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The role of integrated modeling in the development of more robust real-time control algorithms (for NTMs)

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Acknowledgments:

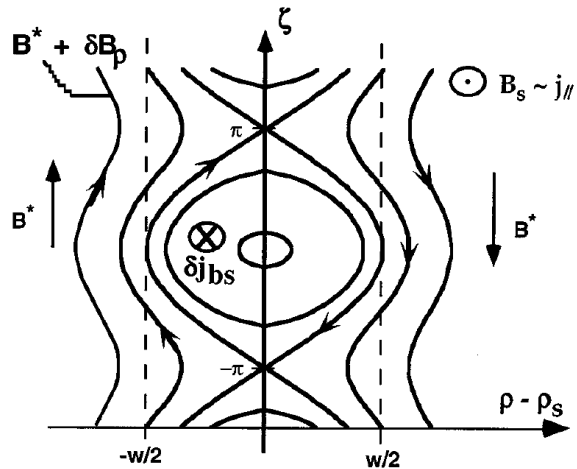
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The view and opinions expressed herein do not necessarily reflect those of the ITER Organization.*

Real-time control algorithms use reduced models, but they can benefit from high fidelity physics models

- Neoclassical Tearing Modes, why we care
- NTMs on ITER: where the standard approaches fail
- What does TRANSP add to NTM control?
- NTM control on ITER: what we have learnt

NTMs can lead to significant confinement degradation



- No hard limit on β_N but confinement degradation
 - $\Delta\tau_E/\tau_E \sim 4\rho_s^3 w_{\text{sat}}/a$
 - $\Delta\tau_E/\tau_E \sim 20\%$ observed for (3,2)-NTM
 - higher for (2,1)-NTM at low q_{95}
 - NTMs can lock and lead to disruptions
 - one of the principal causes of disruption on JET
- => NTM control critical for the success of ITER**

NTM control with ECCD widely used:

- replaces J_{BS} with J_{ECCD}
- highly localized ECCD deposition
- EC power modulation for alignment with O-point
- sweeping over ρ_s to compensate for lack of tracking
- high flexibility in complex control schemes
 - pre-emptive: sawtooth + NTMs
 - active detection and suppression

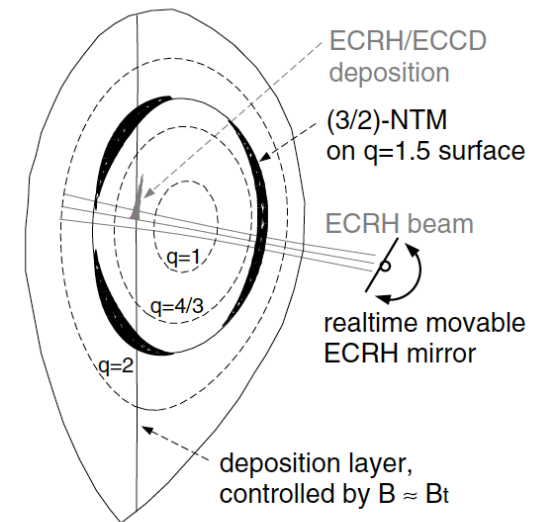


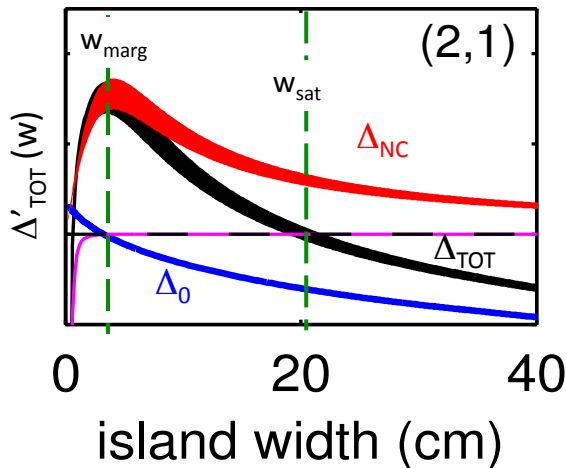
Fig.2 in Maraschek, NF 52 (2012)

Will the same techniques work on ITER?



ITER extrapolations are based on asymptotic solutions

$$\frac{dw}{dt} = 1.22 \frac{\eta}{\mu_0} [\Delta'(w) + \Delta'_{NC} + \Delta'_{pol} + \Delta'_{GGJ} + \Delta'_{ECCD} + \Delta'_{ECH}] \quad \text{Modified Rutherford Equation}$$



- find $dw/dt=0$ for given equilibrium and kinetic profiles

Zohm: $\eta_{NTM} > 1.2$

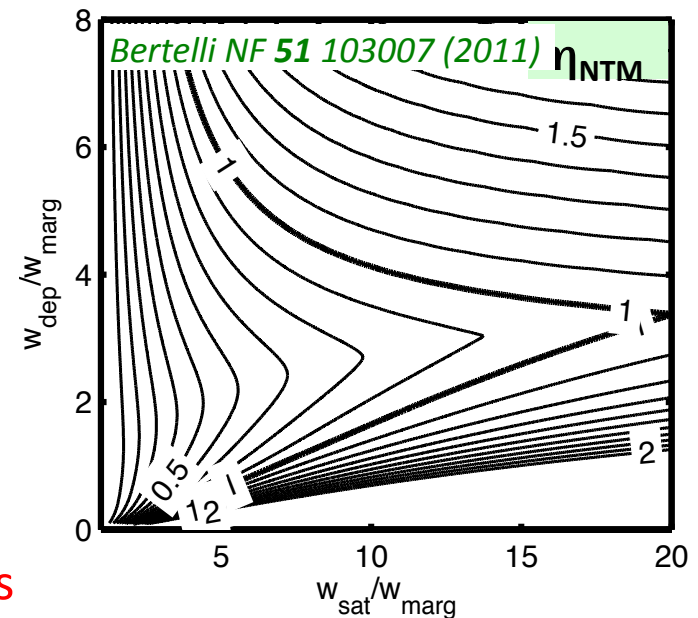
Sauter: $\eta_{NTM} w_{dep} > 5\text{cm}$

