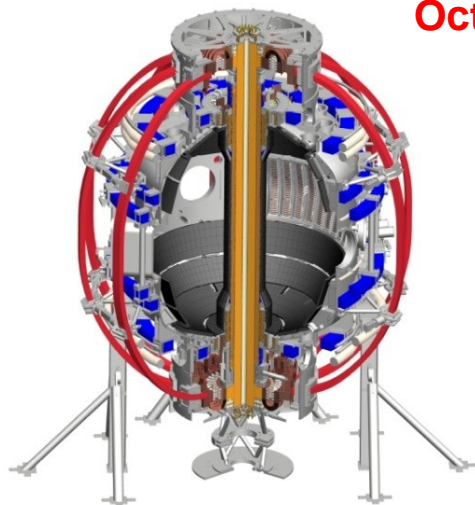


Liquid Lithium Divertor Characteristics and Plasma-Material Interactions in NSTX High-Performance Plasmas

MA Jaworski, T. Abrams, J.P. Allain, M.G. Bell, R.E. Bell, A. Diallo, T.K. Gray, S.P. Gerhardt, R. Kaita, J. Kallman, H.W. Kugel, B.P. LeBlanc, R. Maingi, A.G. McLean, J. Menard, R. Nygren, M. Ono, S.F. Paul, M. Podesta, A.L. Roquemore, S.A. Sabbagh, F. Scotti, C.H. Skinner, V.A. Soukhanovskii, D.P. Stotler, and the NSTX Team

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Why liquids? Because solids may not extrapolate

- Two major failure modes for solids that are known:

- Melting (transient heat loads)
- Net-reshaping (erosion, migration, redeposition)

- Some speculative failure modes:

- Neutron-PMI synergistic effects (aside from bulk material changes)
- Steady-state, self-regulating walls?



B. Lipschultz, et al., "Tungsten melt effects on C-MOD operation & material characteristics", 20-PSI, Aachen, Germany, May, 2012.



Coenen, et al., "Evolution of surface melt damage, its influence on plasma performance and prospects of recovery", 20-PSI, Aachen, Germany, May, 2012.

Klimov, et al., JNM **390-391** (2009) 721.

Wall erosion/redeposition not mitigated by divertor configuration

Table 1

Rough estimate of net erosion rate of main walls based on assumptions in text. Assumes 100% wall coverage by Be, B, C or W.

Device	P_{heat} (MW)	τ_{annual} (s/yr)	$E_{\text{load}}^{\text{year}}$ (TJ/yr)	Beryllium net wall erosion rate (kg/yr)	Boron net wall erosion rate (kg/yr)	Carbon net wall erosion rate (kg/yr)	Tungsten net wall erosion rate (kg/yr)
DIII-D	20	10^4	0.2	0.13	0.11	0.08	0.16
JT 60SA	34	10^4	0.34	0.22	0.19	0.15	0.27
EAST	24	10^5	2.4	1.6	1.2	0.82	1.8
ITER	100	10^6	100	77 (29) ^a	64	44 (53) ^a	92 (41) ^a
FDF	100	10^7	1000	610	500	340	740
Reactor	400	2.5×10^7	10,000	6500 (21,000) ^b	5300	3700	7900 (5000) ^b

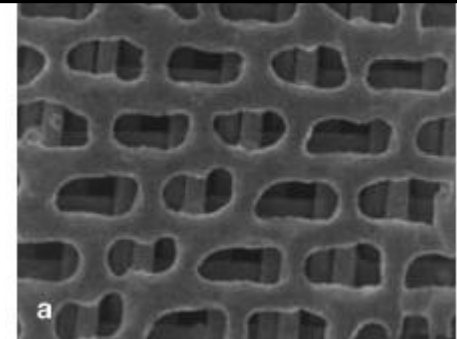
P.C. Stangeby, et al., JNM 415 (2011) S278.

- Charge-exchange processes create steady wall-flux
- Low density plasma at first wall reduces local redeposition
- **1000s of kgs** of eroded material migrating around tokamak vessel
- Likely to redeposit in locations where cooler plasmas exist or behind baffled areas of machine
- Do PFCs remain functional with large amounts of redeposited material?
 - **Need very high duty-factor to even study the problem!**

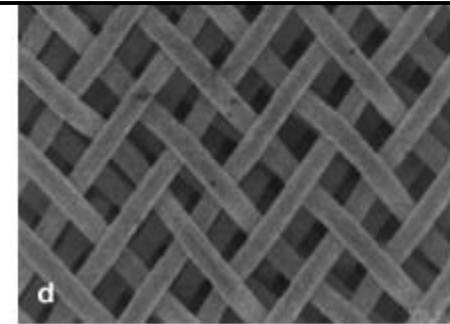
Liquids already shown to outperform solids in some areas

- Red Star Capillary-Porous-System (CPS) long-since shown to resist melting damage – protect the substrate
 - CPS surface consists of metal mesh wicking structure (Mo mesh)
 - Capillary forces maintain liquid lithium on plasma-facing surface
- Also shown to absorb, in steady-state, 1-25 MW/m²
 - Electron beam heating of the surface
 - Tests lasted between 30s-10min
- In principle, all PFCs in fully-flowing system will return to an equilibrium position (i.e. self-healing)

Exposed w/o Li



Exposed w/ Li

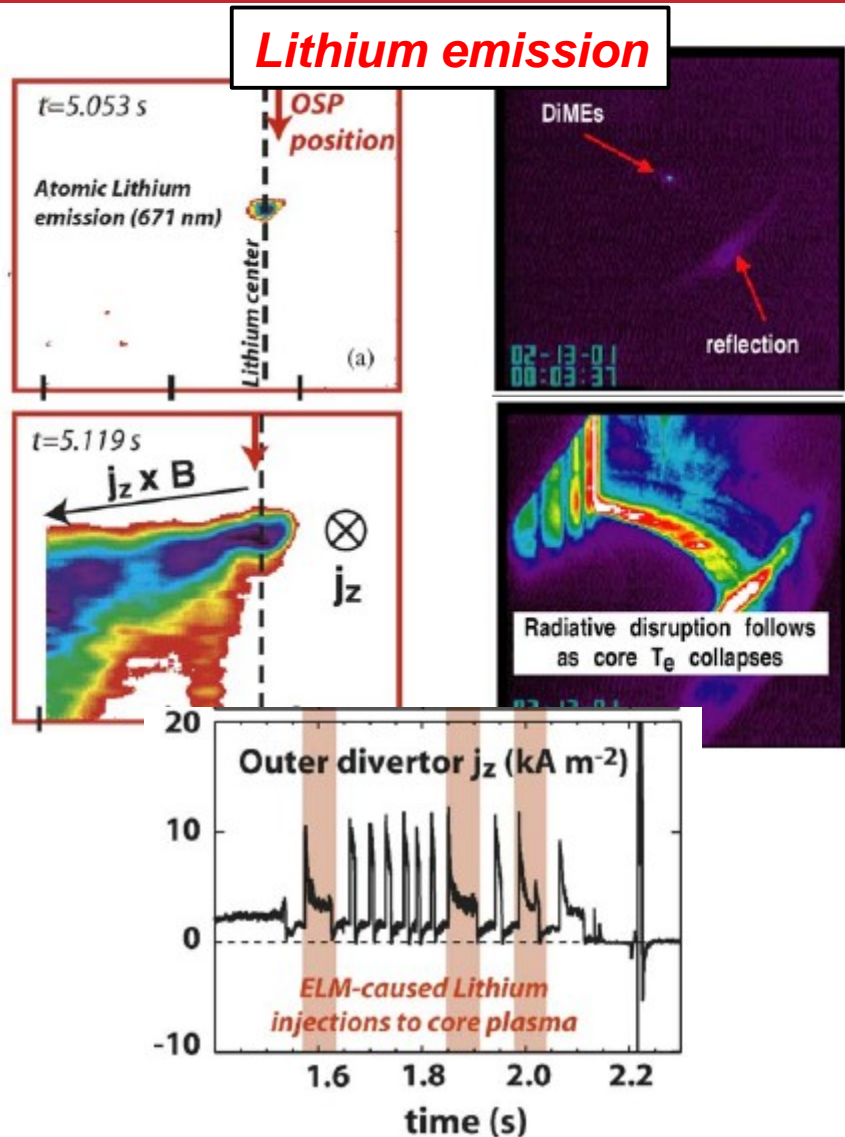


CPS Mo meshes after plasma exposure. Top did not have lithium fill during exposure. 15-100µm pores

Evtikhin, et al., J. Nucl. Mater. 271-272 (1999) 396.

