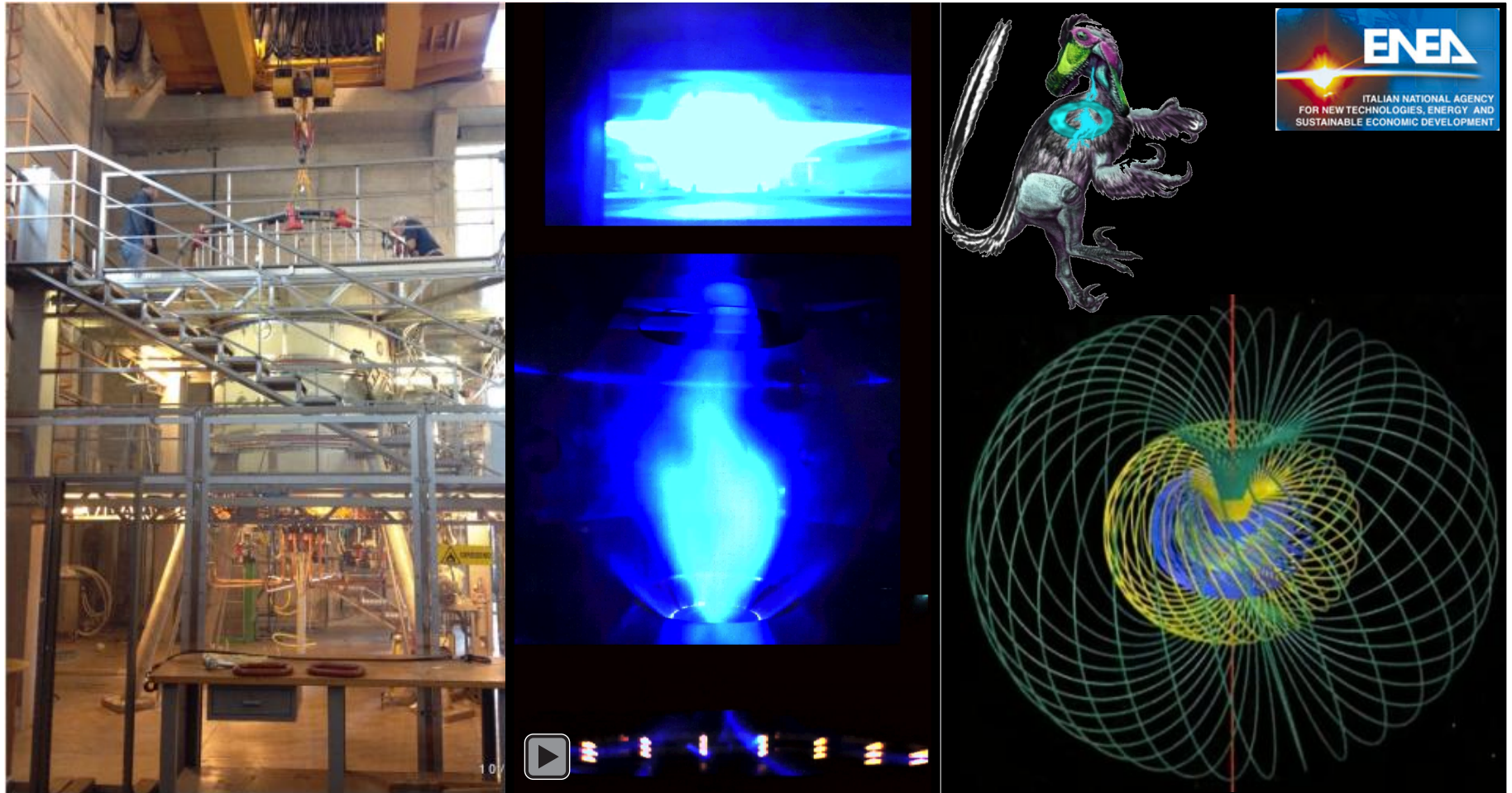


The PROTO-SPHERA experiment, an innovative confinement scheme for Fusion

Franco Alladio¹, P. Micozzi, G. Apruzzese, L. Boncagni, O. D'Arcangelo, E. Giovannozzi, A. Grosso, M. Iafrati, A. Lampasi, G. Maffia, A. Mancuso, V. Piergotti, G. Rocchi, A. Sibio, B. Tilia, O. Tudisco, V. Zanza

CR-ENEA Frascati, ¹franco.alladio@enea.it



19th International Spherical Torus Workshop (ISTW 2017), Seoul National University, 18-22 September 2017

Outline

A Spherical Torus whose Centerpost is a Plasma discharge

Why a new and different magnetic confinement device?

- Possible unlimited sustainment of plasma current by DC voltage
- Natural examples of rings emitted by jets in fluids & plasmas
- High β value ~ 1 calculated for its ideal MHD stability
- If successful it could be the engine of a Fusion Space Thruster

Present experiment produces only Plasma Centerpost

- Modifications of boundary conditions:
 - additional external PF coils
 - insulating materials near the plasma,have allowed achievement of full plasma current in Argon
- Plasma configuration resilient to operation accidents
- Spontaneous rotation of Plasma Centerpost
- Mixed magnetic & electrostatic confinement
- A new vacuum vessel for Hydrogen discharges?
- Perspective

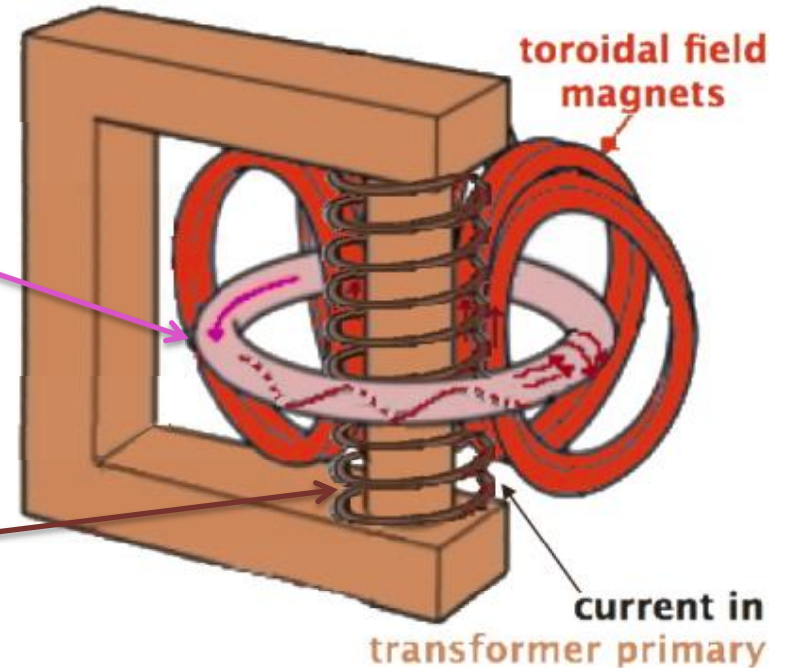
。 。 。 二龙抢珠 èrlóng qiǎngzhū
Two Dragons are snapping at a pearl!



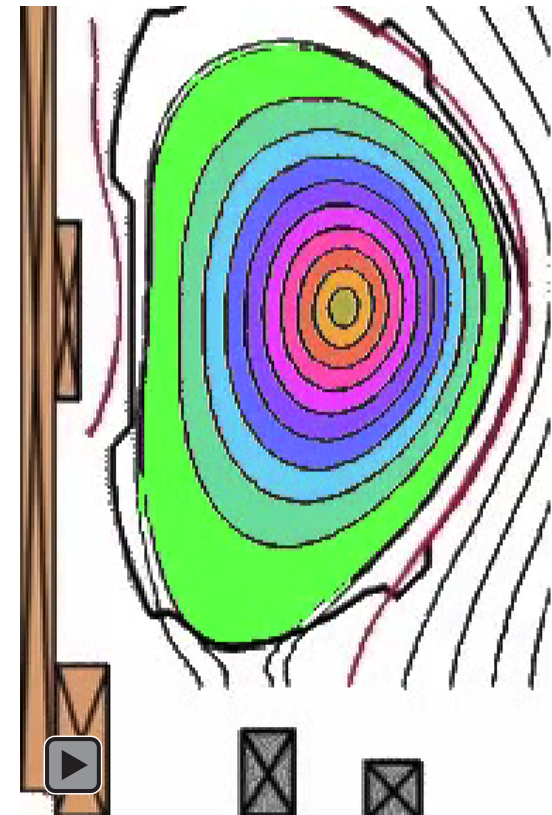
Therefore a **plasma confining current has to flow inside the Torus:**

such a current has to be **induced and sustained by a transformer**

whose current varies in time ...but there are limits: the transformer will break beyond a given current limit...



- The plasma ohmic drive in a Tokamak can be seen as **motion of closed flux surfaces**, that from outside 'feed' the plasma, which dissipates them while they move toward the magnetic axis
- In tokamaks this process is due **to the transformer current change:**
- **Tokamaks cannot have steady drive!**

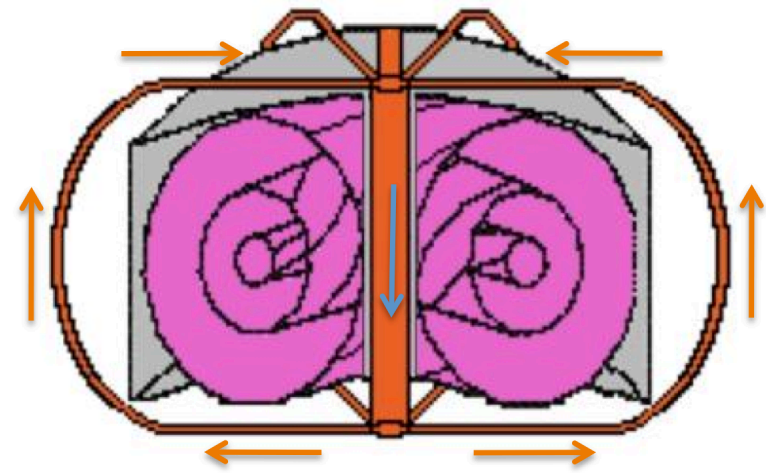


The main idea of PROTO-SPHERA

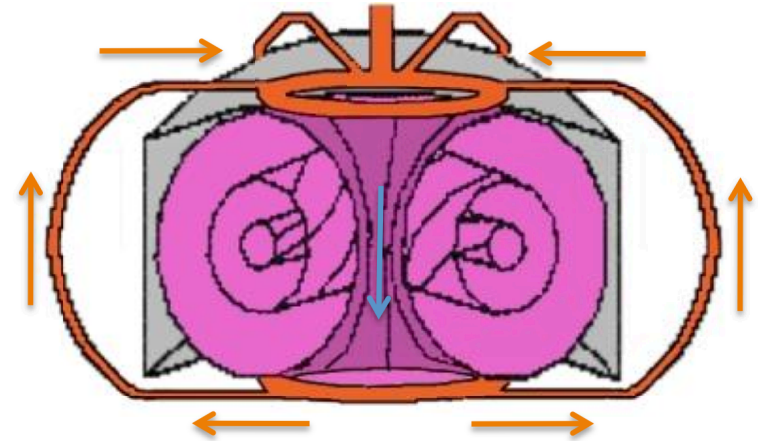
- “Conventional Tokamak”: **magnetic surfaces of toroidal plasma** surround a “**Metal Centerpost**”
- *Vacuum vessel has toroidal geometry*
- **PROTO-SPHERA: magnetic surfaces of toroidal plasma** surround a “**Plasma Centerpost**”; **only current return external legs are made of metal**
- *Vacuum vessel has cylindrical geometry*
...but electrodes are required inside vacuum

Abandon vacuum vessel complicated geometry,
move to a cylindrical vacuum vessel!

→ easy of access & of repair...

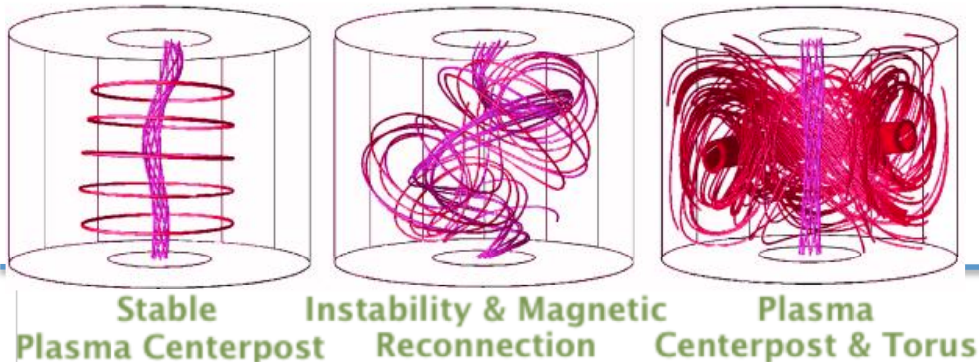


Electric current flow



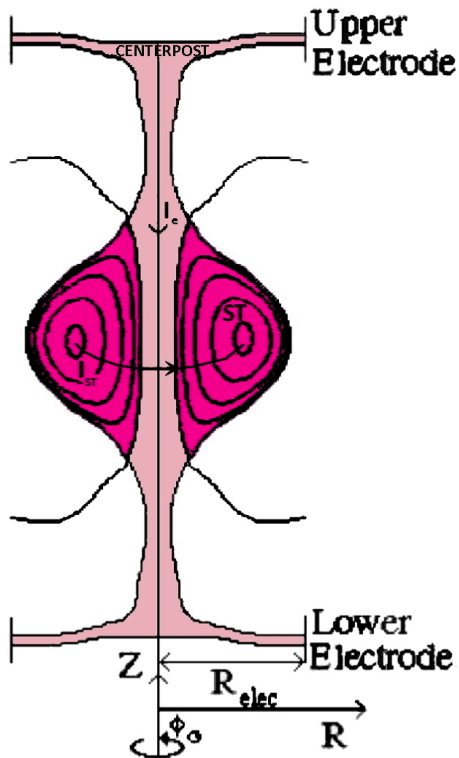
PROTO-SPHERA Japanese precursor

TS-3 (Tokyo University): 1993 removed the metal centerpost, applied 1kV between two plasma guns, produced a $I_c = 40$ kA Plasma Centerpost, non-linear “kink” instability formed a Spherical Torus toroidal plasma current $50 \text{ kA} < I_{ST} < 100 \text{ kA}$



60 μs formation
 20 μs sustainment
 total duration 80 $\mu\text{s} \sim 100 \tau_{\text{Alfvén}}$
 (short but significant...)

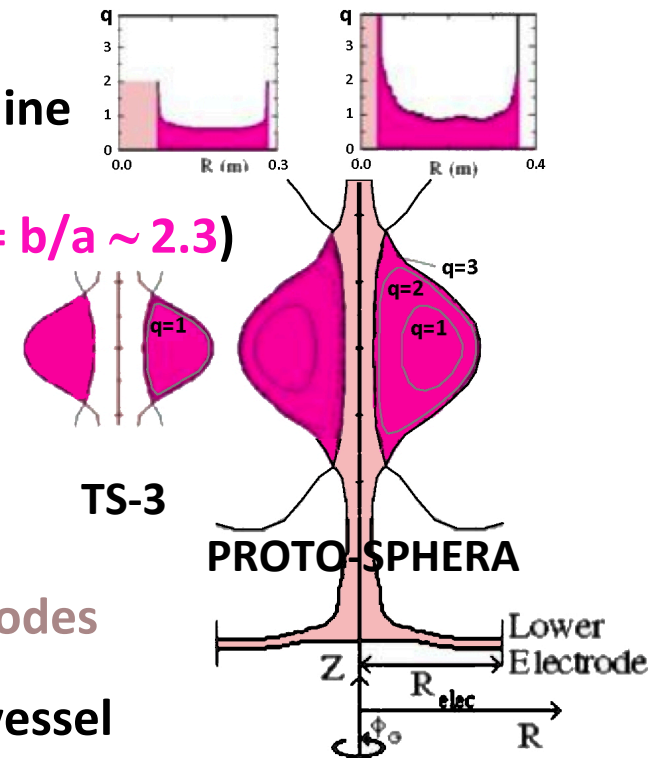
PROTO-SPHERA key differences



- Designed for a Tokamak-like field-line rotational transform ($q_0 \geq 1$, $q_{\text{edge}} \sim 3$) (aspect ratio $A = R/a \geq 1.2$, elong. $k = b/a \sim 2.3$)

- PROTO-SPHERA formed “slowly” as a prolated low aspect ratio Spherical Torus from the pre-existing plasma centerpost, mushroom-shaped in front of electrodes

- At low voltage (100 V), inside big vessel



PROTO-SPHERA main design parameters:

