

# A Component Test Facility (CTF) Based on the Spherical Tokamak

Y-K Martin Peng,

PJ Fogarty, DJ Strickler, TW Burgess, BE Nelson, J Tsai  
Oak Ridge National Laboratory, UT-Battelle

C Neumeyer, R Bell, C Kessel, J Menard, D Gates, B LeBlanc,  
D Mikkelsen, L Grisham, J Schmidt, P Rutherford  
Princeton Plasma Physics Laboratory

A Field, A Sykes, I Cook  
UKAEA Culham Science Center

S Sabbagh, Columbia University  
O Mitarai, Kyushu Tokai University  
Y Takase, University of Tokyo

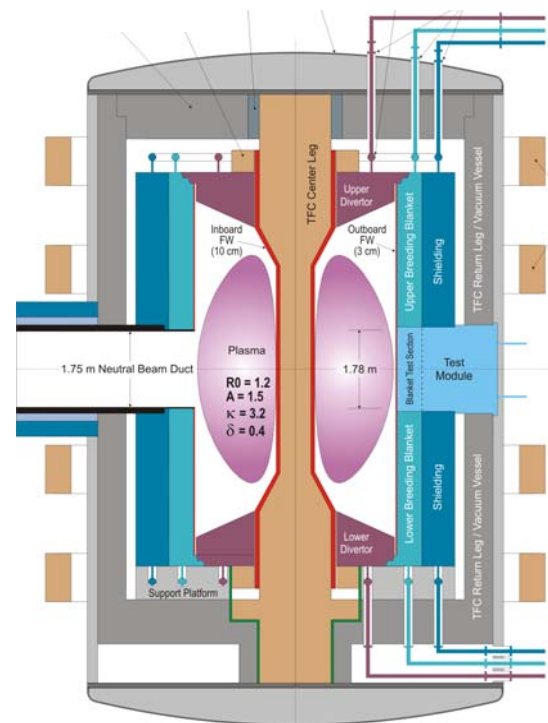
**32<sup>nd</sup> EPS Conference on Plasma Physics**

Combined with the

**8<sup>th</sup> International Workshop on Fast Ignition of Fusion Targets**

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Tarragona, Spain



# CTF – A Facility Required for Developing Engineering and Technology Basis for Fusion Energy

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- **INL operated 45 small research fission facilities during 1951-69**
- **Necessary fusion Demo-relevant testing environment:**  
[M Abdou et al, Fusion Technology, 29 (1999) 1.]
  - **High 14 MeV neutron flux over large wall areas**
  - **High duty factor to achieve high neutron fluence per year**
  - **High accumulated fluence in facility lifetime**
- **Test tritium self-sufficiency – goal: 80 – 100% recovery**
- **This presentation:**
  - **Programmatic importance**
  - **Desired engineering features**
  - **Plasma and device parameters based on latest physics understanding**
  - **Database needs in physics, engineering, & technology**

# CTF Bridges Large Gaps between ITER and Demo in Tritium Self-Sufficiency, Duty Factor, Neutron Fluence, and Divertor Heat Flux

Fusion Power Conditions	ITER	CTF	Demo
Tritium self-sufficiency goal (%)		>80	>100
Sustained fusion burn duration (s)	$\sim 10^3$	$>10^{6-7}$	$\sim 10^{7-8}$
14-MeV neutron flux on wall (MW/m <sup>2</sup> )	$\sim 0.8$	2	$\sim 3$
Duty factor (%)	$\sim 2$	>30	75
Accumulated neutron fluence (MW-yr/m <sup>2</sup> )	$\sim 0.3$	>6	6–20
Divertor heat flux challenge, P/R (MW/m)	24	64	97
Total area of (test) blankets (m <sup>2</sup> )	$\sim 12$	$\sim 65$	$\sim 670$
Expected fusion power (MW)	$\sim 500$	144	2500

- CTF provides prototypical fusion power conditions at *reduced size and power*
- Potential to “buttress” ITER & IFMIF in *accelerating development of fusion power* [I Cook et al., UKAEA FUS 521 (Feb. 2005)]
- DOE Office of Science 20-Year Strategic Plan for Fusion includes *CTF to succeed ITER construction*

# DOE Office of Science 20-Year Strategic Plan for Fusion Includes CTF to Succeed ITER Construction

## Strategic Timeline—Fusion Energy Sciences\*

2003 2005 2007 2009 2011 2013 2015 2017 2019 2021 2023 2025

### The Science

#### Burning Plasma Demonstration

- Initiate experiments on the National Ignition Facility (NIF) to study ignition and burn propagation in IFE-relevant fuel pellets (2012)
- Complete ITER experiments to determine plasma confinement in parameter range required for an energy-producing plasma (2017)
- Complete experiments on NIF to advance the science of ignition and burn propagation needed to design optimized fuel pellets for an Inertial Fusion Energy plant (2020)
- Complete experiments on ITER to determine the impact of the fusion process on the stability of energy-producing plasmas (2020)
- Achieve high fusion power for long durations on ITER to define engineering requirements for fusion power plants (2025)

#### Fundamentals of Plasma Behavior

- Major aspects relevant to burning plasma behavior observed in existing tokamak experiments are predicted
- Achieve a fundamental understanding of tokamak transport and stability in present-day tokamak and ITER plasma experiments (2008)
- Complete a complete integrated test facility for a power-producing fusion plant (2025)

#### Plasma Confinement

- Evaluate stellarator confinement and performance (2008)
- Achieve long-duration, high-pressure confinement in a spherical torus sufficient to design a power-producing Next-Step Spherical Torus (NSST) (2013)
- Demonstrate use of active plasma control to achieve high-pressure/steady-state operation for ITER (2008)
- Evaluate the feasibility/attractiveness of alternative fusion approaches including heavy ion beams, dense plasmas, and inertial fusion for fusion approaches involving high-energy densities (2008)
- Complete first round of testing in a component test facility to validate the performance of chamber technologies needed for a power-producing fusion plant (2025)

#### Materials, Components, and Technologies

- Start production of superconducting wire needed for ITER magnets (2006)
- Deliver to ITER for testing the blanket test modules needed to demonstrate the feasibility of extracting high-temperature heat from burning plasmas and for a self-sufficient fuel cycle (2013)
- Complete first phase of testing in ITER of blanket technologies needed in power-producing fusion plants capable of extracting high-temperature heat from burning plasmas and having a self-sufficient fuel cycle (2024)
- Complete first round of testing in a component test facility to validate the performance of chamber technologies needed for a power-producing fusion plant (2025)

### Component Test Facility

#### Future Facilities\*\*

**ITER:** ITER is an international collaboration to build the first fusion science experiment capable of producing a self-sustaining fusion reaction, called a "burning plasma."

**Next-Step Spherical Torus (NSST) Experiment:** The NSST will be designed to test the spherical torus, an innovative concept for magnetically confining a fusion reaction.