$w_{dep} < 5\text{cm}$

- scan island parameters and EC deposition to find

- figure of merit η_{NTM} : $P_{NTM} = \eta_{NTM} P_{EC} J_{BS} / J_{CD}$

- η_{NTM} useful for real-time control applications



Stabilization criteria depend on plasma parameters and EC deposition width, which change in time



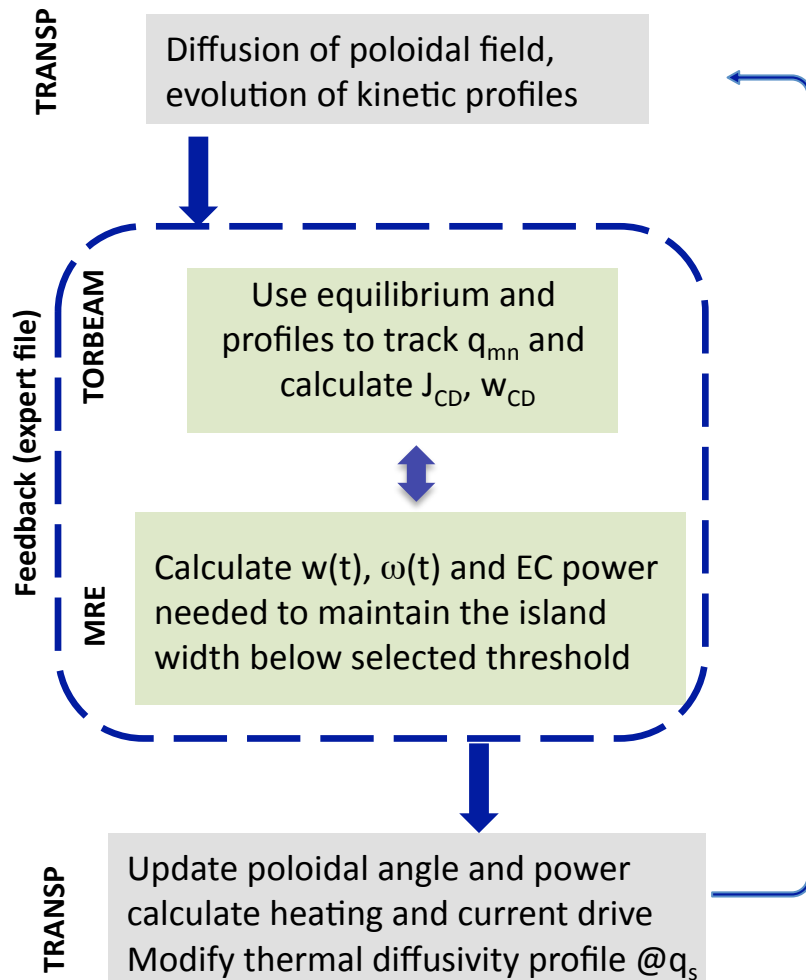
Asymptotic solutions do not account for dynamic response of the system

- effects of misalignment (systematic or transient)
- threshold effects on the detection of the island
- (changing in time) broadening of EC deposition
- time-scales of NTM growth, as compared to hardware constraints
 - ≤ 3 s \Rightarrow how fast the power can be switched between mirrors (switch design)
 \Rightarrow affects combined applications with EL/UL (core heating+MHD)
 - 1 s \Rightarrow how fast the Upper Launcher can sweep over the full poloidal range
 \Rightarrow affects combined applications with UL (sawteeth+NTM)
- the plasma response to ECCD and ECRH.

Assessment of NTM control should account for all these effects for optimization of available resources



Self-consistent evolution of NTMs and plasma profiles can help designing stable discharges and more robust control schemes

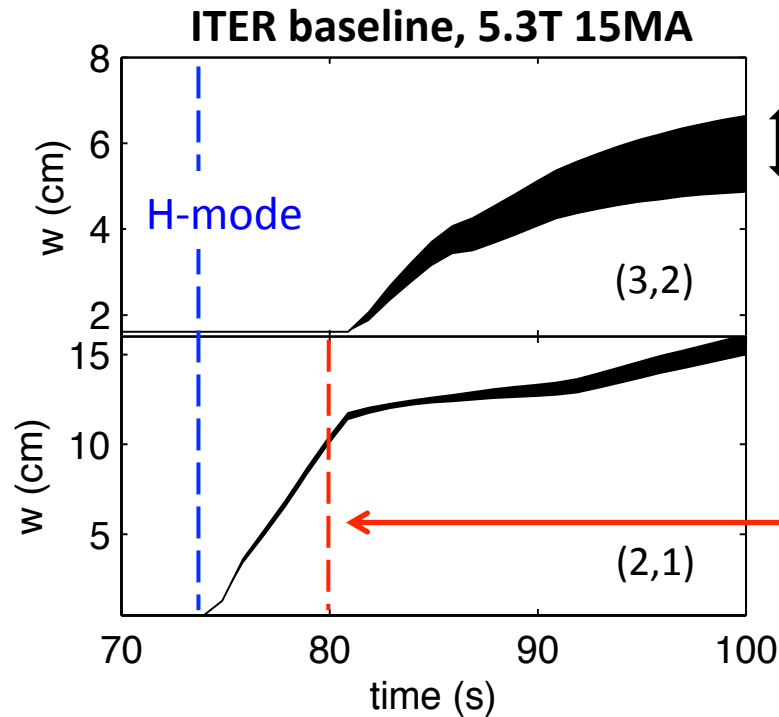


- Interface TRANSP with MRE for self-consistent calculation of plasma equilibrium, HCD and NTM evolution, with EC feedback control.
- Advantages: evaluate plasma response to EC feedback for control schemes assessment

CAVEATS:

- validation against experiments (ASDEX-U, JET, DIII-D, NSTX) in progress.
- NTM onset conditions might require additional stability calculations

(2,1)-NTM grows and locks faster than power switch



Uncertainty due to choice of k_1 :

$$\Delta'_{NC} = k_1 \frac{16J_{BS}}{s \langle J \rangle} \frac{w}{w^2 + w_d^2}$$