Centerpost current

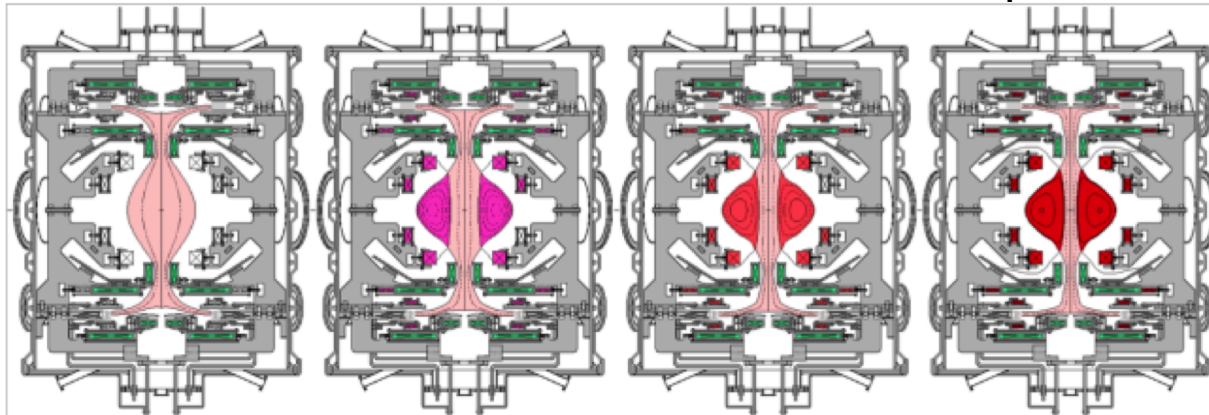
$I_e = 60 \text{ kA}$

ST toroidal current

$I_{ST} = 120 \div 240 \text{ kA}$

ST diameter

$2R_{sph} = 0.7 \text{ m}$

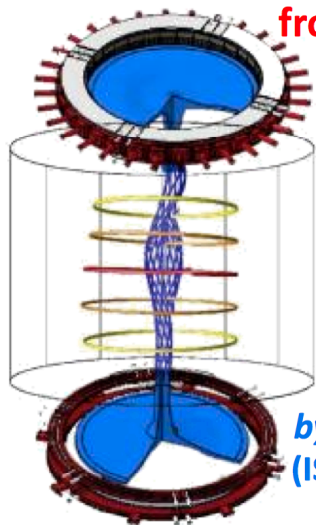
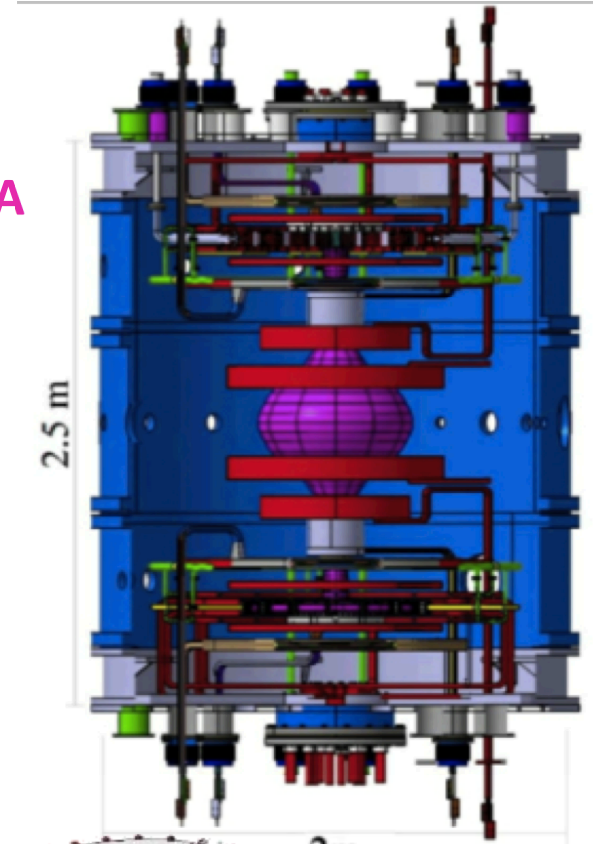


Axisymmetric simulation of ST formation

Formation time scale $(\tau_{\text{Alfvén}} \cdot \tau_{\text{Resist}})^{1/2} \sim 0.6 \text{ ms}$

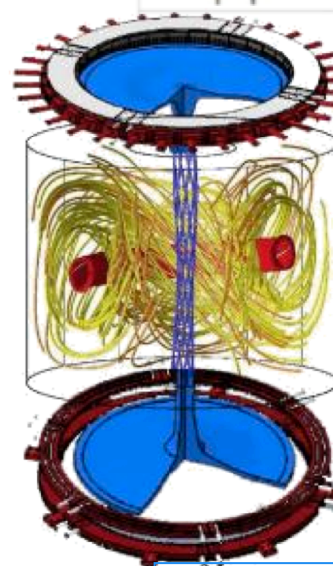
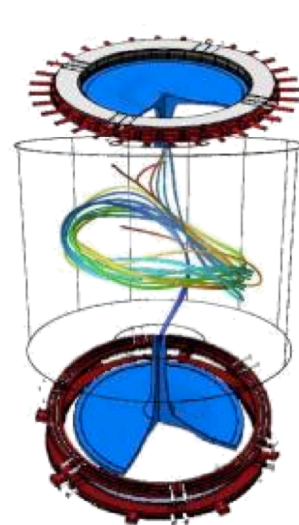
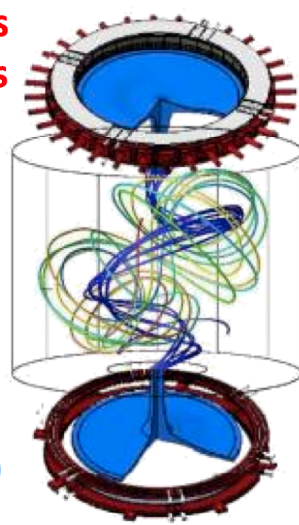
from $\tau_{\text{Alfvén}} \sim 0.5 \mu\text{s}$

$\tau_{\text{Resist}} \sim 70 \text{ ms}$



*Resistive MHD
simulations of
ST formation*

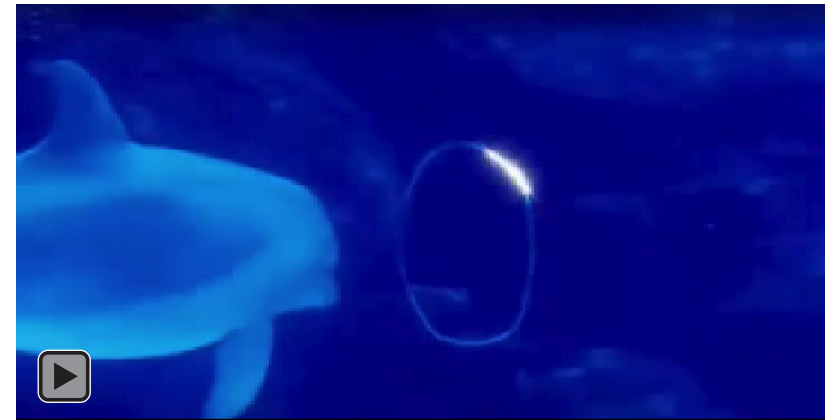
*by Ricardo Farengo
(ISTW2008-Frascati)*



Non-axisymmetric simulation of ST formation

Formation & sustainment of Rings from Jets is a common occurrence in Nature!

Aim is to sustain the Plasma Torus
for at least 1 resistive timescale: $\tau_{\text{Resist}} \sim 70 \text{ ms}$
...but PROTO-SPHERA designed for 1 sec sustainment!

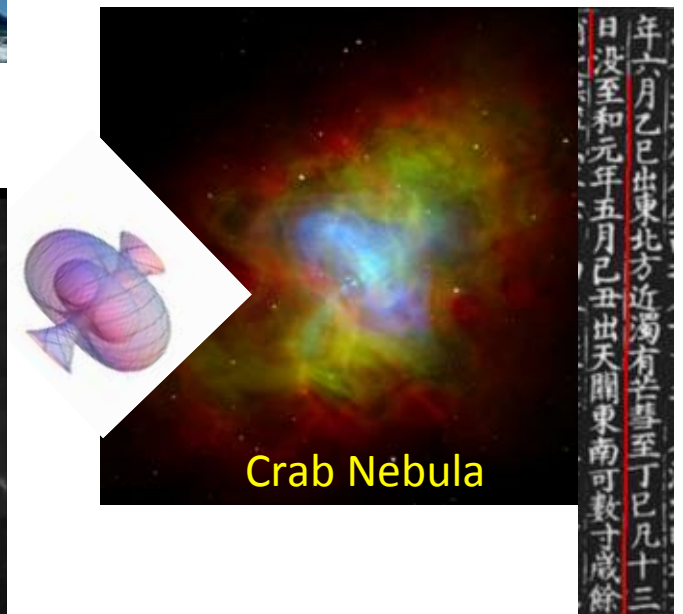


William Irvine-University of Chicago



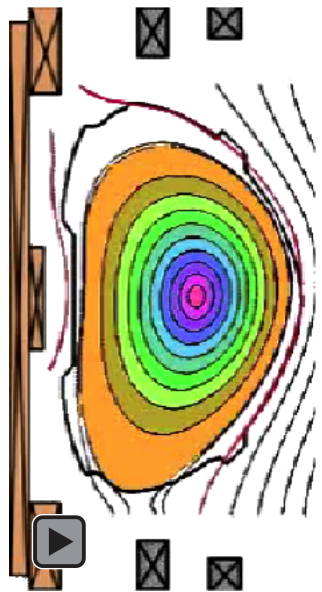
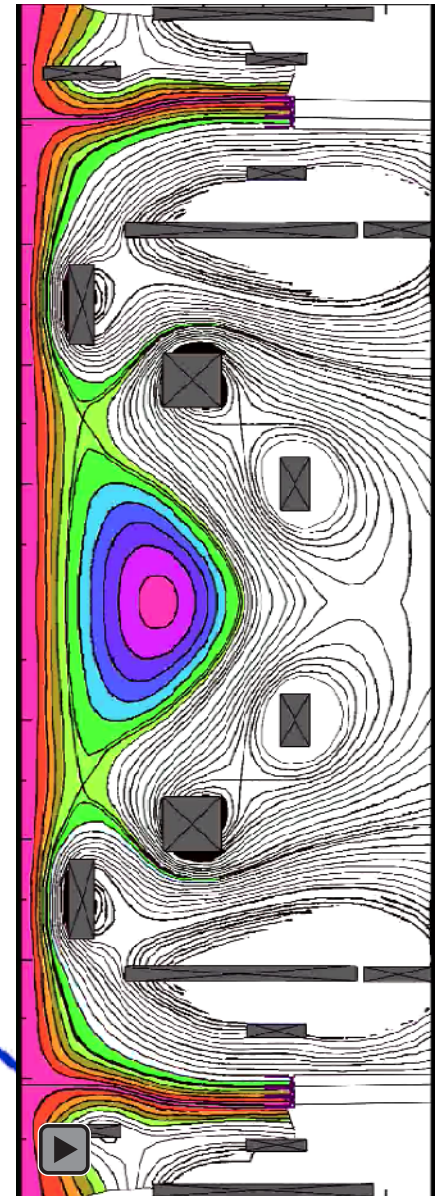
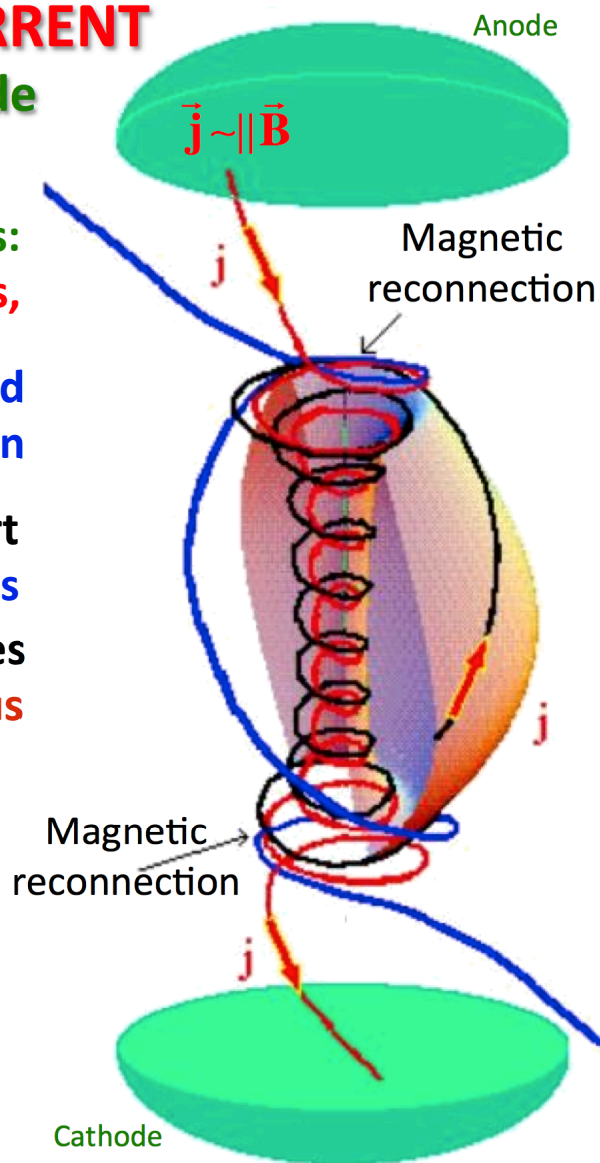
Fluid dynamics examples

Plasma dynamics example



SUSTAIN THE CONFINING CURRENT by DC voltage from anode to cathode

- In front of the electrodes: **open magnetic field lines,**
- Open magnetic field lines are wound in a circular direction
- Magnetic reconnections convert **open \vec{B} lines** into closed \vec{B}, \vec{j} lines **wrapped around the spherical torus**



\vec{E} of Tokamaks relies on **induction** efficient but not forever...

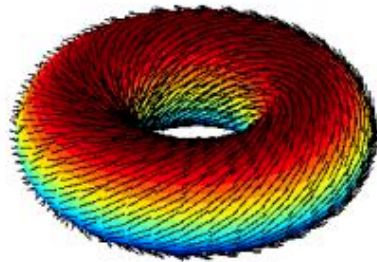
\vec{E} of PROTO-SPHERA relies on $\vec{v} \wedge \vec{B}$ associated with **magnetic reconnections**

← HOW EFFICIENT THE SUSTAINMENT OF TOROIDAL CURRENT BY RECONNECTIONS? →

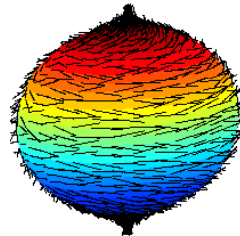
Space Thruster?

abandon vacuum vessel toroidal geometry, move to cylindrical one
... → **natural expulsion of charged fusion products (Space Thruster)**

*Due to filamentary nature of B field
a fundamental mathematical difference appears:*



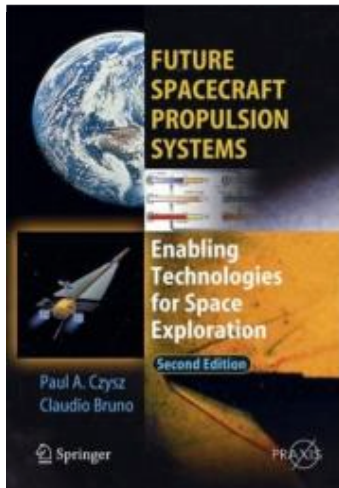
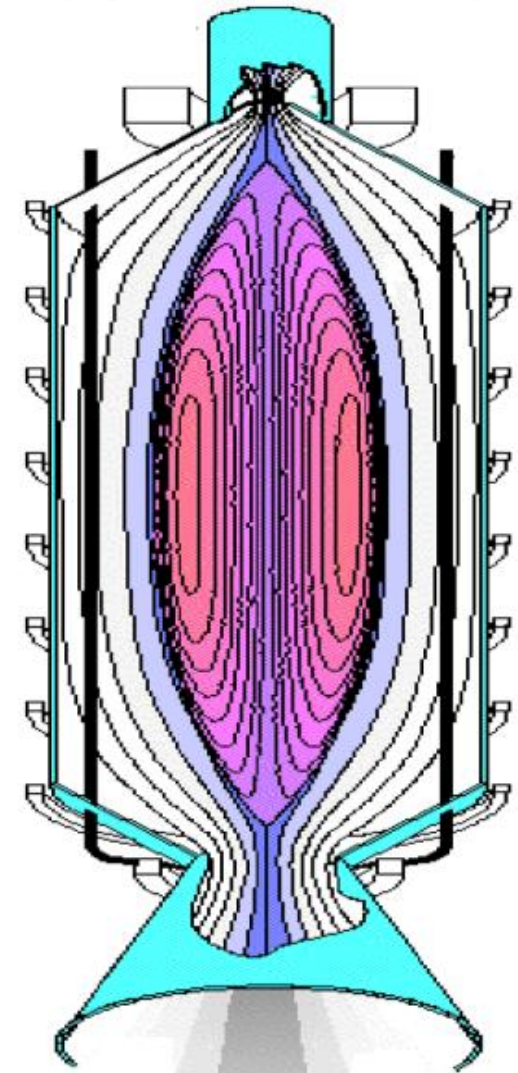
*a hairy torus
can be combed*



*a hairy sphere
cannot!*

From one of the “*tufts*” of the sphere (...not combed)
very high velocity (\sim MeV) charged fusion products emerge

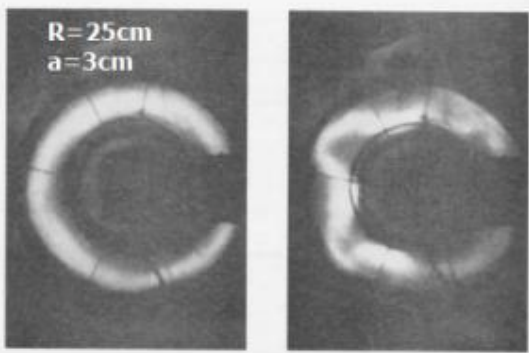
Possible future application as a Space Fusion Thruster...



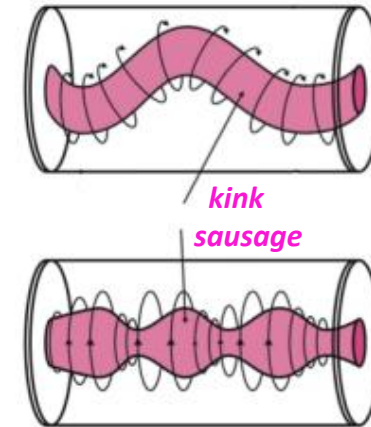
Nozzle observed in PROTO-SPHERA experiment (2015)

Why a new and different magnetic confinement device? one reason is ... "disruption"

Alan Ware & Thomson
Imperial College 1947.



