NSTX

Supported by

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Physics design of the NSTX Upgrade*

J.E. Menard, J. Canik, B. Covele, S. Kaye, C. Kessel,
M. Kotschenreuther, S. Mahajan, R. Maingi, C. Neumeyer, M. Ono,
R. Raman, S. Sabbagh, V. Soukhanovskii, P. Valanju

For the NSTX Research and NSTX Upgrade Project Teams

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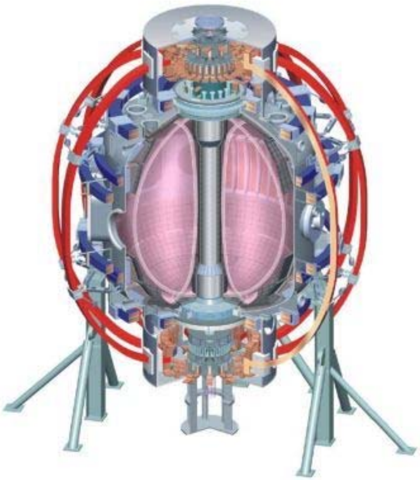

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Abstract

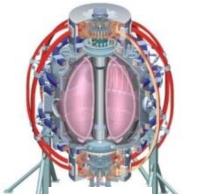
Access to low collisionality is important to more fully understand transport, stability, and non-inductive start-up and sustainment in the ST. For example, NSTX and MAST observe a strong (nearly inverse) scaling of normalized confinement with collisionality, and if this trend holds at low collisionality, high fusion neutron fluences could be achievable in very compact ST devices. Such considerations motivate the proposed upgrade of NSTX to higher toroidal field B_T=0.55T → 1T, plasma current I_P=1MA → 2MA, NBI heating power P_{NBI} = 5MW → 10MW, aspect ratio A =1.3 → 1.5, and pulse length t_{pulse}=1-1.5s → 5s. To enable engineering design of the upgrade, systematic free-boundary equilibrium calculations have been performed to determine the upgrade poloidal field requirements as a function of plasma shape, magnetic balance, internal inductance, and beta. NSTX plasma current ramp-up and flat-top flux consumption scalings and modelling have been utilized to design the Upgrade solenoid to support up to 5s flat-top durations at 2MA flat-top current. Recent assessments of the divertor heat flux scaling in NSTX project to peak divertor heat fluxes $\geq$ 20MW/m^2 in the Upgrade for conventional divertor configurations with flux expansion ~20. Very high flux expansions of ~40-60 have recently been shown to successfully reduce peak heat flux in NSTX, and additional divertor poloidal field coils are being incorporated into the Upgrade design to support high flux expansion "snowflake" and "X/Super-X" divertors and strike point control for high heat flux mitigation. TRANSP simulations indicate that more tangential neutral beam injection (NBI) can increase NBI current drive efficiency by up to a factor of two, support fully non-inductive operation at 1MA plasma current values, enable control of the core q profile, and ramp-up the plasma current from intermediate current (~0.4MA) to near mega-ampere levels. The incorporation of coaxial helicity injection start-up, preliminary global stability calculations, and other design activities will also be described.

Outline

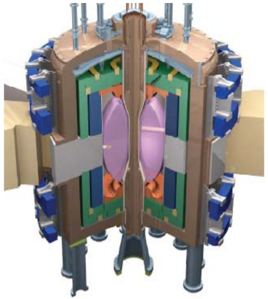
- Motivation for upgrades
- Overview of center-stack and NBI upgrades
- Free-boundary equilibrium studies
- Power exhaust
- NBI current drive studies for sustainment, ramp-up

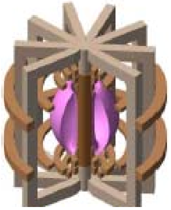
NSTX Upgrade will contribute strongly to toroidal plasma science and preparation for a fusion nuclear science (FNS) program

- NSTX:
  - Providing foundation for understanding ST physics, performance
- NSTX Upgrade:
  - Study high beta plasmas at reduced collisionality
    - Vital for understanding confinement, stability, start-up, sustainment
  - Assess full non-inductive current drive operation
    - Needed for steady-state operating scenarios in ITER and FNS facility
  - Prototype solutions for mitigating high heat, particle exhaust
    - Can access world-leading combination of P/R and P/S
    - Needed for testing integration of high-performance fusion core and edge
- NSTX Upgrade contributes strongly to possible next-step STs:
  - ST Fusion Nuclear Science Facility
    - Develop fusion nuclear science, test nuclear components for Demo
    - Sustain $W_{neutron} \sim 0.2\text{-}0.4 \rightarrow 1\text{-}2\,\mathrm{MW/m^2}$, $\tau_{pulse} = 10^3 \rightarrow 10^6\,\mathrm{s}$
  - ST Plasma Material Interface Facility
    - Develop long-pulse PMI solutions for FNSF / Demo (low-A and high-A)
    - Further advance start-up, confinement, sustainment for ST
    - High $P_{heat}/S \sim 1\,\mathrm{MW/m^2}$, high T_{wall}, $\tau_{pulse} \sim 10^3\,\mathrm{s}$

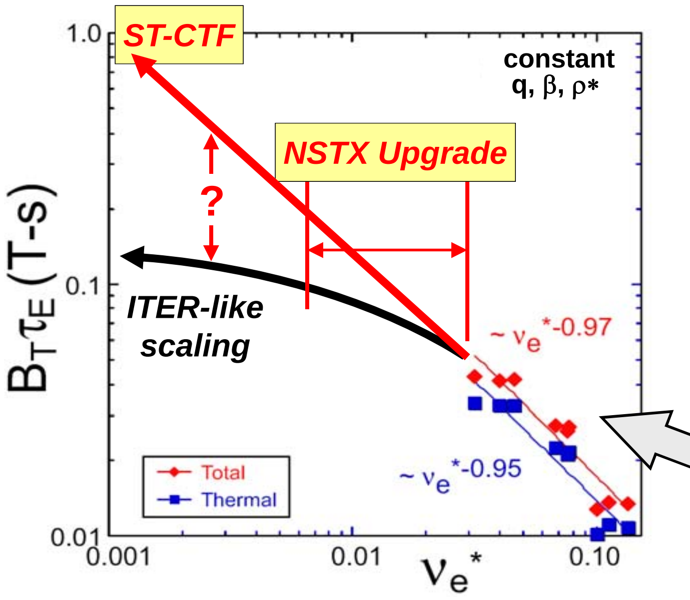

NSTX


NSTX-U


FNSF (ST-CTF)


PMIF (NHTX)

Access to reduced collisionality is needed to understand underlying causes of ST transport, scaling to next-steps



Normalized electron collisionality $\nu_e^* \propto n_e / T_e^2$

- Future ST's are projected to operate at 10-100× lower normalized collisionality ν^*
- Conventional tokamaks observe weak inverse dependence of confinement on ν^*

ITER $B\tau_E$ (e-static g-Bohm) $\propto \rho_*^{-3}\ \beta^0\ \boxed{\nu_*^{-0.14}}\ q^{-1.7}$

Petty et al., PoP, Vol. 11 (2004)

- NSTX observes much stronger scaling vs. ν^*
  - Does favorable scaling extend to lower ν^* ?
  - What modes dominate e-transport in ST ?
    - Electrostatic or electromagnetic?

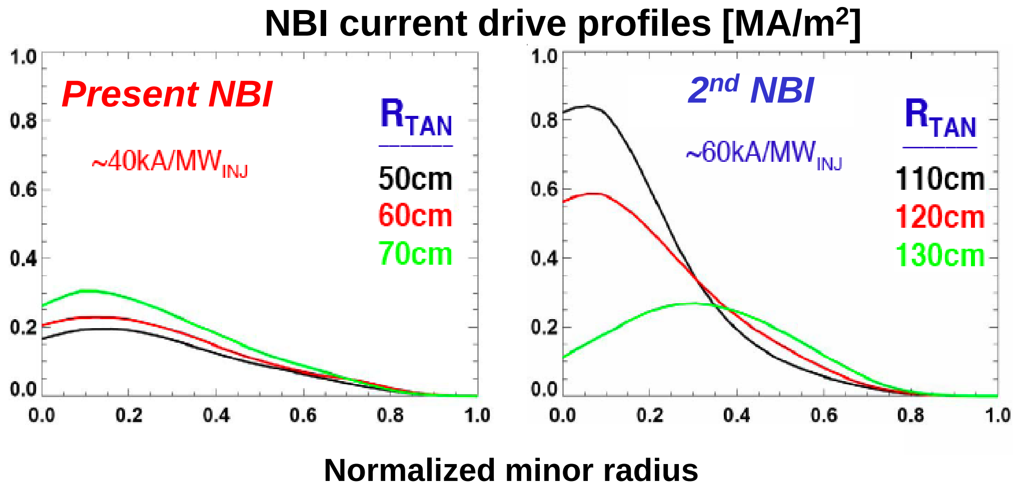
- Higher toroidal field & plasma current enable access to higher temperature
- Higher temperature reduces collisionality, but increases equilibration time

- **Upgrade:** **Double field and current for 3-6× decrease in collisionality → require 3-5× increase in pulse duration for profile equilibration**