(2,1)-NTM onset soon after H-mode

(2,1)-NTM locks after ~5s

ECE threshold ≥ 2 cm



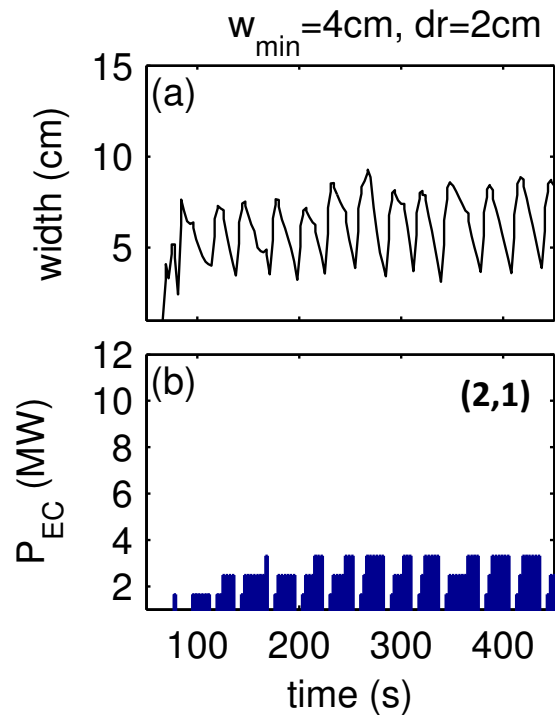
<3s between detection and locking

Equilibrium reconstruction ≥ 2 cm

Not enough time to search for (2,1)-NTM and suppress it.
It has to be prevented from growing above threshold



Switching power between applications not a viable solution



EC feedback control

- Assume EC is used for anything than NTM control
- Wait until island size exceeds w_{\min}
- calculate EC power needed to drop $\Delta'_{\max}=0$
- move EC power to the Upper Launcher (it takes 3s)
- when island $w < w_{\min} \Rightarrow$ drop power to 0

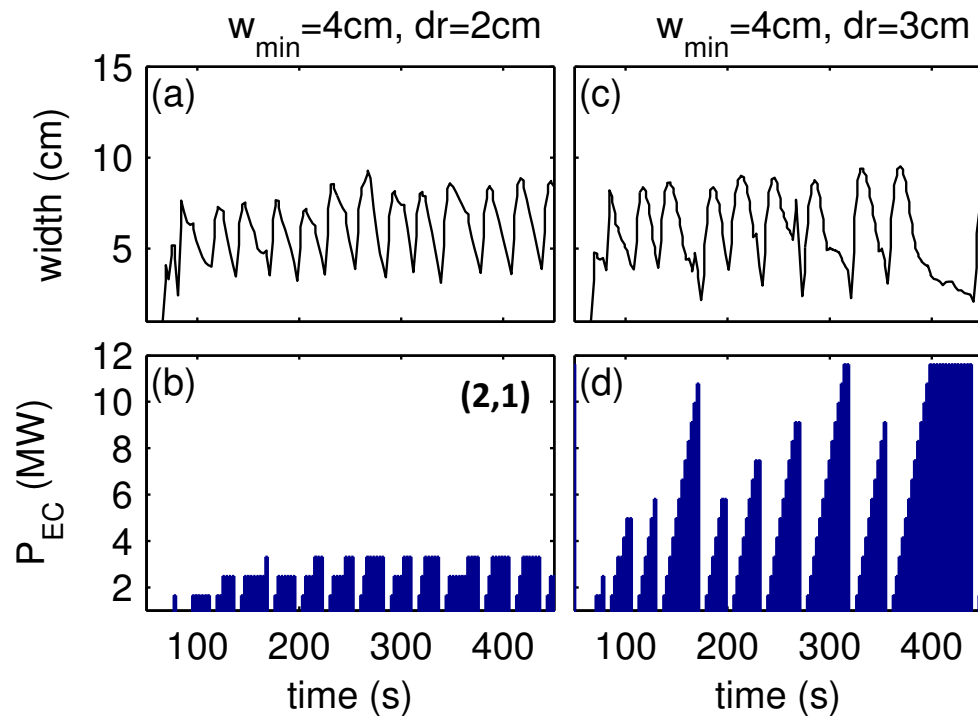
\Rightarrow NTM grows back as EC removed from (m,n)

Implication #1: Power needs to be reserved for control of (2,1)

In 3s the island has time to grow back (high β_{pol} in ITER)
But it takes <100ms to turn on/off a gyrotron



Maintaining good alignment is critical



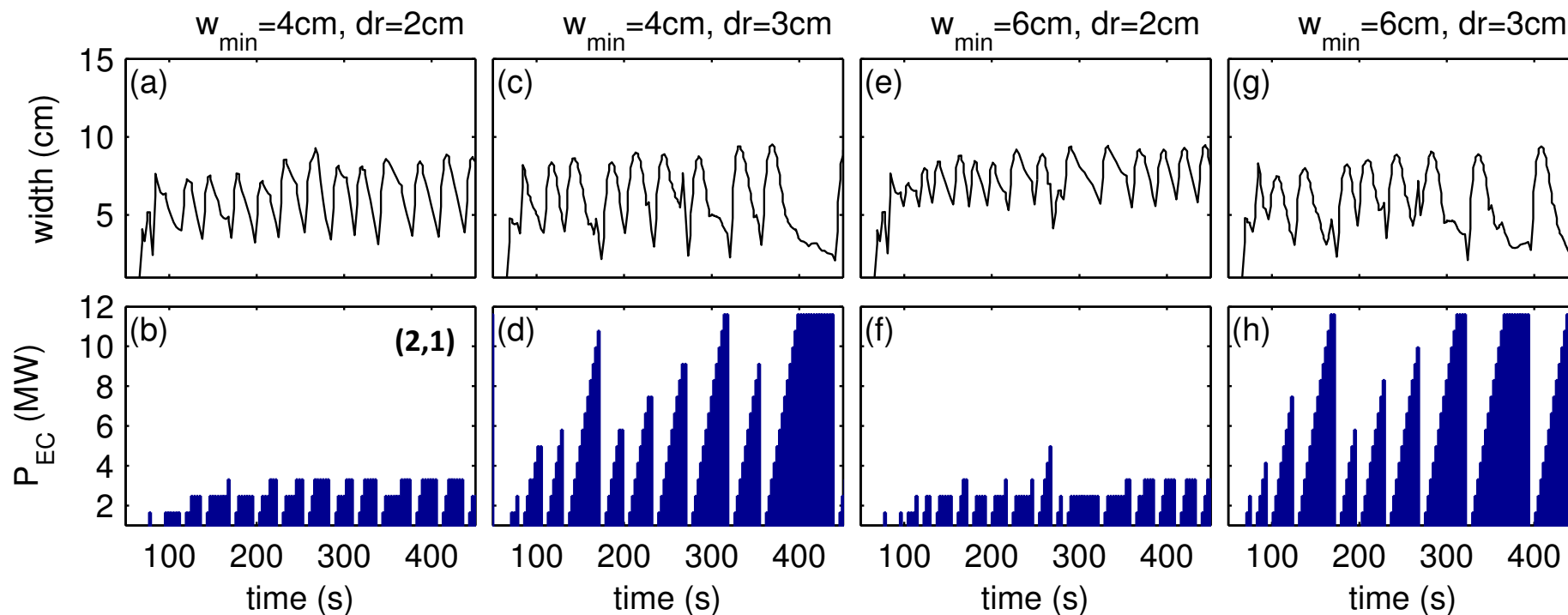
Lower power needed if EC is better aligned.