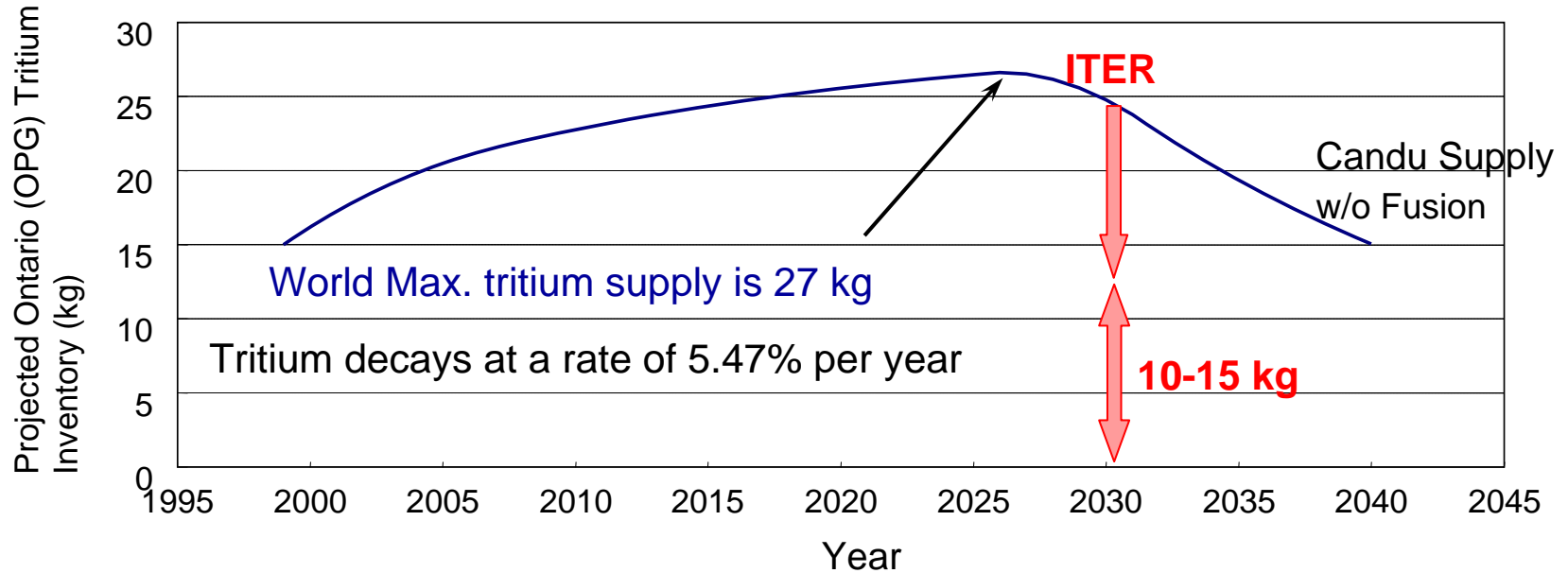
**Fusion Energy Contingency:** If ITER construction and operation goes forward as planned, additional facilities to develop and test power plant components and materials will be needed to complete the process of making fusion energy a viable commercial energy resource by mid-century.

**Integrated Beam Experiment (IBX):** The IBX will be an intermediate-scale experiment to understand how to generate and transmit the focused, high-energy ion beam needed to power an IFE reaction.

\*These strategic milestones are illustrative and depend on funds made available through the Federal budget process.

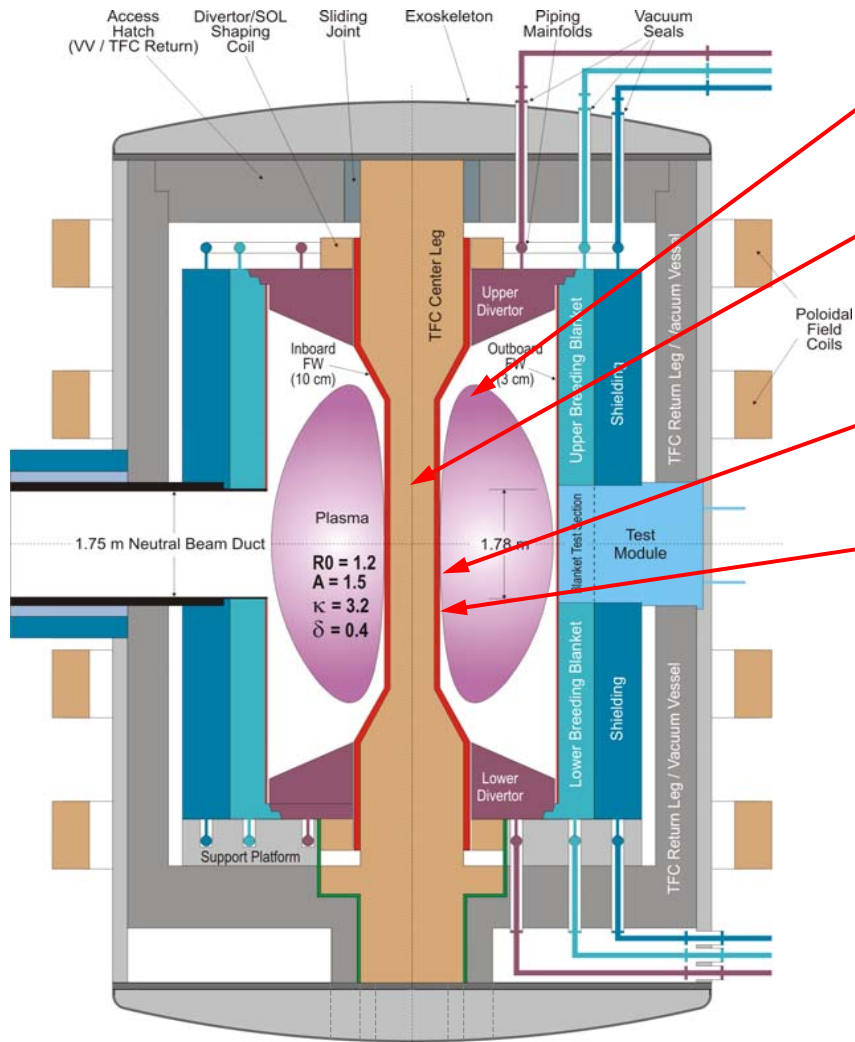
\*\*For more detail on these facilities and the overall prioritization process, see the companion document, *Facilities for the Future of Science: A Twenty-Year Outlook*.

# Projected World Tritium Supply Necessitates Testing in CTF Before Implementation in Demo



- ITER uses ~11 kg T to provide 0.3 MW-yr/m<sup>2</sup>; 10-15 kg remains
- Demo burns tritium @ 2.7 kg/week to produce 2500 MW fusion power
- **To accumulate 6 MW-yr/m<sup>2</sup> (component testing mission), and assuming 80% breeding fraction,**
  - **Demo requires 56 kg**
  - **CTF requires 4.8 kg**