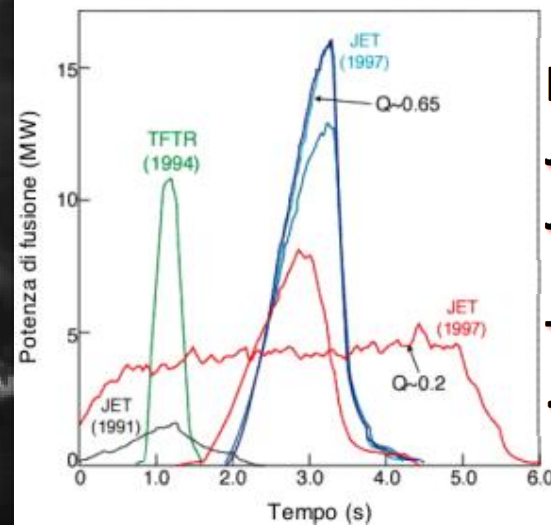
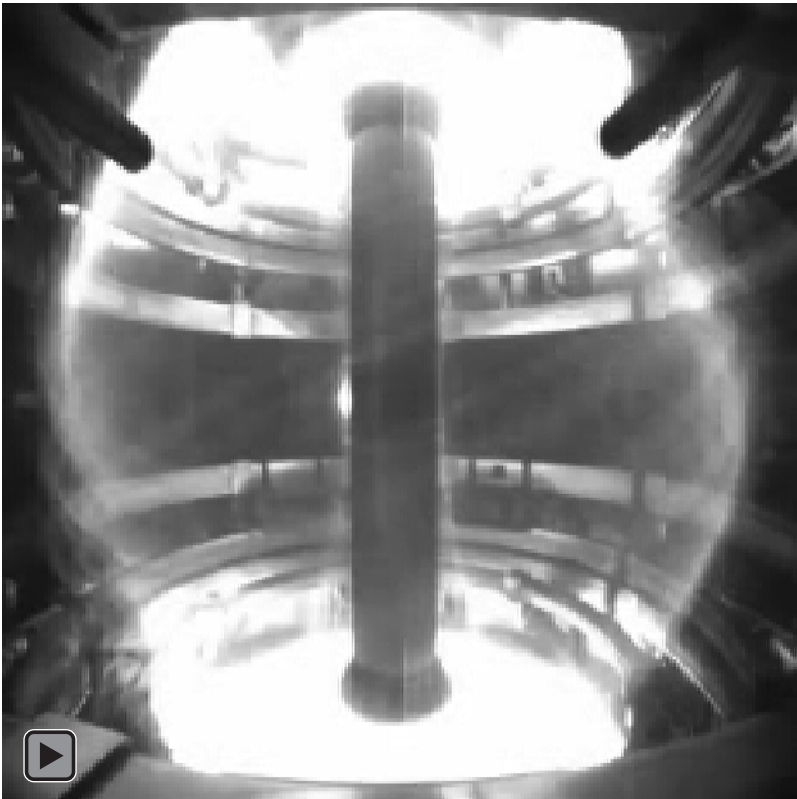
MHD instabilities appeared since the earliest toroidal magnetic confinement devices



Mast 2004

...the problem of disruption has not yet been solved

... Only Stellarator configurations (no net toroidal current!) avoid this inconvenience



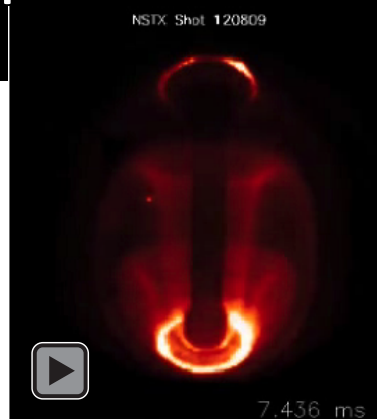
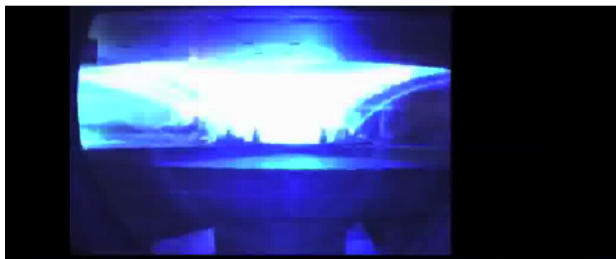
**In D - T experiments:
JET 1991- TFTR 1994
JET 1997**

**The highest neutron yield
...terminates in a disruption**

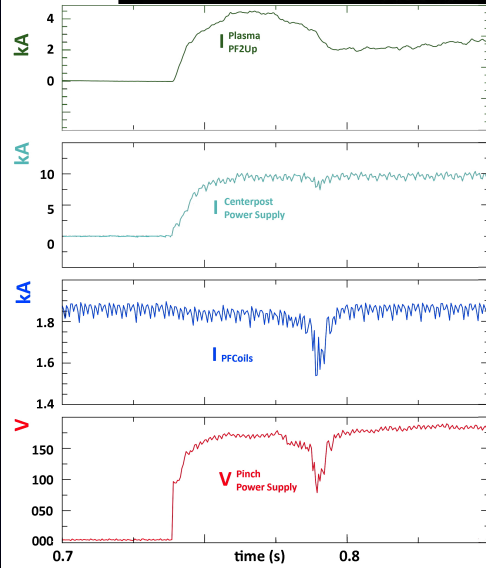
- Disruptions ...toroidal **plasma** vanishes → **damages, very long plasma restart, ...**

DC helicity injection in NSTX Spherical Tokamak (with metal centerpost)

plasmoids are born & reborn



PROTO-SPHERA shot #364 (2016)
Plasma started without B field
Centerpost forms when B field is on



shot #734 (2017)
Langmuir probe
accident

In case of disappearance of toroidal current the configuration can reappear

Why a new and different magnetic confinement device? another reason is ... " β limit"

... Even if the muttered mantra is that tokamak physics is perfectly known ...

$$\beta = \text{plasma beta} = \frac{\text{kinetic plasma pressure}}{\text{confining magnetic field pressure}}$$

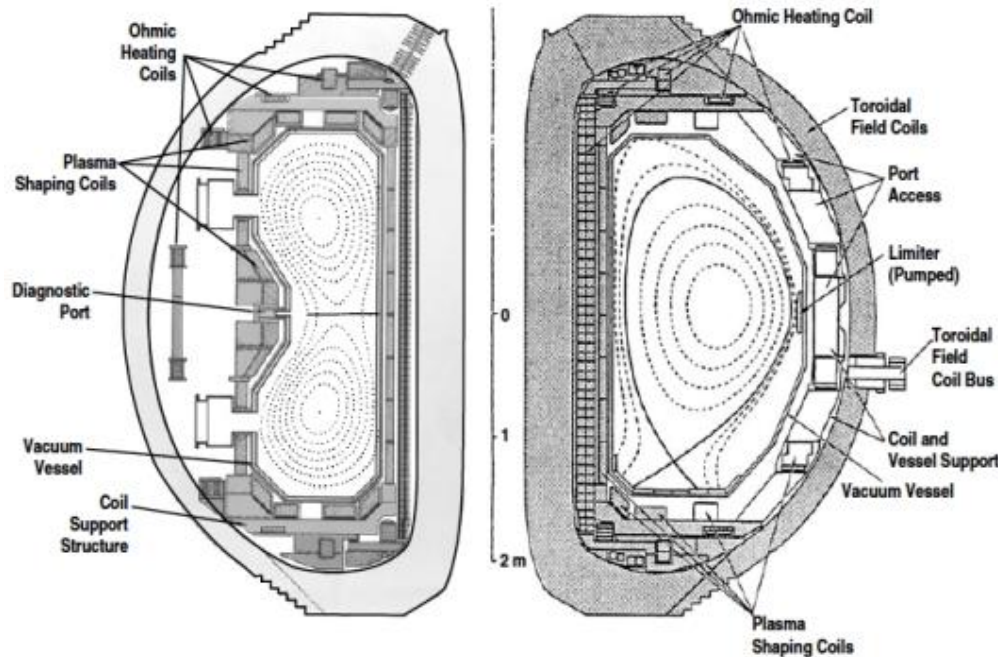
$$\beta = 2\mu_0 \int p dV / \int B^2 dV$$

but in tokamak experimental data one often uses β_{T0}

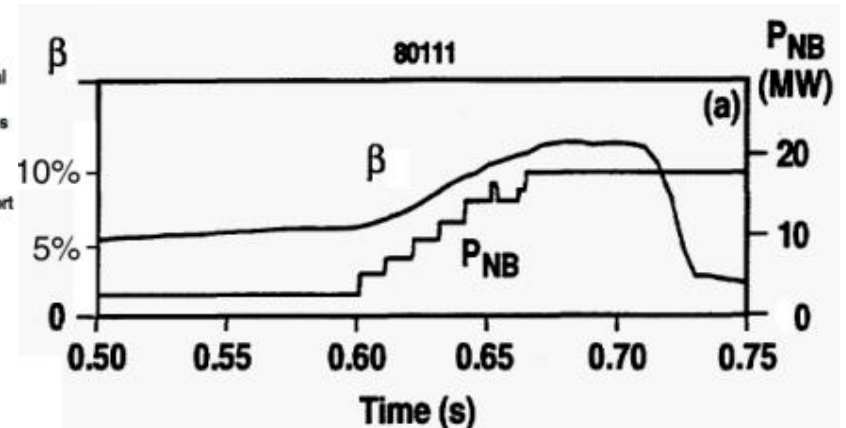
$$\beta_{T0} = 2\mu_0 \int p dV / B_{T0}^2 V$$

where B_{T0} is the vacuum field on the axis of the plasma

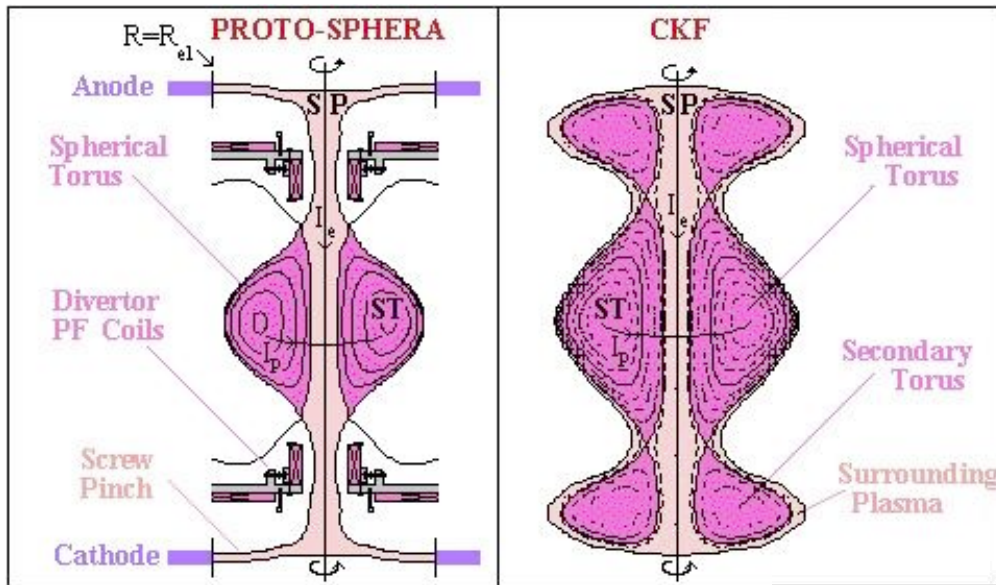
DIII-D in 1994 reached the highest value of β in conventional Tokamaks



**DIII-D reached $\beta_{T0} = 12.5\%$,
but...the plasma "disrupted"
vanished in ~ 1 msec !**



- Beta ... **plasma** pressure few % of magnetic pressure → **cost, size, ...**



Chandrasekhar-Kendall-Furth configuration
CKF an extrapolation of PROTO-SPHERA:

- **internal PF coils replaced by secondary Tori of Plasma**
- **Centerpost hitting electrodes replaced by Surrounding Plasma**

CKF are ideally MHD stable up to $\beta = 1$
but also PROTO-SPHERA can approach $\beta = 1$

For low toroidal numbers $n=1, 2$ & 3
 ideal MHD stability obtained

expressed with $\beta = 2\mu_0 \int p dV / B^2 dV$

ratio of the two plasma currents

I_{ST} / I_e = toroidal ST current/centerpost current

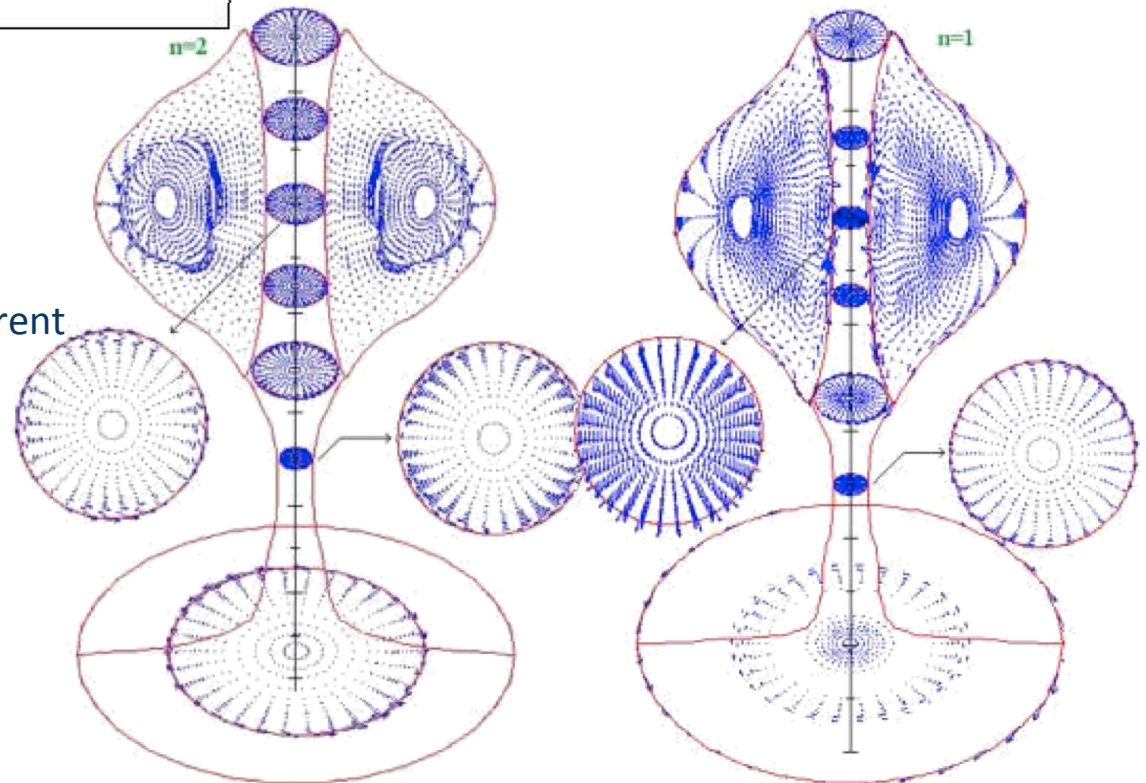
- up to $\beta = 21 \div 26\%$, $I_{ST} / I_e = 0.5 - 1$

- up to $\beta = 14 \div 15\%$, $I_{ST} / I_e = 2-4$

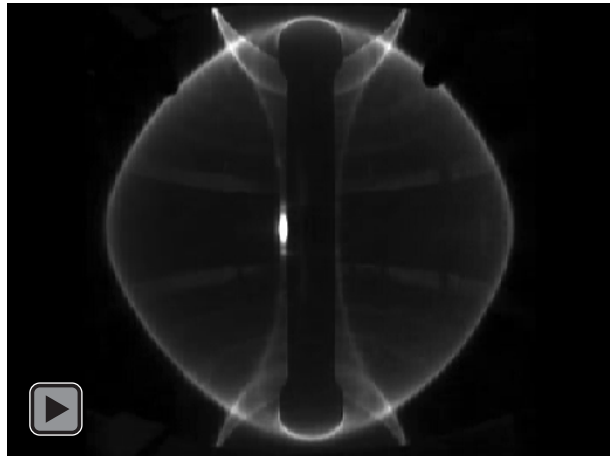
expressed with $\beta_{T0} = 2\mu_0 \int p dV / B_{T0}^2 V$

- up to $\beta_{T0} = 28 \div 29\%$, $I_{ST} / I_e = 0.5 - 1$

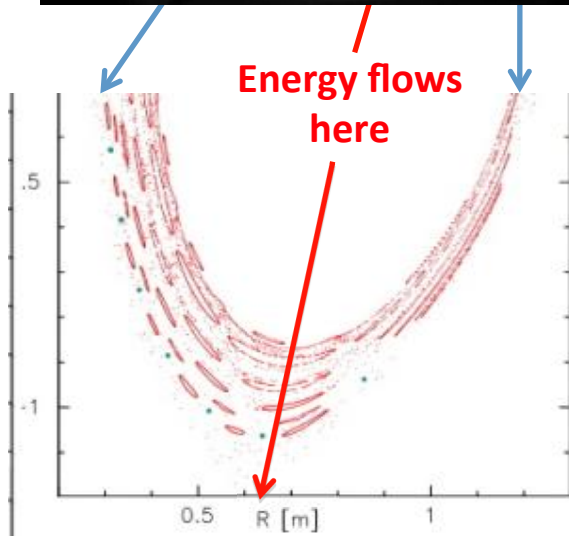
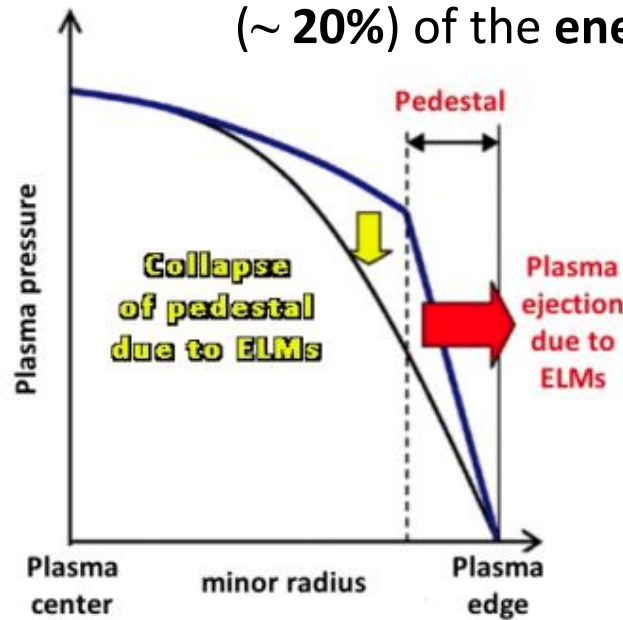
- up to $\beta_{T0} = 72 \div 84\%$, $I_{ST} / I_e = 2-4$



