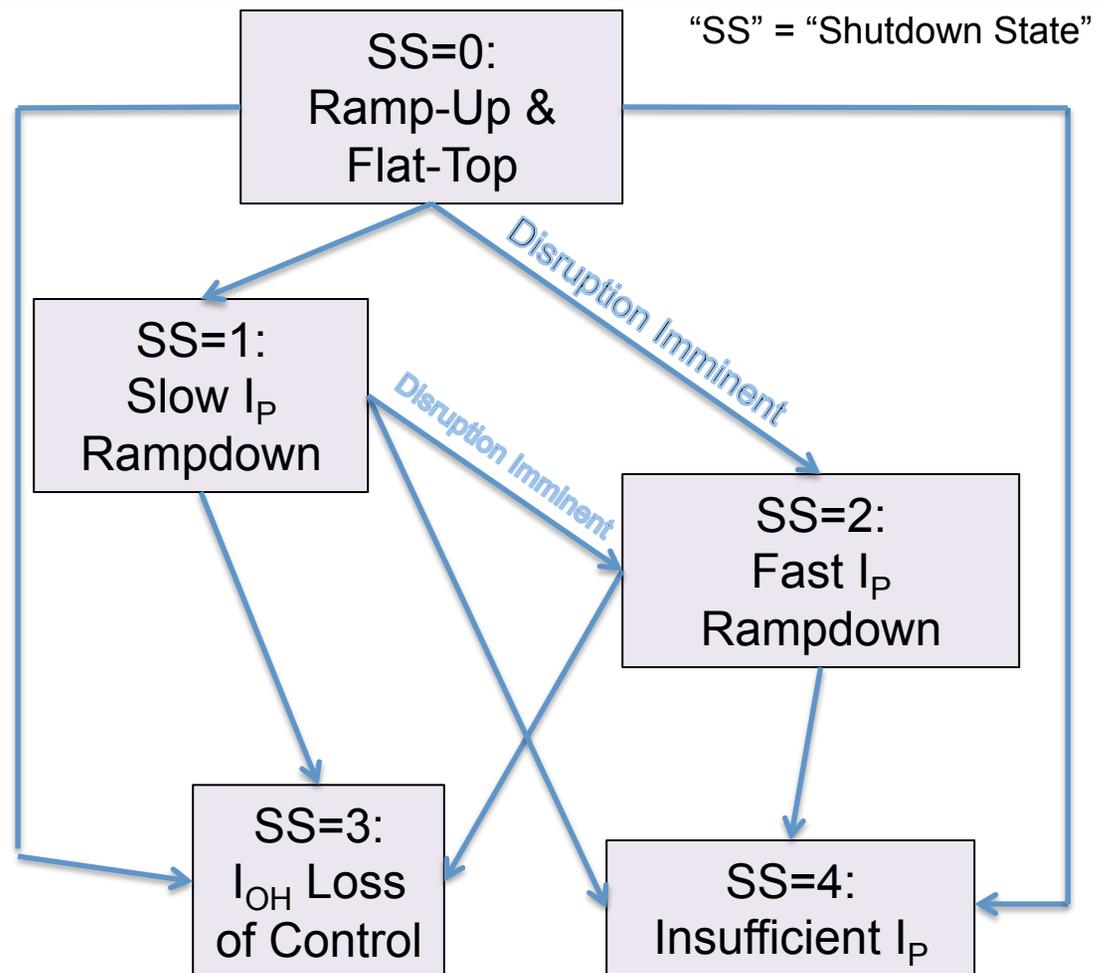
- 1353 Shots & 33 Algorithm Trips
- 3 trips of the TF Total Outer Leg Out-of-Plane Moment
  - This algorithm was deemed unnecessary and subsequently disabled.
  - Instead rely on the total moments on the separate upper and lower halves of the outer leg.
- 4 spurious trips of the aquapour protection algorithm due to garbled data stream (see next slide)
- 3 I<sup>2</sup>t trips on the OH coil during long pulse.
- 23 vertical force trips (mostly related to too-large divertor coil current in L-mode, due to higher I<sub>i</sub>)
  - 1 on PF-1aU
  - 4 on PF-2U
  - 9 On PF-2L
  - 9 on PF-1aL

# Comments on Initial Operating Experience (SPG Opinions)

- **Highly reliable**
  - Only frustrating day was when an arcing Penning gauge power supply was causing garbled realtime data blocks, which DCPS repeatedly noted and caused a crowbar.
- **Should not have put DCPS on the control computer**
  - Sharing a realtime computer with the plasma control system resulted in numerous software and hardware complications.
  - Would have been better to have two independent but identical stand-alone computers.
- **Minimal number of algorithm trips**
  - Only ~2.5% of shots had algorithm trips.