# Features of Optimized ST Fulfill the CTF Mission Effectively

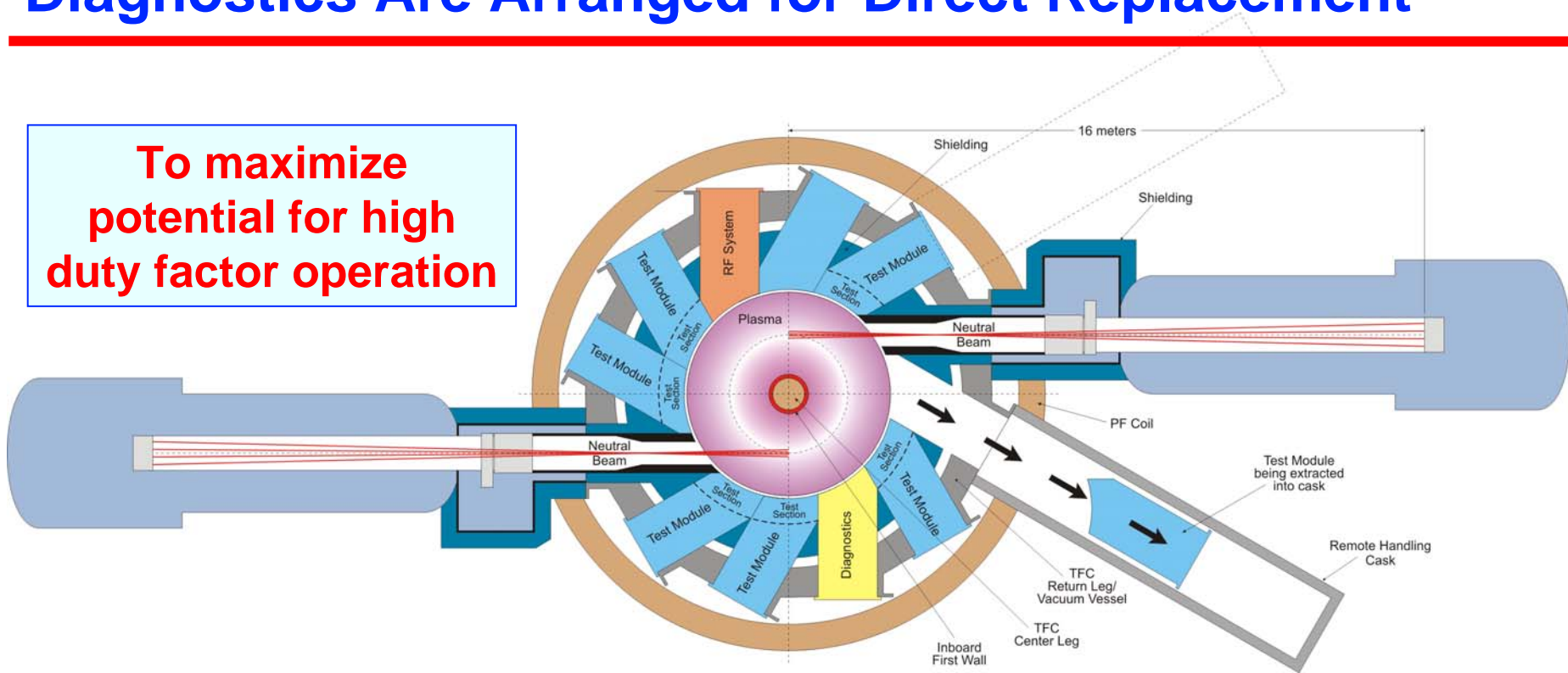


$R_0 = 1.2 \text{ m}, a = 0.8 \text{ m}$

- ◆ **Natural elongation at low  $l_i$**  → simple shaping coils
- ◆  **$I_{TF} \sim I_p$ ; moderate  $B_T$**  → slender, demountable, single-turn TF center leg
- ◆ **No central solenoid** → no inboard nuclear shielding
- ◆ **No inboard blanket** → compact ST device with small radius & aspect ratio
- ◆ **~5% fusion neutrons lost to center leg** → high tritium breeding ratio
- ◆ **Culham CTF: more compact, less fusion power, same  $W_L$**   
[H Wilson et al., IAEA FEC 2004, FT/3-1a.]

# Mid-Plane Test Modules, Neutral Beam Injection, RF, Diagnostics Are Arranged for Direct Replacement

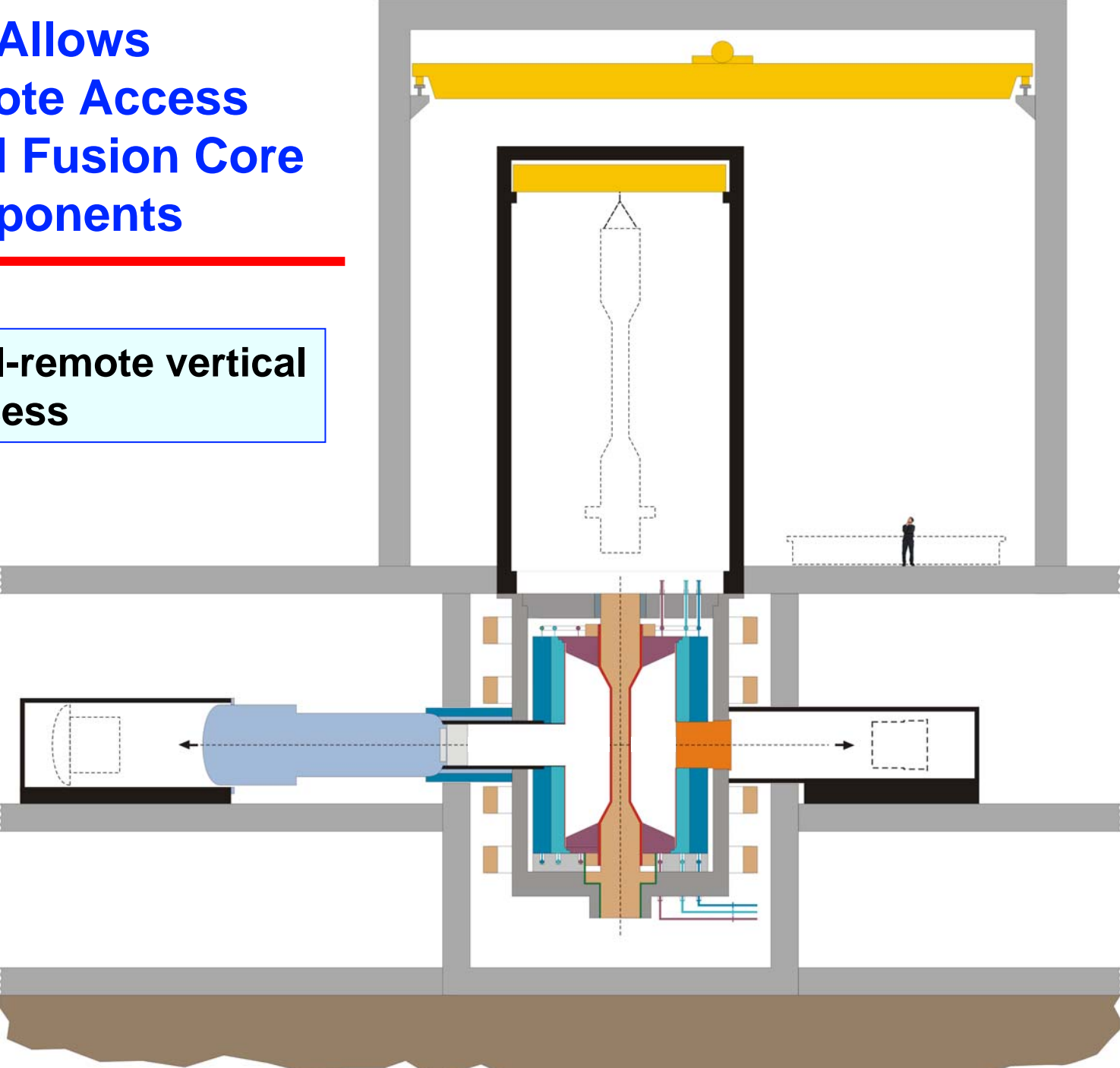
To maximize potential for high duty factor operation



- 8 mid-plane blanket test modules provides  $\sim 15 \text{ m}^2$  at maximum flux
  - Additional cylindrical blanket test area  $> 50 \text{ m}^2$  at reduced flux
- $3 \text{ m}^2$  mid-plane access for neutral beam injection of 30 MW
- $2 \text{ m}^2$  mid-plane accesses for RF (10 MW) and diagnostics
- All modules accessible through remote handling casks ( $\sim$ ITER)