⇒ even 1cm does matter

Implication #1: Power needs to be reserved for control of (2,1)

In 3s the island has time to grow back (high β_{pol} in ITER)
But it takes <100ms to turn on/off a gyrotron

Good alignment more important than S/N detection

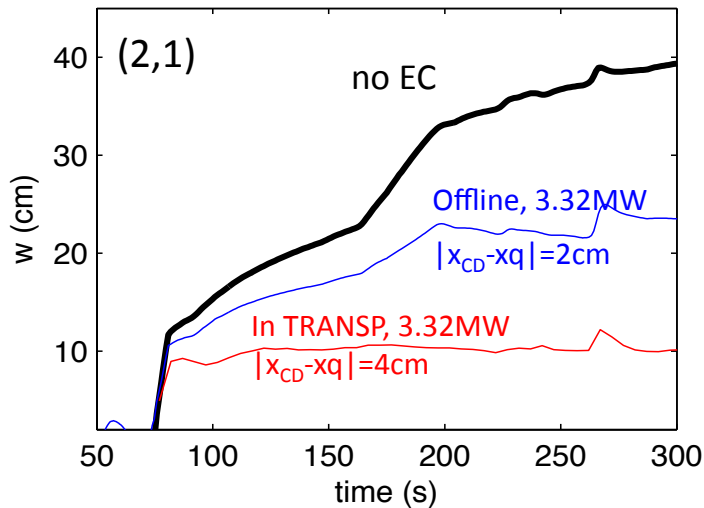


Implication #1: Power needs to be reserved for control of (2,1)

Implication #2: pre-emptive control preferable for stabilization of (2,1)



Self-consistent calculation of NTM evolution and plasma profiles set lower limits on EC power needs

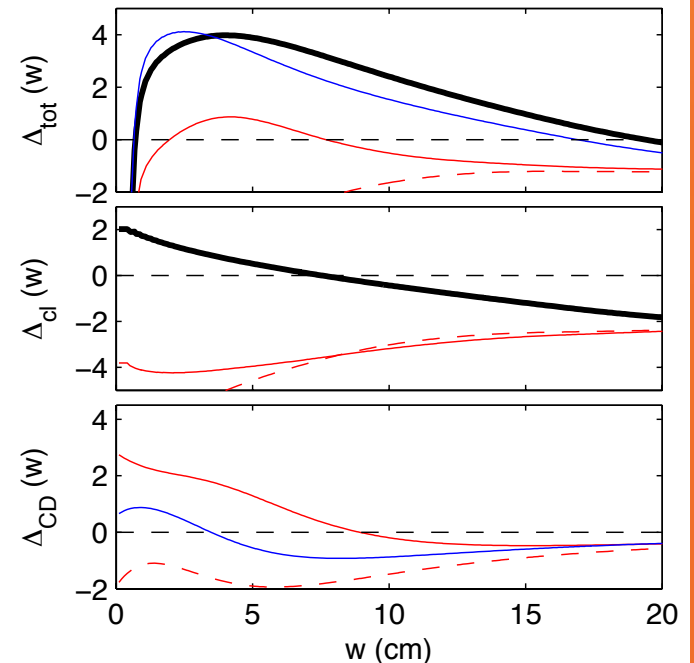


- Δ'_{CL} responds to local modification of current profile
- Δ'_{ECCD} responds to time variations of $|x_{CD}-x_q|$ and w_{CD}

if $|x_{CD}-x_q| = 2\text{cm}$ \Rightarrow full suppression in TRANSP, unstable offline.

$$\Delta'_{CD} = 32\pi^{1/2} \frac{J_{CD,max}}{\langle J_\phi \rangle s} F(\tilde{w}) M(\tilde{w}, D) G(\tilde{w}, x_{dep})$$