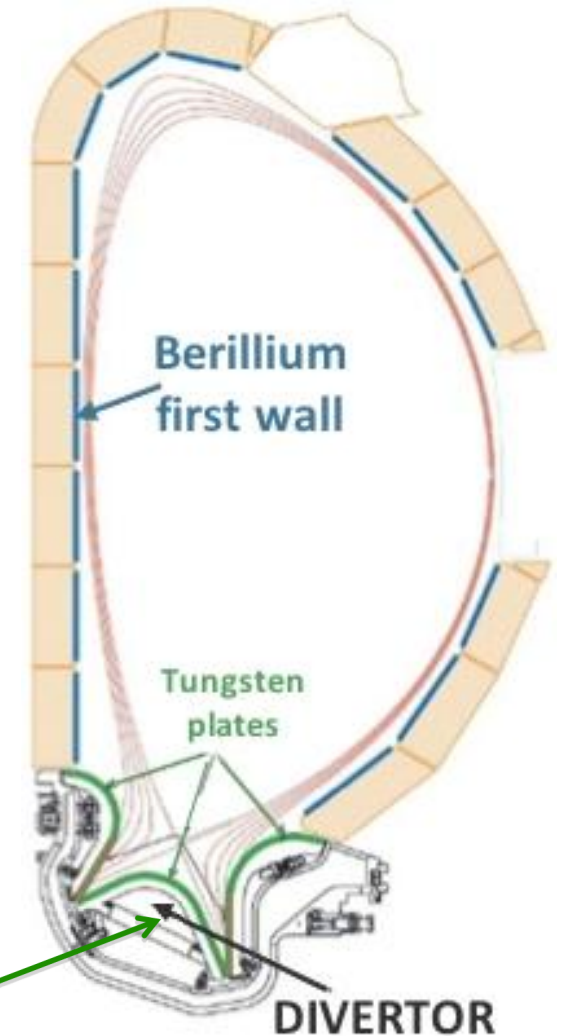
**Why a new and different magnetic confinement device? still other reason are...
"ELMs" (unstable edge localized modes)**



"ELM" mode throw upon the divertor a sizeable portion (~ 20%) of the energy in the pressure pedestal



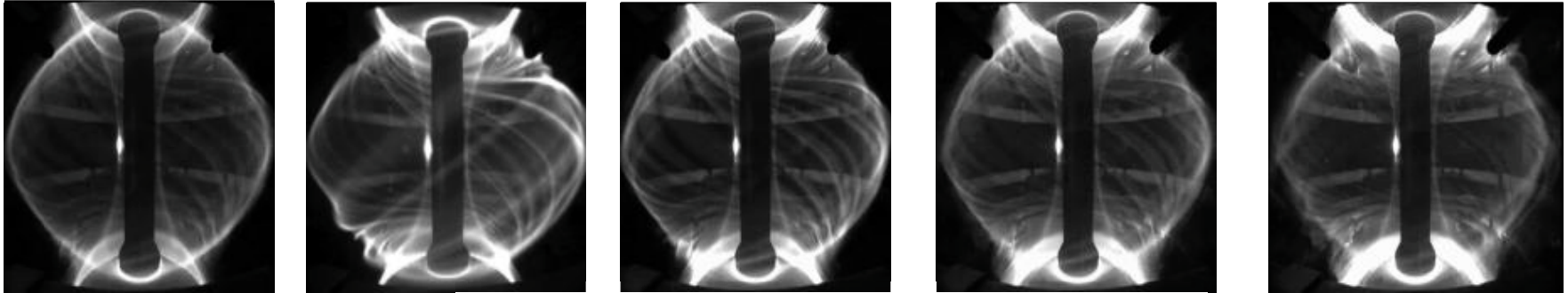
This happens in a very short time (250 μ s) as the plasma edge becomes ergodic (ELM filaments carry current)



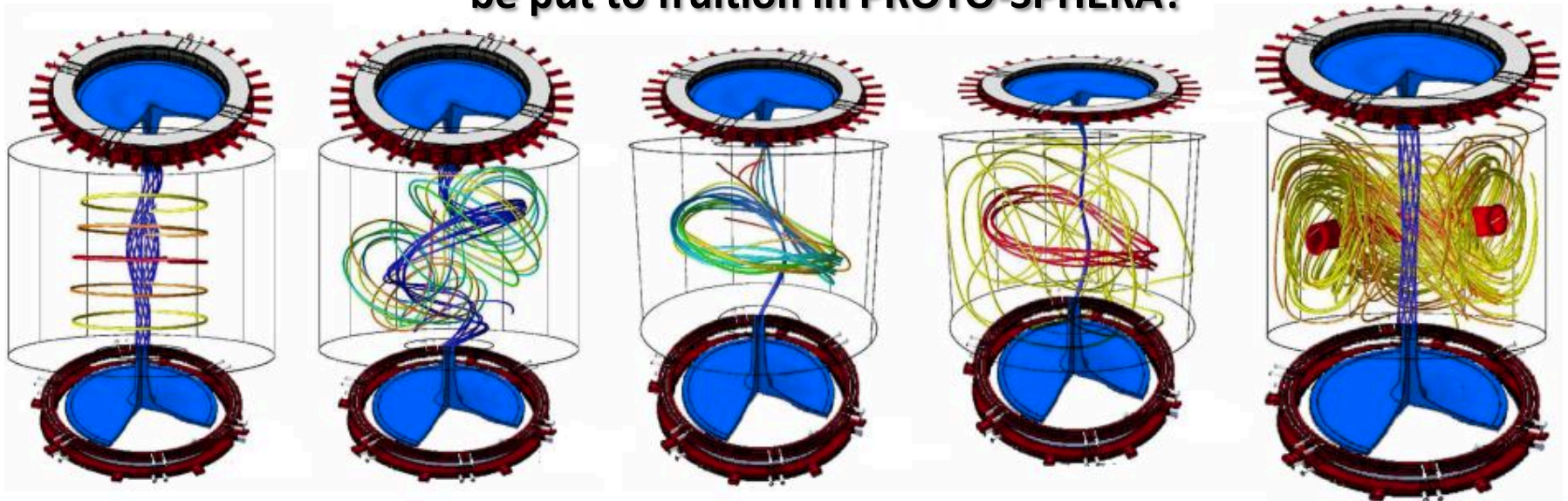
On ITER an ELMs carrying > 3% of pedestal energy can even melt or sublimate the Tungsten of the Divertor plates

"ELMs" (unstable edge localized modes):

can these spontaneous filamentations (which in Tokamaks are only dangerous)



be put to fruition in PROTO-SPHERA?

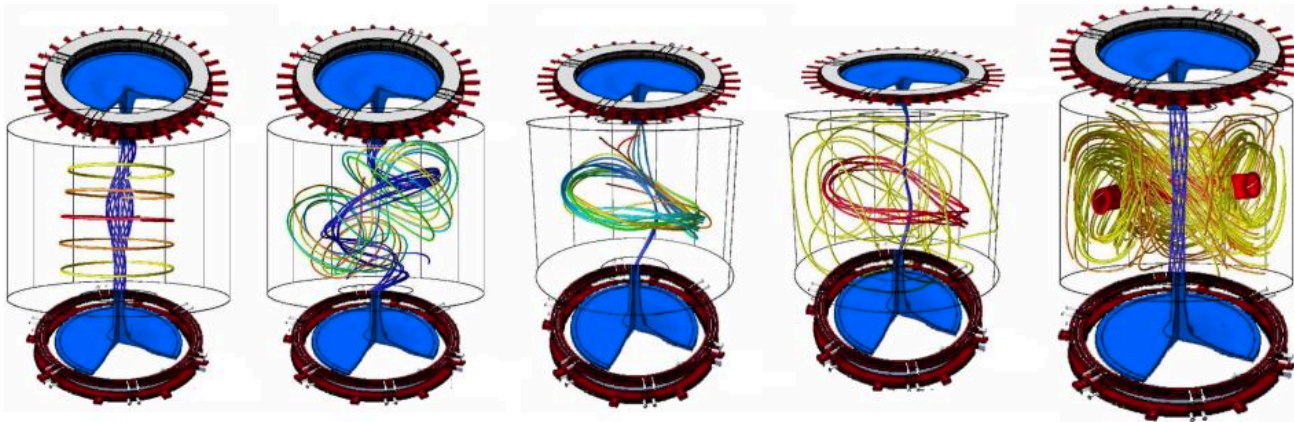
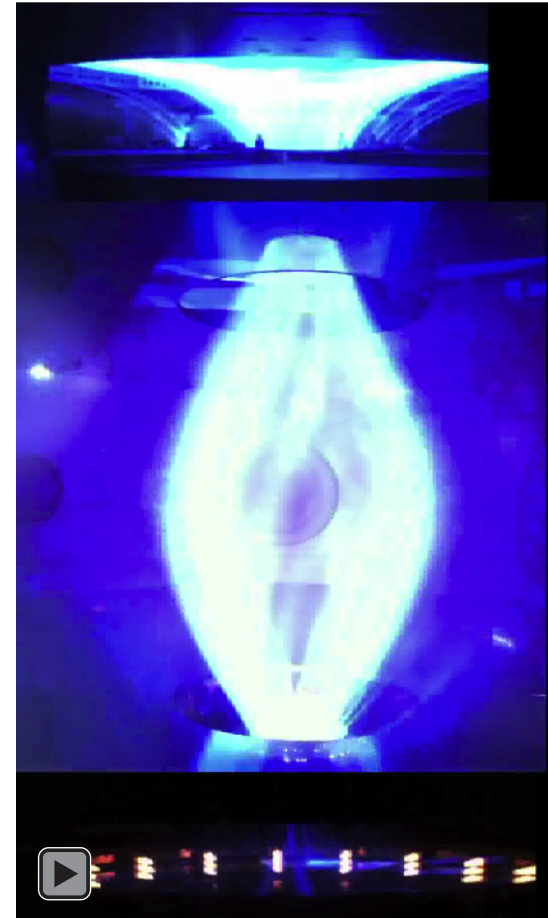


Plasma rotation in Tokamaks is extremely advantageous, as it stabilizes the torus

Plasma rotation induced by additional heatings (Neutral Beam Injection, NBI), becomes more & more difficult on larger tokamak experiments

Plasma Centerpost of PROTO-SPHERA rotates!

Operational experience in Tokamaks shows that the **best way of puffing fuel is from the high field side**

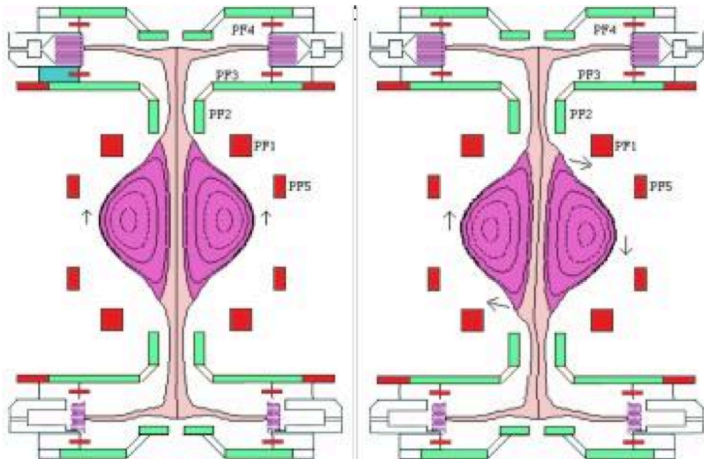


Gas puffed hollow anode

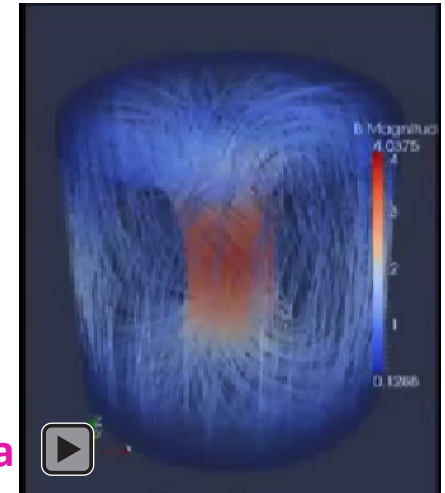


IDEAL MHD STABILITY of PROTO-SPHERA

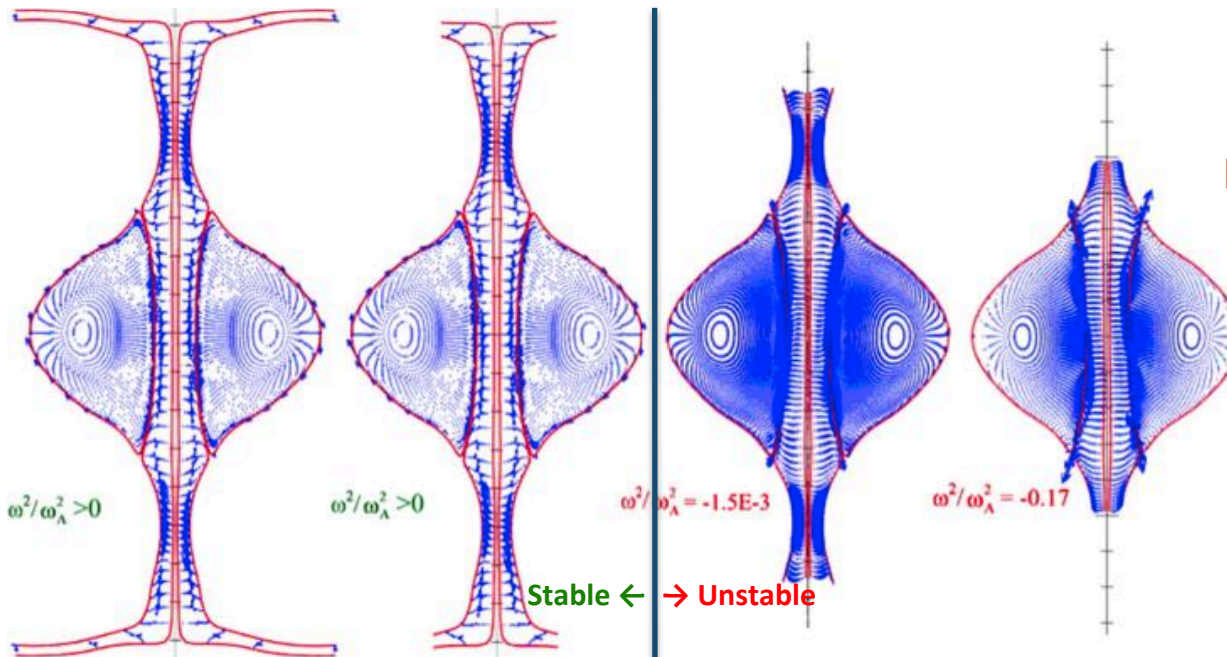
Spheromak tilt instability is due to dipole of containing field opposite to toroidal plasma current dipole



“Group A” PF coils (compression coils) has dipole moment opposite to Plasma but “Group B” PF coils (shaping coils) has dipole moment aligned to Plasma



DISK-SHAPED CENTERPOST PLASMA: IMPORTANT FOR THE IDEAL MHD STABILITY



Cutting shorter & shorter the plasma centerpost PROTO-SPHERA at 120 kA gets destabilized



May 2015 annular anode lowered on top of machine



Up: hollow gas-puffed anode

Down: 3000° K heated cathode

present stage cathode (54 = 18 x 3 emitters): aim 10 kA



final stage cathode, 6 x present (324 = 108 x 3 emitters): aim 60 kA



“Caduceus”-like emitting spirals have now survived > 1000 cycles



INSULATIONS

Only the PF coils necessary for setting up the plasma centerpost have been built

8 PF coils in series inside the machine

Stainless steel up/down new extensions

PF4up

PF3up

PF2up

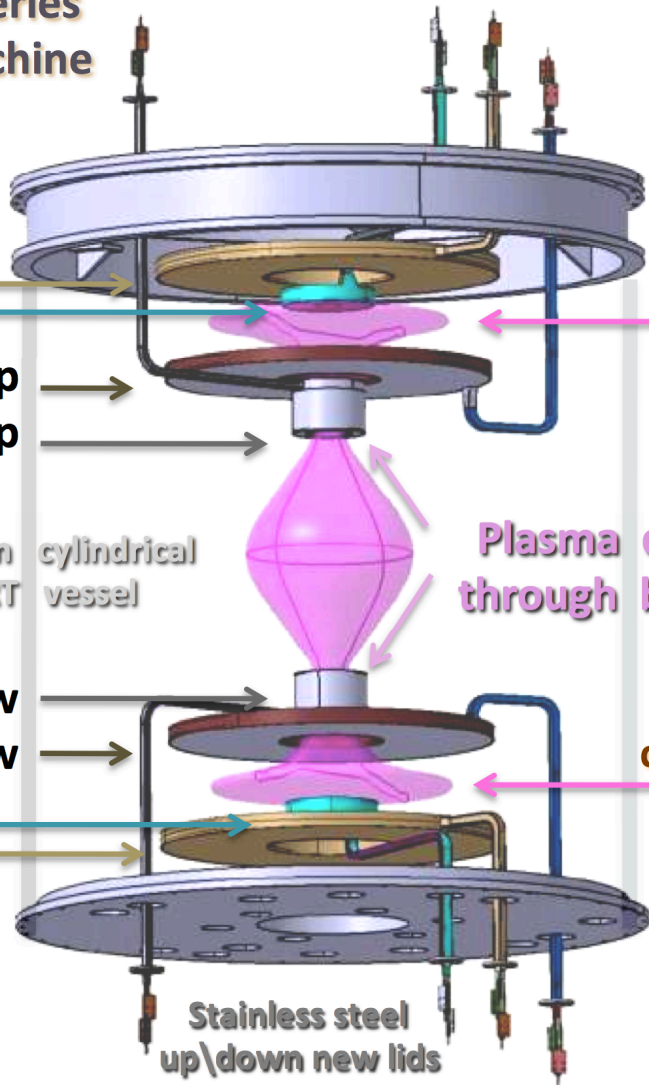
Aluminium cylindrical vessel
START

PF2low

PF3low

PF4low

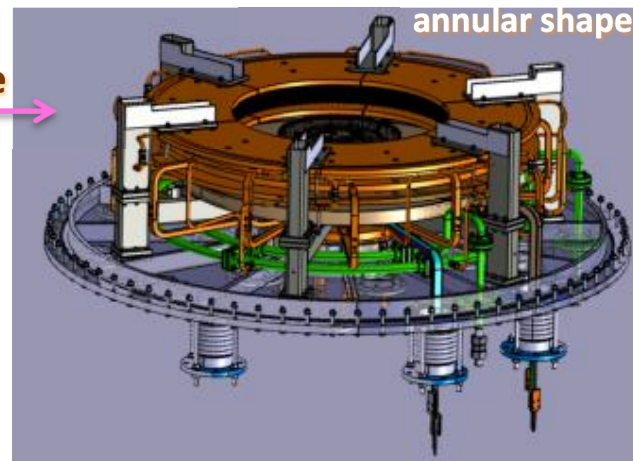
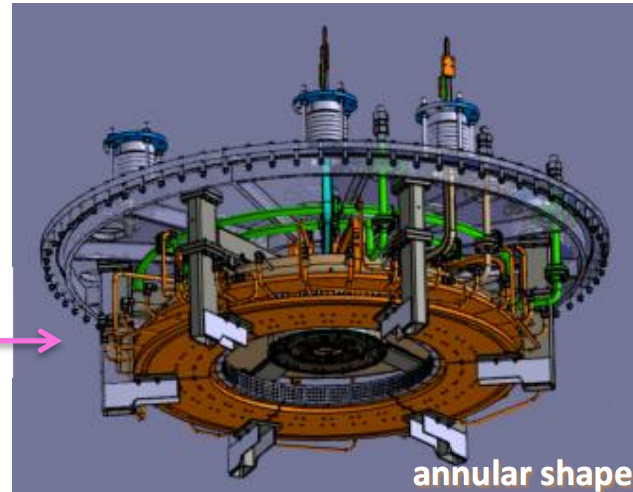
Stainless steel up/down new lids