# CTF Allows Remote Access to All Fusion Core Components

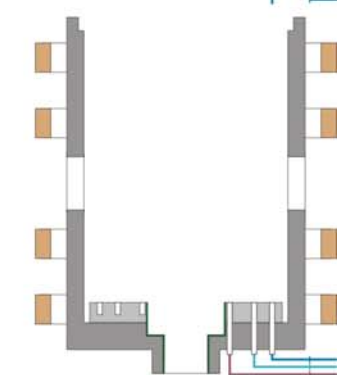
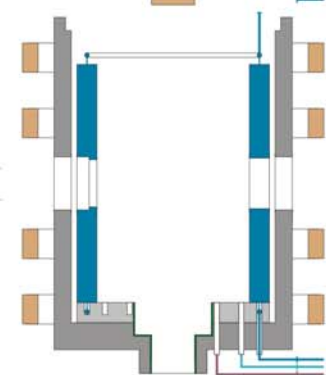
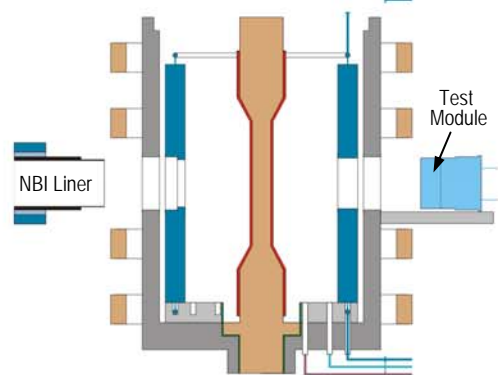
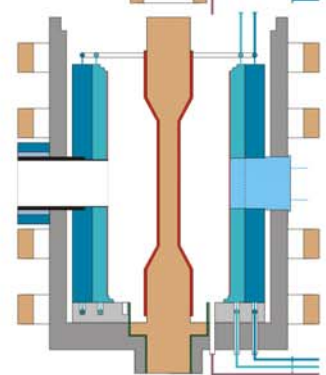
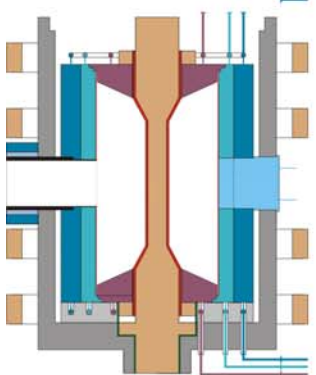
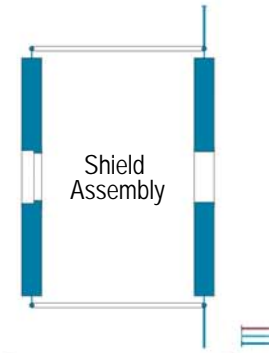
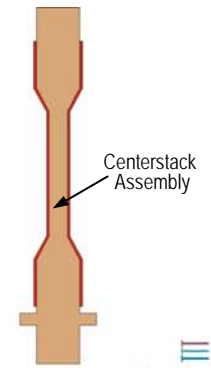
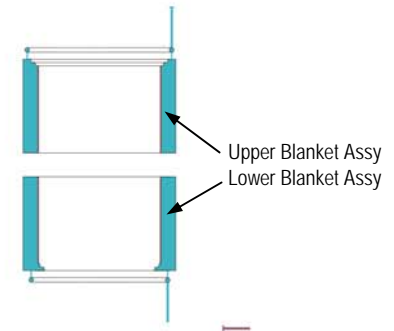
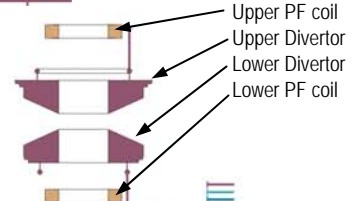
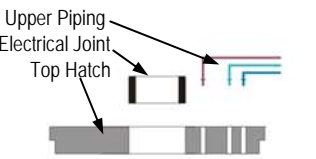
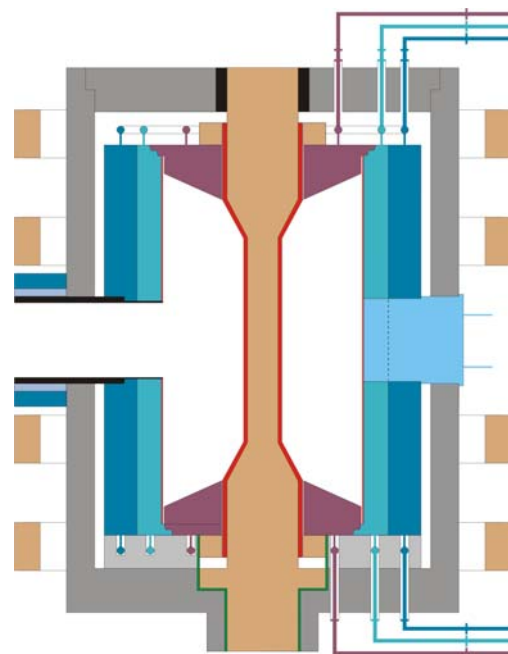
- Full-remote vertical access





# Machine Assembly/Disassembly Sequence Are Made Manageable

- Hands-on connect and disconnect service lines outside of shielding and vacuum boundaries
- Divertor, cylindrical blanket, TF center leg, and shield assembly removed/installed vertically



- Disconnect upper piping
- Remove sliding electrical joint
- Remove top hatch

- Remove upper PF coil
- Remove upper divertor
- Remove lower divertor
- Remove lower PF coil

- Extract NBI liner
- Extract test modules
- Remove upper blanket assembly
- Remove lower blanket assembly

- Remove centerstack assembly

- Remove shield assembly

# Initial CTF Parameters Are Estimated Based on the Design Concept & Present Physics Understanding

Systems Code  $\Rightarrow R_0 = 1.2$  m,  $a = 0.8$  m,  $\kappa = 3.2$ ,  $B_T = 2.5$  T

14MeV neut. flux, MW/m <sup>2</sup>	2.0	4.0
$I_p$ , MA	12.8	16.1
Combined $H_{98pby}$ factor	1.48	1.38
$\beta_T$ , %	24	39
$\beta_N H_{89P}$	11.3	16
Safety factor, $q_{cyl}$	3.0	2.4
$n/n_{GW}$	0.17	0.21
$I_{BS}/I_p$	0.43	0.44
$P_{fusion}$ , MW	144	288
$P_{NBI+RF}$ , MW	40	65
Neutral beam energy, kV	160	250
$f_{rad}$ , % (for $P_{div} = 15$ MW/m <sup>2</sup> )	75	90
Net $T_{consumption}/yr$ goal, gm	14	180

- **Baseline (2 W/m<sup>2</sup>) parameters within ST plasma operation limits**
- **Higher neutron fluxes reach progressively more limits**
  - In  $\beta$ ,  $q_{cyl}$ , and  $f_{rad}$
  - Requires densities  $\ll$  limit
- **Technology & physics of CTF advances in synchrony**
  - 2 MW/m<sup>2</sup> – medium ST physics to test technologies beyond ITER
  - 4 MW/m<sup>2</sup> – more advanced ST physics to test DEMO level technologies

# CTF Can Utilize Attractive ST Physics Properties



## Encouraging NSTX & MAST results

C Roach: I2.006,	A Kirk: O4.001
J Menard: O4.007,	P Helander: I5.003
S Kaye: P5.042,	A Sykes: P4.112
B Stratton: P1.060,	E Fredrickson: P1.061
R Raman: P1.063,	V Rozhanski: P2.017
I Chapman: P2.062,	D Howell: P2.061
V Soukhanoskii: P4.016,	R Maingi: P4.017
B Dudson: P4.019,	M Wisse: P4.100
E ElChambre: P5.015,	M Redi: P5.041
D Applegate: P5.101,	G Madison: P5.102
A Surkov: P5.103,	G Antar: D5.005

## Utilizes applied field efficiently

- Strong plasma shaping & self fields (vertical elongation  $\sim 3$ ,  $B_p/B_t \sim 1$ )
- Very high  $\beta_T$  ( $\sim 40\%$ ) & bootstrap current

## Contains plasma energy efficiently

- Small plasma size relative to gyro-radius ( $a/\rho_i \sim 30-50$ )
- Large plasma flow ( $M_A = V_{\text{rotation}}/V_A \leq 0.4$ )
- Large flow shearing rate ( $\gamma_{\text{ExB}} \leq 10^6/\text{s}$ )

## Disperses plasma fluxes effectively

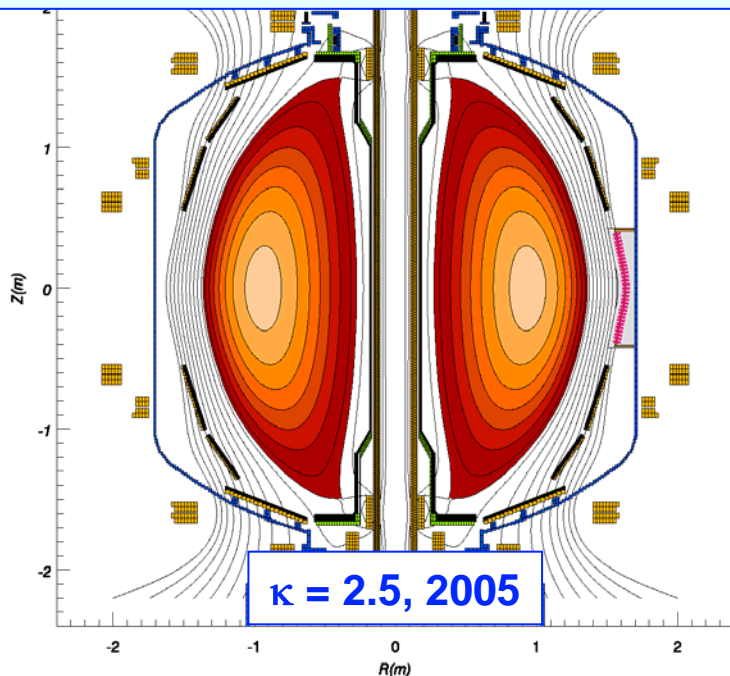
- Large mirror ratio in edge B field ( $f_T \lesssim 1$ )
- Strong SOL expansion