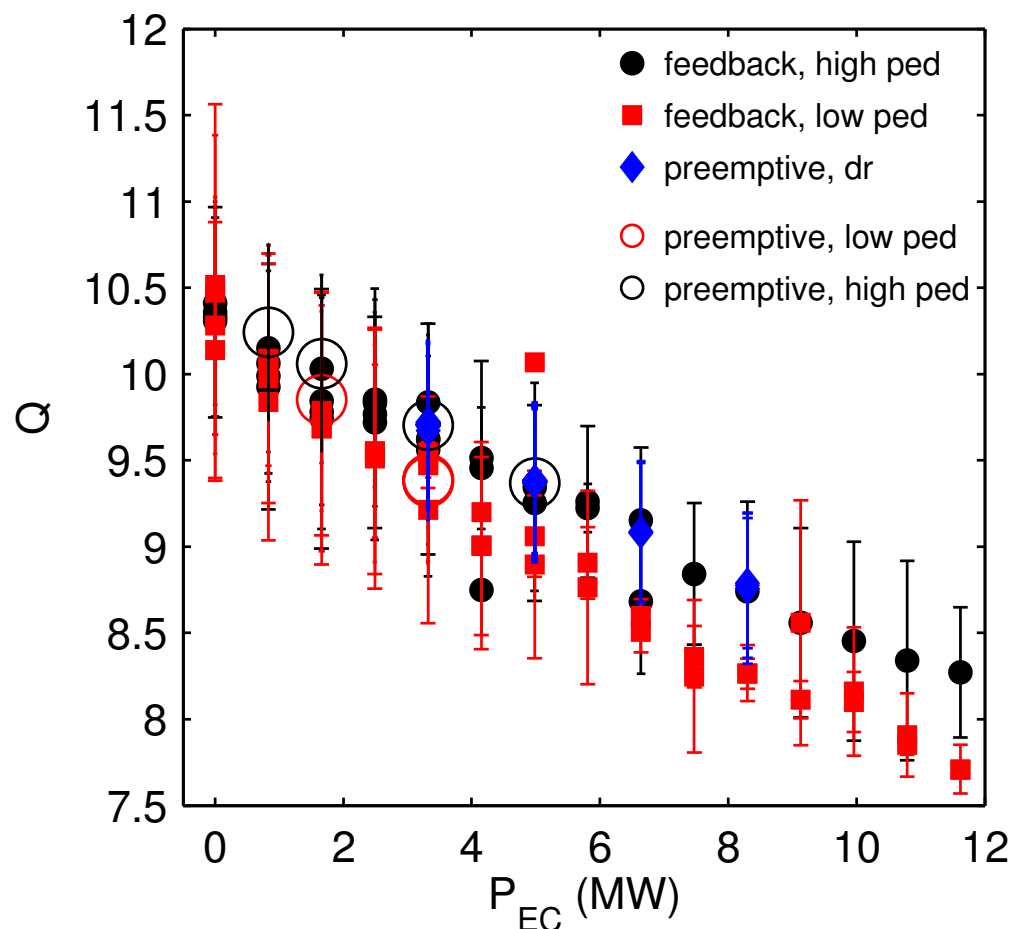
↑ Deposition profile
 ↑ Modulation
 ↑ Alignment



\Rightarrow 5-8 MW need to be reserved for NTM control
 (instead of 20MW as previously assessed with offline calculations)



Pre-emptive control is a good compromise between NTM control and minimum reduction of Q



Active search for NTM =>

$Q \sim 7.5 - 10$

P_{EC} up to 12 MW

Pre-emptive control =>

$Q \sim 9$

P_{EC} up to 5 MW

In both cases $w \sim 6-10\text{cm}$ @ $q=2$

$\Delta\tau_E/\tau_E \sim 10-15\%$



Self-consistent calculations set lower limits on EC power requirements on ITER, but more constraints on control

- NTM control techniques used on present-day experiments might not be directly applicable to ITER
- When plasma response is taken into account in the assessment, upper limit on EC power is reduced to 5-8MW.
- Fast growth rate raises question on active search and combined sawtooth-NTM control on ITER
- Need to pre-emptively stabilize the (2,1)-NTM
- Pre-emptive control minimizes power usage
- Broadening deposition profile up to 6-7cm required on $q=2$
- EC alignment within $0.5w_{CD}$ required
- Alignment more important than S/N of detection diagnostic



Recycle an old code for TFTR and include EC

E. Fredrickson PoP 7 4112 (2000)

$$\frac{\partial w}{\partial t} = 1.22 \frac{\eta}{\mu} [\Delta'(w) + \Delta'_{nc} + \Delta'_{pol} + \Delta'_{GGJ} + \Delta'_{CD}]$$

$$\Delta'_{NC} \approx k_1 \frac{16 J_{BS}}{s w \langle J \rangle} \approx \frac{16 J_{BS}}{s \langle J \rangle} \frac{w}{w^2 + w_d^2}$$

$$w_d \approx 5.1 k_d \frac{r_s}{\epsilon s n} \left(\frac{\chi_{\perp}}{\chi_{\parallel}} \right)^{1/4}$$

Threshold condition

$$\Delta'_{pol} \approx -k_2 \frac{\rho_{\theta i}^2 \beta_{pol} g(\epsilon^{3/2}, v_i/\omega_{*e})}{w^3} \left(\frac{L_q}{L_p} \right)^2$$

NOTE: island rotation frequency not included yet in TRANSP

$$\Delta'_{GGJ} \approx -5.4 k_4 \frac{\beta_{pol} \epsilon^2 L_q^2 q^2 - 1}{r_s w |L_p| q^2}$$