anode

Plasma current must run through both PF2 throttles

cathode

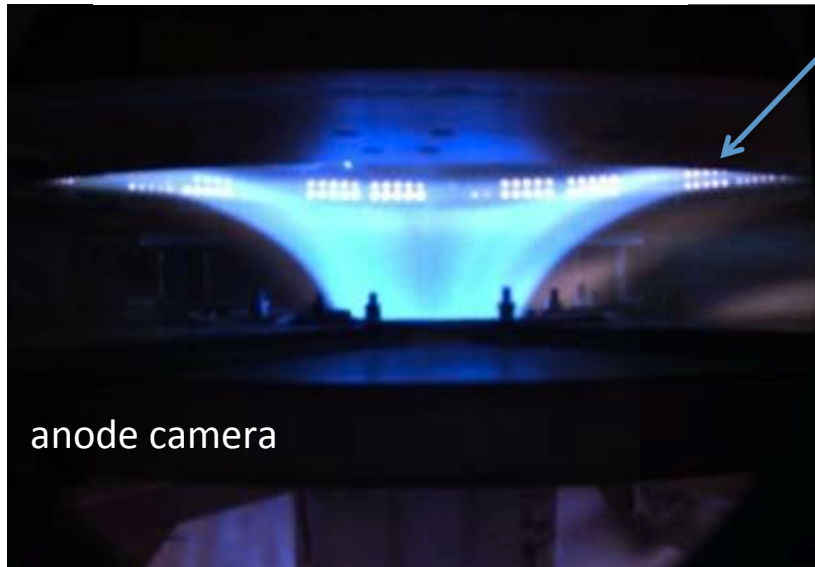


vacuum vessel is GND potential

PF coils casings built as floating, can be connected to potentials: anode +, cathode -, vessel 0

No Anode Arc Attachment!

Argon plasma: break-down 80 V



Hollow annular anode performs

- plasma goes through both PF2 throttles
- plasma enters anode gas-puffing holes
- no sign ($I_e < 8.6 \text{ kA}$) of anode attachment
- filling pressure $10^{-3} - 10^{-2} \text{ mbar}$

annular anode plasma is never filamented
whereas annular cathode plasma is filamented (due to sparse emitters)



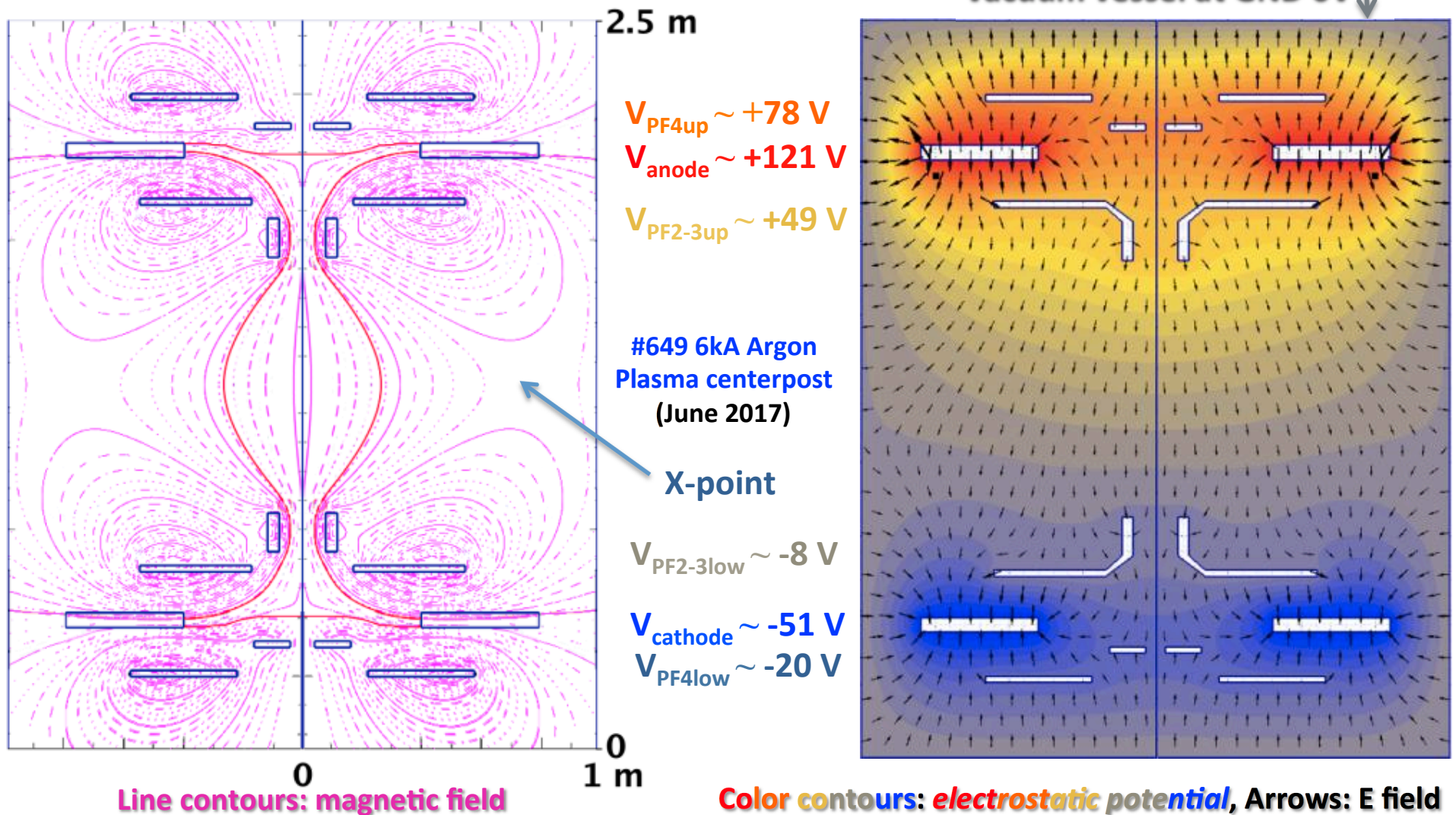
No Anode Arc Attachment: Electrostatic plasma effects!

PF coils casings built as floating, can be connected to: **anode +**, **cathode -**, vessel 0

Electrostatic potential is dominated by the plasma; **PF coils casings better left floating!**

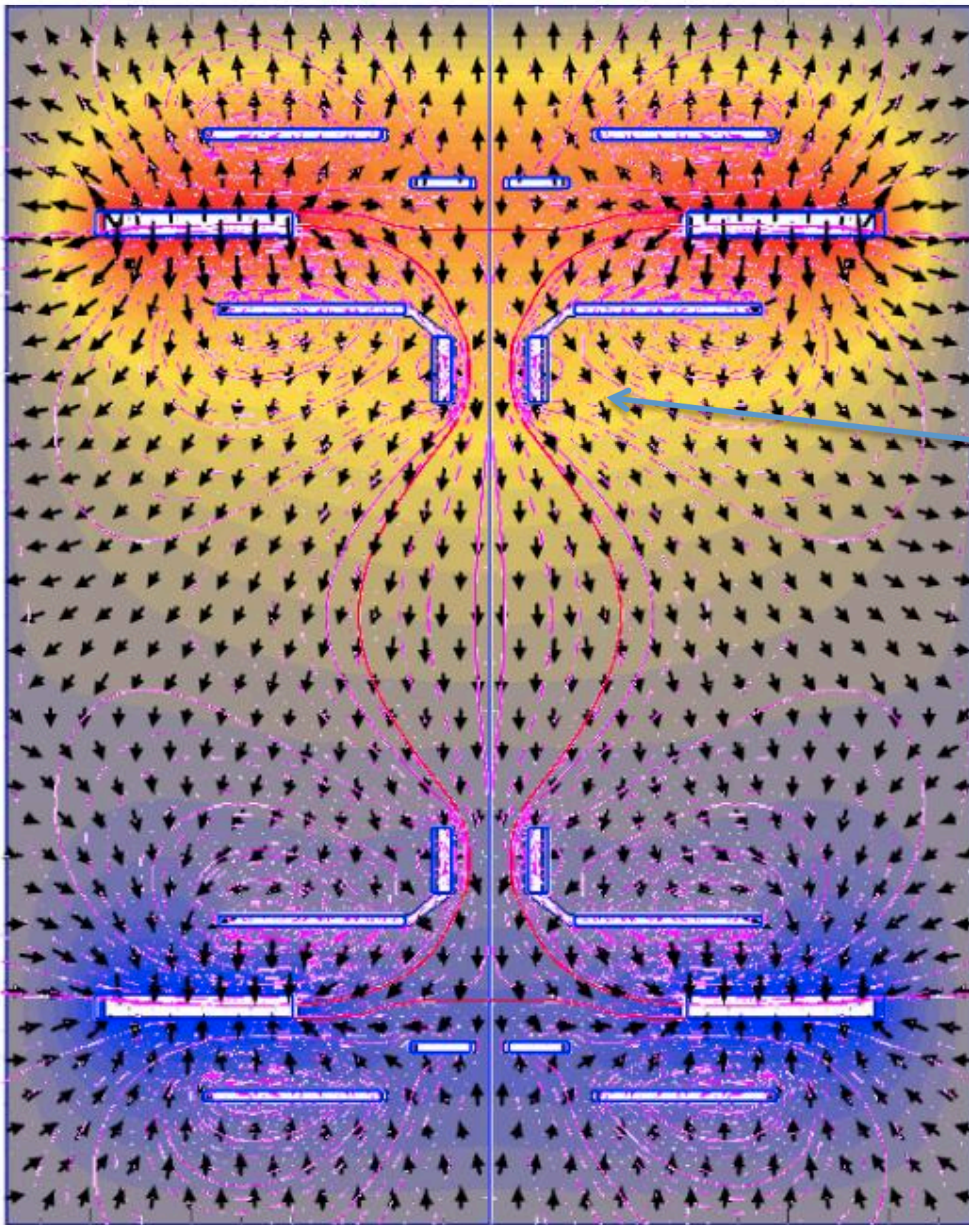
the magnetic field is up\down symmetric but electrostatic field not up\down symmetric

vacuum vessel at GND 0V ↓



Color contours: electrostatic potential, Arrows: E field

2.5 m



Plasma-induced electric potential:

near the annular anode

the E field is in part perpendicular to the B field

... $\vec{E} \wedge \vec{B}$ azimuthal plasma rotation

... starting from PF2up throttle

$$v_{\text{ExB}} = (E/B) \sim 10^2 - 10^3 \text{ m/s}$$

near the annular cathode

the E field is \sim parallel to B field

... less $\vec{E} \wedge \vec{B}$ plasma rotation

Self-organization at work inside annular electrodes plasma

#649, 6 kA Argon

0

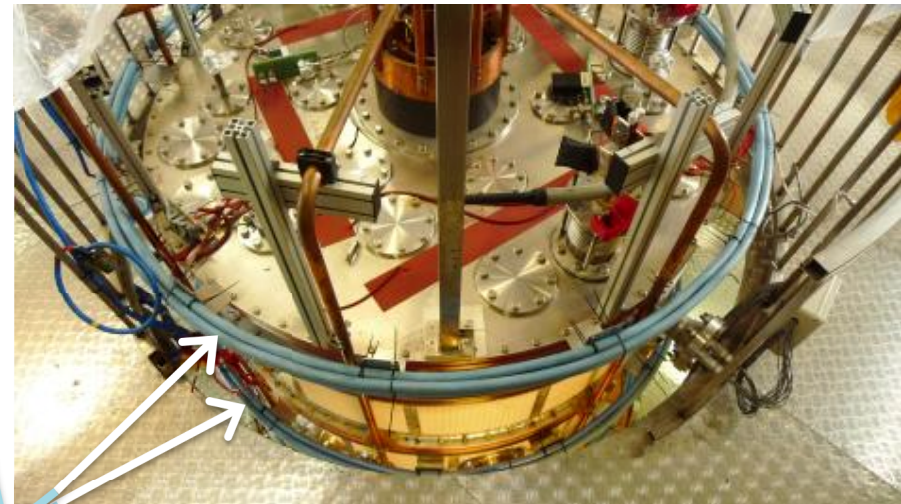
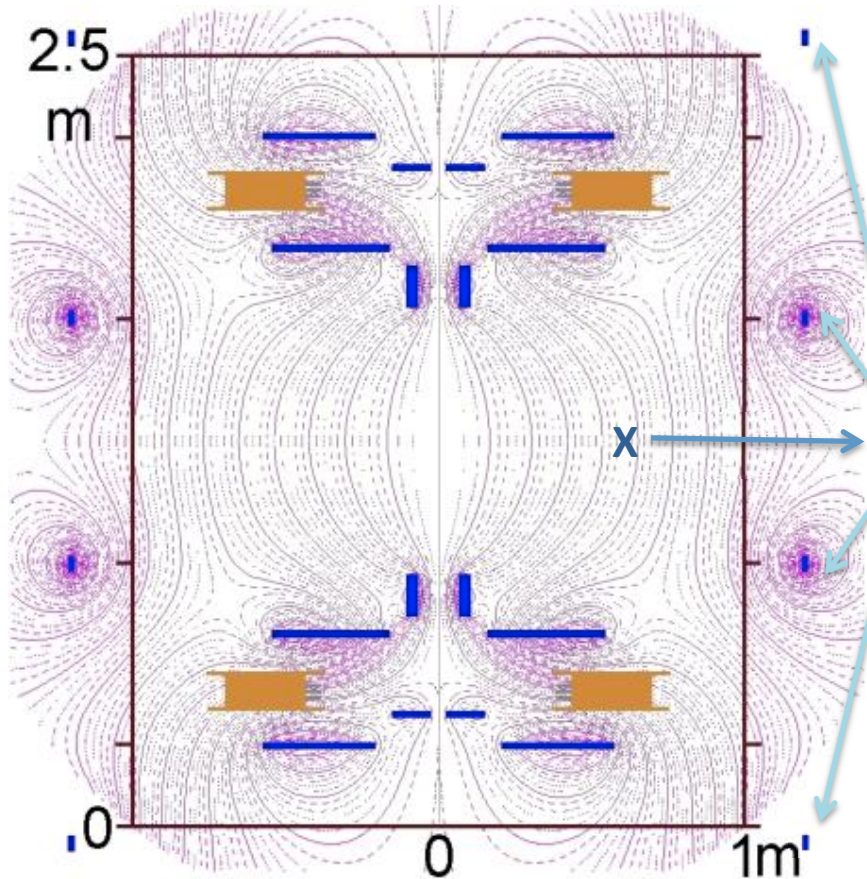
1 m

Line contours: magnetic field

The equatorial X -point has been removed from inside the vessel

4 External PF coils have been added (home-made from spare connection cables)

...and fed in series with the internal PF coils (PF coils power supply has sufficient margin)



4 External PF coils



Plasma fired after 0.75 s of PF current to allow for skin current diffusion in Al vessel and SS lids
Within 2017 a new Super-capacitor based Power Supply for External PF coils should operate!