Increased auxiliary heating and current drive are needed to address ST start-up, sustainment, and boundary issues

- Need additional heating power to access high temperature and β at low ν^*
  - → 4-10MW more heating, depending on confinement scaling
- Need increased <u>current drive</u> to access and study 100% non-inductive
  - → 0.25-0.5MA more current drive compatible with ramp-up, sustainment plasmas
- Need to learn to manage ≥ ITER→FNSF-level high-heat-flux challenge
  - → high divertor power density (P/R ≤ 20MW/m) + flexible divertor PF coil set

- **Upgrade: Double neutral beam power + more tangential injection**
  - More tangential injection → up to 2 times higher efficiency, current profile control

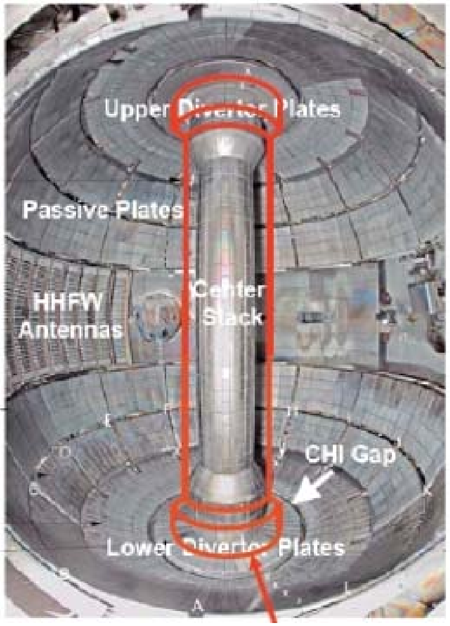


Upgrades provide major step along ST development path

(next factor of 2 increase in current, field, and power density)

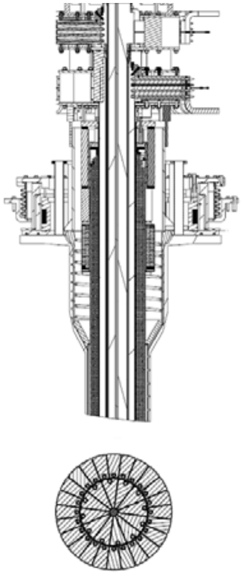
	NSTX	**NSTX Upgrade**	**Plasma-Material Interface Facility**	**Fusion Nuclear Science Facility**
Aspect Ratio = R_0 / a	≥ 1.3	≥ 1.5	≥ 1.7	≥ 1.5
Plasma Current (MA)	1	2	3.5	10
Toroidal Field (T)	0.5	1	2	2.5
P/R, P/S (MW/m,m^2)	10, 0.2*	20, 0.4*	40, 0.7	40-60, 0.8-1.2

***** Includes 4MW of high-harmonic fast-wave (HHFW) heating power**



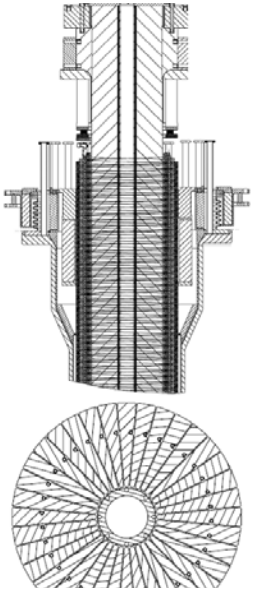
Outline of new center-stack (CS)

Present CS



TF OD = 20cm

New CS



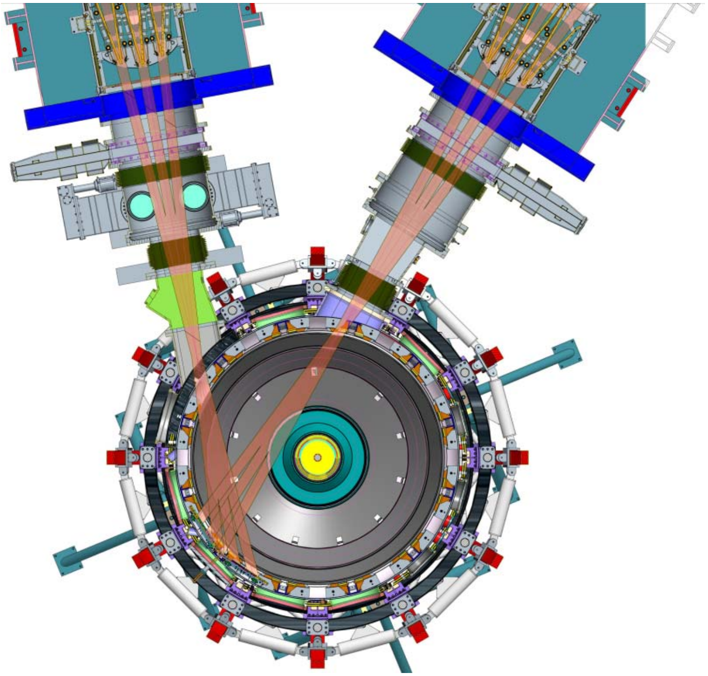
TF OD = 40cm

New 2nd NBI

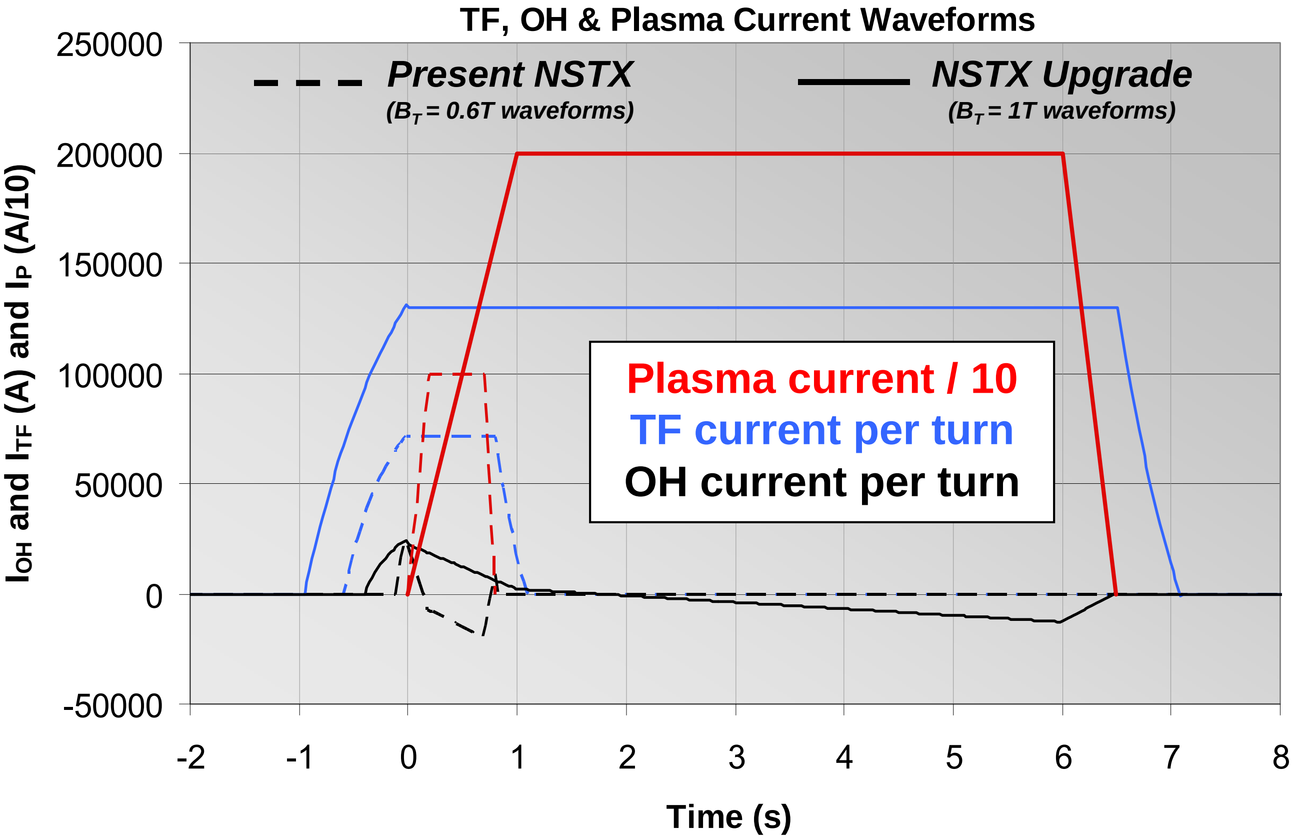
(R_{TAN}=110, 120, 130cm)

Present NBI

(R_{TAN}= 50, 60, 70cm)



Upgrade provides substantial increase in device performance



	Base NSTX	NSTX Upgrade
R_0 [m]	0.854	0.934
Min. aspect ratio	1.28	1.5
I_p [MA]	1	2
B_T [T]	0.55	1
T_{pulse} [s]	1	5
$T_{repetition}$ [s]	600	1000
R_{center_stack} =R_0-a [m]	0.185	0.315
$R_{antenna}$=R_0+a [m]	1.574	1.574
Total OH flux [Wb]	0.75	2.1