# Shutdown Handler Designed to Gracefully End the Plasma

- Why do this?
  - Want to limit control transients at the end of the discharge.
  - Want to support critical research in disruption detection/avoidance.
- State machine implementation
- Coding of the state machine is largely free of detailed plasma physics/control.



*Diagram of the State Machine Presently Implemented in PCS*

# What Controls, and is Controlled By, the Shutdown Handler?

## Controls It

- Can go into fast rampdown by:
  - Detection of large  $n=1$  mode.
  - Detection of large loss of plasma current.
  - Detection of excessive vertical motion.
  - $I_p$  drops beneath value required for rtEFIT while using ISOFLUX
  - Operator request
- Can go into slow rampdown by:
  - Detection that OH coil is approaching a heating limit.
  - Detection that OH coil is approaching a current limit.
  - Operator request

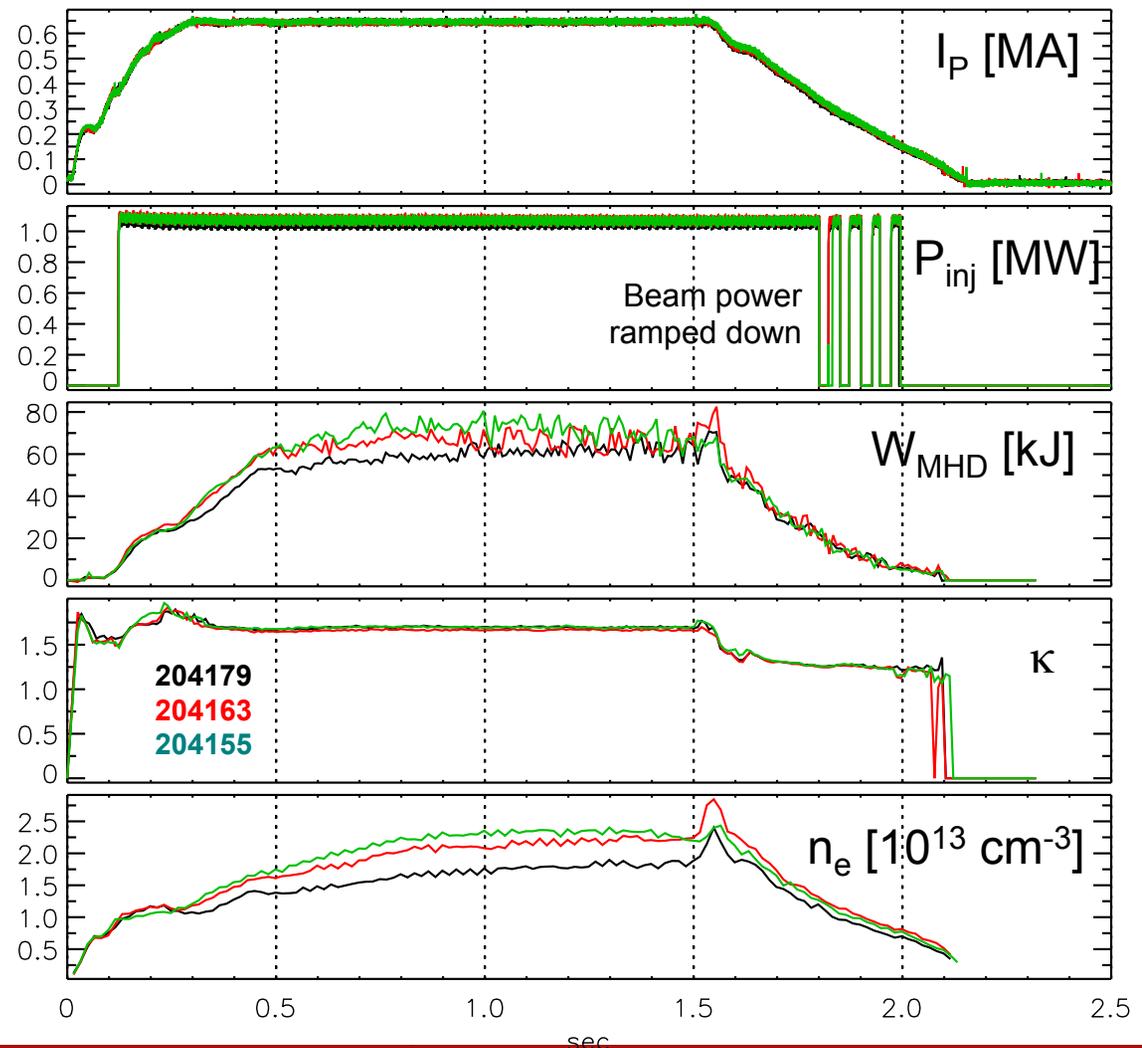
## It Controls

- At each state change, switch the control algorithm used by actuators.
  - For instance, switch from diverted to inner-wall limited shape.