2015/16 experiments produced a heavy metallization on top (anode) & bottom (cathode) bus-bar vacuum entrance flanges,

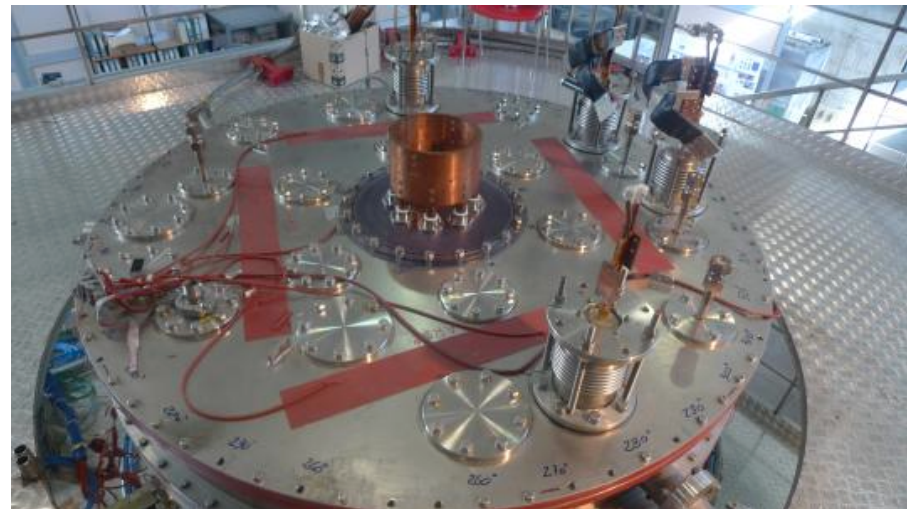
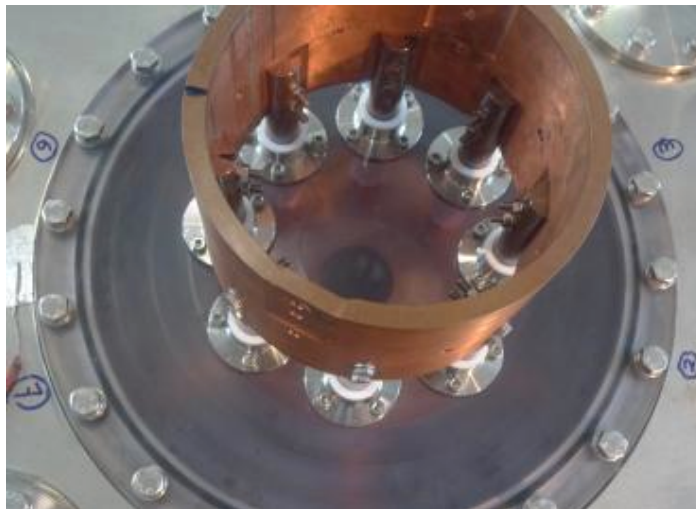
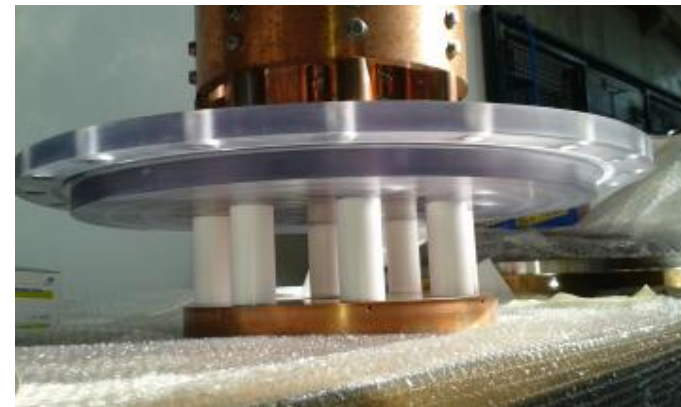
associated with magnetic “nozzles”



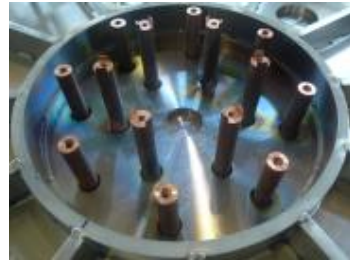
June 2016: insertion of Polycarbonate (transparent) anode bus-bar flange on top of machine

Heavily metallized
top & *bottom* bus-bar flanges

4 cm thick Polycarbonate
(required by atmospheric pressure)



At the bottom (near cathode) a SS flange, pierced by 14 bus-bars, such a flange has been substituted by a **Polycarbonate one**



July 2016: **Polycarbonate flange** on machine bottom



Secondary discharges from electrodes hitting Al vacuum vessel wall (plenty of scars!)



Polycarbonate flanges got rid of all metallization from bus-bars:
2mm thick Polycarbonate lining covers the Al vacuum vessel

December
2016



secondary
2mm thick
Polycarbonate
screen
surrounds
rear of anode

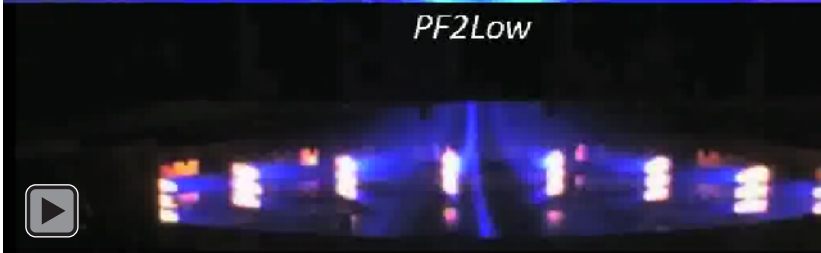
Shot 591



PF2Up

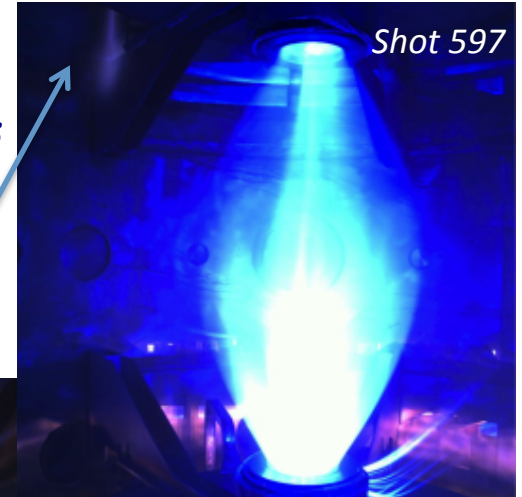


PF2Low



Secondary discharges hitting vacuum vessel wall have been cured by Polycarbonate lining, but **Spurious plasma currents still flow outside the centerpost (albeit inside the vacuum vessel)**

January 2017
patterns of spurious currents are either diffused or filamentary

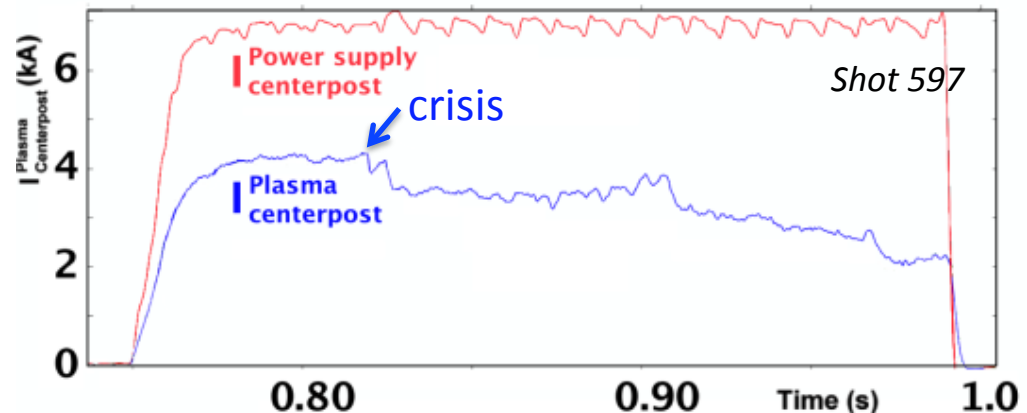


Shot 597

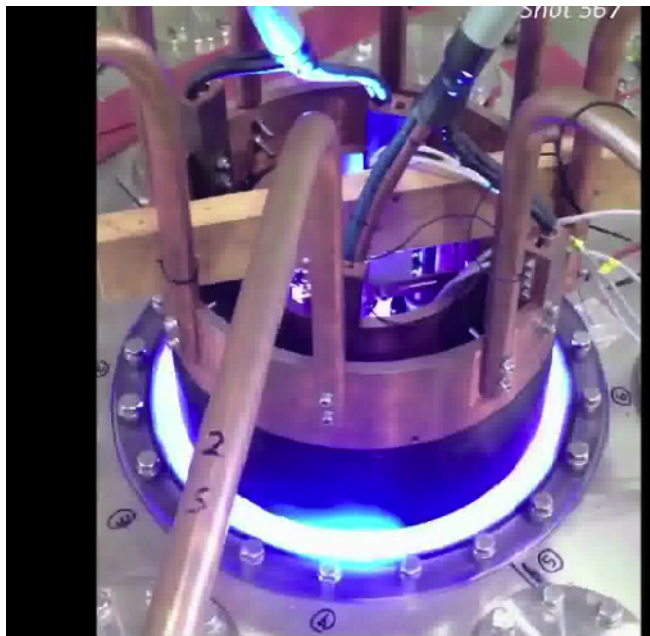


Shot 597

Input 0.6 MW
7 kA from power supply
Centerpost drives 60%

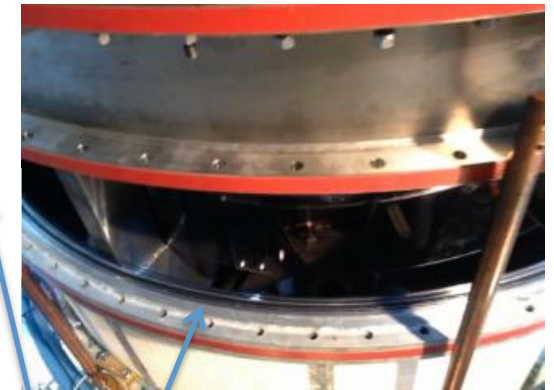
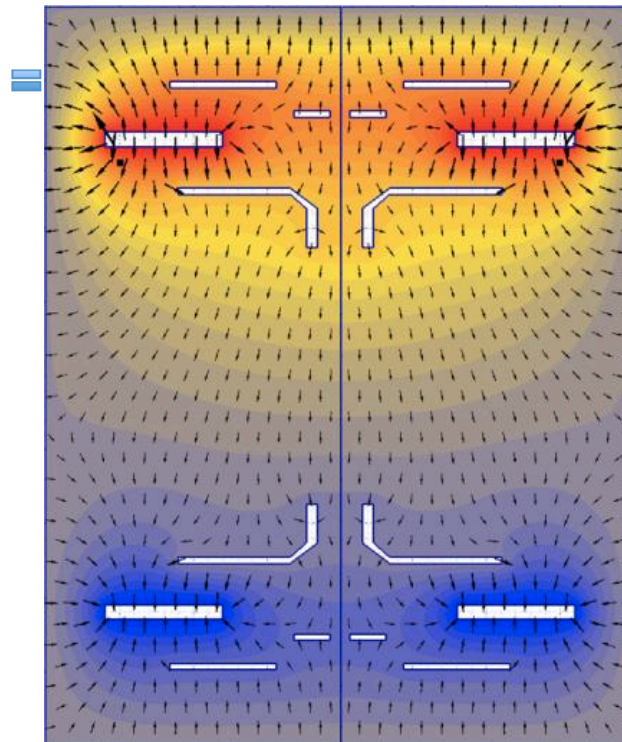


January 2017

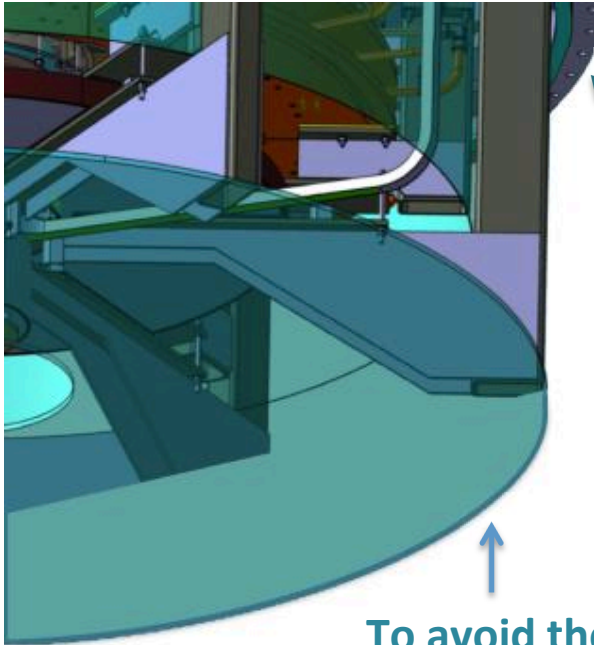


Secondary discharges hitting vacuum vessel wall have been cured by Polycarbonate lining, but **In Hydrogen (250 V breakdown) there was still a problem of current through the vessel, this was triggered in Argon (80 V breakdown),** connecting the common star potential of the six-phased cathode power supply to the machine GND

Most critical electric field is at contact between SS upper extension & Al vacuum vessel

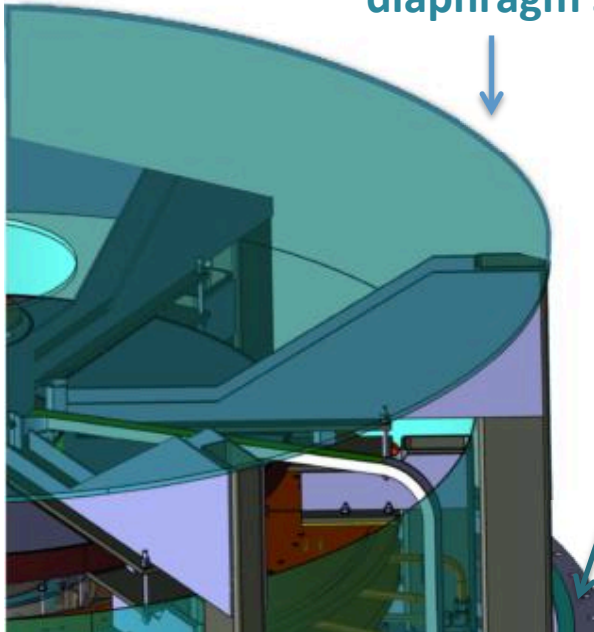


A spacing insulating ring was inserted in **May 2017**

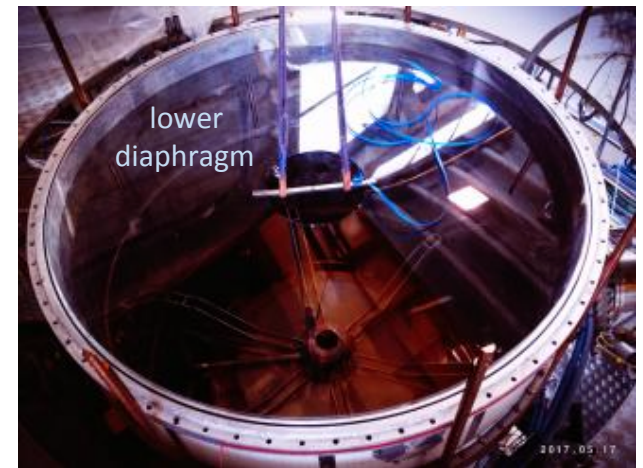


to avoid the bus-bar to vessel current flow an insulating spacer ring has been inserted

To avoid the flowing of plasma currents outside the desired path of the plasma centerpost two large insulating polycarbonate diaphragm separators have been inserted



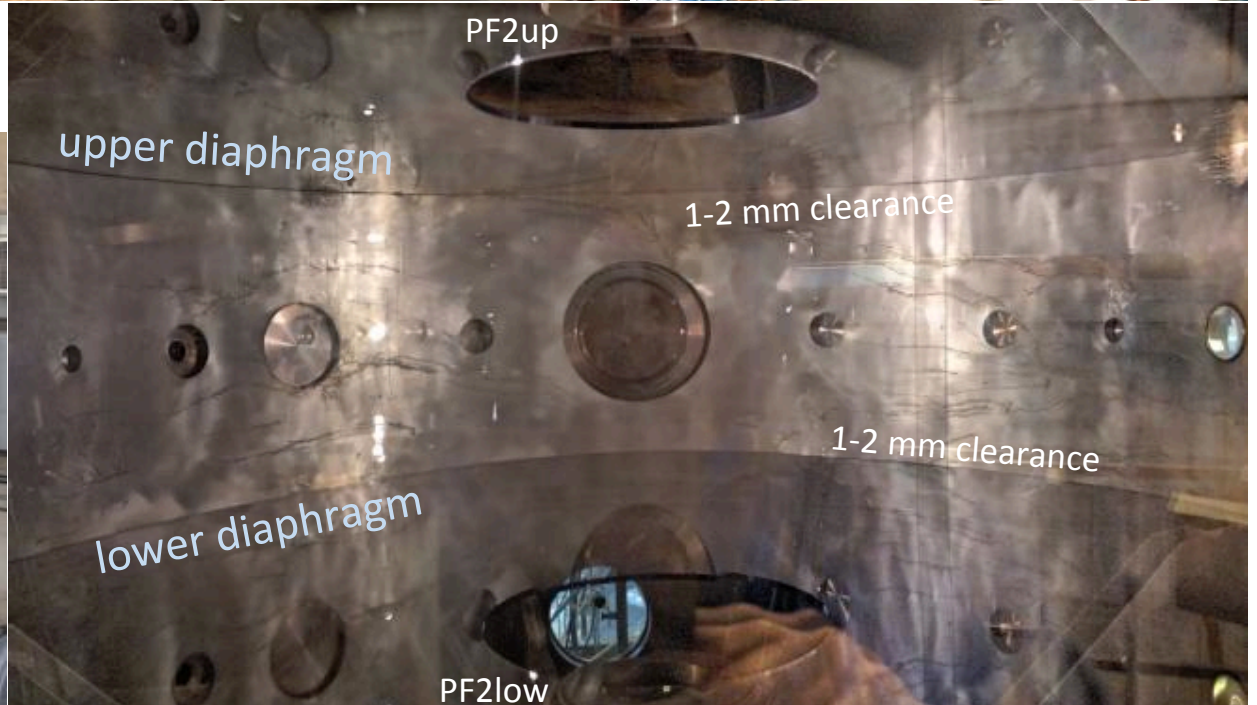
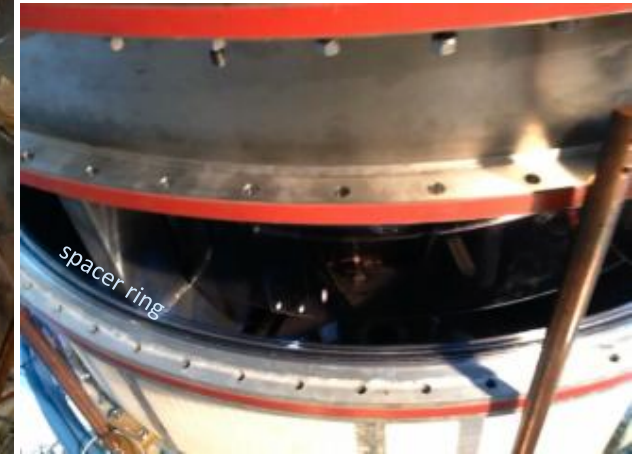
Lower spacer ring not yet inserted