Stability of the free-surface LM is critical

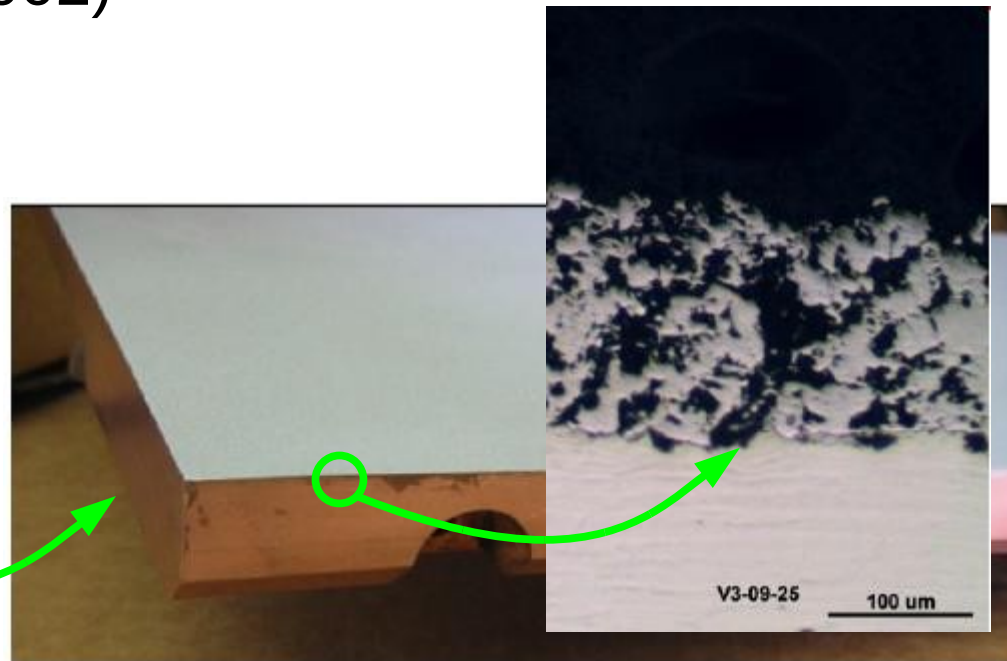
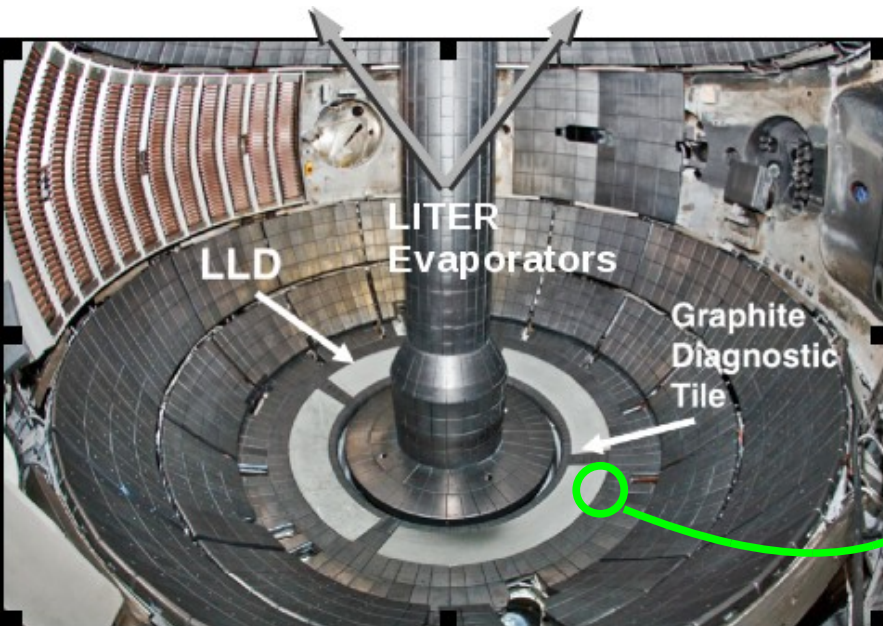
- DIII-D Li-DIMES experiments ended in plasma disruption
 - Introduced small sample of Li into divertor of DIII-D
 - Current perturbations measured up to 10 kA/m^2
 - Li plume observed when lithium ejected from sample holder
 - Disruption shortly follows lithium ejection
- If relying on LM to protect substrate, need robust solution
 - Protect against steady-state and transient events
 - **We show NSTX LLD exhibits stability in the divertor**



Whyte, et al., Fusion Eng. Des. **72** (2004) 133.

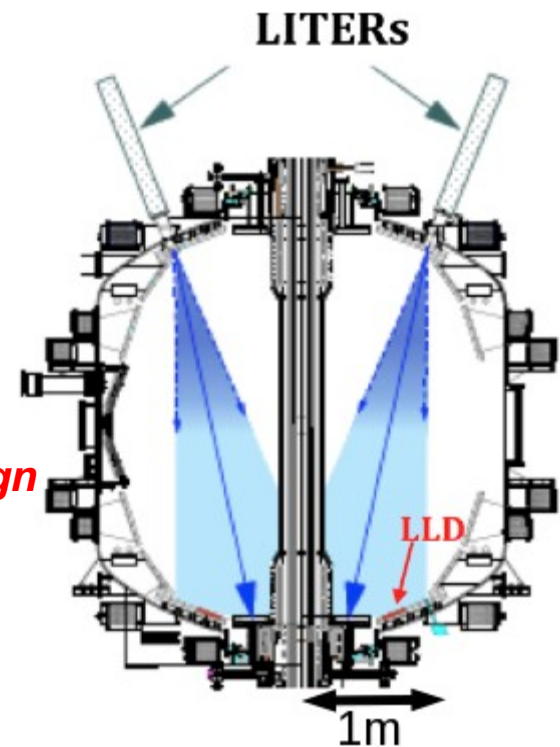
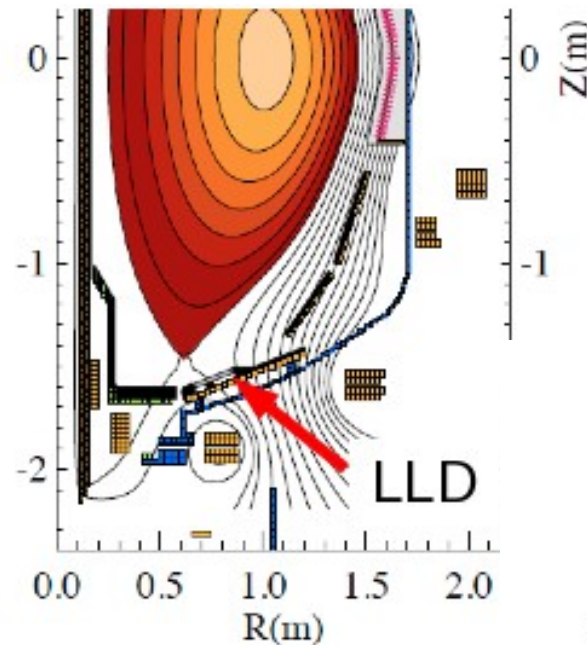
NSTX experience with the Liquid Lithium Divertor

- Liquid lithium divertor installed for FY2010 run campaign
- 2.2cm copper substrate, 250 μ m SS 316, ~150 μ m flame-sprayed molybdenum, loaded via LITER evaporators
- 37g estimated capacity, 60g loaded by end of run campaign
- Motivated to explore liquid lithium pumping of deuterium (c.f. Baldwin, *et al.* Nucl. Fusion 2002)



Overview of experiments

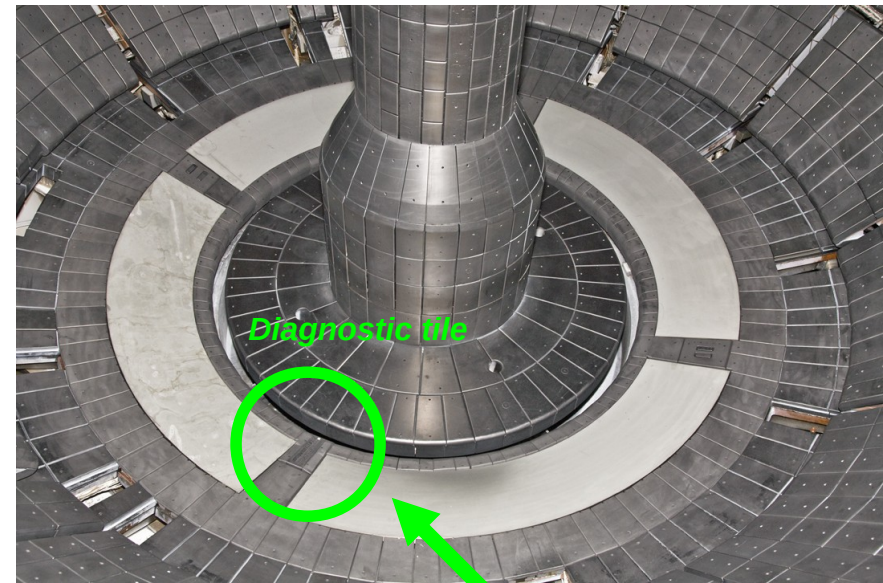
- Experiments diverting onto the LLD occurred throughout run campaign
- Either diverted onto LLD or just inboard on ATJ graphite
- LITER only available filling method for the LLD
 - 7% filling efficiency estimated
 - Always coating entire lower divertor in addition to LLD
- Database of shots taken throughout run year