W. Houlberg PoP 4 3230 (1997)

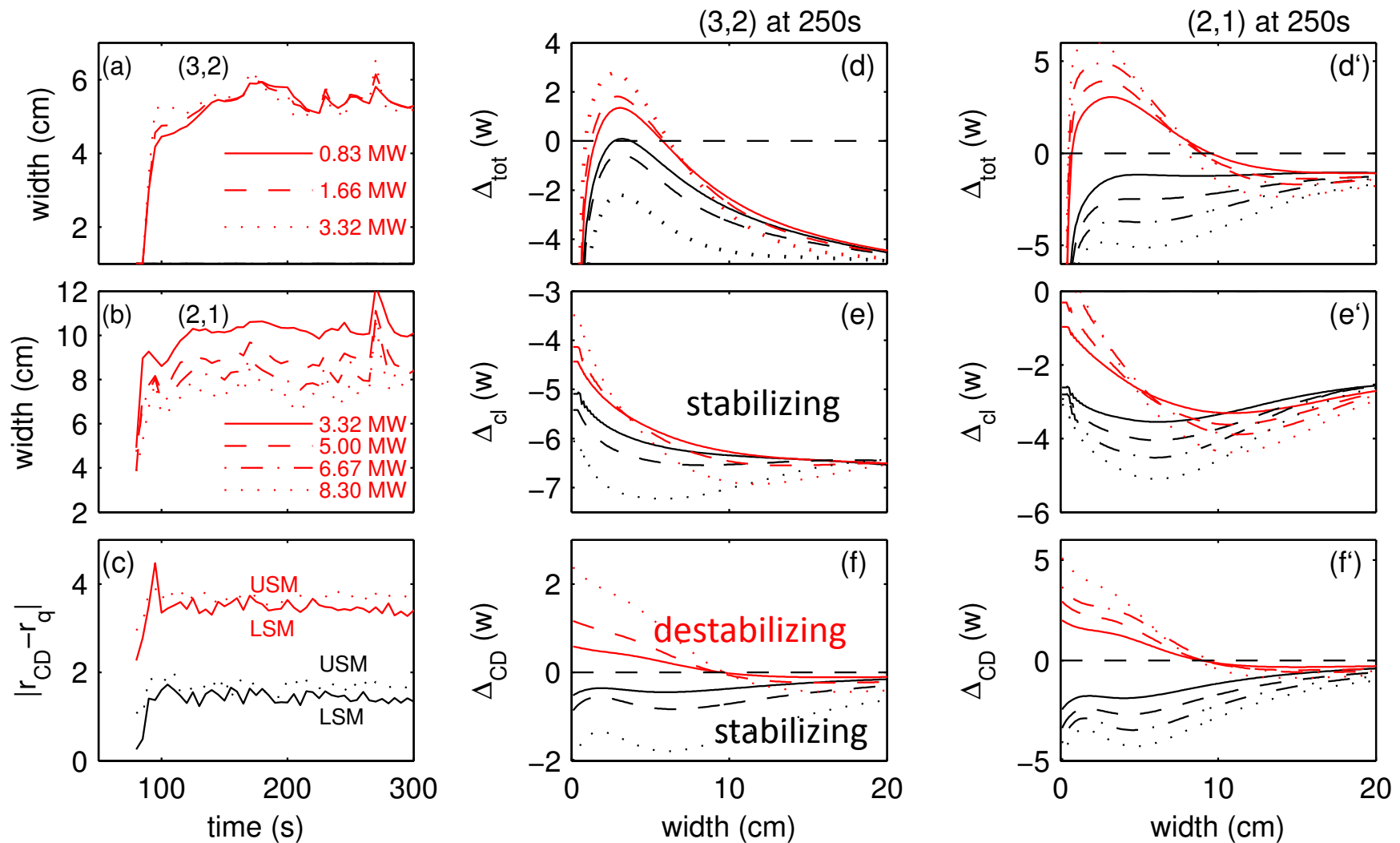
$$\Delta'_{CD} = k_6 16 \pi^{1/2} \frac{\mu_0 L_q}{B_p} \frac{J_{CD,max}}{w_{CD}} F(w) M(w)$$

N. Bertelli NF 7 51 103007 (2011)

$$F(w) = 0.25 \frac{1 + 0.96 \tilde{w}}{1 + \tilde{w} (1.5 + \tilde{w} (0.43 + 0.64 \tilde{w}))}$$