Relative performance of Upgraded NSTX vs. Base:

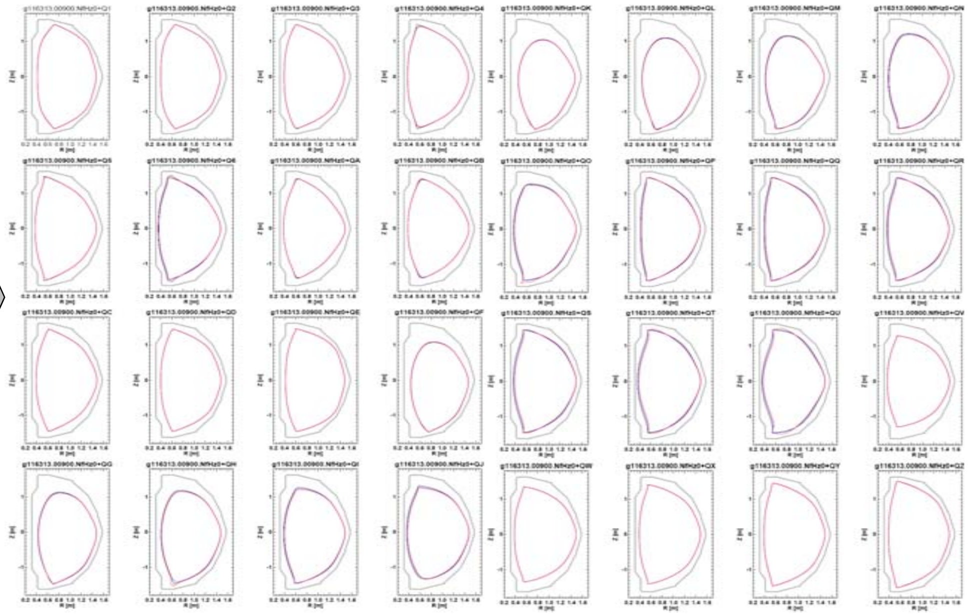
- Center-stack radius increased 13cm → A=1.3 → 1.5
- Available OH flux increased 3×, 3-5× longer flat-top
- I_P increased 2×, B_T increased 2× at same major radius
- Plasma stored energy increased up to 4× (0.25→ 1MJ)

Range of I_P = 2MA free-boundary equilibria generated to support design of TF and PF coil support structures

Free boundary equilibrium parameters:

- Aspect ratio A: 1.6 – 1.9
- Internal inductance l_i: 0.4 – 1.1
- Elongation κ: 2.1 – 2.9
- Triangularity δ: 0.2 – 0.7
- Squareness ζ: -0.15 – 0.12
- Magnetic balance: -1.5 – 0cm
- I_{OH}: zero and +/- supply limit
  - For computing PF needed for cancellation of OH leakage flux
- Pressure variation: β_N = 1, 5, 8

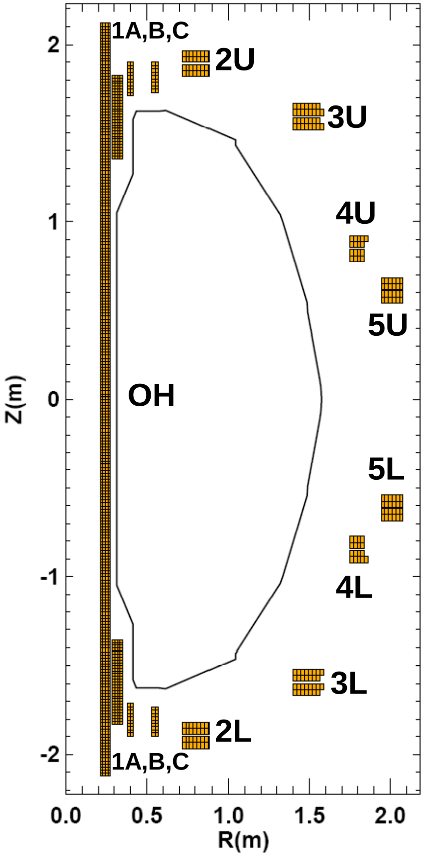
32 free boundary equilibria × 3 OH conditions = 96 cases



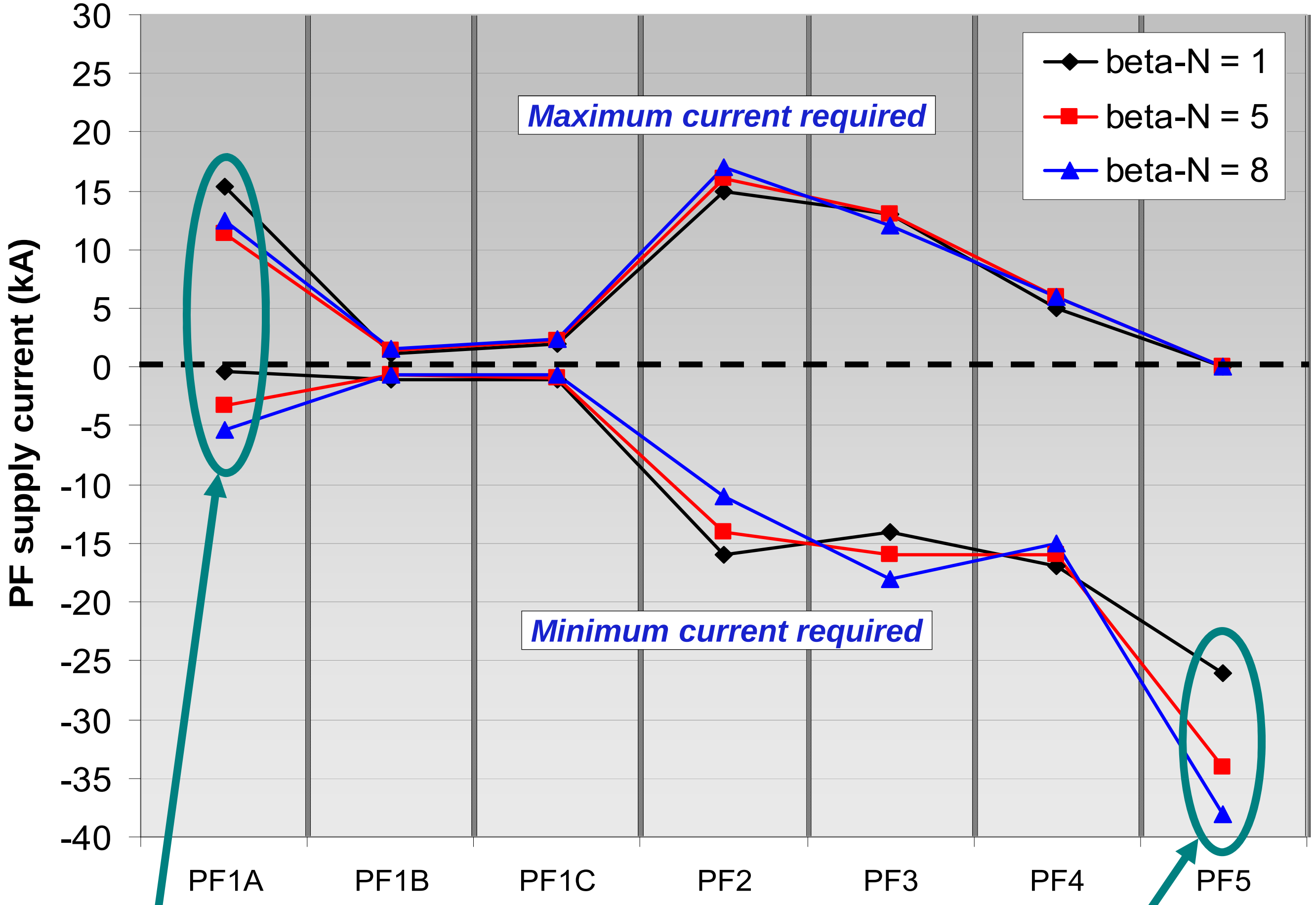
- NOTE: Negative “squareness” boundary shape cases are included:
  - More shaping flexibility/capability than in present NSTX (requires PF4 usage)
  - Expect could be important for controlling edge stability (NSTX will test in FY2010)
- With coil/machine protection system + nominal operating currents, analysis indicates enhanced vertical field coil structure can support above scenarios

High β_N increases vertical field requirement, and shifts primary divertor coil (PF1A) current requirement to bipolar