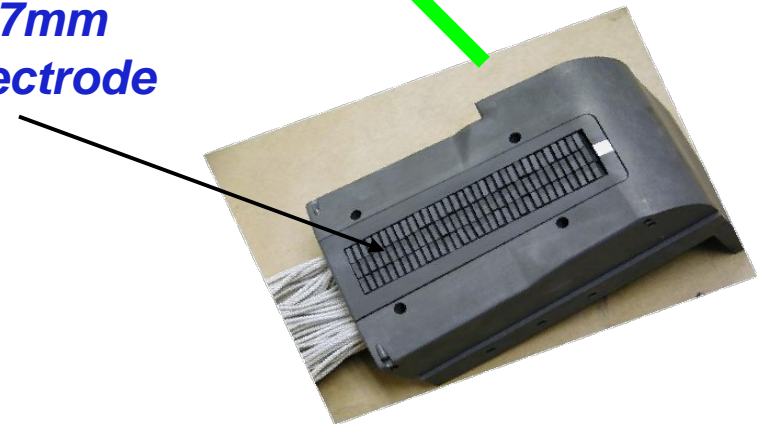
No boronization campaign prior to lithium introduction
Database already starts with 60g inventory in vessel

High-density Langmuir probe array installed for divertor plasma characterization

- Liquid Lithium Divertor (LLD) installed to study lithium plasma-material interactions
- Probe array characterizes local plasma properties in a range of experiments
- Provides high spatial density of measurements
- Oblique incidence yields smaller effective probe size



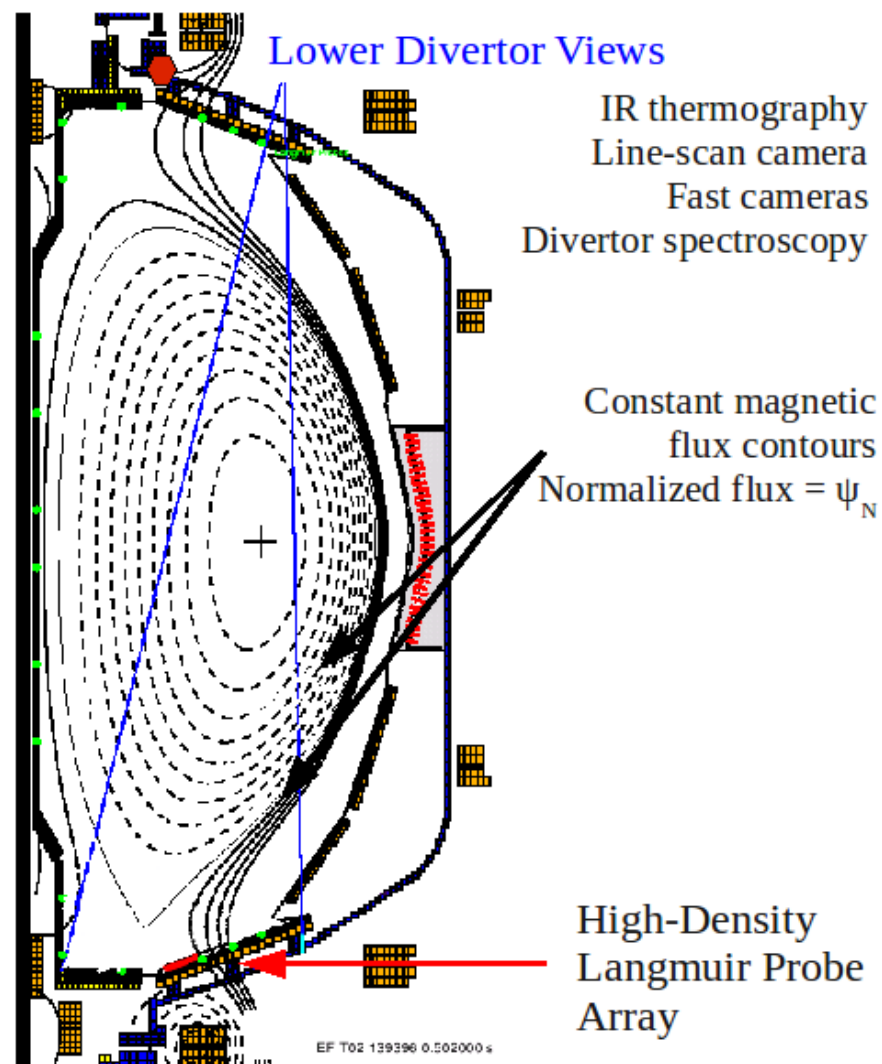
**2x7mm
electrode**



**J Kallman, RSI 2010
MA Jaworski, RSI 2010**

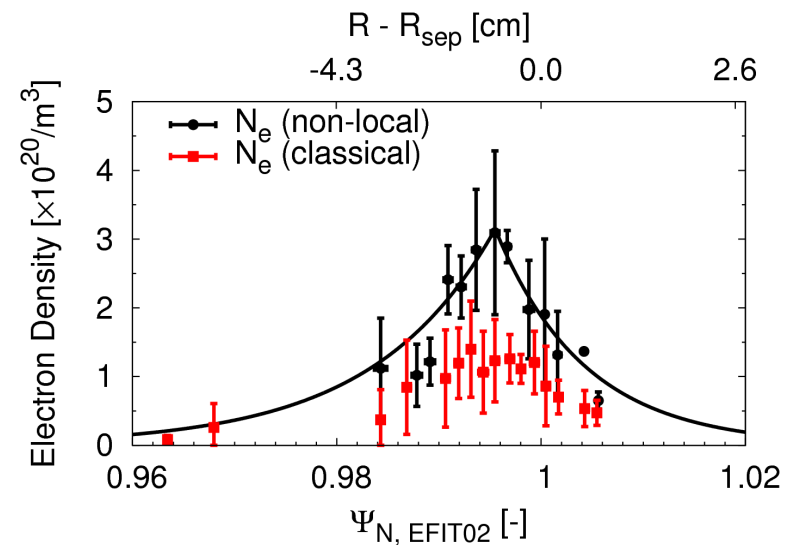
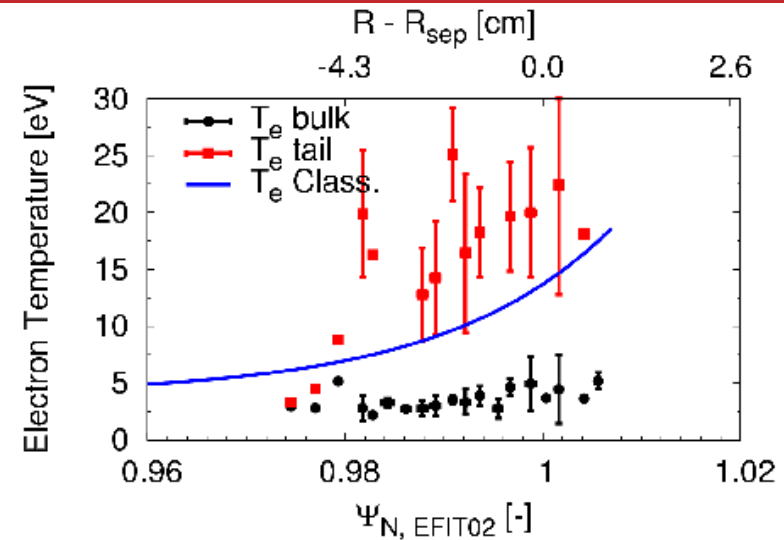
Empirical plasma reconstruction provides framework for checking consistency between diagnostics