## Allows easier solenoid-free operation

- Small magnetic flux content ( $\sim \ell_i R_0 I_p$ )

## Heating and Current Drive opportunities

- Supra-Alfvénic fast ions ( $V_{\text{fast}}/V_A \sim 1-5$ )
- High dielectric constant ( $\epsilon = \omega_{pe}^2/\omega_{ce}^2 \sim 50$ )



# CTF Stable $\beta$ Values Rely on Continued Progress in ST Macro-Stability Research



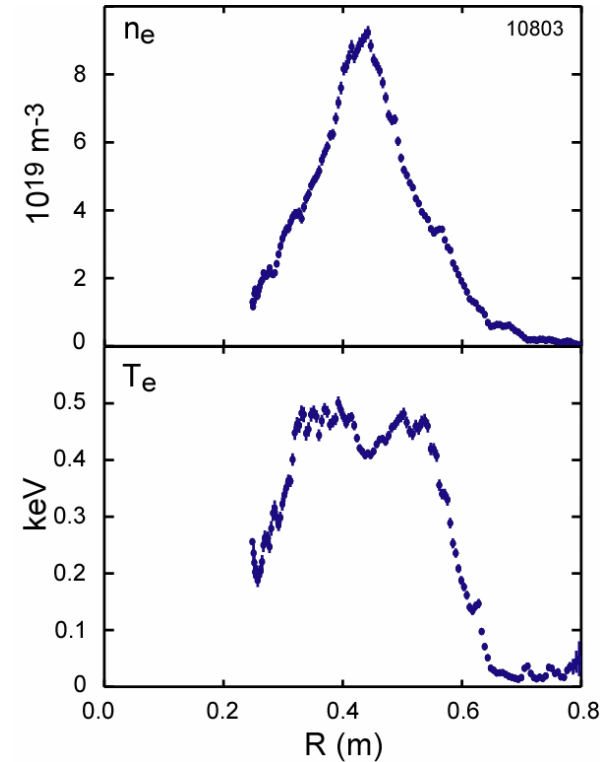
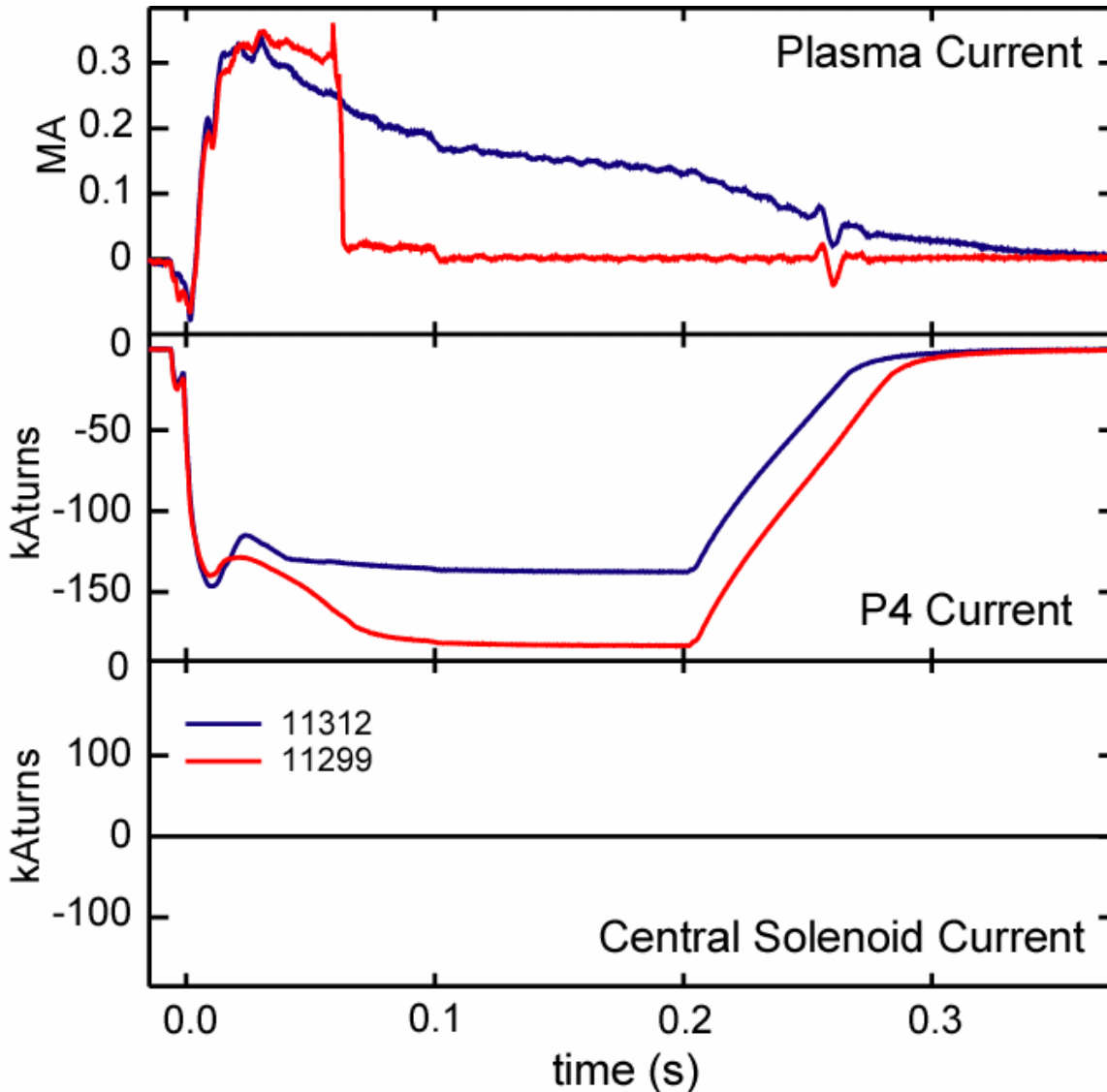
Sustained Parameters	CTF ( $\tau \gg \tau_{skin}$ )	Long Pulse Data ( $\tau > \tau_{skin}$ )
$I_p/aB_T$ (MA/m-T)	$\leq 6.4$	$\leq 4.4$
Safety factor, $q_{cyl}$	$\geq 3.0$	$\geq 2.2$
$\beta_N$ (%-m-T/MA)	$\leq 3.9$	$\leq 5$
$\beta_T$ (%)	$\leq 24$	$\leq 23$
Start-up to $\mu_0 l_i R I_p$ (Wb)	$\geq 3.8$	$\sim 0.13$ (goal)

## Required Investigations

- Macro-stability near CTF conditions:  $\kappa \leq 2.7$  and  $\tau \gg \tau_{skin}$
- Error field & resistive wall mode, with strong plasma rotation, toward high reliability & higher  $\beta_N$
- Solenoid-free start-up to  $\sim 0.5$  MA plasma target for NBI and EBW

**Issue: solenoid-free startup** [Raman: P1.063; Sykes: P4.112]

# 'Double Null Merging' Scheme on MAST: Plasma Current up to 340kA Formed and Plasma Sustained for 0.3sec with Zero Current in Central Solenoid (Sykes: P4.112)



Plasma is hot ( $\sim 0.5\text{keV}$ )  
and dense ( $9 \times 10^{19} \text{m}^{-3}$ )