May 2017: Insertion of Polycarbonate lower diaphragm



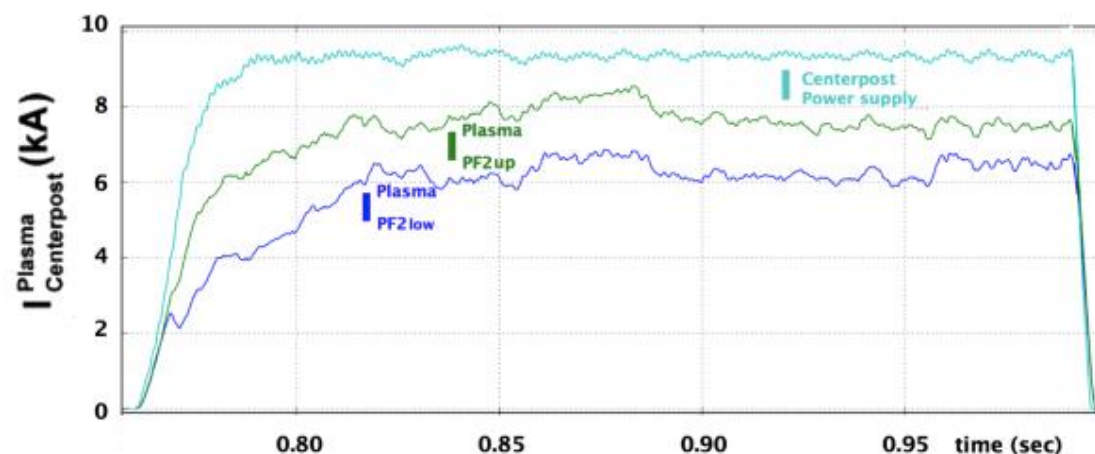
May 2017: Insertion of Polycarbonate upper diaphragm & Polycarbonate spacer ring



June 2017: Plasma with Polycarbonate two diaphragms & upper Polycarbonate spacer ring

High currents, external PF coils are on

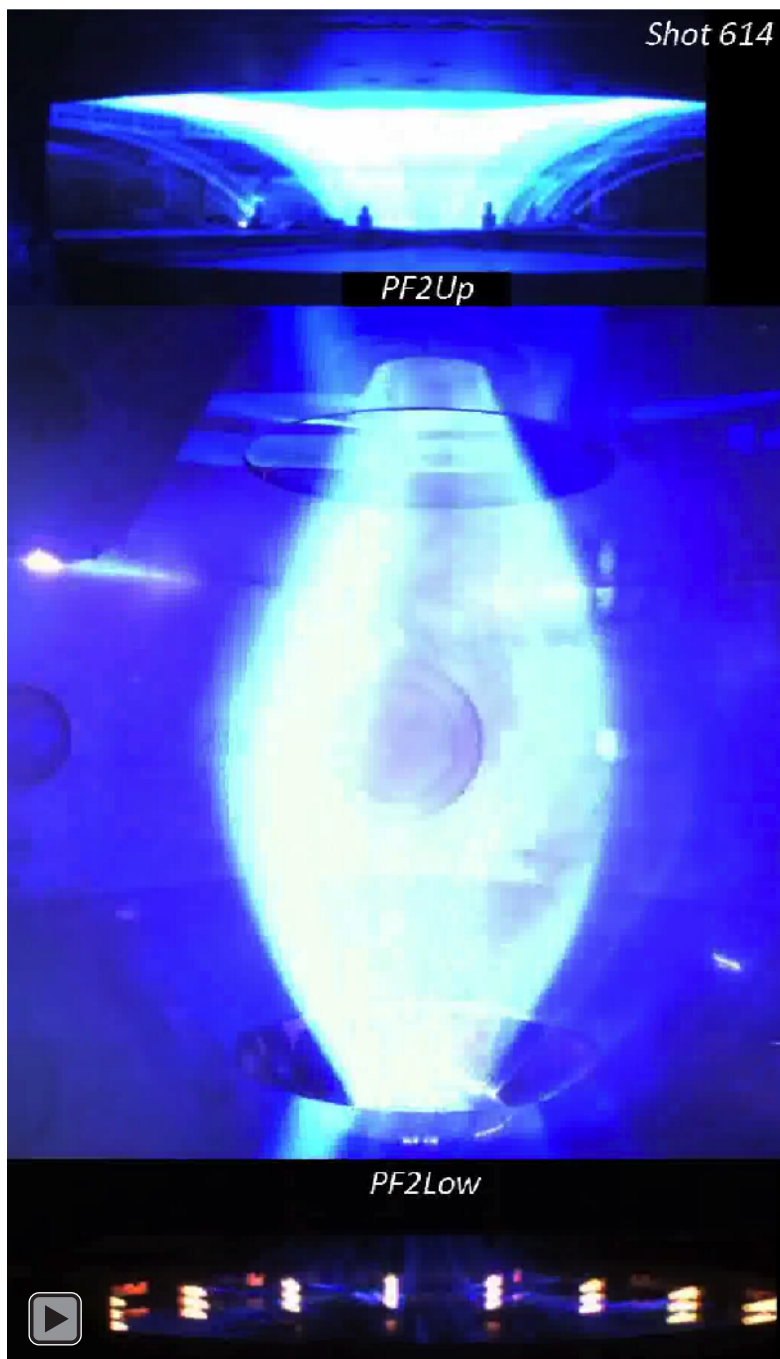
Some spurious and concentrated plasma current still sneaks through the narrow clearance (1-2 mm) bet'wn polycarbonate cylindrical lining and diaphragm, plasma currents with 8.6 kA through PF2 are achieved
Power input 1.65 MW, Anode-cathode voltage 195 V



With currents through PF2 exceeding ~ 6 kA the rotational transform of plasma centerpost ($q_{\text{Centerpost}} \sim 2$) becomes clearly visible

The plasma centerpost seems to rotate azimuthally in clockwise direction (looking from above)

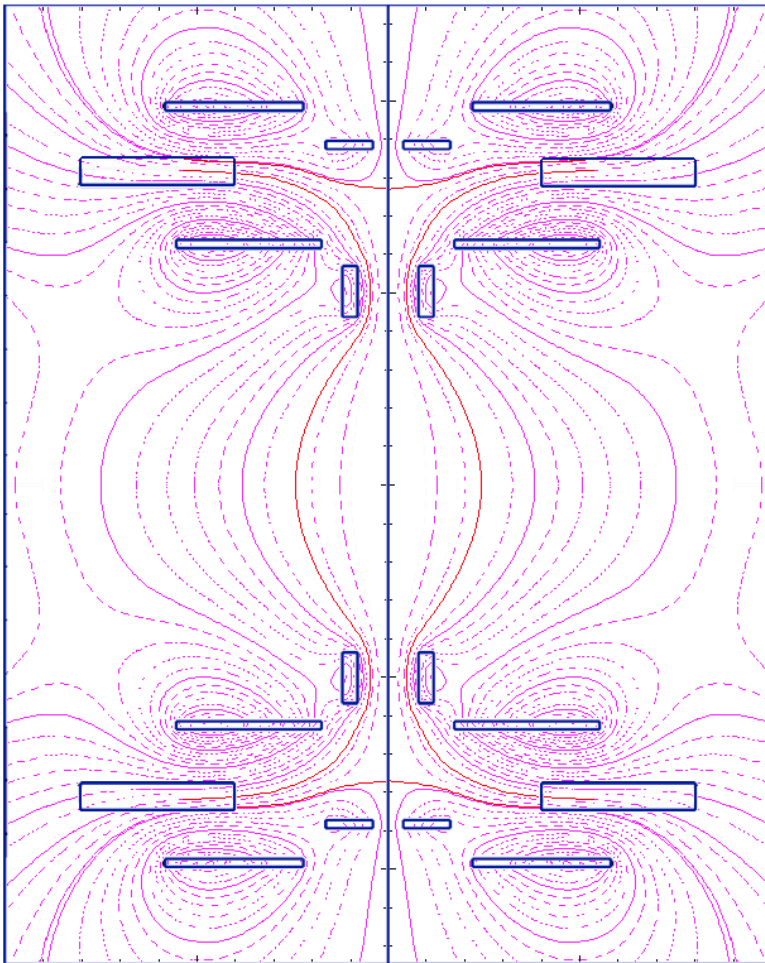
the spurious plasma current closes on the outside of PF2low, producing bright filaments



High currents (8 kA), switching on the external PF coils: PF coils casings built as floating
 Electrostatic potential is dominated by the plasma; **PF coils casings better left floating!**
 SS upper lid & upper extension also better left floating!

through Polycarbonate spacer ring

upper lid & extension float at 90 V ↓



$V_{PF4up} \sim 130 \text{ V}$

$V_{anode} \sim +150 \text{ V}$

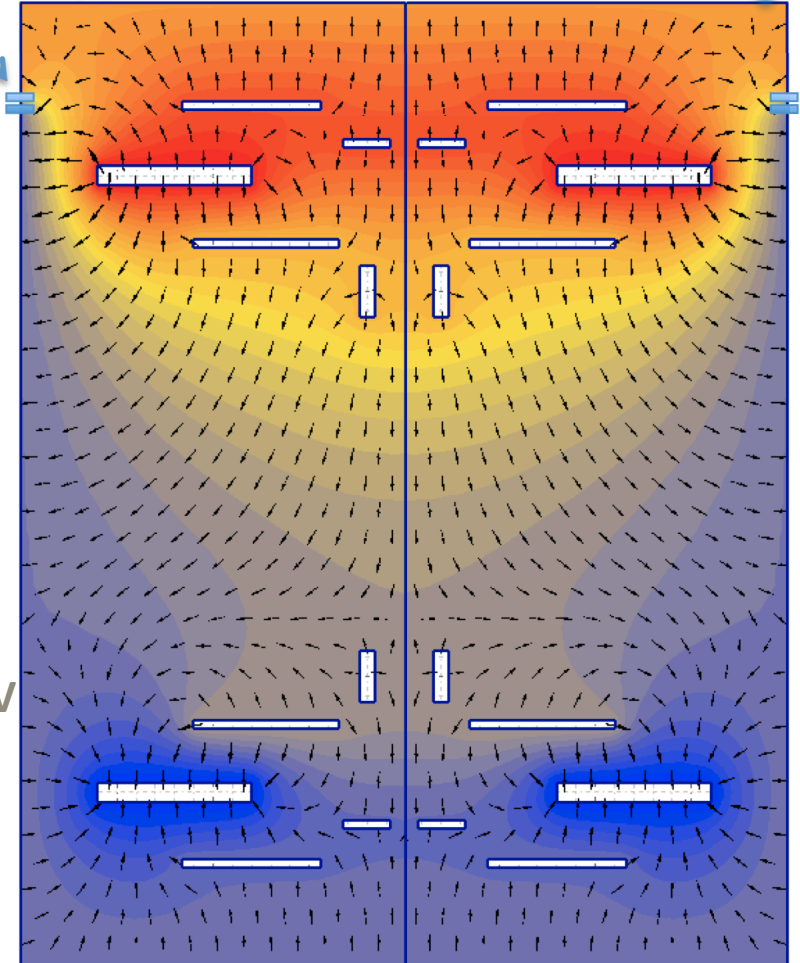
$V_{PF2-3up} \sim +75 \text{ V}$

#614, 8kA Argon
 Plasma centerpost
 June 2017

$V_{PF2-3low} \sim +20 \text{ V}$

$V_{cathode} \sim -45 \text{ V}$

$V_{PF4low} \sim -7 \text{ V}$



vacuum vessel at GND (0 V) ↑

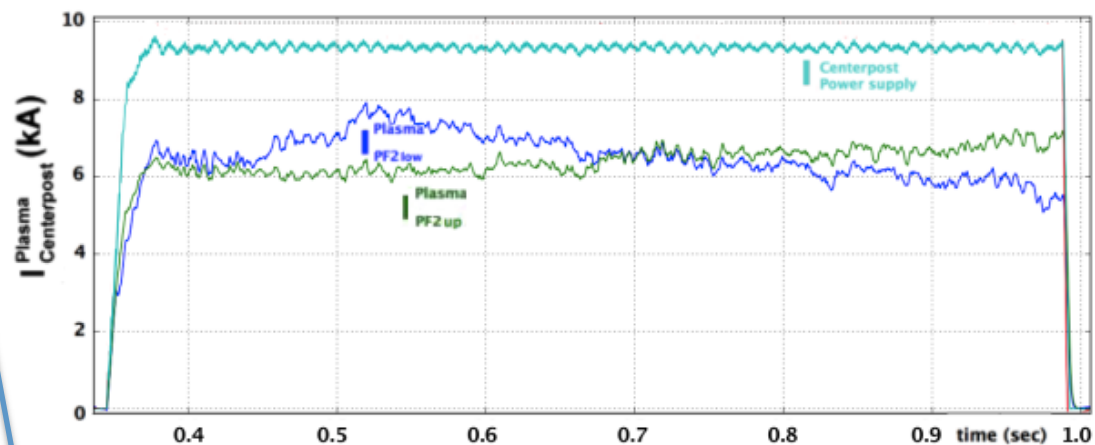
Line contours: magnetic field

Color contours: *electrostatic potential*, Arrows: E field



External PF coils are off, lower currents, 0.7 s persisting discharge

Switching off the external PF coils, long duration plasma centerposts have been obtained with plasma currents through the PF2 coils $\sim 6\div 7$ kA



The plasma centerpost discharge is quite near to the rotational transform value $\iota \sim \frac{1}{2} \rightarrow (q_{\text{Centerpost}} \sim 2)$

Autumn 2017: the narrow clearances will be closed completely by a bonding material (able to sustain the diaphragms' weight)

Shot 645



PF2Up

Kink destabilization persists for 0.7 s

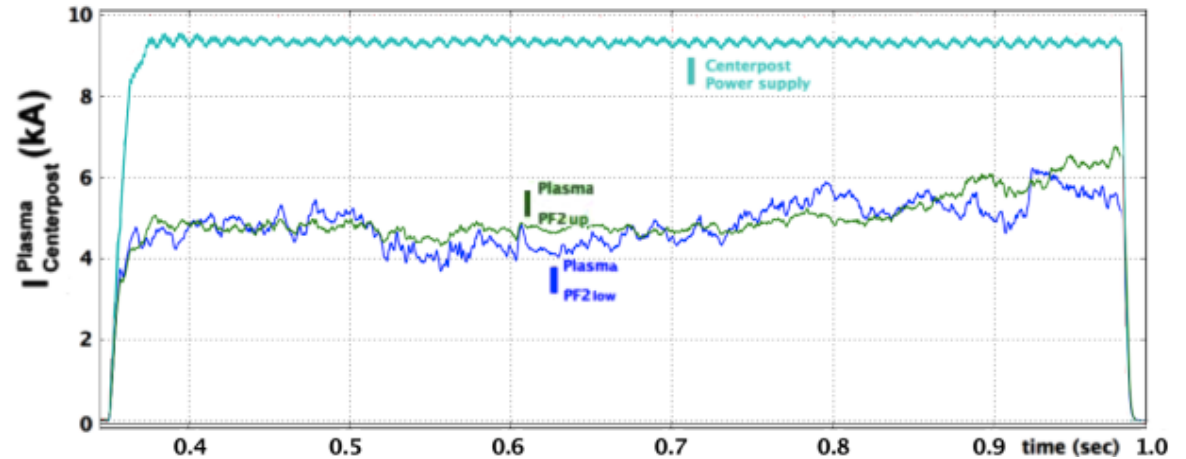
The anode plasma wobbles gently

Reducing by a factor of 4 the magnetic field of the internal PF coils, **the plasma centerpost has been destabilized**

A long duration kink-bended plasma centerpost has been obtained with plasma currents through the PF2 coils $\sim 5 \div 6$ kA



PF2Low



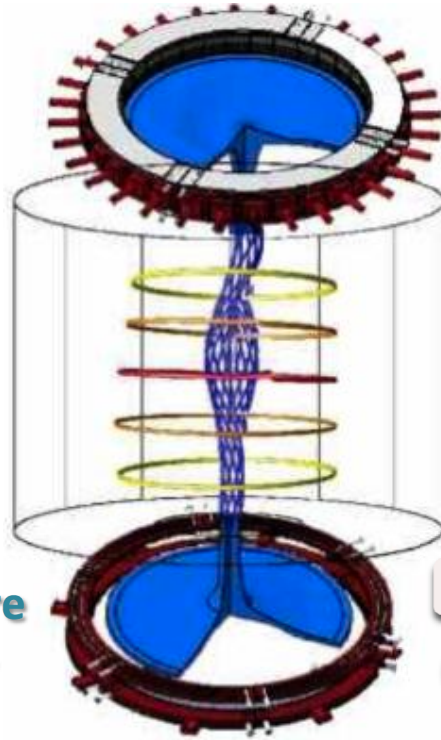
This plasma kink-bended centerpost discharge survives at a rotational transform value $\iota \sim 1.66 \rightarrow (q_{\text{Centerpost}} \sim 0.6)$

Cathode plasma wobbles more than centerpost, but the discharge survives till the DC voltage is applied!