- Utilizes measured data points as starting point in constraining plasma models to fill the gaps between diagnostics
- Solution improves as more and more data constrains background
- OEDGE code suite used here: Onion-Skin Method (OSM2)+EIRENE+DIVIMP
 - OSM2 solves plasma fluid equations
 - EIRENE performs Monte Carlo neutral hydrogen transport, iteratively coupled to OSM2
 - DIVIMP performs Monte Carlo impurity transport
- Utilized here to compare probe interpretation methods against other diagnostics



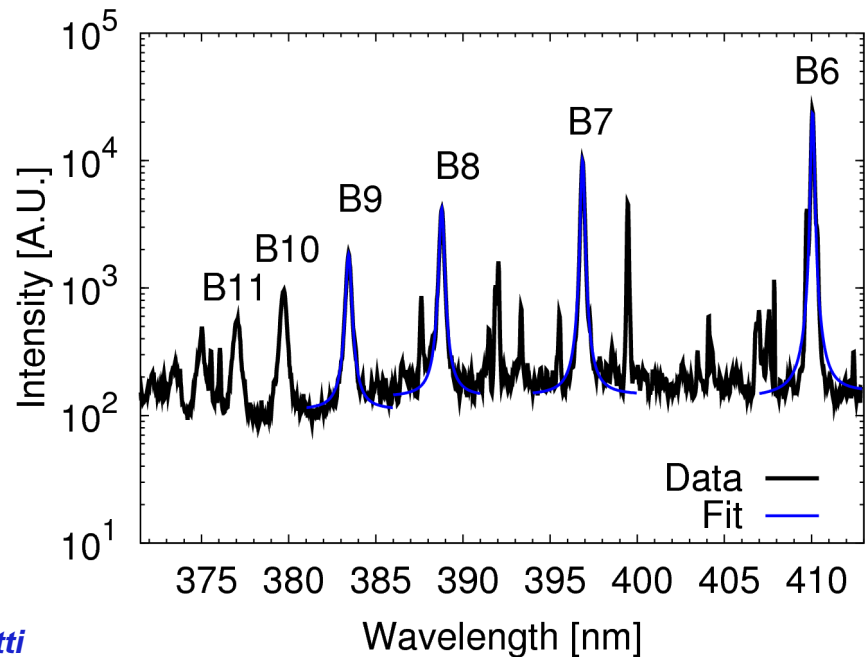
Accurate diagnosis of plasma parameters critical to assessing local PMI

- Plasma motion sweeps out profile during discharge, data aggregated and averaged
 - Nominal equilibrium separatrix location at $\psi_N = 1.0$
 - I_{sat} peak provides indicator of LP-based separatrix location
- Significant temperature variance between interpretation methods
 - 10-20eV temperatures with classical method
 - 2-5eV temperatures with non-local interpretation
- Lower temperatures result in higher densities with kinetic interpretation

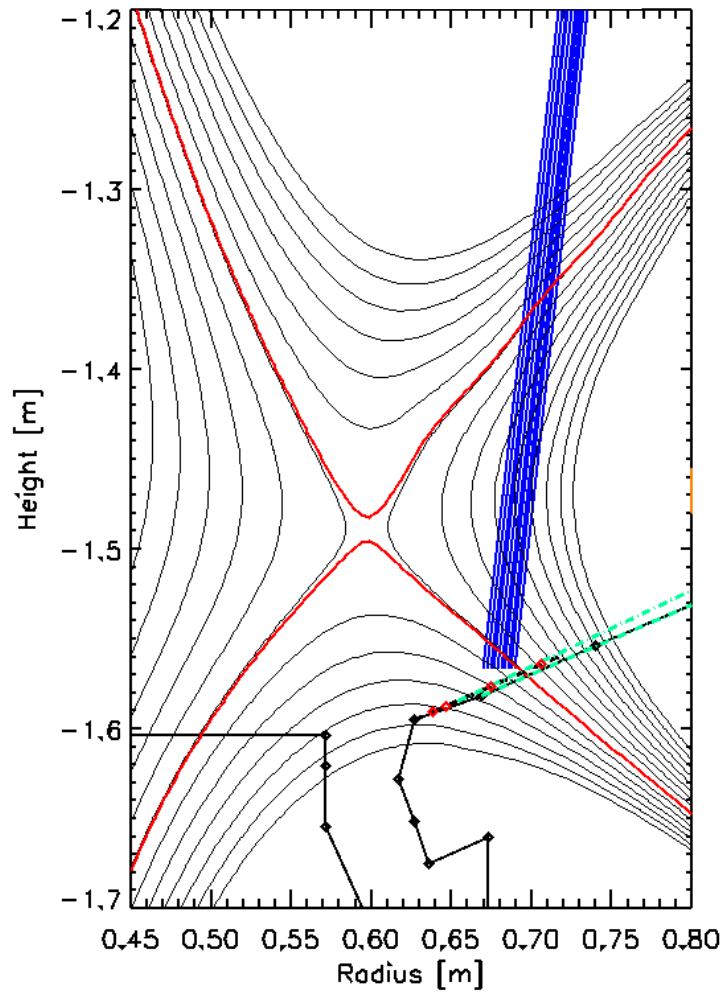


Density measurement from spectroscopy first confirmation of kinetic probe interpretation

- Divertor spectrometer viewing strike-point region during discharge
- Deuterium Balmer lines shown in spectra
- Pressure broadening analysis indicates density of $3.6 \times 10^{20} \text{ m}^{-3}$
 - Existence of high-n Balmer lines indicates low temperature

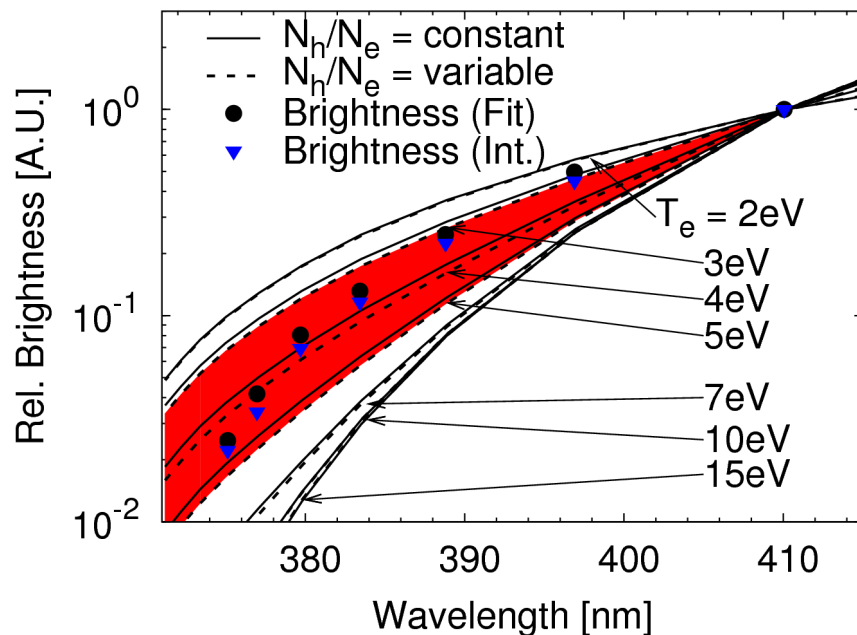
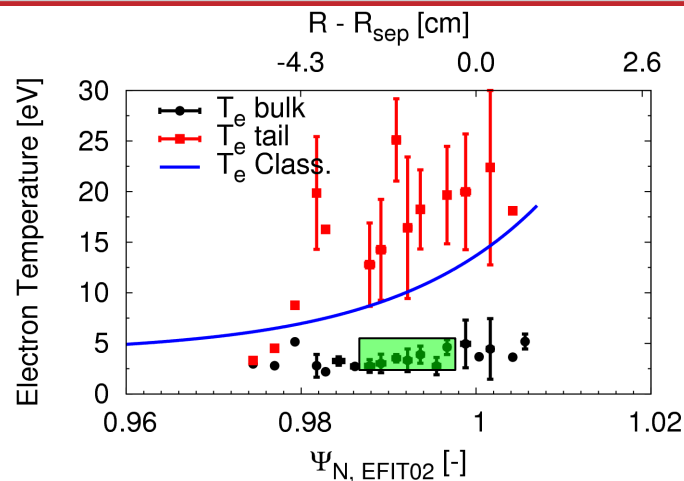
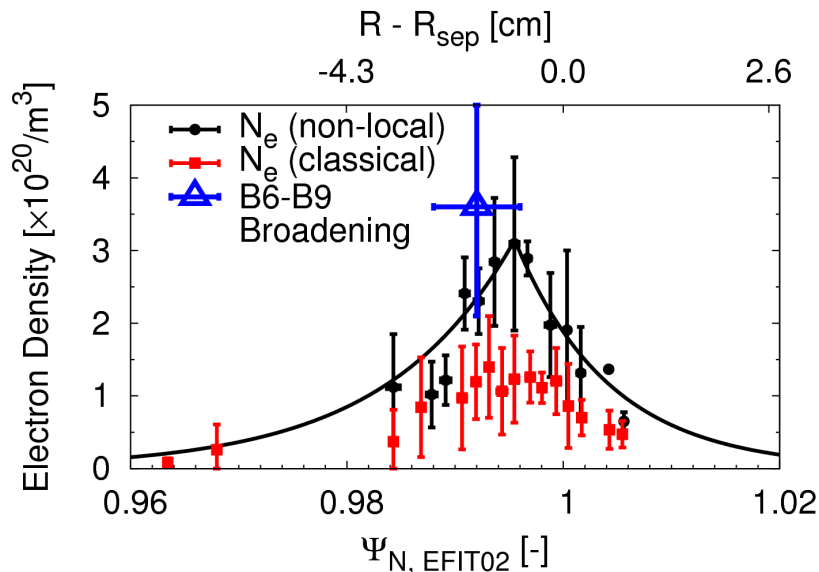