# CTF Confinement Assumptions Are Suggested by Long-Pulse Plasmas in NSTX & MAST

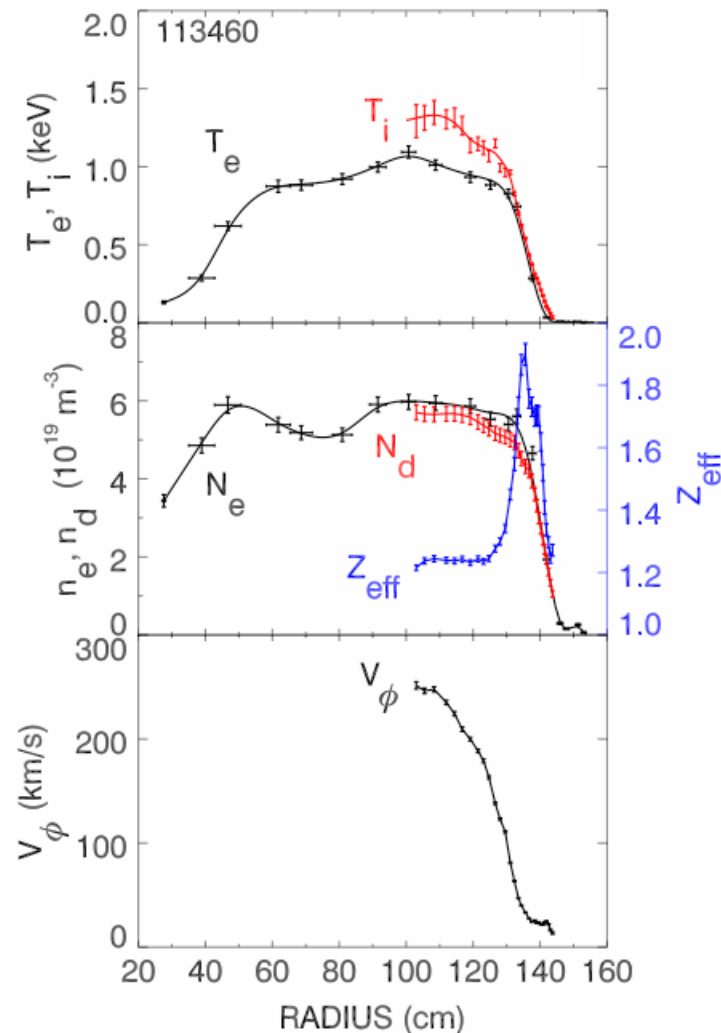


Sustained Parameters	CTF ( $\tau \gg \tau_{\text{skin}}$ )	Long Pulse Data ( $\tau > \tau_{\text{skin}}$ )
$\langle T_i \rangle / \langle T_e \rangle$	$\sim 2$	$\leq 1.5$ via co-NBI
$n_e / n_{\text{GW}}$	$\sim 0.2$	0.2 – 0.8, rising in pulse
$a / \rho_i (= 1 / \rho_i^*)$	$\sim 50$	$\sim 30$
$H_{98\text{pby}2}$	$\leq 1.5$	$\leq 1.3$ for $> \tau_{\text{skin}}$

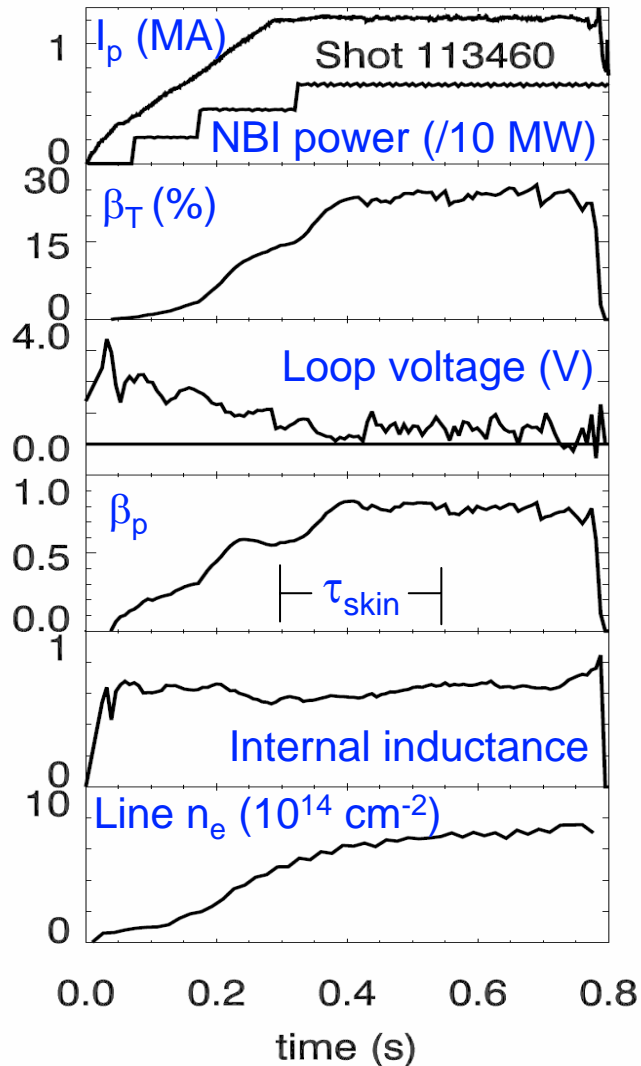
## Required Investigations

- Strongly rotating plasma with ion “internal transport barrier” via co-NBI
- Beta-exponent in scaling
- Density control at low  $n_{\text{GW}}$ , such as via lithium
- Electron transport vs.  $\beta$  effects:  $\tau_{Ee}$  [Kaye: P5.042]
- Ion transport vs. neoclassical:  $\tau_{Ei}$  [Roach: I2.006]

## Long-pulse H-mode



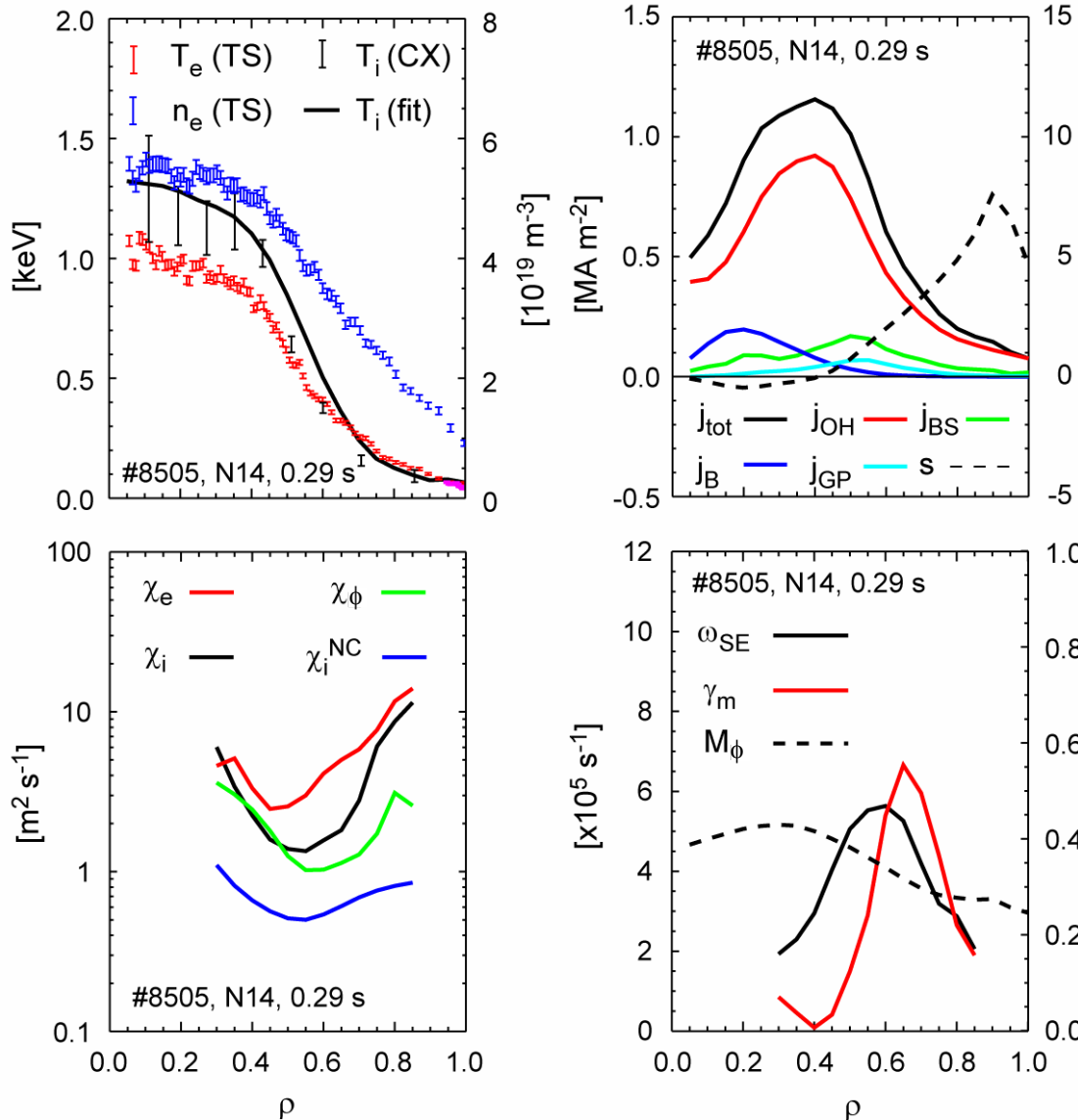
# NSTX Has Made Significant Progress Towards Goal of High- $\beta_T$ , Non-Inductive Operation



