

# Profile Effects on DT Fusion Performance

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- ◆ For pure thermalized DT near optimum temperature ( $\sim 15\text{keV}$ )

$$\langle \sigma v \rangle \sim T^2 \Rightarrow P_{\text{fusion}} = E_{\text{DT}} \int n_D n_T \langle \sigma v \rangle dV \propto \int n^2 T^2 dV \propto \int p^2 dV$$

- ◆ For  $P_\alpha \ll P_{\text{aux}}$  (no self heating)

$$P_{\text{aux}} = P_{\text{loss}} = 3 \langle nT \rangle / \tau_E \quad [\langle \rangle \Rightarrow \text{volume average}]$$

$$\Rightarrow Q \equiv P_{\text{fusion}} / P_{\text{aux}} \propto [\langle n^2 T^2 \rangle / \langle nT \rangle] \tau_E$$

- This is often approximated either as

$$Q \propto n_e(0) \cdot T_i(0) \cdot \tau_E$$

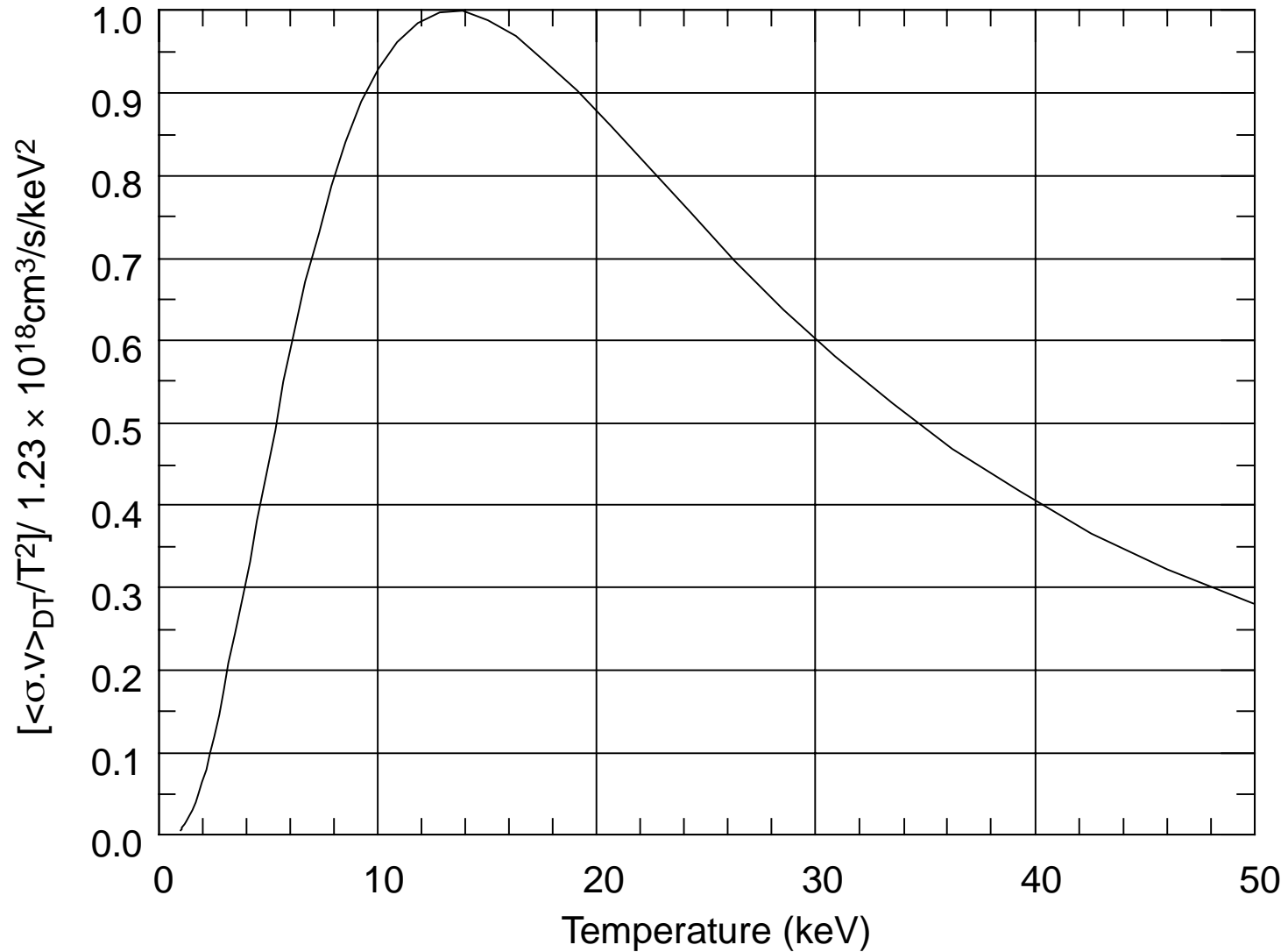
or

$$Q \propto \beta_T \cdot \tau_E \cdot B_T^2$$

- ◆ In real world

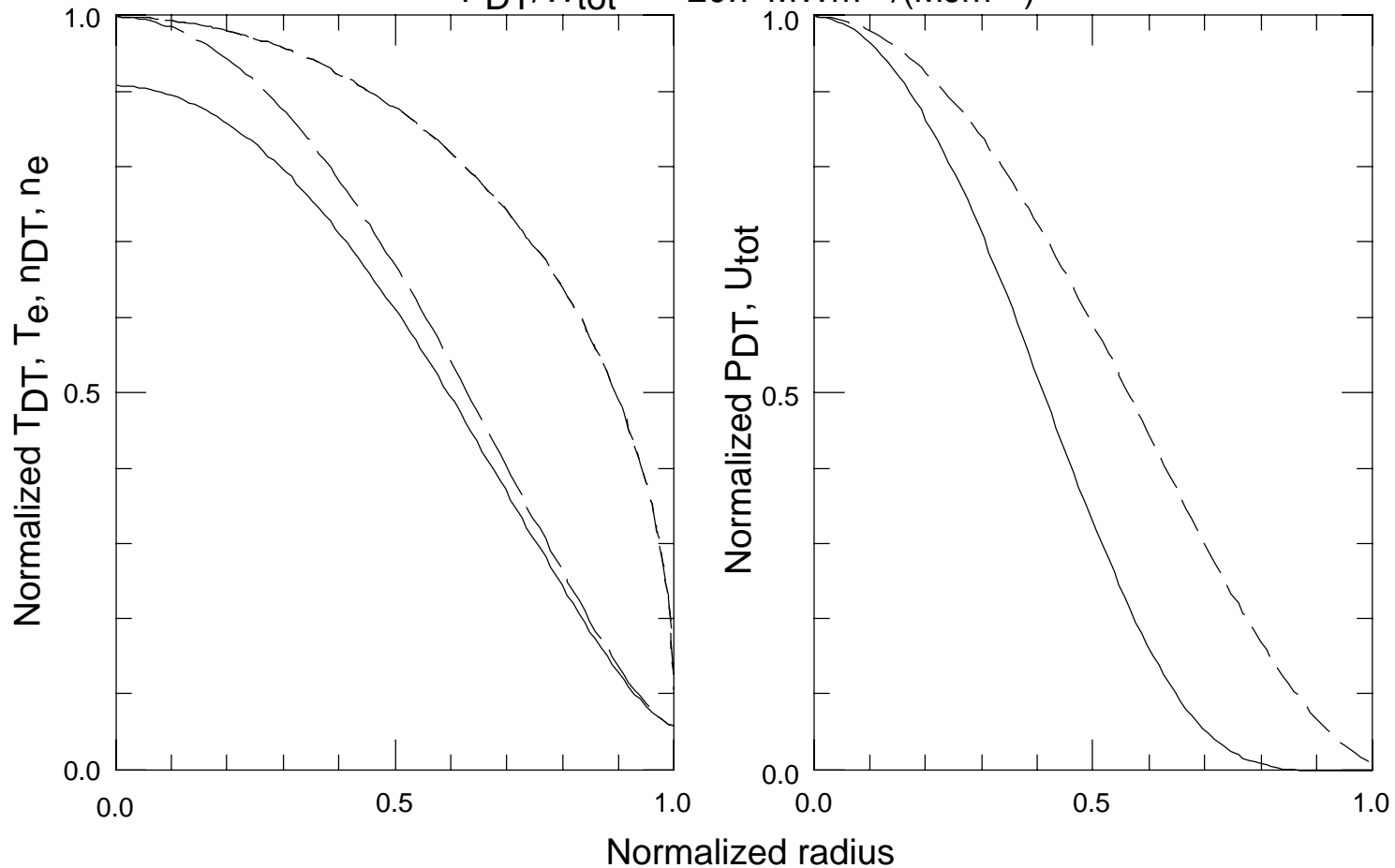
- Edge temperature must be well below optimum fusion temperature
  - Edge can contribute to  $\langle nT \rangle$  while not generating much  $P_{\text{fusion}}$
- $\langle n^2 T^2 \rangle \neq \langle nT \rangle^2$