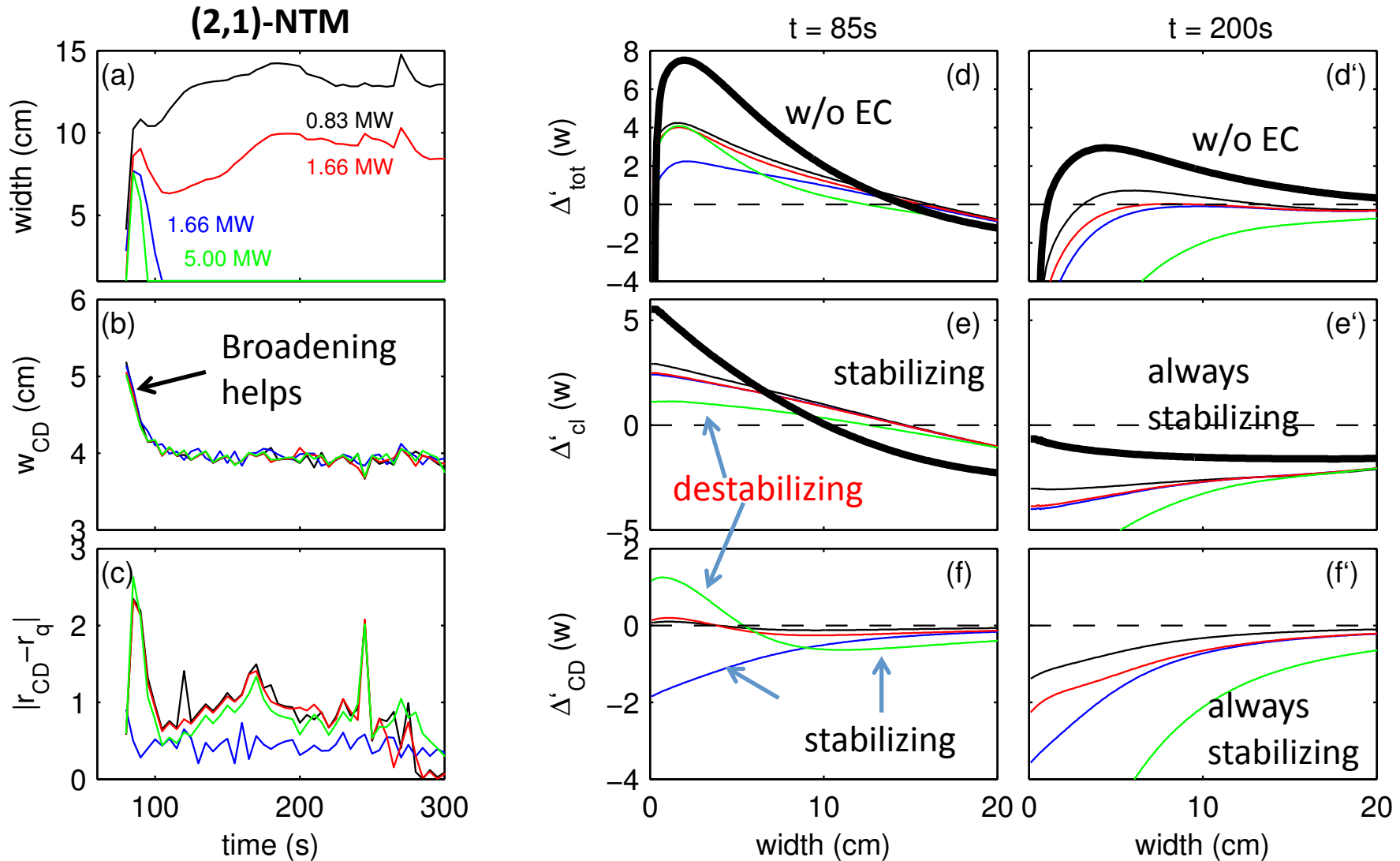
$$\tilde{w} = w/w_{CD}$$

Full suppression obtained only if $dr < 0.5w_{CD}$

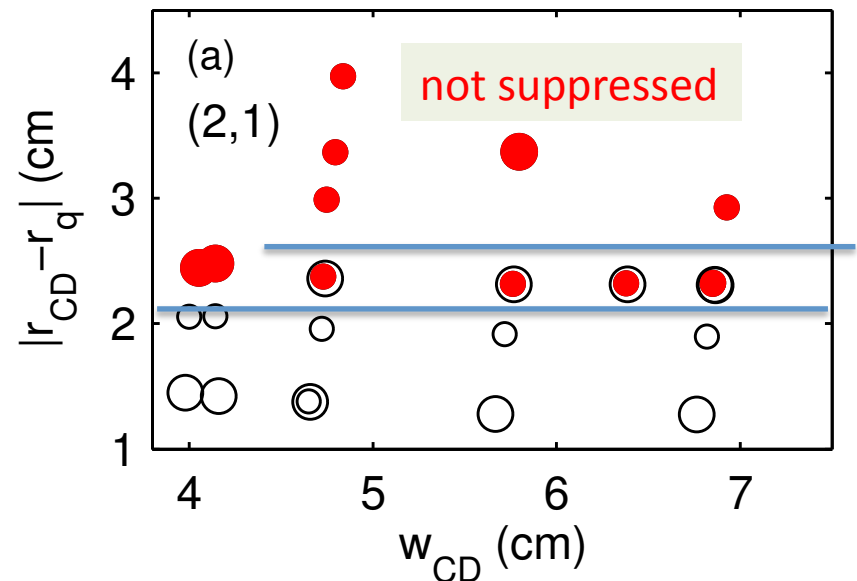
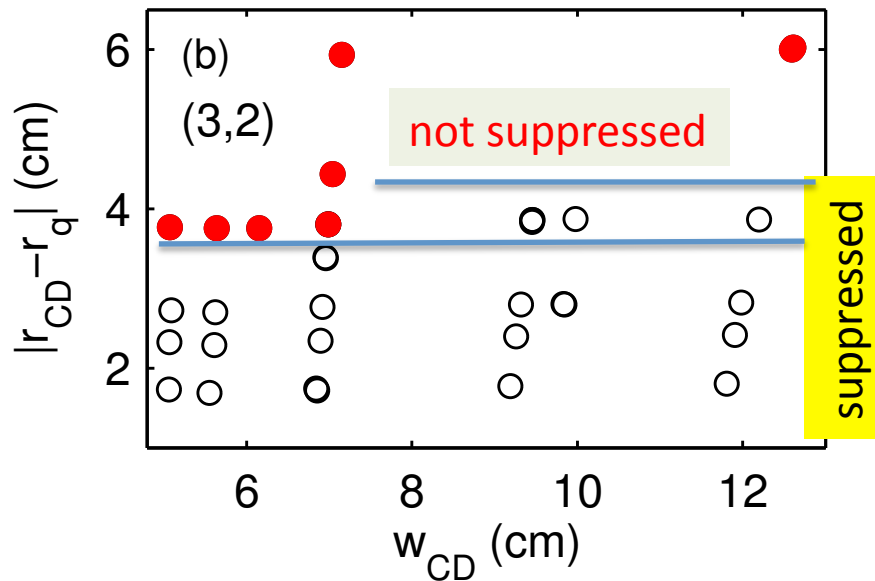


Not much benefit in increasing EC power if $dr = |r_{CD} - r_q| \sim w_{CD}$

Loss of alignment at NTM onset affects stabilization at later times



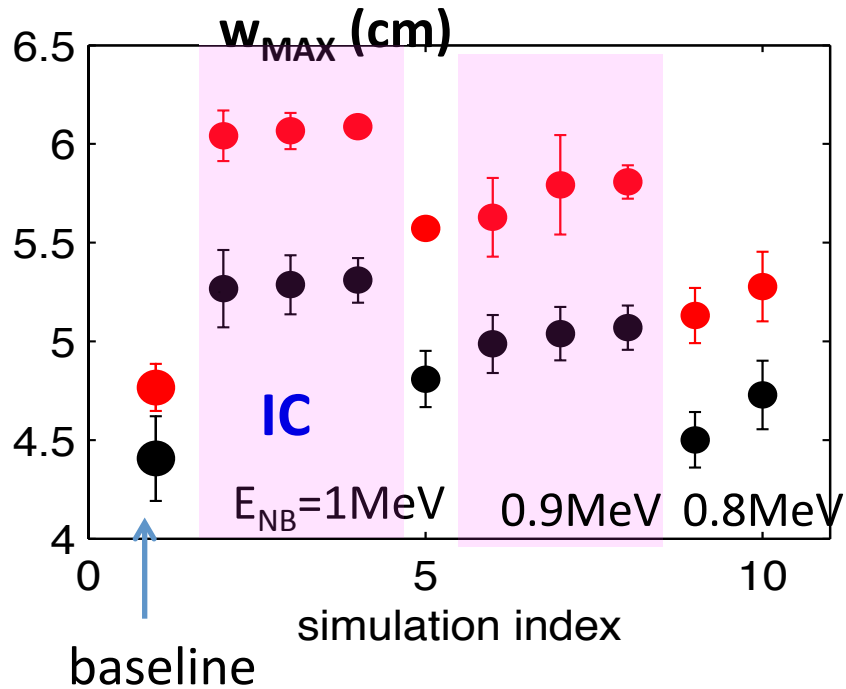
Broadening of w_{CD} is a good boost for early stabilization



(3,2) suppressed always with $dr < \sim 0.5w_{CD}$
 suppressed with $>50\%$ broadening and $dr \sim w_{CD}$

(2,1) suppressed always with $dr < 0.5w_{CD}$
 with 50% broadening and larger power if $dr \sim 0.5w_{CD}$

Discharge design becomes critical at half-field



$w_{CD} \Rightarrow$ 2.6 cm @ $q=1.5$ (5 cm at full field)
 1.5 cm @ $q=2.0$ (4 cm at full field)
 J_{max} comparable (total driven current is half)
 \Rightarrow Alignment is most important

Trend observed with NBI energy and with IC heating scheme:

- w_{max} size decreases with NBI energy
- at constant E_{NB} , w_{max} increases with H minority fraction
- at constant E_{NB} , w_{max} drops w/o IC.