Note: all current limits are 10% above current required for actual equilibrium



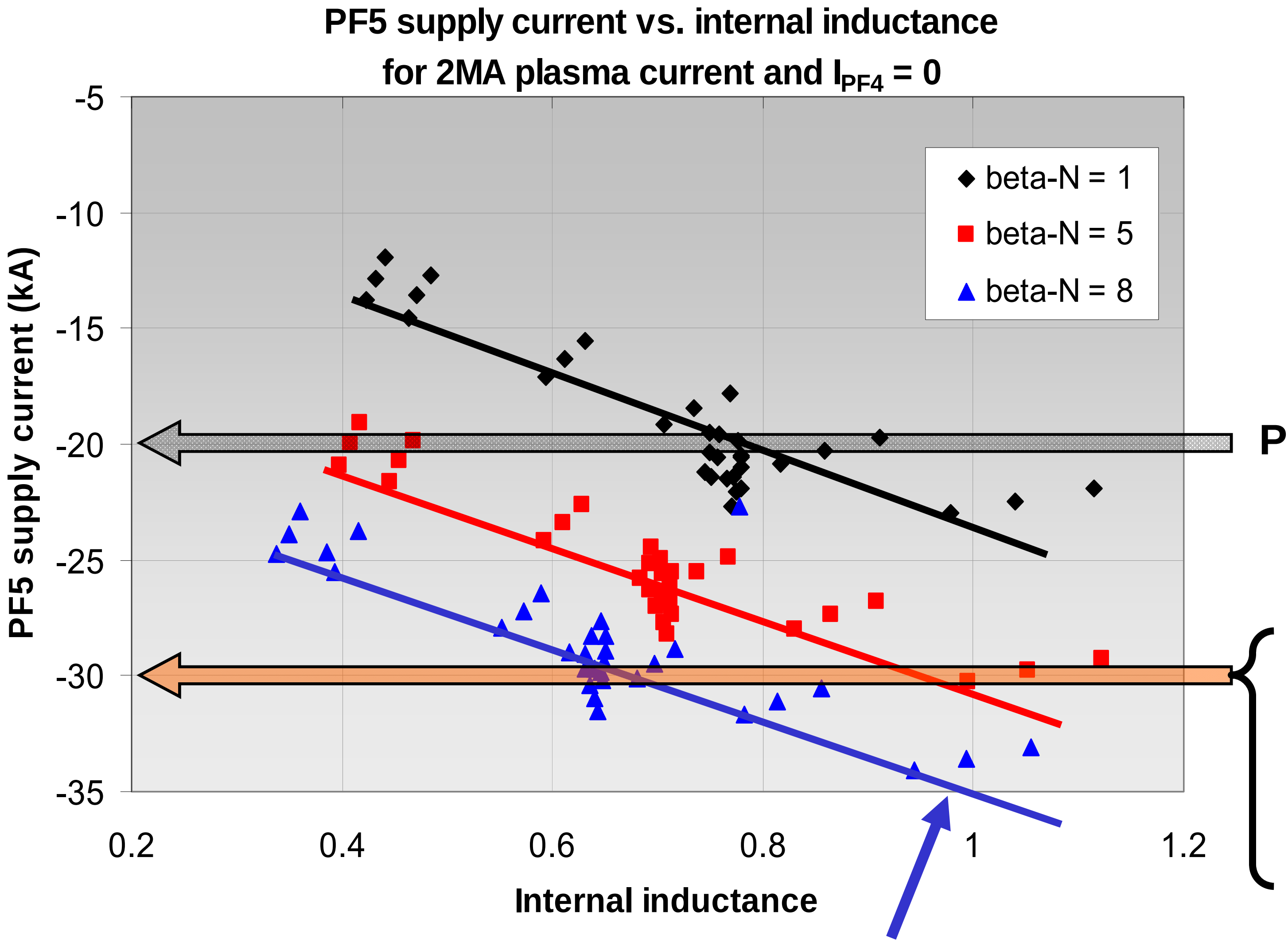
PF supply limits - 2MA, expected OH operation, full PF



Primary divertor field (PF1A) requires -5kA reduction at high β_N

Vertical field (PF5) required increases ~50% from low to high β_N

PF and TF support structure being designed to support $\beta_N = 5$, $l_i \leq 1$ and $\beta_N = 8$, $l_i \leq 0.6$ at I_P = 2MA