Divertor spectrometer view



Broadening measurement and modeling of hydrogen spectrum consistent with kinetic interpretation

- Pressure broadening yields density
- OEDGE plasma+neutral solution provides local parameters
- Collisional-radiative model by D. Stotler calculates excited state populations
- Brightness ratios normalized to B6 consistent with 3-5eV



Empirical reconstruction indicates classical values for the sheath heat transmission coeff. obtained with bulk T_e

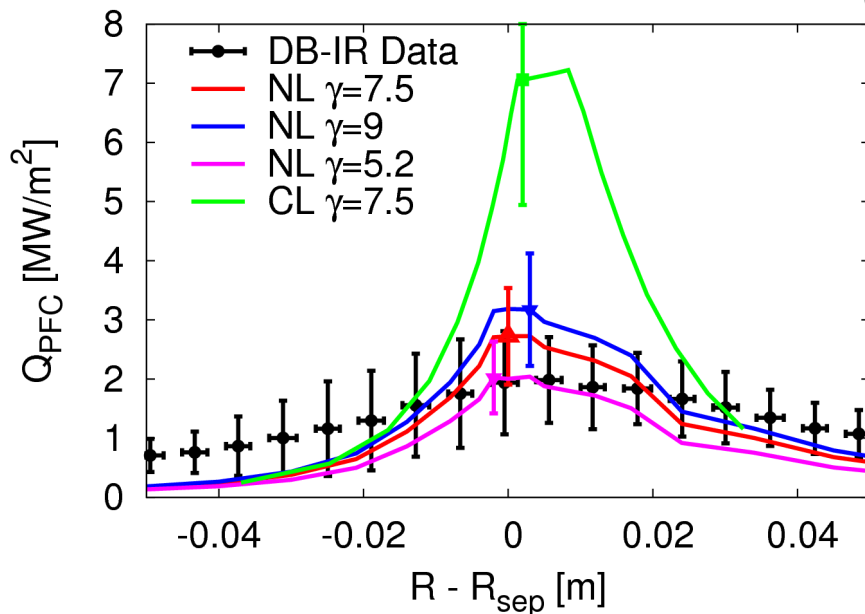
- Sheath heat transmission coefficient, γ , determines the amount of power transferred to a material surface
 - Fluid theory provides theoretical minimum of 5.2 for D plasma¹
 - Previous experiments often indicate lower γ (e.g. $\gamma \sim 2$)^{2,3}
- Calculated γ depends sensitively on T_e
- OEDGE (OSM2 + EIRENE) background plasma created from LP data
 - Total heat flux to PFCs calculated using plasma, neutrals and rad.
 - Bi-modal distribution $\gamma \sim 9$ estimated from multi-component plasma
- Dual-band IR heat flux⁴ indicates non-local interpretation in better agreement

$$q_{classical} = \gamma \Gamma k T_e = \gamma \frac{j_{sat}^+}{e} (k T_e)$$

$$\gamma(V) = -\frac{eV}{kT_e} + 2.5 \frac{T_i}{T_e} + \dots$$

$$2 \left[\left(1 + \frac{T_i}{T_e} \right) \left(\frac{2\pi m_e}{m_i} \right) \right]^{-1/2} e^{\frac{eV}{kT_e}}$$

$$\gamma_{min,D} \approx 5.2 \quad \gamma = \frac{q_{tot}}{\Gamma k T_e}$$



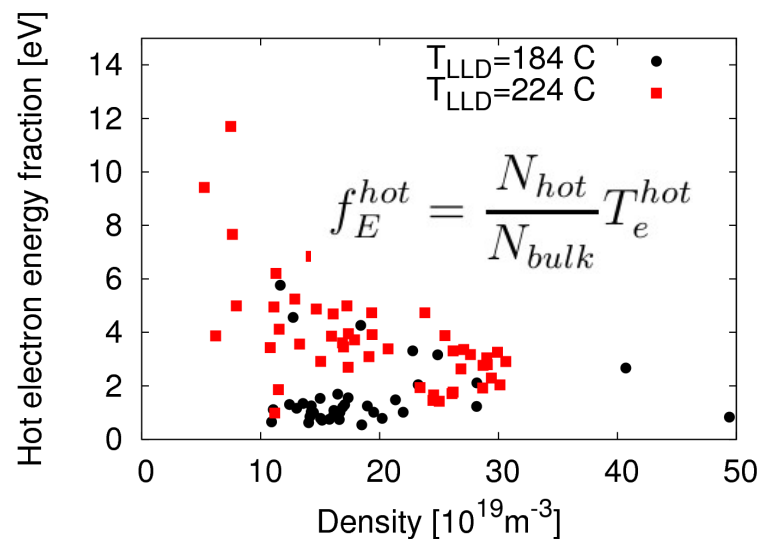
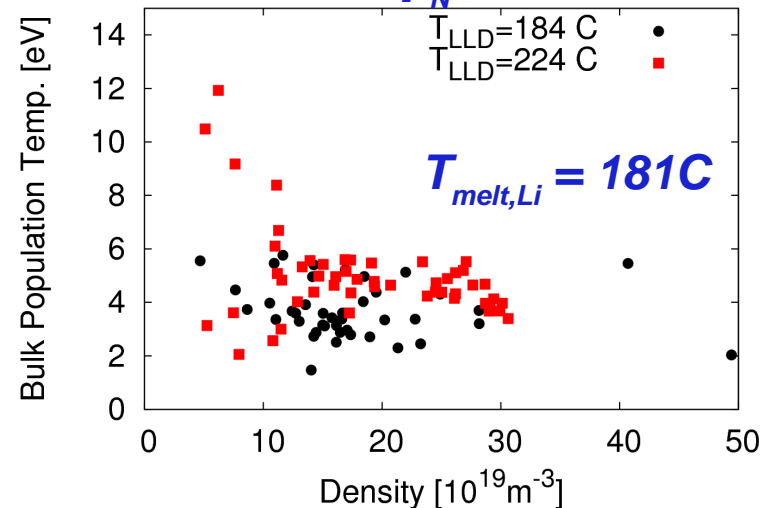
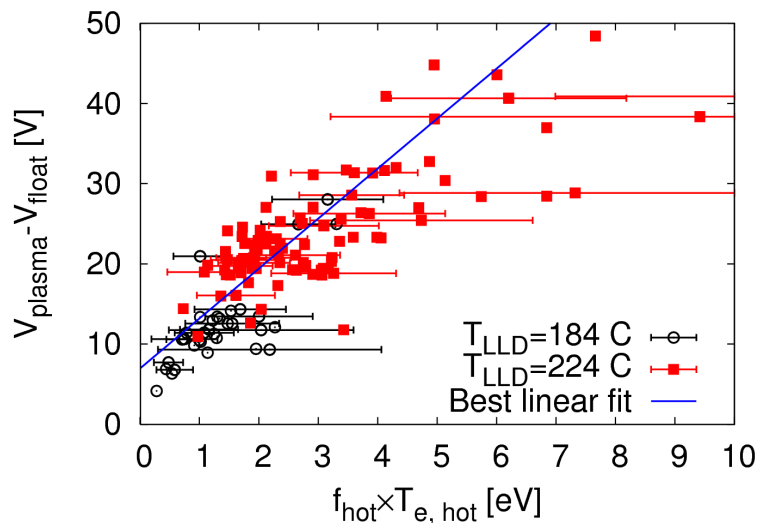
¹ PC Stangeby, 2000, *ibid.*; ² D Buchenauer, JNM, 1992;

³ J Kallman, PP9.00043; ⁴ AG McLean, PP9.00069

Distribution function analysis indicates some local changes in plasma conditions on plasma-heated LLD

- Discharge sequence repeatedly heated and plasma-conditioned the LLD surface
- Local plasma temperatures elevated with hotter LLD surface temperature ($T_{LLD} > T_{melt,Li}$)
- Increase in plasma temperatures correlated with increase in $V_p - V_f$ potential difference¹
- Understanding the changes during lithium experiments requires us to first find some model for the non-Maxwellian distributions...