# Shutdown Handler Used to Create Smooth L-Mode Rampdown

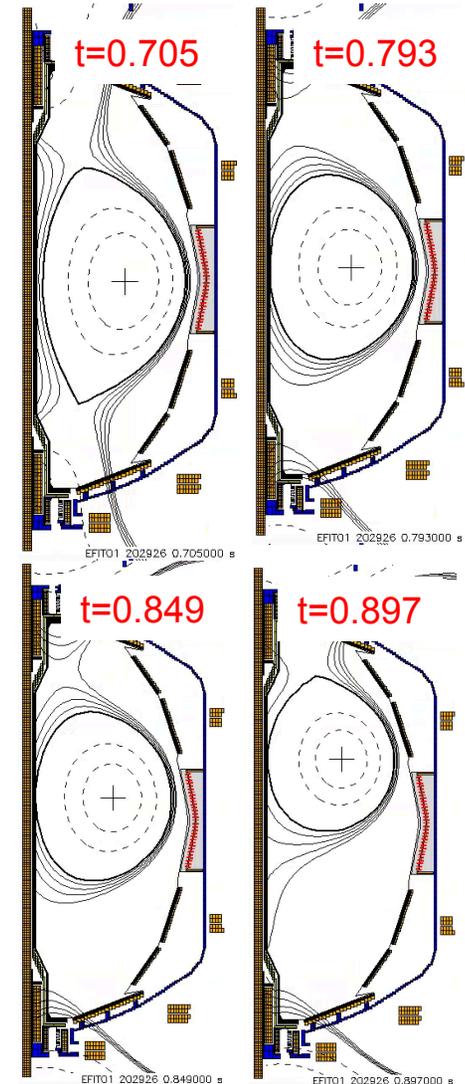
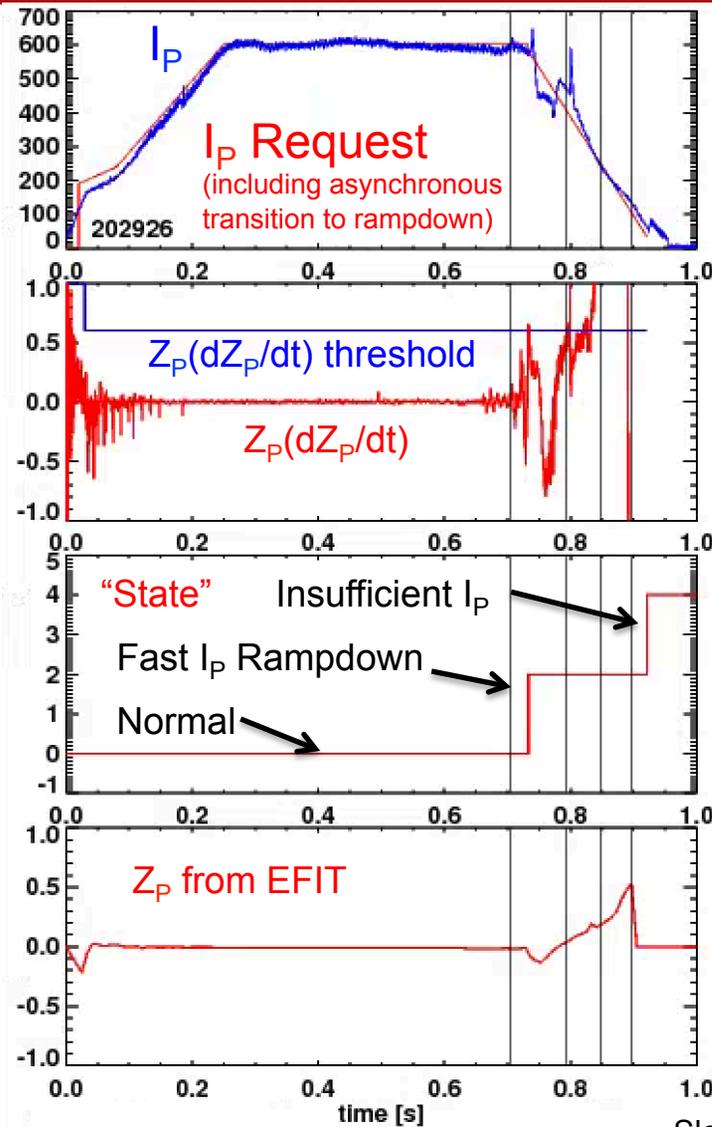
- Three AM fiducial shots from week of 4/4/2016.
- Single operator waveform modified at  $t=1.5$  to start the rampdown.
- Rampdown is IWL, with power and  $I_p$  slowly ramped off.