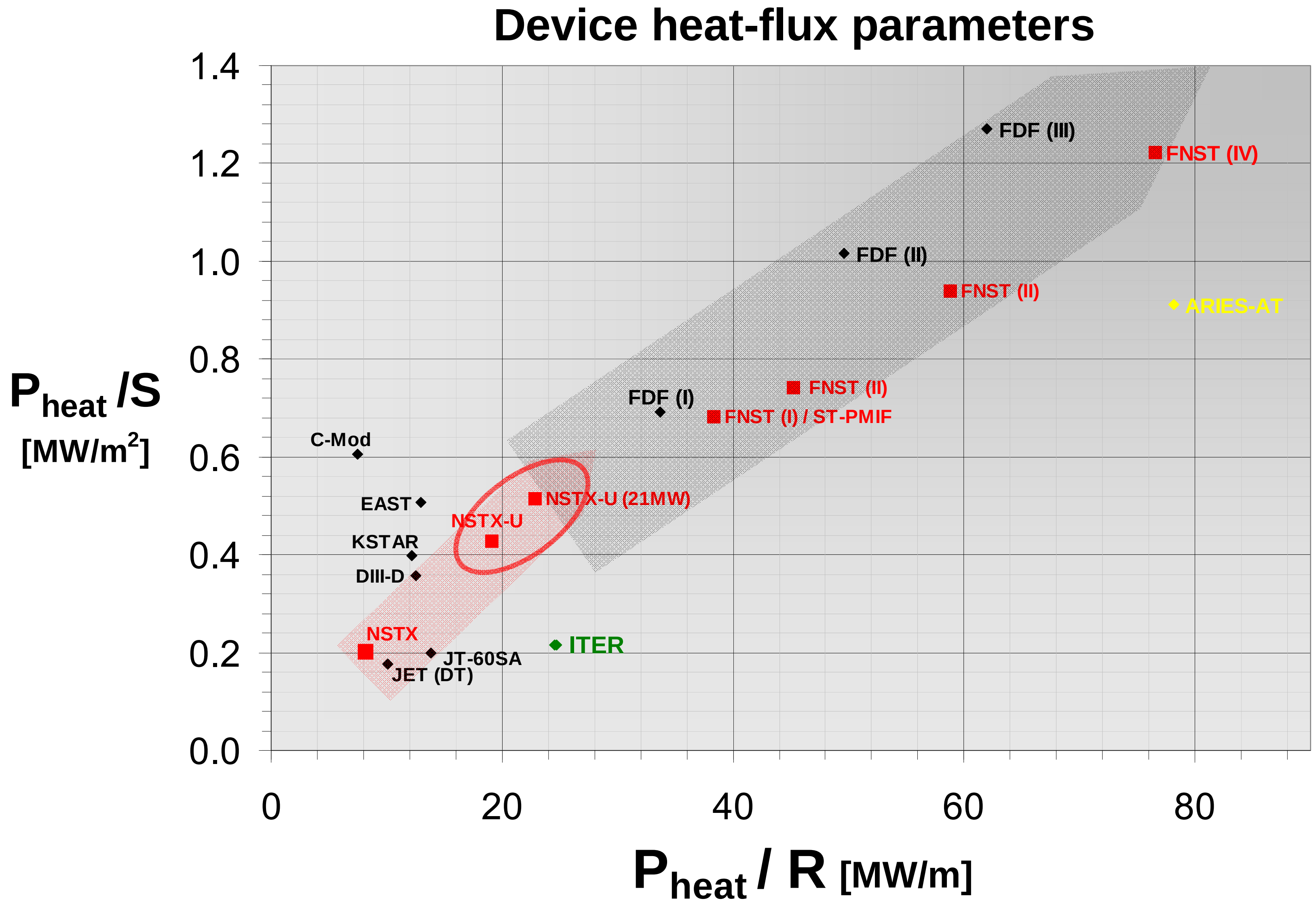


Present PF5 limit

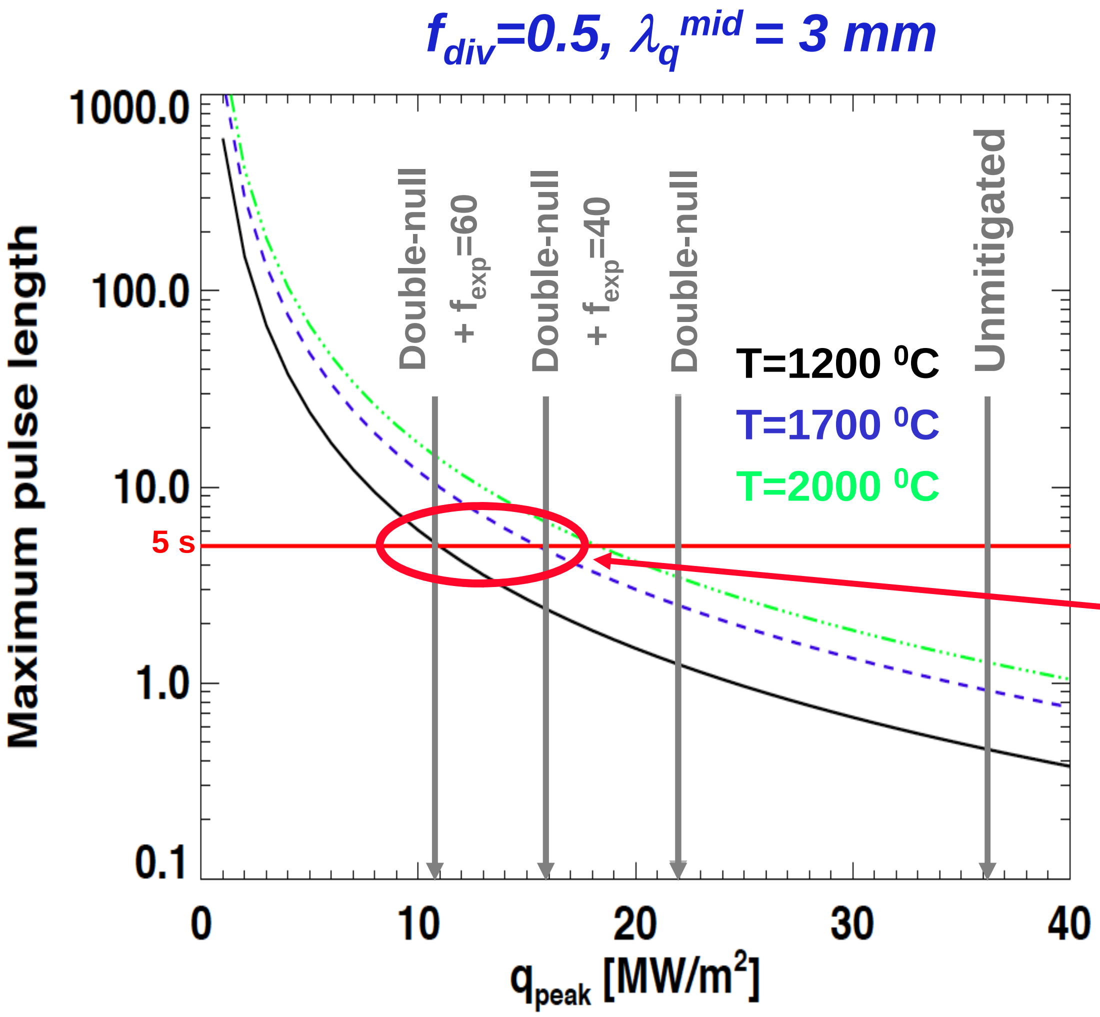
Upgrade design targets $I_{PF5} \leq$ 30kA with 10% current margin for radial position control

High l_i, high-β_N scenarios determine maximum PF5 current required

NSTX Upgrade will extend normalized divertor and first-wall heat-loads much closer to FNS and Demo regimes



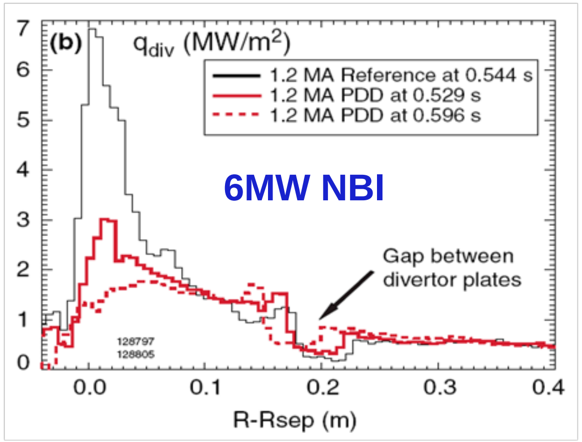
High current 2 MA, high P_{NBI} scenario requires extra flux expansion for full pulse length with existing tiles



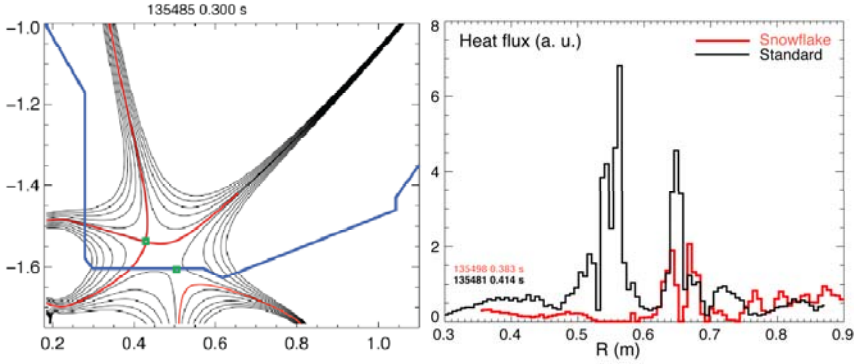
- **High-current LSN case 2 MA, n/n_{GW}=0.5, P =15 MW (e.g. 10 MW NBI + 5 MW RF)**
  - **Actual scenarios can use n/n_{GW}=0.7-1, which is expected to widen the SOL**
- **Using DN and increasing flux expansion (e.g. SFD) would just manage for 5s**
- **Molybdenum tile for higher temperature being considered for 2011-2012**

A combination of advanced PMI solutions will likely be required to manage the power exhaust of NSTX Upgrade

- **High divertor heat flux can be reduced in NSTX with partially detached divertor (PDD)**



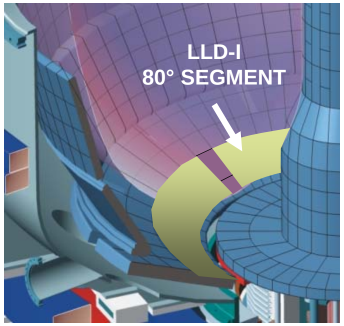
- **High flux expansion (~40-60) "snowflake" divertor demonstrated in NSTX**
- **50% reduction in peak heat flux, impurities**



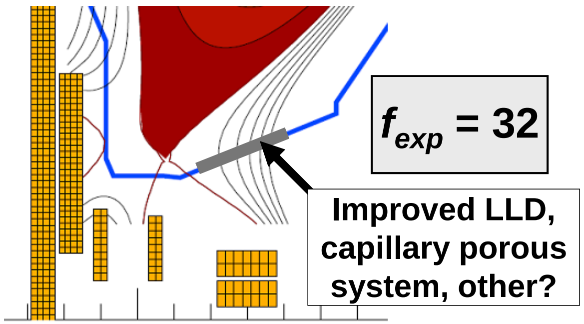
- **The PDD operating regime and other PMI solutions will be challenged in NSTX-U due to:**
  - 2-3× higher input power
  - 30-50% reduction in Greenwald fraction
  - 3-5× longer pulse duration, leading to substantial increase in $T_{divertor}$

- **NSTX and NSTX-U will test the compatibility of high flux expansion, PDD, and a liquid lithium divertor (LLD) at higher power/energy**

NSTX LLD

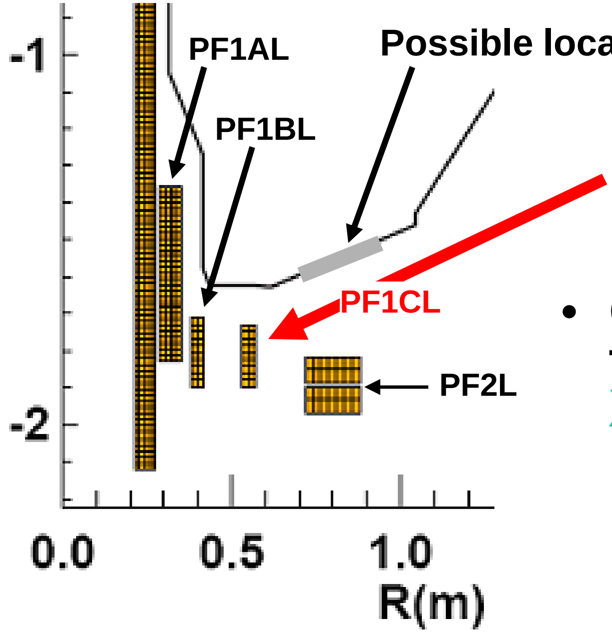


NSTX-U high flux expansion:



Improved LLD, capillary porous system, other?

The divertor PF coil system for NSTX Upgrade includes an additional coil to enhance control of power exhaust

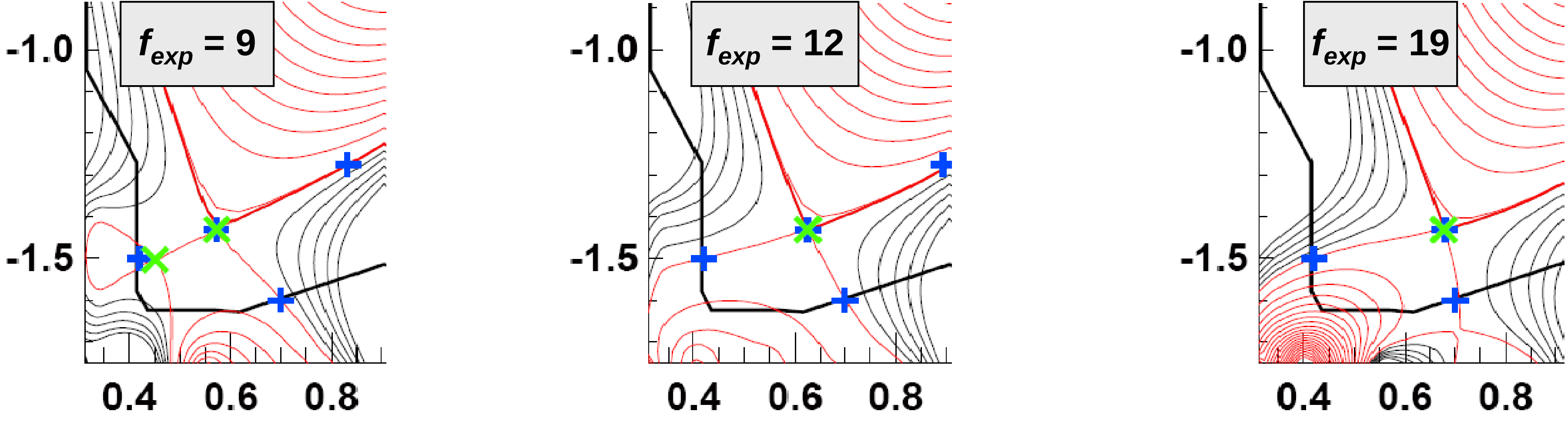


Possible location of liquid lithium divertor in Upgrade

Additional coil added = PF1C

- Combination of PF1A,B,C + PF2 enables **flux expansion variation** with fixed **X-point** height and strike-point location:

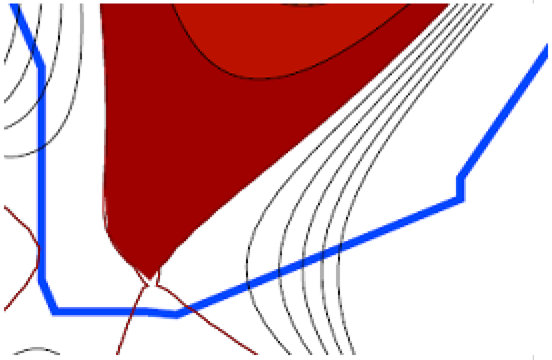
Outboard poloidal flux expansion factor $f_{exp} \equiv |\nabla\psi|_{\text{mid-plane}} / |\nabla\psi|_{\text{strike-point}}$



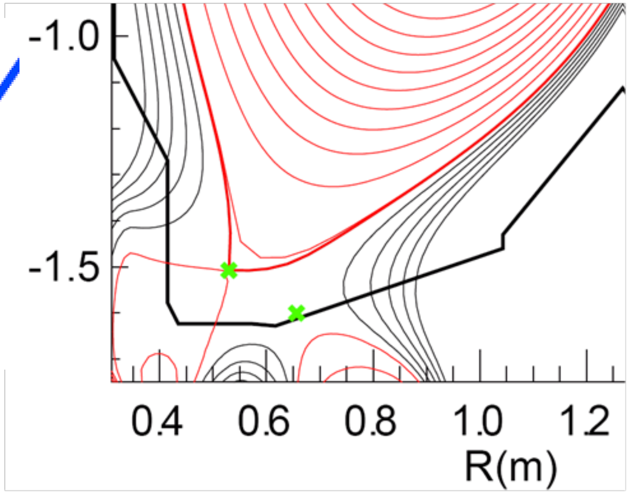
Center-stack Upgrade divertor coil set supports conventional, snowflake, and X/Super-X divertor options

- **Implication:** CS divertor coil location and configuration now finalized

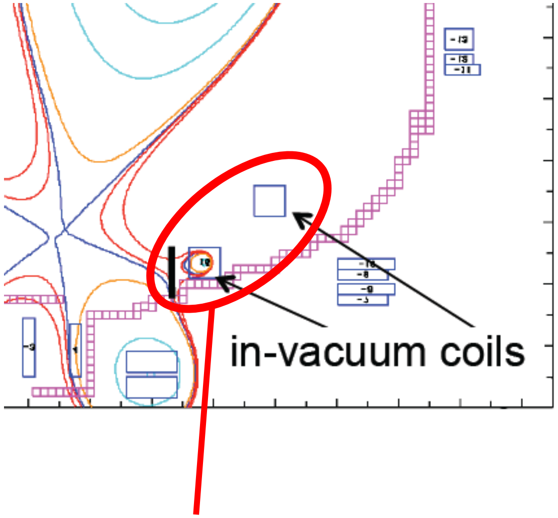
Conventional



Snowflake



X/Super-X



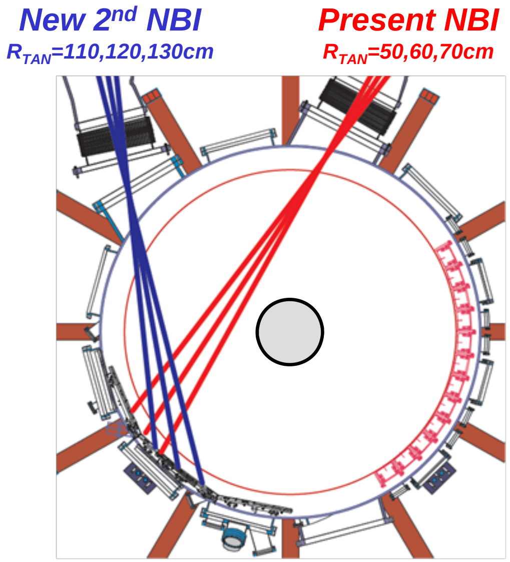
Possible location for cryo-pumps?

- X/Super-X requires in-vessel PF coils which are <u>not</u> part of Upgrade project
- Design/analysis of Upgrade divertor is collaborative effort (ORNL, LLNL, UT, PPPL)

Vlad Soukhanovskii (LLNL) recently received DOE-SC Early Career Award for proposal to study “Advanced High Heat Flux Divertor Program on the NSTX”

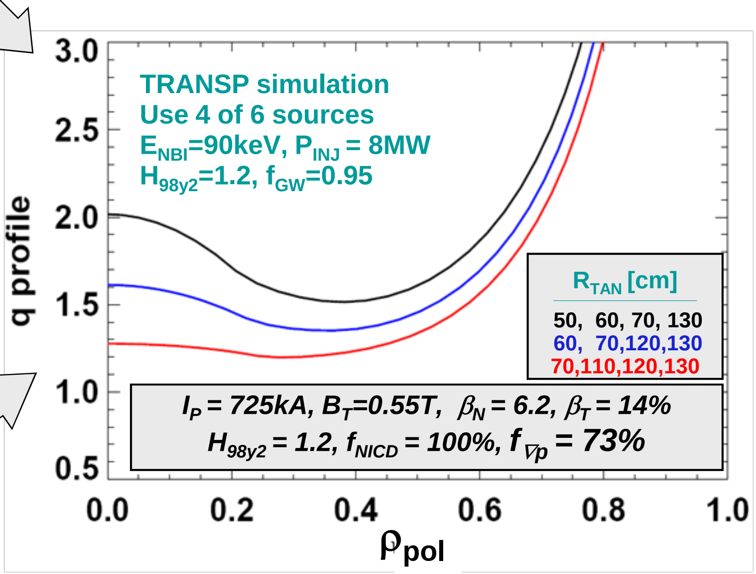
- NSTX-U divertor design will be strongly influenced by NSTX LLD results
  - To be prepared for possible favorable results from LLD, NSTX is initiating a conceptual design study of heated inboard Mo divertor tiles to support test of high-δ LLD-pumped plasma

Upgrade 2nd NBI injecting at larger $R_{tangency}$ will greatly expand performance and understanding of ST plasmas



- Improved NBI-CD and plasma performance
  - Higher CD efficiency from large R_{TAN}
  - Higher NBI current drive from higher P_{NBI}
  - Higher β_P, f_{BS} at present $H_{98y2} \leq 1.2$ from higher P_{HEAT}
  - Large R_{TAN} → off-axis CD for maintaining $q_{min} > 1$
  - Achieve 100% non-inductive fraction (presently < 70%)
  - Optimized $q(\rho)$ for integrated high τ_E, β, and f_{NI}

- Expanded research flexibility by varying:
  - *q*-shear for transport, MHD, fast-ion physics
  - Heating, torque, and rotation profiles
  - β, including higher β at higher I_P and B_T
  - Fast-ion $f(v_{||},v_{\perp})$ and *AE instabilities
    - 2nd NBI more tangential – like next-step STs
  - Peak divertor heat flux, SOL width

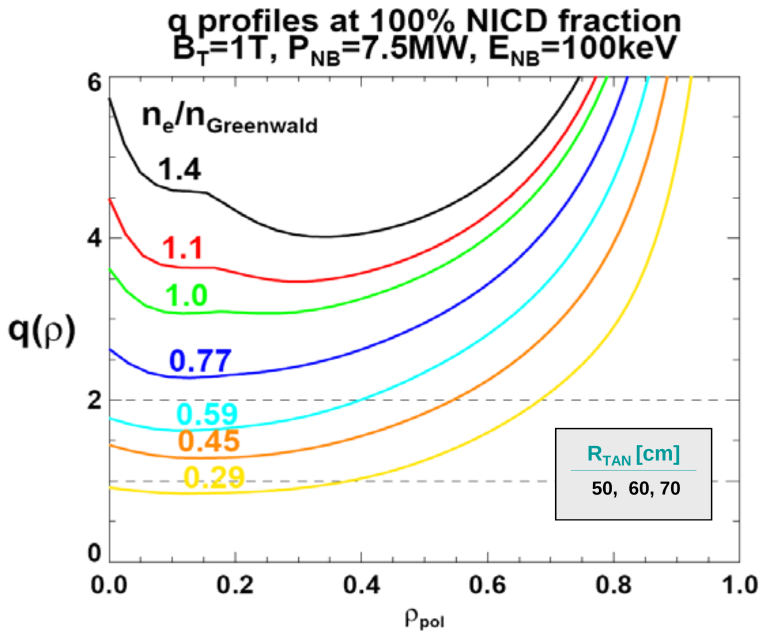


- q(r) profile variation and control very important for global stability, electron transport, Alfvénic instability behavior