- $\tau_{I_p \text{ flattop}} \sim 2 \tau_{skin}$
- $\tau_{W \text{ flattop}} \sim 9 \tau_E$
- $\beta_T > 23\%$ ,  $\beta_N > 5.3$
- $H_{89P} \sim 2$
- Internal inductance  $\sim 0.6$
- $n_e \sim 0.5 \times 10^{13} / \text{cm}^3$
- 1.5-s pulses in 2005

[J Menard: O4.007 – NSTX progress]

# MAST Measured Sawtooth-Free L-Mode Plasma with Improved Core Confinement and Weak Central Shear, Potentially Suitable for CTF



## Transport analysis:

- $n_e/n_G \sim 0.7$ ;  $P_{\text{NBI}} \sim 1.8 \text{ MW}$
- $Q_i \sim Q_e$ ;  $T_i \geq T_e \sim 1.0 \text{ keV}$
- Hollow  $j(r)$  profile
- $\chi_i \sim 2\text{-}3 \chi_i^{\text{NC}}$  at  $\rho \sim 0.4\text{-}0.6$
- $\chi_e \sim 1\text{-}2 \chi_i$
- ExB shear  $\omega_{\text{ExB}} > \gamma^{\text{ITG}}$  at  $\rho < 0.6$

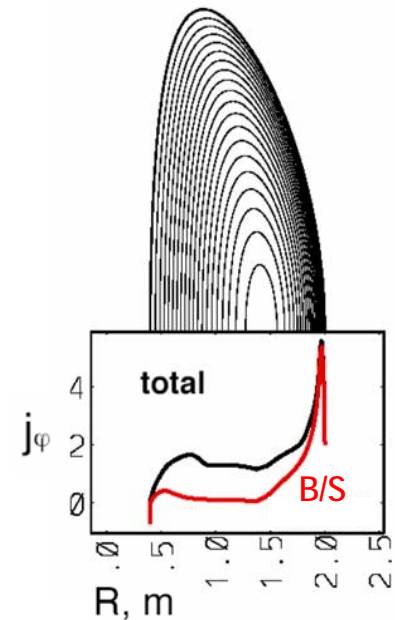


# ST Research Addresses CTF Heating & Current Drive Physics in the Same Regime



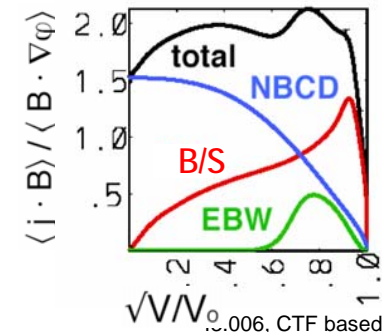
Sustained Parameters	CTF ( $\tau \gg \tau_{\text{skin}}$ )	Long Pulse Data ( $\tau > \tau_{\text{skin}}$ )
$V_{\text{Fast}}/V_{\text{Alfvén}}$	3 – 6	1 – 4
$I_{\text{CD}}/I_{\text{p}}$	~0.5	$\leq 0.3$
$I_{\text{BS+diam+PS}}/I_{\text{p}}$	~0.5	$\leq 0.6$
<b>P/R (MW/m)</b>	<b>64</b>	$\leq 9$
<b>SOL area expansion</b>	<b>10 – 20</b>	~5
<b>Radiation fraction (%)</b>	<b>~75</b>	$\leq 30$

**CTF Plasma Shape & Stable Current Profile**

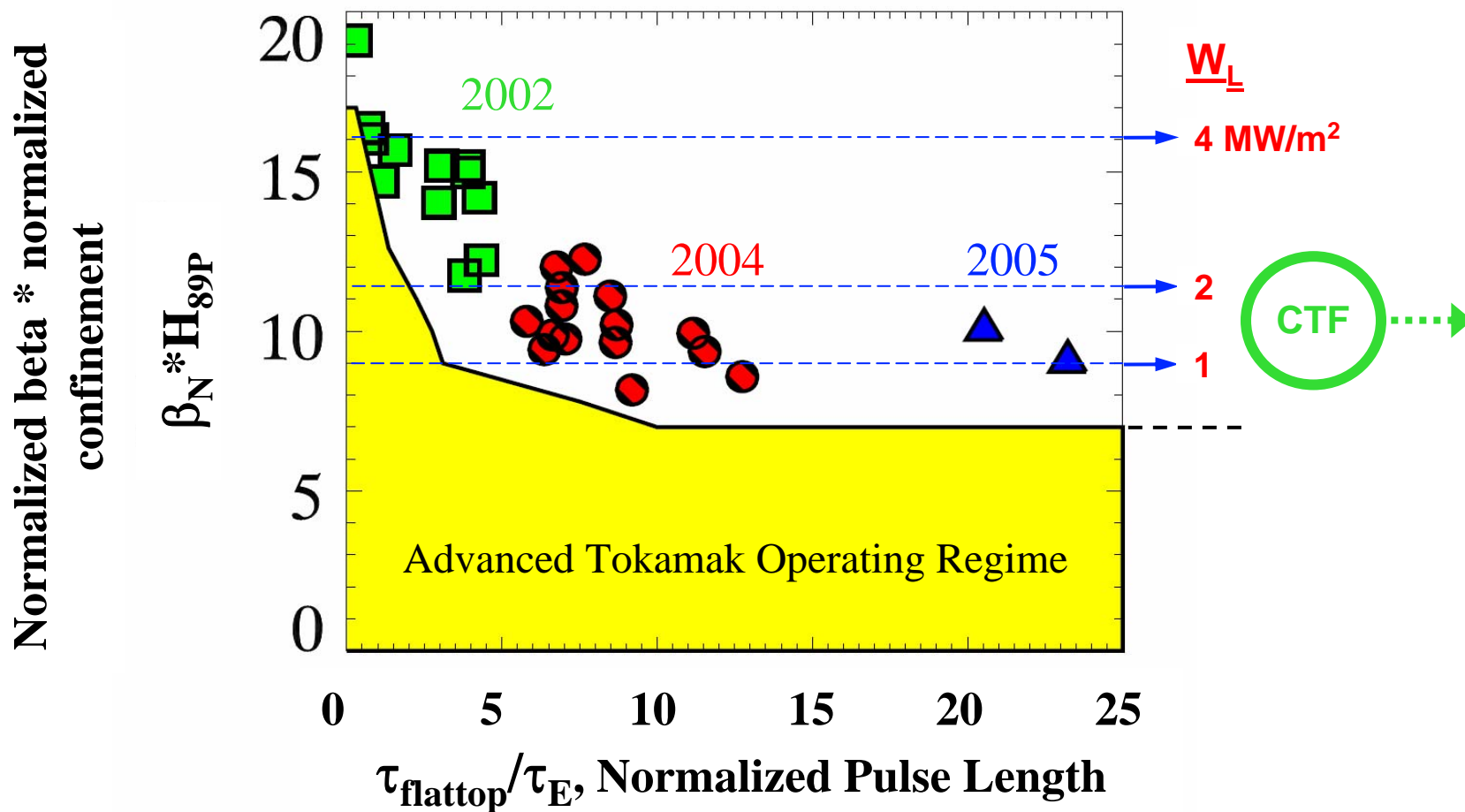


## Required Investigations

- Supra-Alfvénic ion driven modes, transport, and current
- Combined NBI-EBW, stable long-pulse operation with good confinement and substantial B/S and driven currents
- **Innovative divertor physics solutions**
  - lithium divertor (NSTX); divertor biasing (MAST)