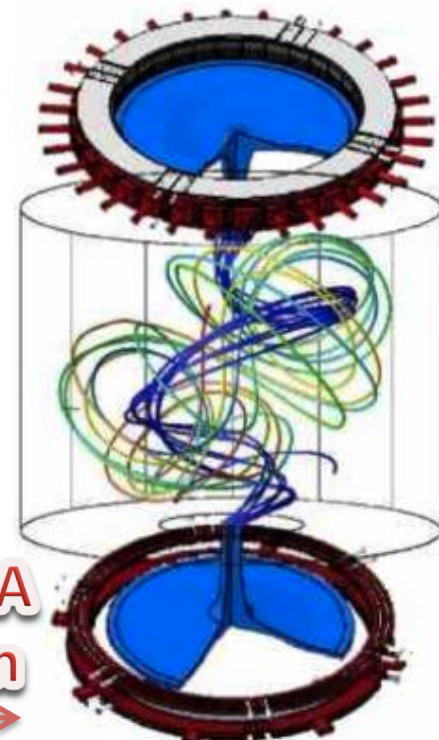


**Physics Design
1997-2008**

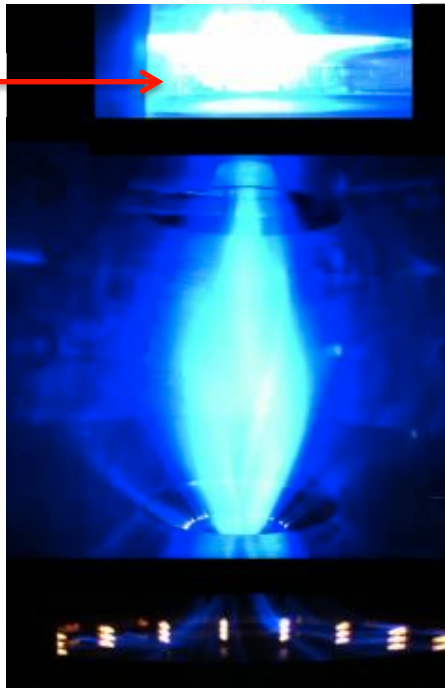
Langmuir probe
measurements give
 $10 \div 3$ eV temperature
 $2 \div 5 \cdot 10^{19} \text{ m}^{-3}$ density
at edge of anodic
plasma mushroom



**PROTO-SPHERA
destabilization**

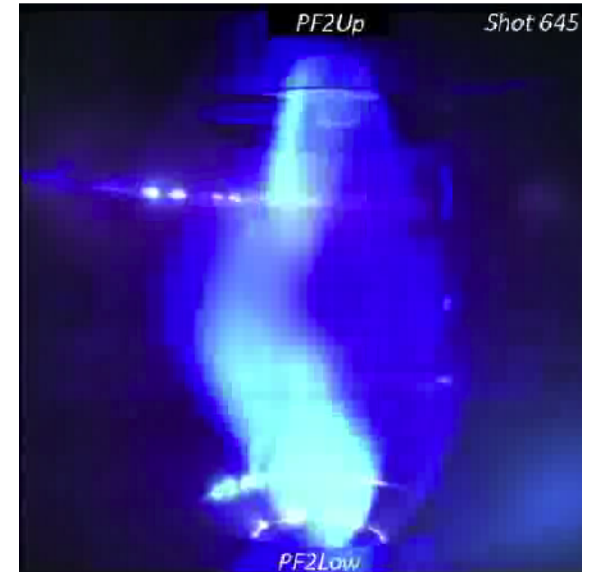
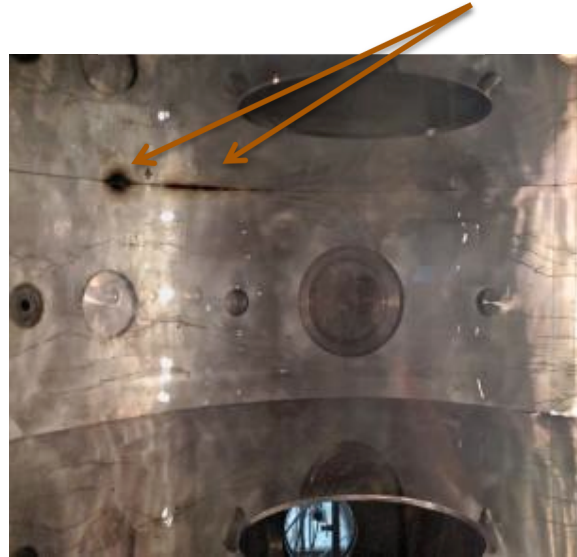


**Experiment
2017**

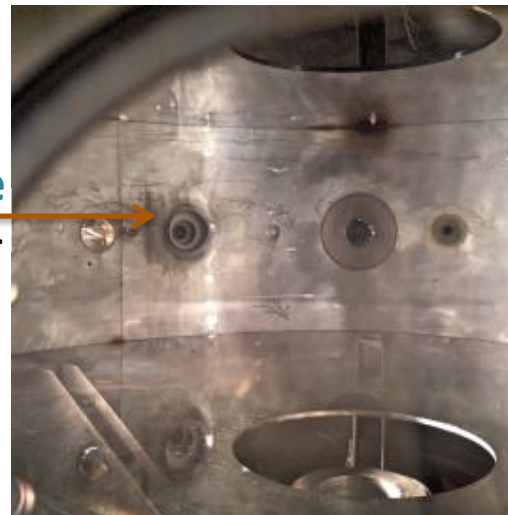


The plasma current sneaking through the narrow clearance (1-2 mm) between polycarbonate cylindrical lining and diaphragm induces damages

The narrow clearance has to be closed completely by a bonding material (able to sustain the diaphragms weight)



The port where the polycarbonate lining was cut, in order to allow for vacuum gauges measurements, has to be closed & the gauges moved elsewhere



A new insulating & transparent vacuum vessel has to be built: will be Phase-II ready

If whole current of power supply (10 kA) is successfully driven in the Argon centerpost plasma

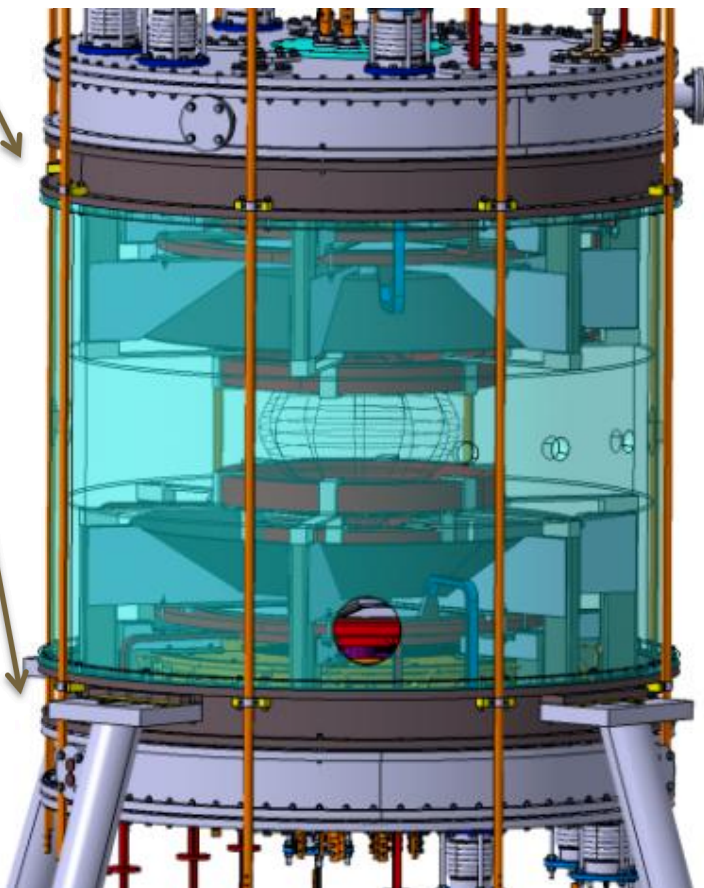
it will be necessary to substitute the Al vacuum vessel with a

a Polymetacrylate (PPMA) transparent and insulating vessel (5 cm thick, 2m \varnothing , 1.6 m high)

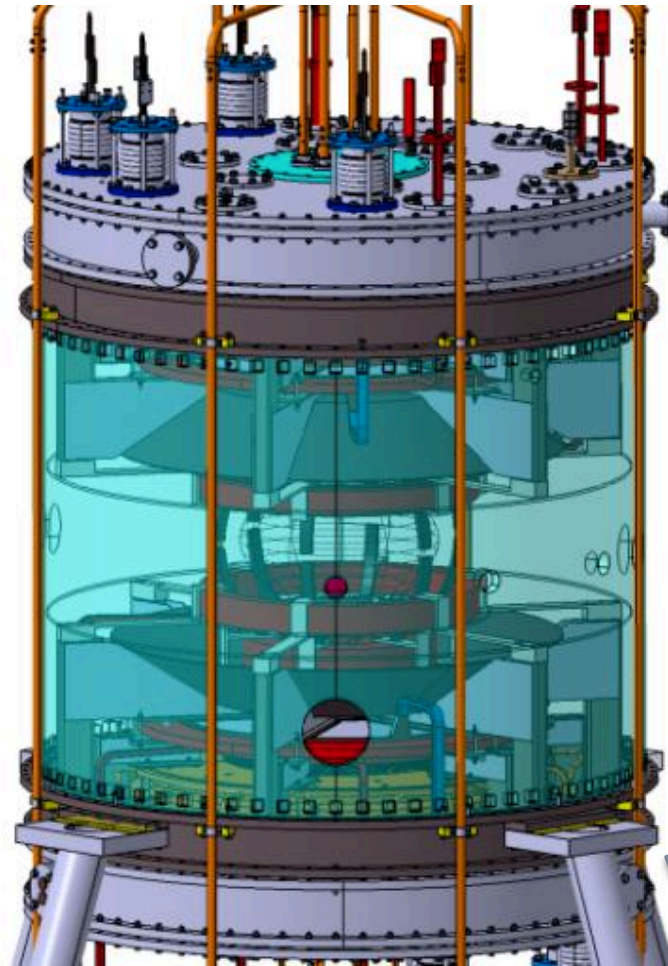
adding 2 further SS rings on top & bottom of the experiment,

keeping all internal components attached to the existing SS upper/lower lid and extension

then try Hydrogen plasma

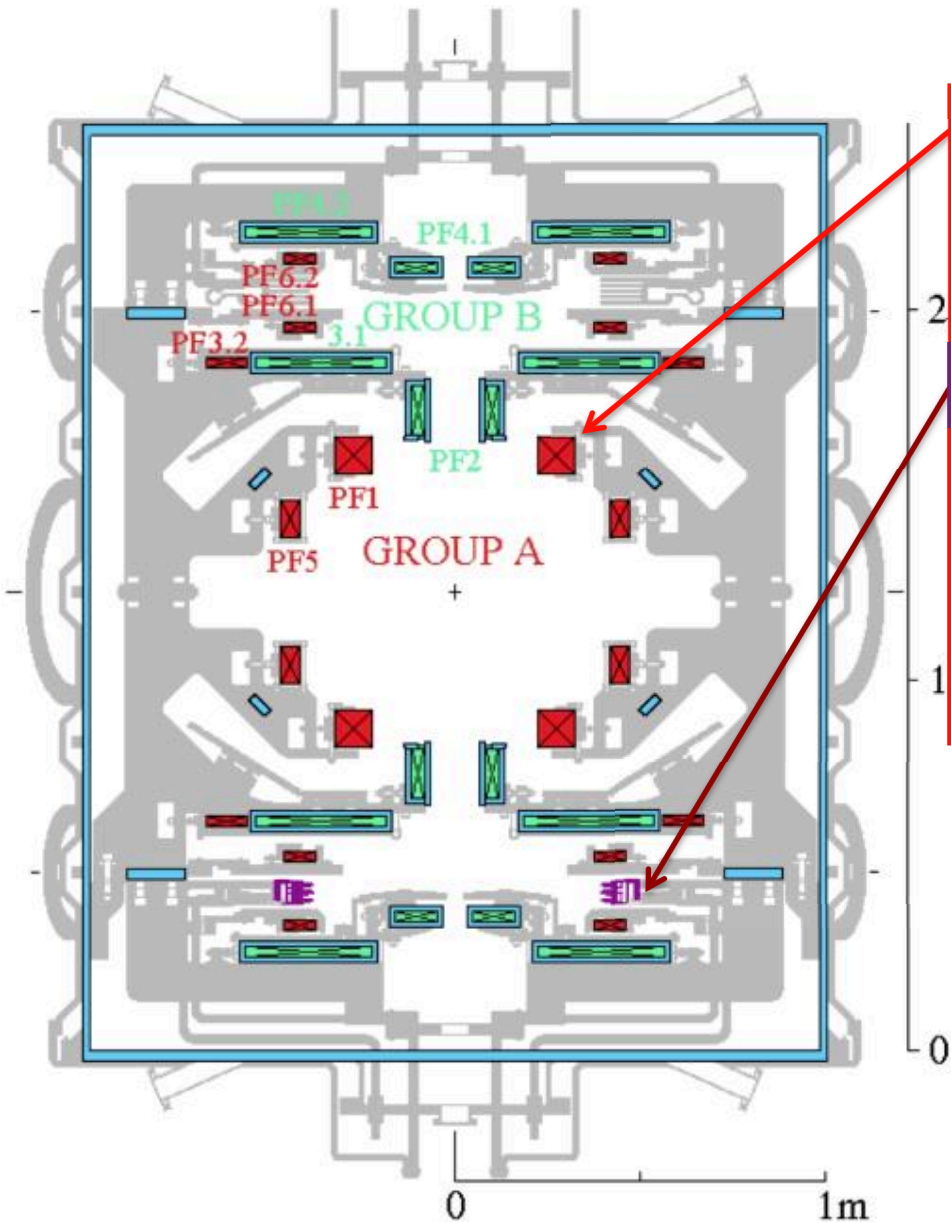


flanged PPMA cylinder



carved PPMA cylinder

To be build, after 10 kA plasma centerpost routinely achieved, full PROTO-SPHERA load assembly and power supplies



Group A: ST compression coils (5+5 series)
Not yet built, but inner vessel ready to host

- high voltage (~ 20 kV) insulation
- thin Inconel casings

cost ~ 0.5 M€

Tungsten filaments (54 \rightarrow 324) cost ~ 0.2 M€

Final Power Supplies for:

- 1) Group A PF coils cost ~ 0.1 M€
- 2) Cathode ($I_{\text{cath}} 10 \rightarrow 60$ kA) cost ~ 0.2 M€
- 3) Centerpost ($I_e 10 \rightarrow 60$ kA) cost ~ 0.6 M€

SuperCapacitors will be used

Cost up to now ~ 2.0 M€
Cost for final stage of experiment ~ 1.6 M€



No additional heatings for PROTO-SPHERA?

...magnetic reconnections quite efficient in heating up the Solar Corona!

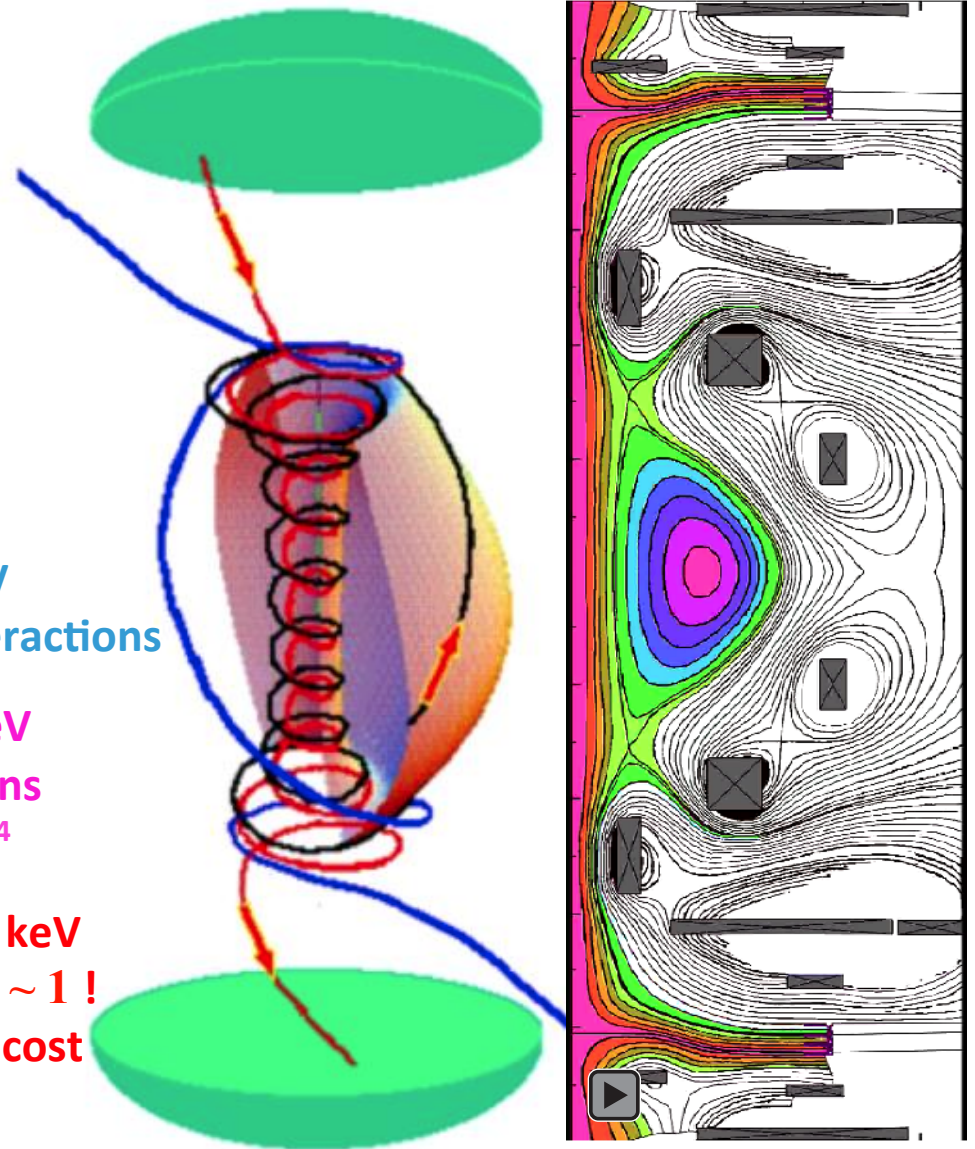


Power injected into the centerpost should be $> 250 \text{ V} \cdot 60 \text{ kA} = 15 \text{ MW}$...

It is a huge power into such a small plasma
...however how much will go into the confining Spherical Torus, through magnetic reconnections?

No one is able to predict:

- should it be \sim zero, then ST plasma $T = 10 \text{ eV}$
PROTO-SPHERA studies plasma-electrode interactions
- should it be 1 MW, then ST plasma $T = 100 \text{ eV}$
PROTO-SPHERA studies magnetic reconnections at relevant magnetic Lundquist number, $S=10^4$
- should it be many MW, then ST plasma $T = 1 \text{ keV}$
... $\beta \sim 1$!
...would do as a Tokamak, but at 1/100 of the cost



Perspective

。。。放龙如海! fànglóng rùhǎi
...set free the Dragon into the sea!



Proto-Sphera will assess a new magnetic confinement configuration

- simply connected (easier construction & maintenance)
- sustained (indefinitely?) by helicity injection, through magnetic reconnections
- mixed magnetic & electrostatic confinement, major role of plasma velocity?
- (if magnetic reconnection efficient) high plasma beta? (minimal geometrical size)

Proto-Sphera can develop this program:

at very modest costs (~ 1.6 M€); in a flexible way (new components can be easily added)

PROTO-SPHERA Phase2 will be much more demanding in manpower and effort than the present Phase1 of PROTO-SPHERA with Centerpost plasma only

Will be an experiment as much challenging for Frascati as START was for Culham

- *with sophisticated control requests (very fast rise of currents for Torus formation)*
- *with demanding diagnostic requests*
- *challenging physicists, engineers and technologists creativity with its adaptability*
- *easily modifiable and therefore an ideal ground for student and PhD theses*

Fasten seatbelts: surprises along the road!



+ Other authors