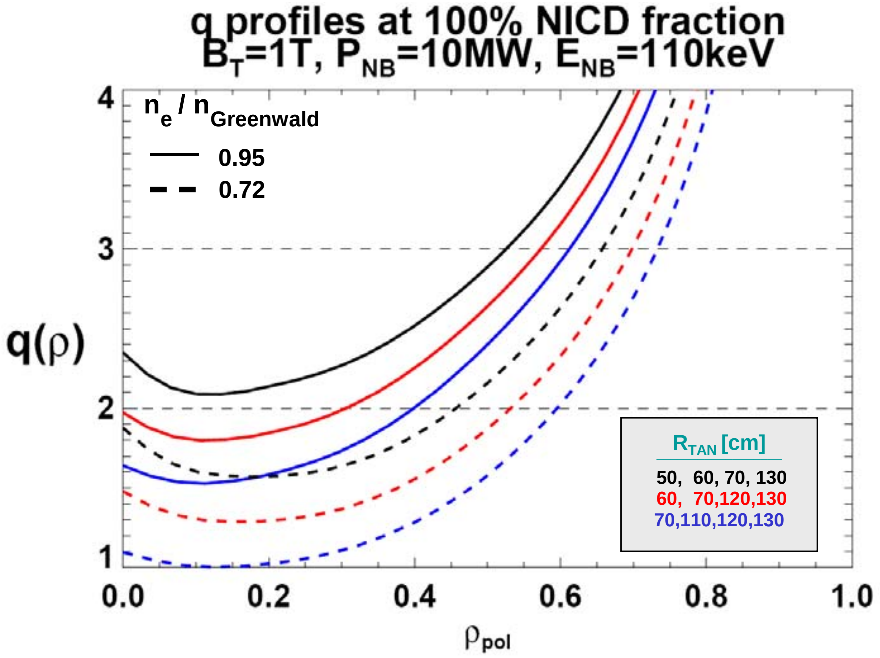
Higher field B_T=1T from new CS + 2nd NBI would enable access to wide range of 100% non-inductive scenarios

- **New CS + present NBI-CD + fast wave:**
  - Study confinement scaling vs. I_P and B_T
    - Limited range of auxiliary power levels
  - 100% non-inductive for 1-1.5s (~1 τ_{CR})
    - NBI duration limited to 2s at 7.5MW
    - Vary q_{min} with density (CD efficiency $\propto T_e/n_e$)

- **Addition of 2nd NBI would enable:**
  - Study confinement scaling vs. I_P and B_T with:
    - Full range of auxiliary power available
    - Assured access to high-β at reduced ν*
  - 100% non-inductive for 3-4 τ_{CR} → relaxed J(r)
    - 10MW NBI available for 5s
    - Control q_{min} & q-shear w/ NBI source, n_e, & B_T
    - Study long-pulse NTM stability with q > 2
  - Study compatibility of high-β w/ PMI solutions


q profiles at 100% NICD fraction
B_T=1T, P_{NB}=7.5MW, E_{NB}=100keV

I_P = 0.8-1.2MA, H_{98y2} = 1.2-1.4, β_N = 4.5-5, β_T = 10-12%, 4MW RF


q profiles at 100% NICD fraction
B_T=1T, P_{NB}=10MW, E_{NB}=110keV

I_P = 0.95MA, H_{98y2} = 1.2, β_N = 5, β_T = 10%, 4MW RF

2^{nd} NBI also needed to support long-pulse (5s) high-I_P partial-inductive scenarios at high-power at full TF ($B_T = 1T$)

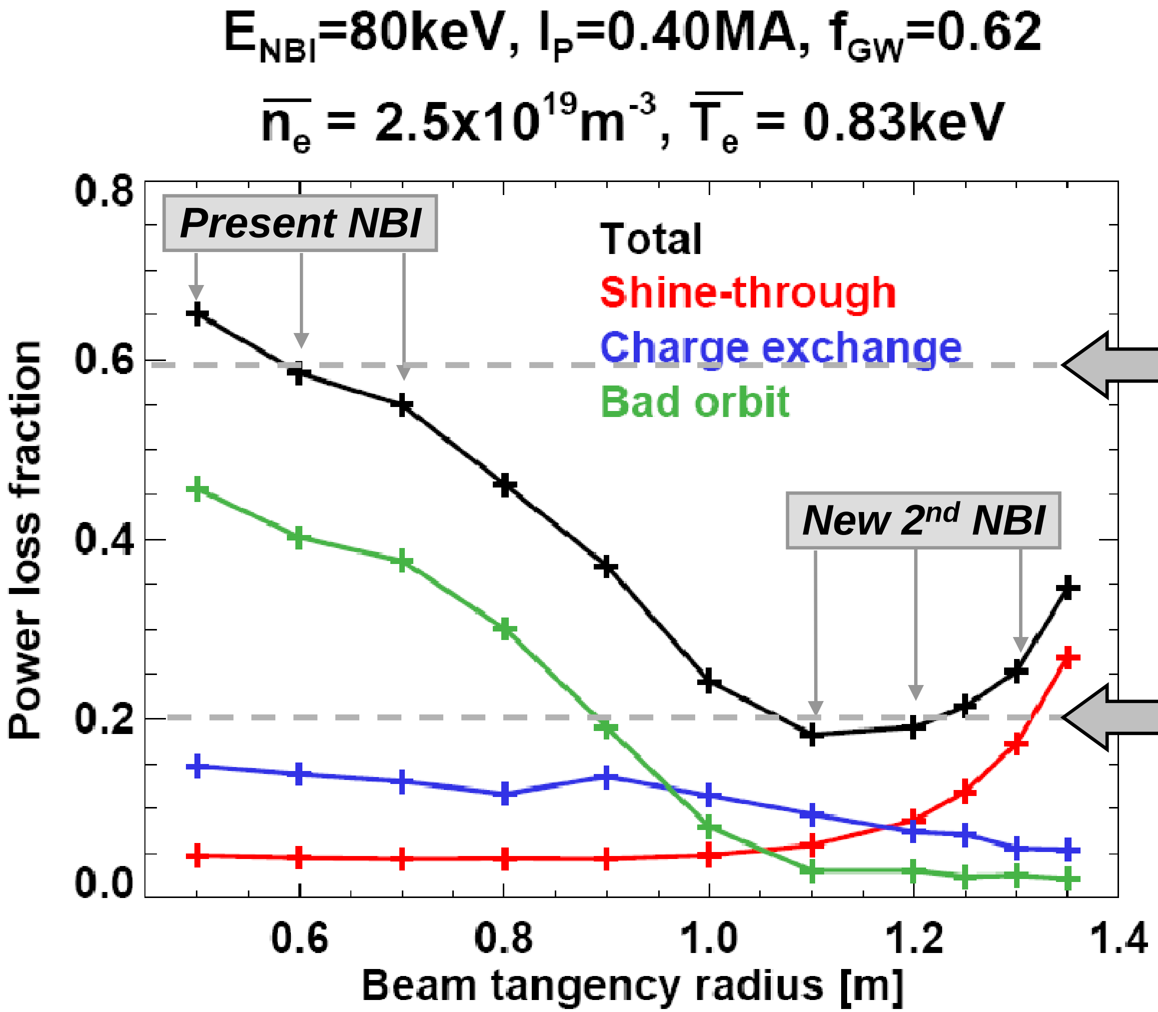
- Higher current expected to expand range of accessible T and ν^*
  - Accessible ν^* will depend on how confinement scales at higher field and current

- Access to higher current important for variety of physics issues – examples:
  - High-β_T physics at lower ν^* (RWM, NTV) – requires access to high I_P/aB_T
  - Core transport and turbulence at reduced ν^*, reduced $\chi_{i\text{-neoclassical}}$
  - Pedestal transport/stability, SOL width, heat flux scaling vs. current, …

- I_P =1.6-2MA and $B_T = 1T$ partially-inductively driven scenarios identified:
  - f_{NICD} = 50-65% with **q_{min} > 1**, β_N = 4-5, NBI profile computed with TRANSP
    - Similar to present high NI-fraction discharges, but with 2× field and current
  - These scenarios also require ≥ 8MW of NBI heating power for $H_{98} \leq 1.2$

- Solenoid in new CS can support 2MA plasmas for 5s (flat-top $\Delta\Phi_{OH}$~1.2Vs)

For NBI I_P ramp-up, more tangential 2nd NBI has 3× lower power loss than present NBI at low I_P = 400kA



- 60% of power of present NBI lost
  - Absorb 2 of 5 MW (80kV)