## L-mode Rampdowns Triggered By a Single Switch



# Shutdown Handler Also Used to End Failing Discharges

- Shot requested to go longer, but vertical motion detected.
- Rampdown initiated.
- Plasma inboard limited, only slowly drifts up.

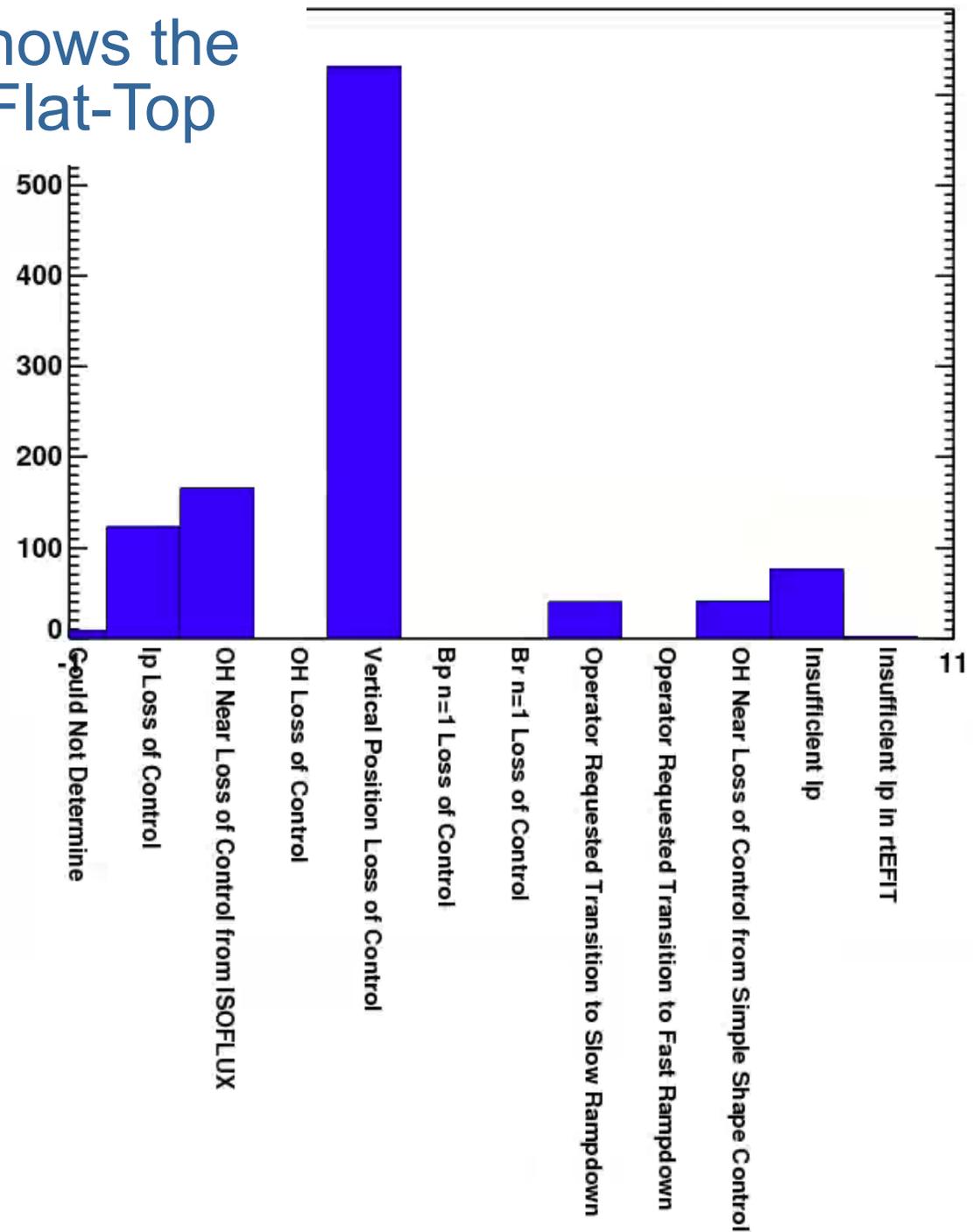


Slow Drift Up, But No VDE or Disruption



# Database Analysis Shows the Causes of Leaving Flat-Top

- By far the most common is **Vertical Position Loss of Control (LoC)**
  - But beware, those sensors are sensitive to  $n=1$  modes as well as  $n=0$ ,
- **OH Near LoC** triggers shutdown based on OH current or heating limit.
- **$I_p$  LoC** looks for large values of the  $I_p$  error.
- We never activated the **BP & BR  $n=1$  LoC**.
  - Therefore don't read anything into its having no instances...wait till next year.



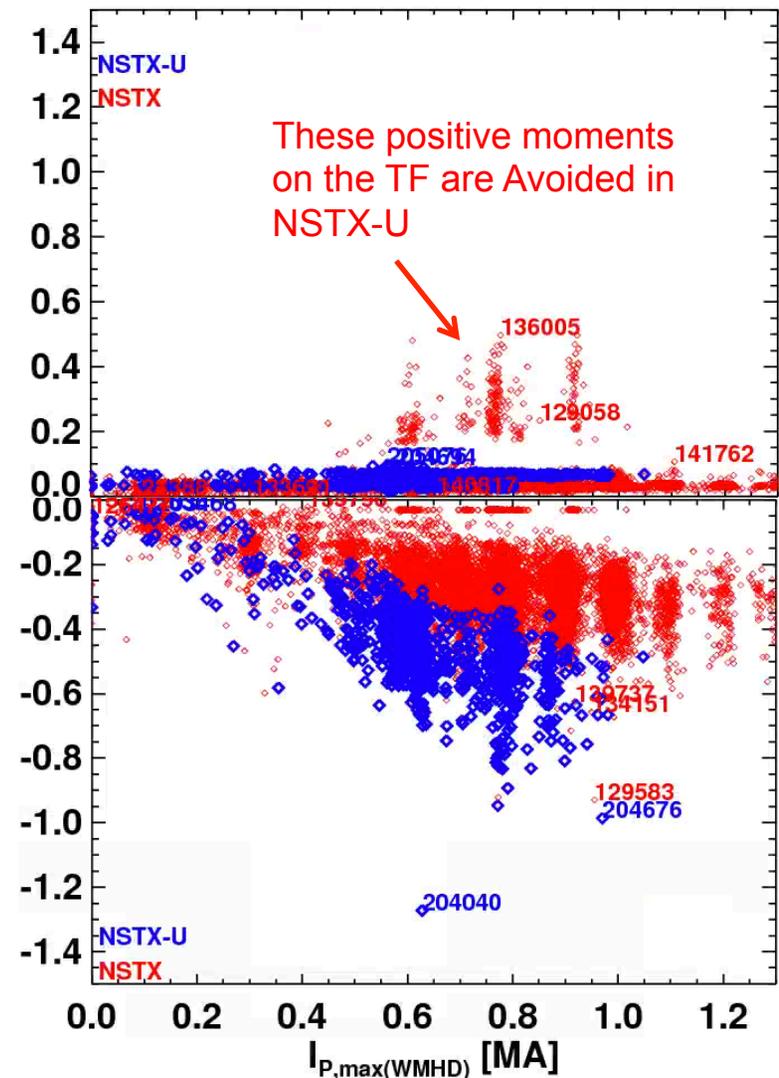
# Shutdown Handler Allows Us to Reduce Stress on Components

- Consider moment on the TF outer leg due to  $I_{TF}$  crossing the poloidal field.

**NSTX:** Large PF transients during disruptions -> moment was both positive and negative -> more mechanical fatigue on coils.

**NSTX-U:** Reduced PF transients -> the moment on coils is one-sided -> reduced mechanical fatigue.

Note: The shot with the worst moment (204040) was due to a misconfiguration of the shutdown handler.



# Next Steps For Shutdown Handler

- During this run, we never activated the part of code allowing a transition from slow to fast rampdown:
  - Fixed a code bug, but didn't get a chance to test it before PF coil failure.
- Need to allow the RWM sensors to trigger the rampdown
  - They were running in realtime, but never flipped the switches to enable them in this functionality.
- Need to see if some other configuration of the vertical position sensing code can be less sensitive to  $n=1$  modes.
- Longer term:
  - Use to trigger MGI?
  - Incorporate additional tests of disruption proximity as per DECAF?