# Normalized Plasma Performance ( $\beta_N * H_{89P}$ ) with Long Pulse Lengths on NSTX Reached the CTF Level



# CTF Technology Draws from and Extends Present Fusion Program Plans

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## To Achieve Baseline Performance (2 MW/m<sup>2</sup>)

- **Plasma facing components – twice ITER fluxes**
  - Take advantage of DEMO-relevant ITER designs
  - Needs highly reliable and remotely replaceable divertor components; explore lithium options
- **Heating, current drive, and fueling – similar to ITER**
  - Positive & negative ion beam under development by LHD, JT60U; ITER NBI R&D
  - MW-level EBW at ~70 or 140 GHz being developed and used
  - Highly reliable and remotely replaceable RF launchers
- ***Requires database from long-pulse high performance tests (Tore Supra, KStar, LHD, ITER, test stands, etc.)***

## New: TF system engineering – single turn copper

- TF center leg optimization and fabrication technology
- Multi-MA, low-voltage TF power supply

# **ST CTF Has Attractive Physics and Engineering Features to Fulfill a Critical Fusion Development Need**

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- **CTF required for developing engineering and technology basis to accelerate fusion energy development**
  - **Bridges large development gaps between ITER and Demo**
  - **Limited tritium supply necessitates CTF testing before Demo**
- **ST features fulfill the CTF mission effectively**
  - **Fast replacement of test modules**
  - **Remote access to all fusion core components**
- **ST promises good physics basis for CTF**
  - **NSTX & MAST results encouraging**
- **Additional ST physics data needs are identified**
- **CTF technology draws from and extends present fusion program plans; single-turn toroidal field coil is new**

# Comparative Costing of CTF ( $W_L=1 \text{ MW/m}^2$ ) – I (in 2002 M\$)

SuperCode Costing Components	$R_0=1.2\text{m}$ $A= 1.5$	Comments
<b>1. <u>Toroidal Device</u></b> <ul style="list-style-type: none"> <li>– TF magnets                             <ul style="list-style-type: none"> <li>• TFC center post</li> <li>• TFC outer magnet (VV)</li> </ul> </li> <li>– PF magnets</li> <li>– Device structure</li> <li>– Vacuum vessel</li> <li>– Blanket modules</li> <li>– Device, penetration shielding</li> <li>– Divertor, PFCs</li> <li>– Fueling</li> </ul>	<b>193</b> 38 (12) (26) 50 11 0 10 43 29 12	$U_{\text{TFcenter}} = \$0.075\text{M/ton}$ (single-turn cooled GlidCop) $U_{\text{TFouter}} = \$0.03\text{M/ton}$ (single-turn Al, combined with VV) $U_{\text{PF}} = \$0.058\text{M/ton}$ (no OH solenoid) $U_{\text{MS}} = \$0.052\text{M/ton}$ Combined with TFC outer conductor ITER-FEAT: 220; FIRE (reflector): 19*; CTF: basic T-breeding blankets cost 1/3 of advanced test blankets** ITER-FEAT: 109; FIRE: 42; CTF: $U_{\text{Div}} = 1.61/\text{m}^2$ ITER-FEAT: 10; FIRE: 9
<b>2. <u>Device Ancillary Systems</u></b> <ul style="list-style-type: none"> <li>– Machine assembly tooling</li> <li>– Remote handling equipment</li>   <li>– External cryostat</li> <li>– Primary heat transport</li> <li>– Thermal shield</li> </ul>	<b>187</b> 29 152  0 6 0	ITER-FEAT: 72; FIRE: 0; CTF only: $\propto R^{3/4}$ ITER-FEAT: 145; FIRE: 101; CTF only: requires high duty factor RH operation, $\propto R^{1/2}$  $U_{\text{PHT}} = \$72.3/\text{W}^{0.7}$
<b>3. <u>Tokamak Gas &amp; Coolant Systems</u></b> <ul style="list-style-type: none"> <li>– Vacuum</li> <li>– Tritium (and fuel) handling</li> <li>– Aux heat transport</li> <li>– Cryogenic plant</li> <li>– Heat rejection</li> <li>– Chemical control</li> </ul>	<b>88</b> 19 41 8 0 8 12	ITER-FEAT: 37; FIRE: 14; CTF only: $\propto R^{1/4}$ ITER-FEAT: 104; FIRE: 9; CTF only: $\propto P_F^{1/2}$ $U_{\text{AHT}} = \$33.9/\text{W}^{0.7}$

\* ITER-FEAT-FIRE Cost Comparison, Fusion Study 2002, Snowmass; \*\* Comments by M. Abdou, B. Nelson

# Comparative Costing of CTF ( $W_L=1 \text{ MW/m}^2$ ) – II (in 2002 M\$)

SuperCode Costing Components	$R_0=1.2\text{m}$ $A=1.5$	Comments
<b>4. <u>Power Supplies &amp; Control</u></b> <ul style="list-style-type: none"> <li>– Magnet power supplies                             <ul style="list-style-type: none"> <li>• <i>Resistive TFC</i> (52)</li> <li>• <i>Resistive PFC</i> (11)</li> </ul> </li> <li>– Heating system power supplies 0</li> <li>– Site electric plant, transformers, etc. 21</li> <li>– Device operational I&amp;C 36</li> </ul>	<b>120</b>	$U_{TFC} = \$0.4\text{M/MW}$ (4X conventional power supply) $U_{PFC} = \$0.13\text{M/MVA}$ Included in heating systems costs ITER-FEAT: 38; FIRE: 18 ITER-FEAT: 72; FIRE: 23
<b>5. <u>Heating, Current Drive, Diagnostics</u></b> <ul style="list-style-type: none"> <li>– ECH-EBW 40</li> <li>– NBI 125</li> <li>– LH 0</li> <li>– Plasma operational I&amp;C 45</li> </ul>	<b>210</b>	8, 10 MW @ 100 GHz, 12 MW @ 200 GHz (ITER-FEAT: 111)* 30, 33, 34 MW at ~ 400 kV (ITER-FEAT: 138) ITER-FEAT: 214; FIRE: 29
<b>6. <u>Site, Facilities and Equipment</u></b> <ul style="list-style-type: none"> <li>– Land, site improvement 0</li> <li>– Buildings 180</li> <li>– Hot cell 0</li> <li>– Radwaste management 38</li> <li>– Coolant supply and disposal 18</li> <li>– General test and qualification 16</li> <li>– Magnet fabrication tools 0</li> </ul>	<b>252</b>	Government site ITER-FEAT: 546; FIRE: 126 Included in Buildings ITER-FEAT:12; FIRE: 11 (CTF requires FNT testing at high duty factors, substantially increasing radwaste) ITER-FEAT: ?; FIRE: 18 (CTF requires acceptance verification of all incoming test components.)
<b>Total Construction Cost, no Contingency</b>	<b>1,050</b>	
<b>with 40% Contingency</b>	<b>1,470</b>	Included in the ST development cost

\* Comments by D. Rasmussen, R. Temkin