# Temperature Dependence of DT Reactivity

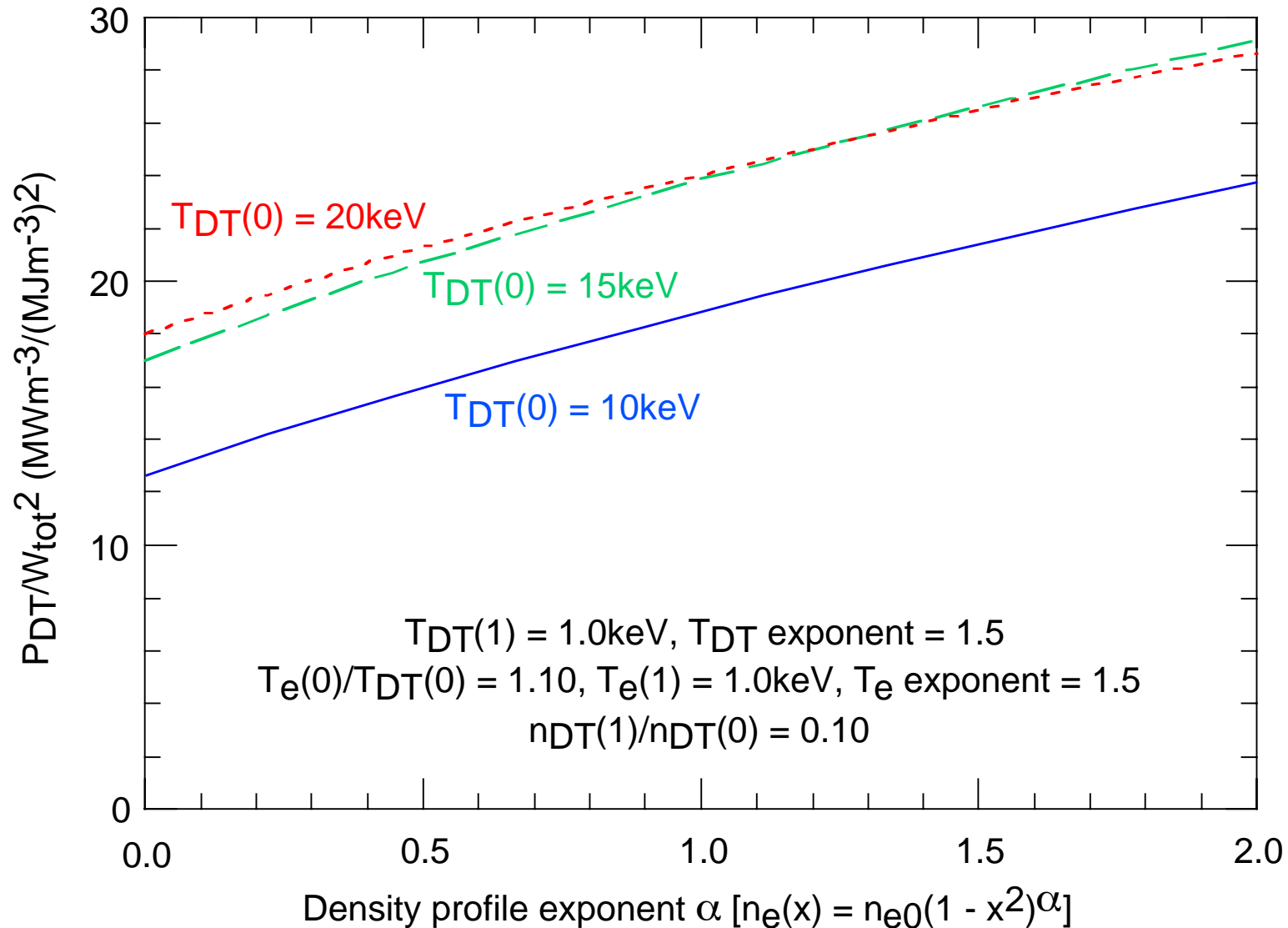


# Fusion Power Profile with Realistic Edge

$$\begin{aligned}T_i(0) &= 15.0\text{keV}, T_i(1) = 1.0\text{keV}, T_i \text{ exponent} = 1.5 \\T_e(0) &= 16.5\text{keV}, T_e(1) = 1.0\text{keV}, T_e \text{ exponent} = 1.5 \\n_{DT}(1)/n_{DT}(0) &= 0.10, n_{DT} \text{ exponent} = 0.5 \\P_{DT}/W_{tot}^2 &= 20.7 \text{ MWm}^{-3}/(\text{MJm}^{-3})^2\end{aligned}$$



# Peaked Profiles Demand Lower $\beta$



# Confinement is the Issue for Tokamaks

| Central values                            | ITER <sup>1</sup> | TFTR      | JET <sup>2</sup>        | JT-60U <sup>3</sup>            |
|---|-------------------|-----------|-------------------------|--------------------------------|
| Plasma composition                        | DT                | DT        | DT                      | D                              |
| Mode                                      | ELMy H-mode       | Supershot | Hot-ion ELM-free H-mode | Reversed-shear High- $\beta_p$ |
| $n_e$ [ $10^{20}\text{m}^{-3}$ ]          | 1.3               | 1.02      | 0.42                    | 0.85                           |
| $n_{DT}$ [ $10^{20}\text{m}^{-3}$ ]       | 0.8               | 0.60      | 0.35                    | 0.48 ( $n_i$ )                 |
| $n_{He}$ [ $10^{20}\text{m}^{-3}$ ]       | 0.2               | 0.002     |                         |                                |
| $T_i$ [keV]                               | 19                | 40        | 28                      | 16                             |
| $T_e$ [keV]                               | 21                | 13        | 14                      | 7                              |
| $Z_{\text{eff}}$                          | 1.8               | 1.8       | 2.1                     | 3.2                            |
| $\rho_{\text{tot}}$ [MPa]                 | 0.8               | 0.75      | 0.37                    | 0.22                           |
| $P_\alpha$ [ $\text{MWm}^{-3}$ ] (source) | 0.5               | 0.45      | 0.14                    |                                |
| $P_{\text{aux}}$ [ $\text{MWm}^{-3}$ ]    | 0                 | 3.4       | 0.8                     | 0.3                            |

- ◆ Tokamaks have confined plasma with pressure needed for ignition
  - Higher  $\beta$  is only an advantage if required  $\langle n^2 T^2 \rangle$  is achieved
- ◆ All confinement improvements are not created equal
  - In particular,  $dW/dt$  doesn't make fusion power