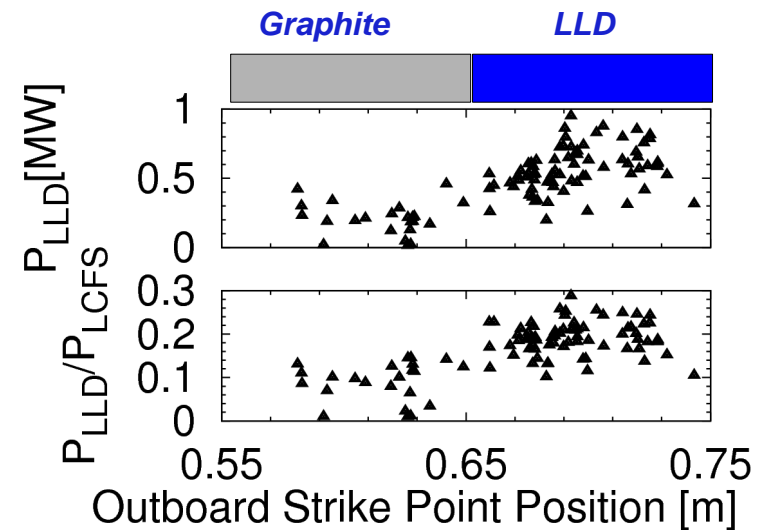
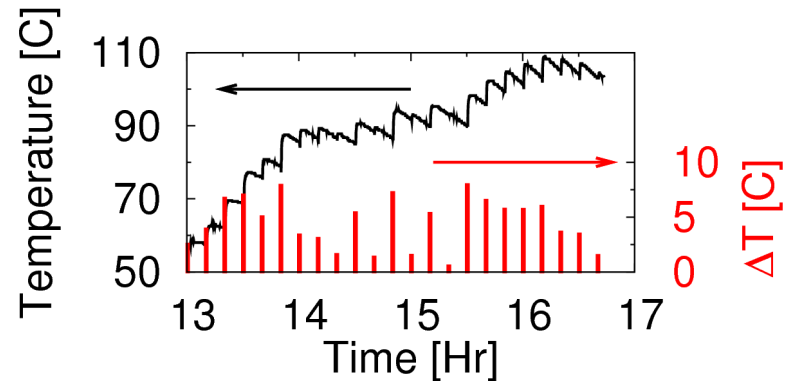
Comparisons made on identical ψ_N locations



¹Jaworski et al., *Fusion Eng. Des.* **87** (2012) 1711.

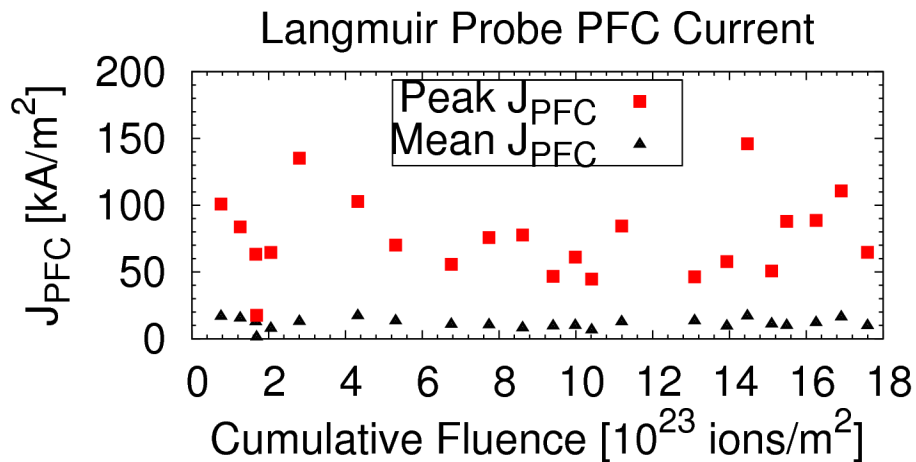
Significant power onto LLD measured

- Embedded thermocouples provide measure of temperature changes from before and after discharge
- Each plate is 43kg of copper
 - $\Delta E = mc_p \Delta T$ per plate
 - $P_{LLD} \sim 4\Delta E / \tau_{pulse}$
 - $P_{LCFS} = P_{NBI} + P_{OHM} - P_{RAD} - dW/dt$
- LLD absorbing about 25% of exhaust power
 - $\sim 1\text{MW}$ in some cases
- No molybdenum observed in the plasma after melted (Soukhanovskii, **RSI**, 2010)

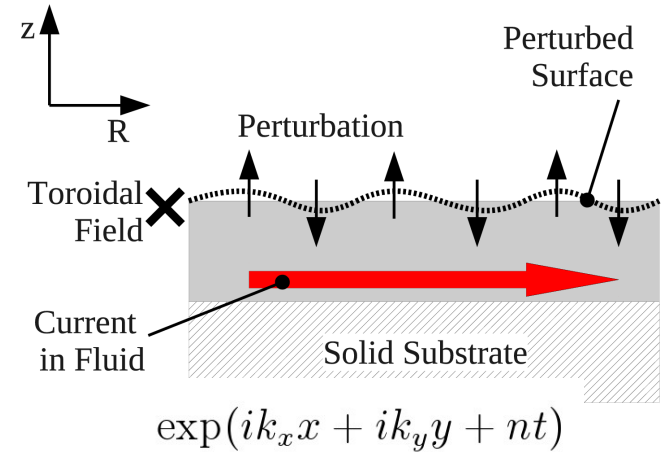


Jaworski, et al., IAEA FEC 2012

No macroscopic ejection of lithium observed; Demonstration of Stable Operation of LM PFC in Divertor Configuration

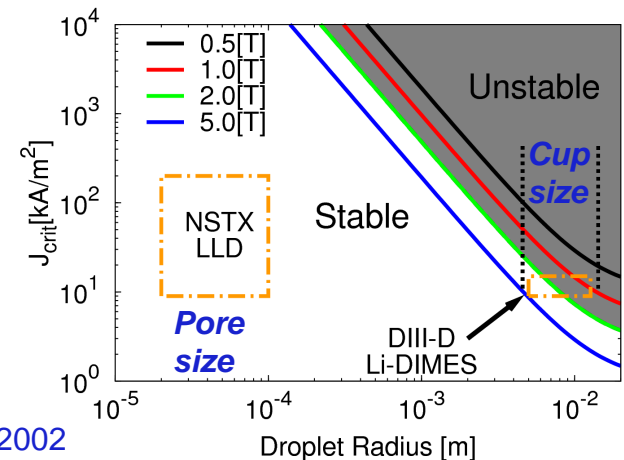


- Large transient currents measured with Langmuir probes
- Magnetized Raleigh-Taylor analysis provides stability curves
- Indicates strong stabilization expected with small feature sizes
- CPS tests also reduced droplet ejection with smaller pore sizes*



$$n^2 = k(jB/\rho - g) \left[1 - \frac{k^2 \Sigma}{(jB/\rho - g)\rho} - \frac{B^2 k_x^2}{2\pi\mu_0(jB/\rho - g)\rho k} \right]$$

$$k_{Cr} = \sqrt{\frac{jB - \rho g}{\Sigma}} \quad \text{For the fastest growing modes}$$



Jaworski JNM 2011, Jaworski IAEA FEC 2012, Whyte FED 2004, *Evtikhin JNM 2002

Surface contamination indicates this was not a “fair” test of a liquid lithium PFC

- Divertor filterscopes provide indicator of impurities
 - Relative fraction of impurity should be reflected in sputter yield
 - Particle flux proportional to power
- Normalization against flux indicates no difference diverted onto the LLD
- Plasma cleaning in PISCES-B did show oxygen reduction*
 - 400s, $T > 600K$
 - LLD transiently exceeded these temperatures, but not steady

What is relevant time scale?

