

Performance of Discharges with High Elongation and β in NSTX and Near-Term Paths Toward Steady State.

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The steady-state spherical torus is being developed for studying high-power plasma-wall interactions, for nuclear component testing, or as the core of a fusion reactor. In all cases, strong shaping and high β are required in order to maximize the bootstrap current fraction; high neutral-beam current drive efficiency is further assumed in the non-reactor scenarios. Scenario development research in NSTX has addressed the needs of these applications, by developing high- κ and β scenarios i) with the highest β_p and non-inductive fraction, ii) with the longest possible pulse for equilibrated profiles, and iii) high- β_T at large normalized current, of relevance to an ST reactor.

Waveforms for a representative discharge in each case are shown in Fig. 1, all with $\kappa \approx 2.6$ and $\delta \approx 0.8$. The discharges range from $\beta_p \sim 1$ at high current and low q^* , to $\beta_p = 1.8$ at low current. Normalized- β $\beta_N > 4.5$, exceeding the no-wall stability boundary, has been achieved for long periods, facilitated by the use of resistive wall mode (RWM) control, dynamic $n=1$ error field correction, and static $n=3$

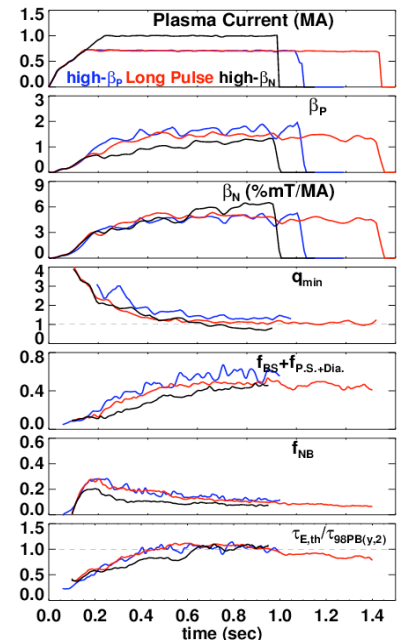


Fig1: Time evolution of high- β discharges with $\kappa \sim 2.6$.

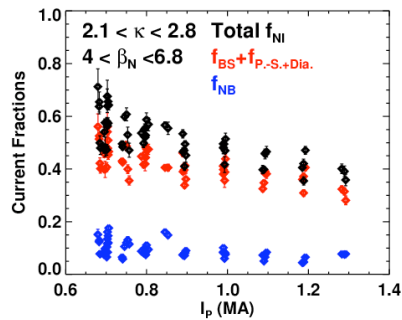


Fig 2. Non-inductive current fractions as a function of plasma current for many high-performance discharges.

error field correction [1]. The two scenarios at lower current have achieved steady-state values of $q_{\min} > 1$, which is highly desirable for avoiding core MHD, while the higher-current case evolves to $q_{\min} < 1$ before disruption. The high- β_p scenarios have NSTX record low flat-top averaged surface-voltages of 130mV. The pressure driven currents increase through the discharge as the density increases, exceeding 40% in all scenarios and 60% in the case with highest β_p . The neutral beam current fraction can approach 30% in the early, low-density phase, but the rising density decreases it to typically $\leq 15\%$ at the end of the discharge. In all cases, the confinement is comparable

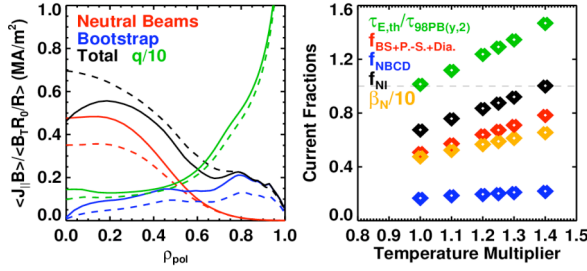


Fig. 3 left) Experimental profiles (dashed) and fully non-inductive profiles (solid) with scaled temperatures, and right) non-inductive fractions, required confinement, and normalized β , as a function of the temperature multiplier.

to or better than that predicted by the standard H-mode scaling. All of these examples utilized lithium evaporation to improve confinement [2].

The high- β_P configuration at higher toroidal field (0.48 T) reliably sustained $\beta_N \sim 5$ without disruption, using the available 6 MW of input power. The high- β_T case tended, even with the use of $n=1$ mode control, to develop RWs when the input power was too high ($\beta_N/l_i \sim 11$). Reducing the

power, however, led to a more rapid approach to $q_0=1$, typically resulting in the onset of rotating core $n=1$ modes with a large reduction in confinement. These results emphasize the need to control β near, but below, the ideal stability limit in order to maintain elevated q_{min} through increases in the bootstrap fraction and the slowing of resistive diffusion.

The current profile constituents as a function of plasma current are shown in Fig. 2. The total non-inductive fraction approaches 70% for the best 700 kA cases, but falls off approximately linearly with current. Poor confinement of the heating ions prevents increasing f_{NI} by reducing I_P in NBI heated plasmas. Predictive simulations with the TRANSP code, based on a 700 kA discharge (blue in Fig. 1), have been used to explore alternative routes to higher non-inductive fraction. The high κ & δ experimental plasma boundary was used with $Z_{eff}=3$, and the input thermal profiles scaled. This base configuration had $f_{BS}=45\%$ and $f_{NBCD}=17\%$. A 25% reduction in density, consistent with that predicted by lithium pumping with the Liquid Lithium Divertor (LLD) [3], coupled to an 18% rise increase in temperatures ($\tau_E \propto n_e^{0.4}$), resulted in f_{NBCD} increasing to 27%, but the bootstrap fraction decreased to 38%. If, however, the electron temperature changed inversely to the density, then the bootstrap current was mostly unchanged ($f_{BS}=45\%$) while the neutral beam current increased (to $f_{NB}=30\%$); the total non-inductive fraction was then $\sim 83\%$. One route to fully non-inductive operation is shown in Fig. 3, where the electron & ion temperatures were both scanned with the density fixed. Increasing the temperatures by 40% is sufficient to achieve essentially non-inductive operation, via increases in both the bootstrap and beam driven current; the final plasma had $\beta_N \approx 6.5$, and $H_{H-98}=1.5$ (for 6 MW injected beam power). Decreasing Z_{eff} to 2 leads to a 25% required increase in the temperatures for fully non-inductive operation. Achieving this increase in temperature at similar density may be possible with the LLD, if confinement increases beyond the $\sim 20\%$ improvement observed with solid lithium coatings [2]. These simulations indicate that the thermal transport response to the liquid lithium surface pumping is of critical importance in determining the impact of LLD on integrated performance. Alternatively, fast wave electron heating may provide the needed temperature increase.

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- [1] S. Sabbagh et al., Nuclear Fusion **50** 025019 (2010)
- [2] M. Bell, et al., Plasma Phys. Control Fusion **51**, 124054 (2009)
- [3] H. Kugel et al., Fusion Engineering and Design **84**, 1125 (2009)