Generalized NTM stabilization criteria

N. Bertelli et al, NF 51 (2011) 103007

$$0.82 \frac{\tau_r}{r_s} \frac{dw}{dt} = r_s \Delta'_0 + r_s \delta \Delta'_0(w) + r_s \Delta'_{BS}(w) + r_s \Delta'_{CD}(w) + r_s \Delta'_H(w)$$

Stabilization criteria obtained from GRE, assuming $dw/dt=0$

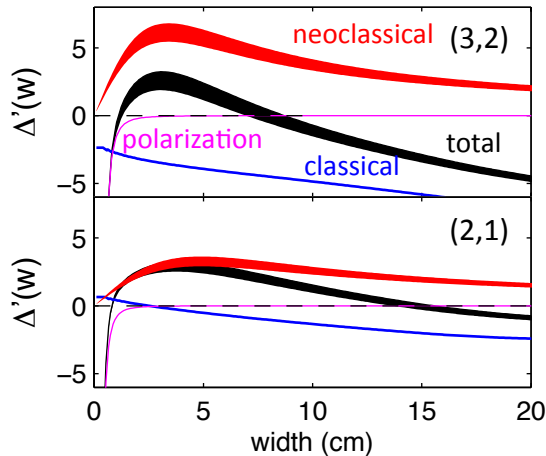
$$\eta_{NTM} = \text{Max} \left[\frac{4w_{dep}}{3\pi^{3/2}} \left(\frac{w^{-1} f(w, w_{m \text{ arg}}) - w_{sat}^{-1} f(w_{sat}, w_{m \text{ arg}})}{F_{CD} + \frac{w_{dep}^2}{w_{m \text{ arg}}^2} \bar{\eta}_H F_H + 0.25 D_{mod} \text{erfc}\left(\frac{w}{w_{dep}}\right)} \right); \quad 0 \leq w \leq w_{sat} \right]$$

General form: includes heating term (it changes the trend for narrow deposition width) => want to be as general as possible

ECCD term calculated under the hypothesis of:

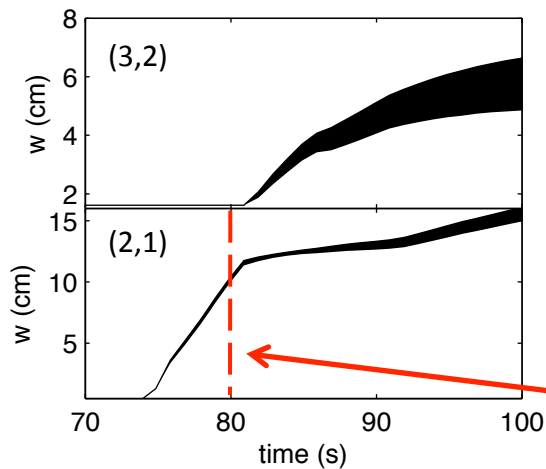
- EC deposition perfectly aligned with (m,n)

(2,1)-NTM grows faster than mirror switching time



$w_{SAT} \Rightarrow$ uncertainty depending on assumptions and pressure profiles

Calculation of $D'cl$ makes a difference
Allows for effects on modified current profile



(2,1) $w_{seed} \sim 1$ cm
 \Rightarrow difficult to detect (ECE threshold > 2 cm)
 \Rightarrow Difficult to track (equilibrium > 2 cm)

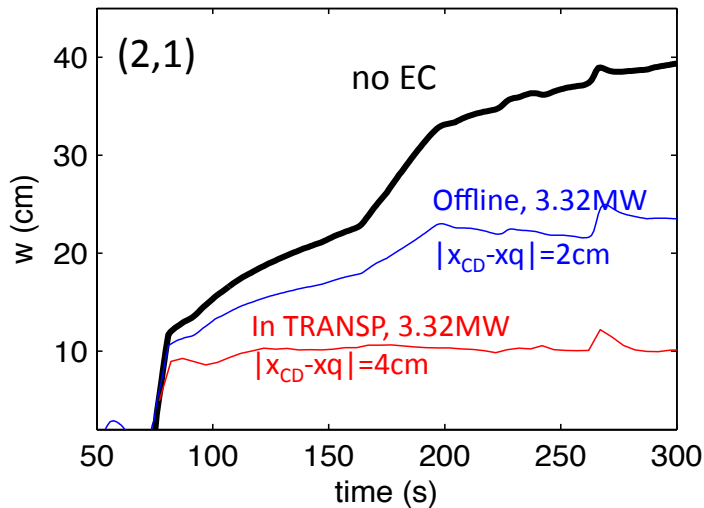
(2,1)-NTM grows to 10cm and LOCKS in ~ 5 s

(3,2) $w_{ECCD} \gg w_{seed}, w_{ECCD} \gtrsim w_{max}$ as in present-day experiments

(2,1) $w_{ECCD} \gg w_{seed}, w_{ECCD} \lesssim w_{max}$ not as in present-day experiments



Self-consistent calculation of NTM evolution and plasma profiles set lower limits on EC power needs



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$$F(\tilde{w}) = 0.25 \frac{1 + 0.96\tilde{w}}{1 + \tilde{w}(1.5 + \tilde{w}(0.43 + 0.64\tilde{w}))}$$

$$G(w) = 1 - 2 \frac{x_{dep}}{g(\tilde{w})} e^{-\left(\frac{x_{dep}}{g(\tilde{w})}\right)^2} \int_0^{x_{dep}/g(\tilde{w})} dt e^{t^2}$$

$$g(\tilde{w}) = \frac{0.38\tilde{w}^2 + 0.26\tilde{w} + 0.5}{\tilde{w} + 1}$$