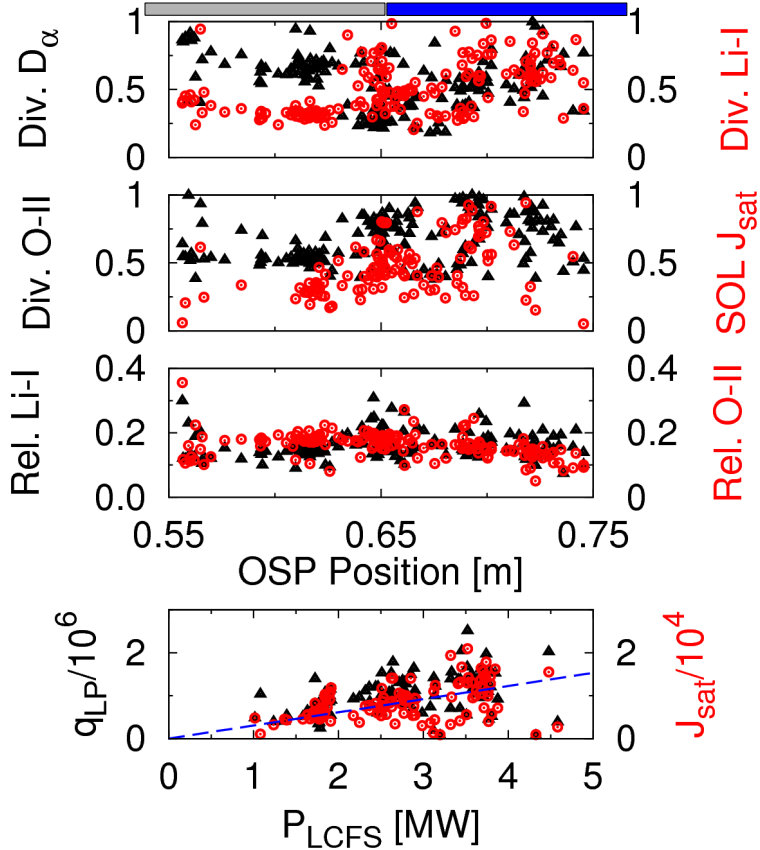
$$\epsilon_{imp} \propto N_{imp} \propto Y_{imp} J_{sat}$$

$$Y_{imp} \propto Y_{imp}^0 \theta_{imp}$$

$$P \propto \gamma J_{sat} T_e$$

$$\theta_{imp} \propto \frac{\epsilon_{imp}}{P}$$

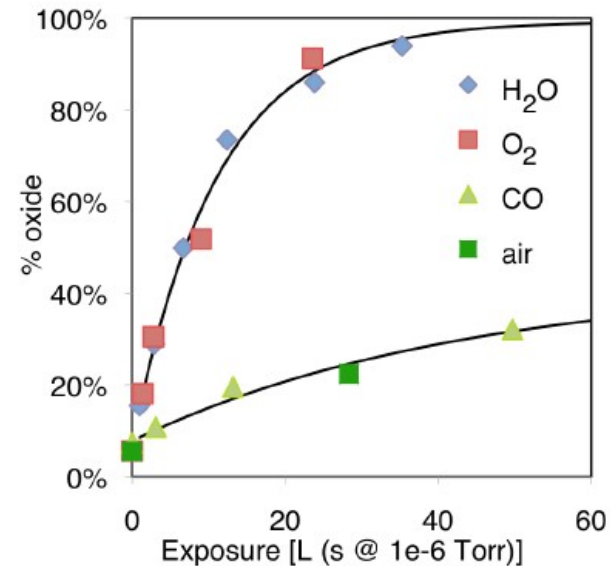
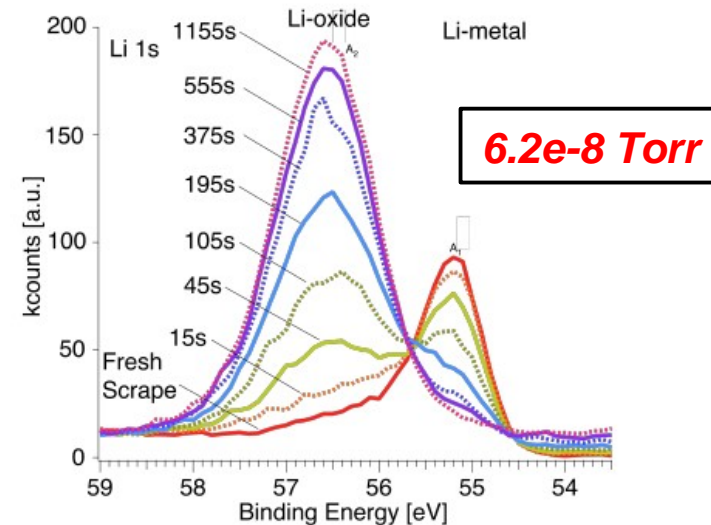
Emission ϵ
Coverage θ
Divertor Power P



Jaworski IAEA FEC 2012, *Baldwin NF 2002.

Laboratory studies show rapid contamination

- New surface science laboratories at PPPL via Princeton Univ. collaboration
- High Resolution X-ray Photo-Spectroscopy (HR-XPS) measurements
 - Measure amount of oxide vs. clean lithium metal on TZM substrate
 - Expose to different gases
- Significant oxidation in 20s @ $1e-6$ Torr partial pressure O_2 , H_2O
 - NSTX intershot pressure $\sim 1e-7$ Torr
 - $\tau_{\text{intershot}} \sim \tau_{\text{oxidize}}$ indicates oxidation likely

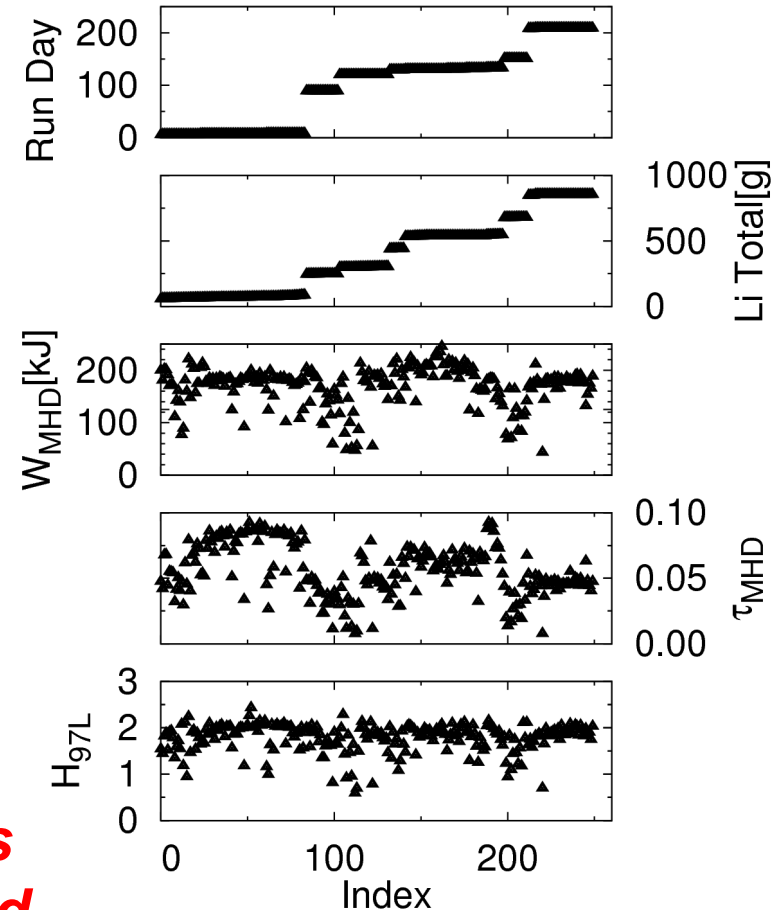


Skinner, et al., 20th PSI, submitted to JNM.

Performance should be independent of lithium quantity *if* surface contamination is key variable

- FY2010 LLD experimental set
 - Experiments span 60g to nearly 1kg of deposited lithium
 - Includes 75hr deposition at mid-year
 - Calculate ITER 97L H-factor *average* from 400-600ms for each discharge
- Discharges look about the same between start and end of run
 - Consistent with surface contamination hypothesis

Fully-flowing PFC can provide a means of sweeping away gettered material and creating “stationary” surface conditions.



Flowing system studies are being pursued in the US

- Thermoelectric MHD systems

- “Passive” pumping
- Mixed convective/conductive heat removal scheme
- U-Illinois LIMIT

- Actively-supplied, capillary-restrained systems

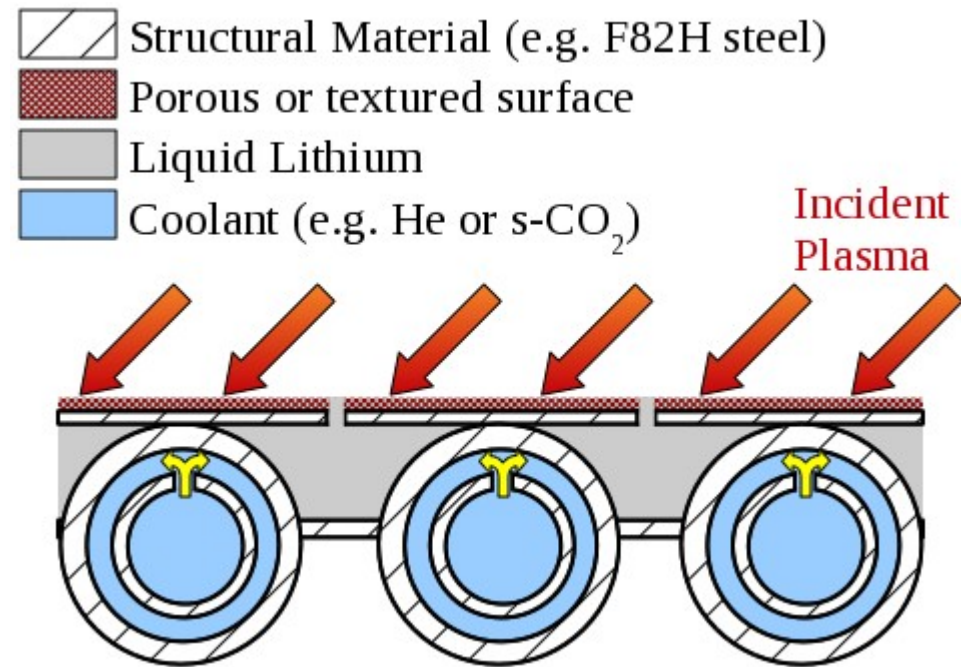
- Thin layers of liquid metal
- Conduction dominated
- PPPL efforts

- Fundamental studies of interface dynamics, wetting, surface chemistry

- “Liquid Metals as Plasma-Facing Materials for Fusion Energy Systems: From Atoms to Tokamaks” -H. Stone (Princeton U)
- Newly funded work this year

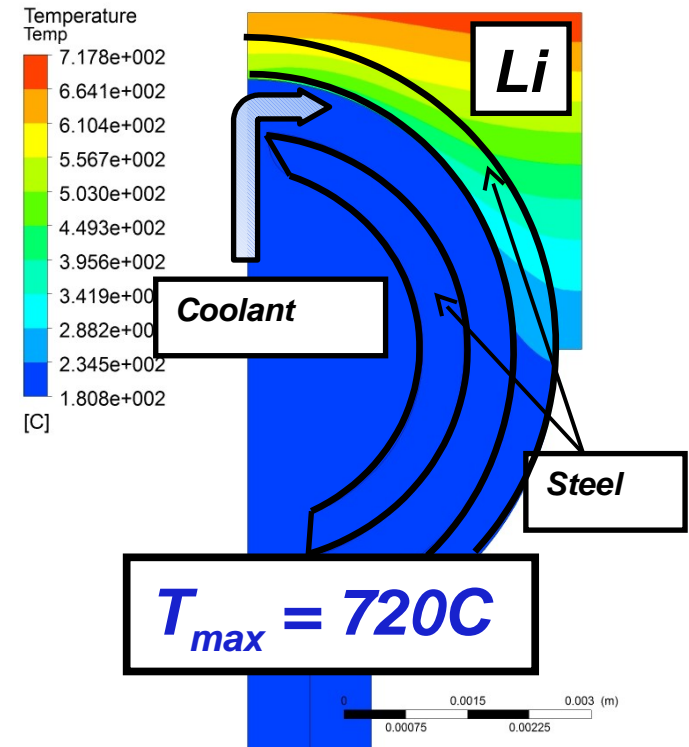
Active supply, capillary-restrained systems (PPPL)

- Hybrid approach to join flow-thru loop with active cooling
 - Leverage numerous results an experience with thin, capillary-restrained concepts
 - Maintain thin structures (as thin as possible) to maximize heat transfer to coolant
- Modular approach considered to provide optimization space
 - T-tube concept shown, other gas cooling schemes available (e.g. SOFIT, vapor-box/heat pipes)
 - Surface could be flame-sprayed or other scheme (e.g. laser textured)



Current work-in-progress: steel with low-Z lithium coating

- T-tube size reduction to reduced required wall thickness, s-CO₂ coolant
- F82H steel properties with liquid lithium
 - Liquid lithium evaporative cooling included
 - 10 MW/m² heat flux simulated, no nuclear heat
 - No provision for plasma response
- Steel structure maintained below ~650C, close to range for ODS-steel operation*



**Still optimizing/developing 3D solution,
720C might be too hot****

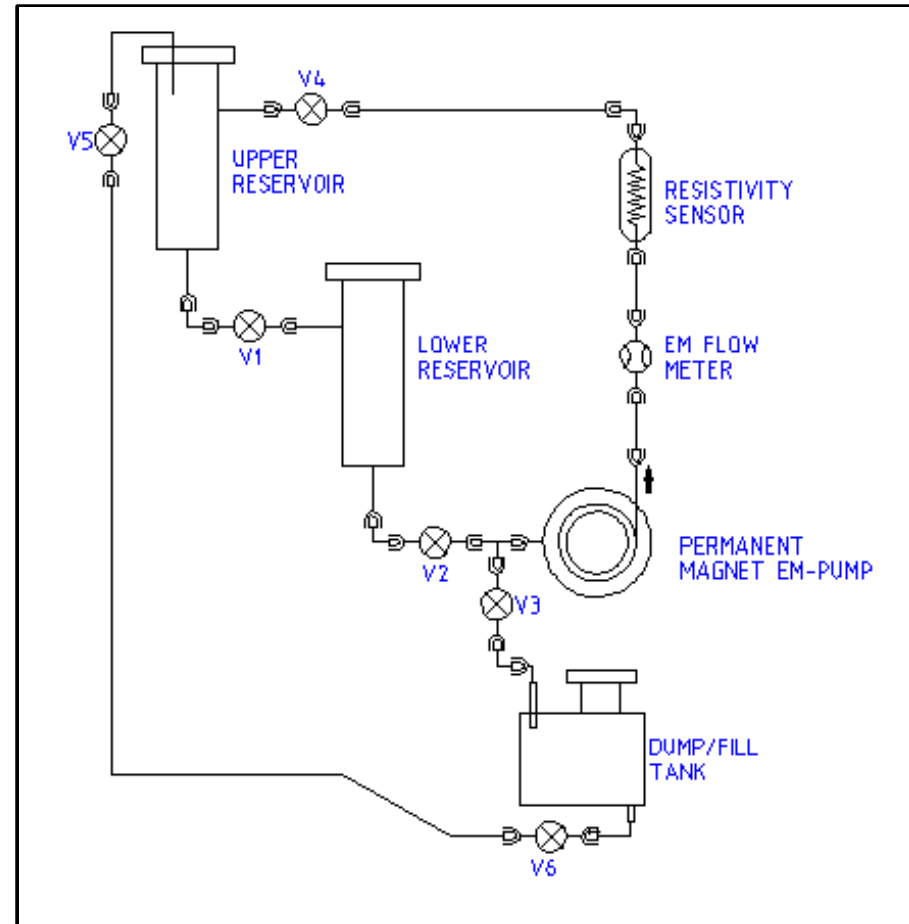
*Zinkle,, Ghoniem, Fusion Eng. Des. **51-52** (2000) 55.

Apiccella, et al., PPCF **54 (2011) 035001.

Experiment construction underway to provide testbed for PFCs and demonstration of necessary technologies

- Liquid lithium loop for experimental demonstration
 - Safe operation of loop
 - Robust operation and maintainability
 - Develop control systems, handling procedures
 - Look toward integration with tokamak systems
- PFC proof-of-principle tests
 - Couple to vacuum system
 - Demonstrate LM concepts in relevant vacuum environment

Liquid Lithium Test Stand Loop Diagram



Liquid metal research proceeding on multiple fronts

- Liquid metals offer potential solutions to the problems facing solid PFCs
- NSTX Liquid Lithium *Divertor* experience confirms many results obtained on limiter machines
- Contamination by residual gases motivates a flowing system
- Liquid metal PFC development ongoing at PPPL to develop next-step divertor solutions

Reprints