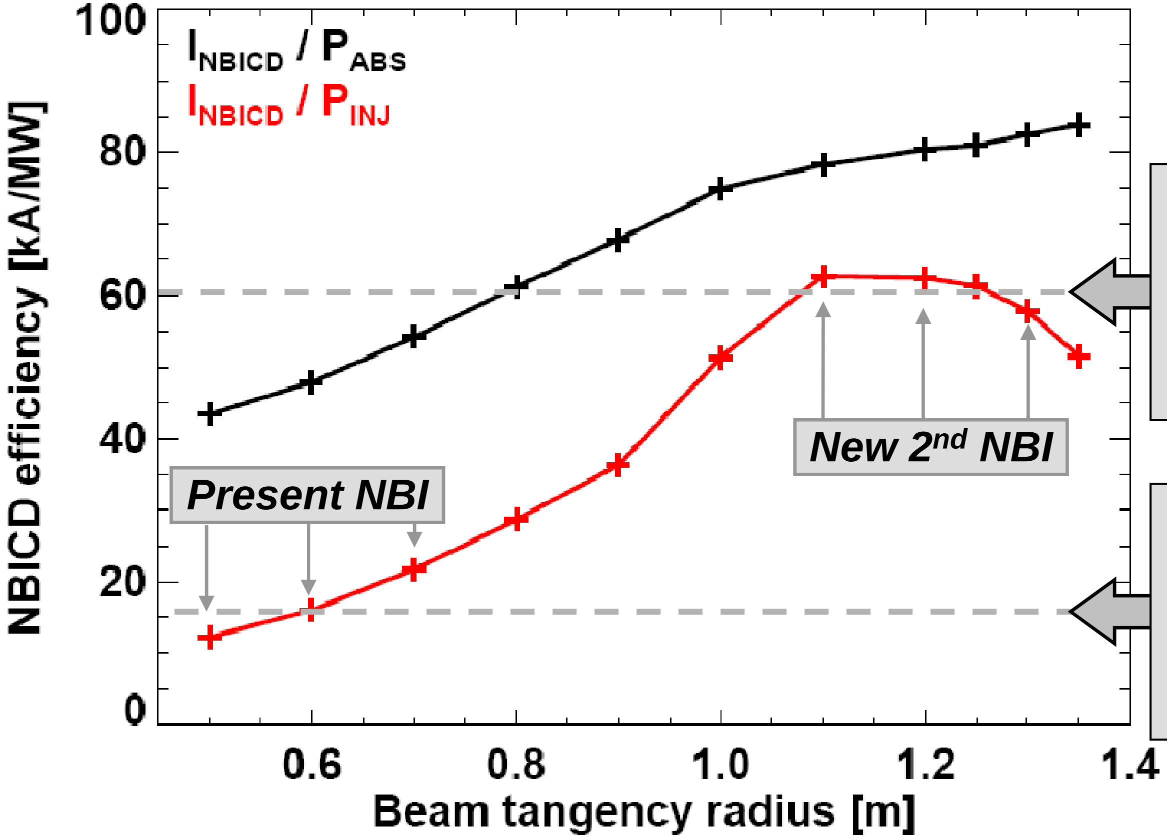
- 20% of power of new 2nd NBI lost
  - Absorb 4 of 5 MW (80kV)

→ 2nd NBI can efficiently heat 400kA HHFW-driven ramp-up plasma

For NBI I_P ramp-up, more tangential 2nd NBI has 4× higher NBI-CD than present NBI at low I_P = 400kA

E_{NBI}=100keV, I_P=0.40MA, f_{GW}=0.62

$\overline{n_e} = 2.5\text{x}10^{19}\text{m}^{-3}$, $\overline{T_e}$ = 0.83keV



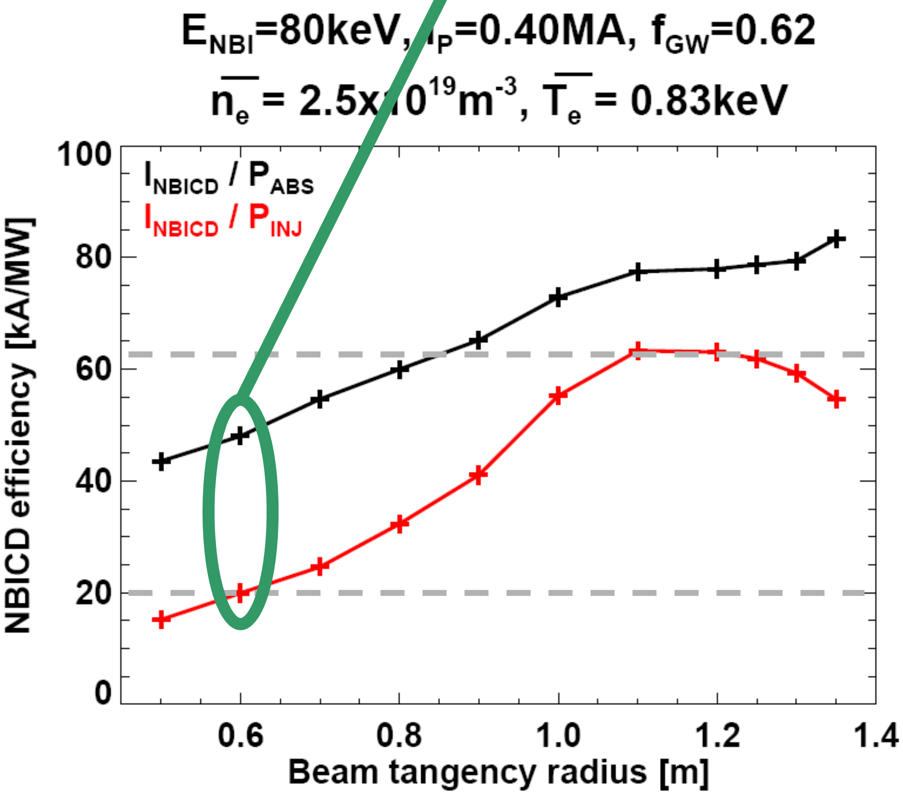
- 2nd NBI → 60kA/MW current drive efficiency
  - 450kA CD for 7.5MW injected at E=100keV
- Present → 15kA/MW current drive efficiency
  - 110kA CD for 7.5MW injected at E=100keV

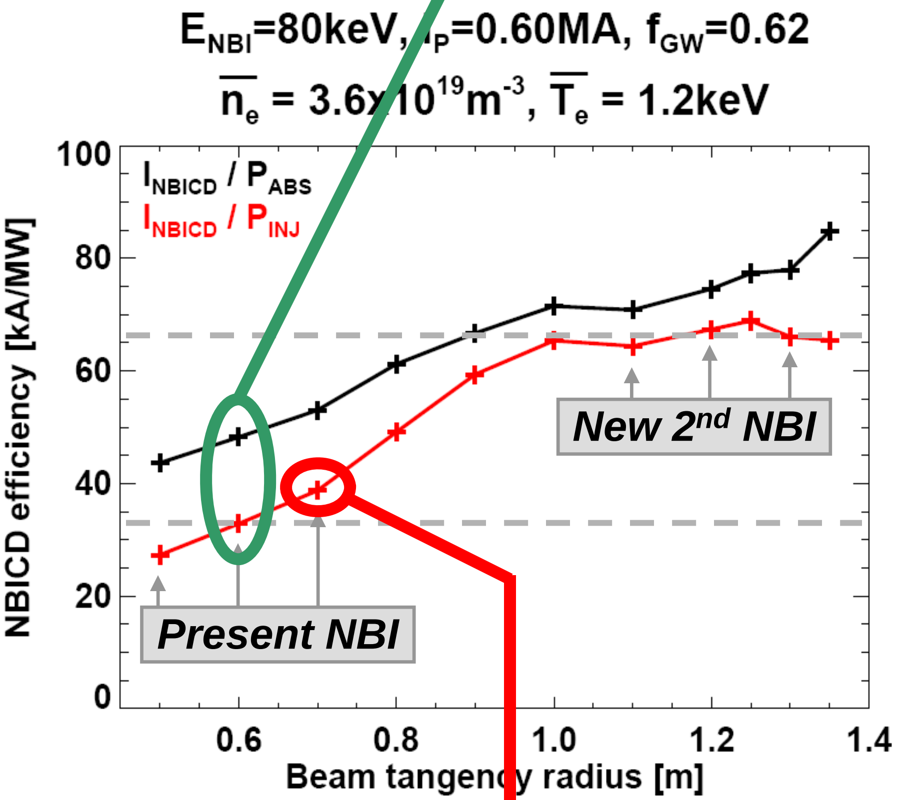
→ 2nd NBI can provide sufficient current for ramp-up to ~800kA

For NBI I_P ramp-up, absorbed fraction and CD of *present* NBI increases by factor of 1.7 for plasma current = 400kA→600kA

- I_P = 400kA, present NBI:
  - 60% loss, 20kA/MW

- I_P = 600kA, present NBI:
  - 32% loss, 33kA/MW





Most tangential of present sources has > 70% absorption for $I_P \geq$ 600kA and would be the most effective of the present sources for ramp-up

Non-inductive ramp-up to ~0.4MA possible with RF + new CS, ramp-up to ~1MA possible with new CS + more tangential 2nd NBI

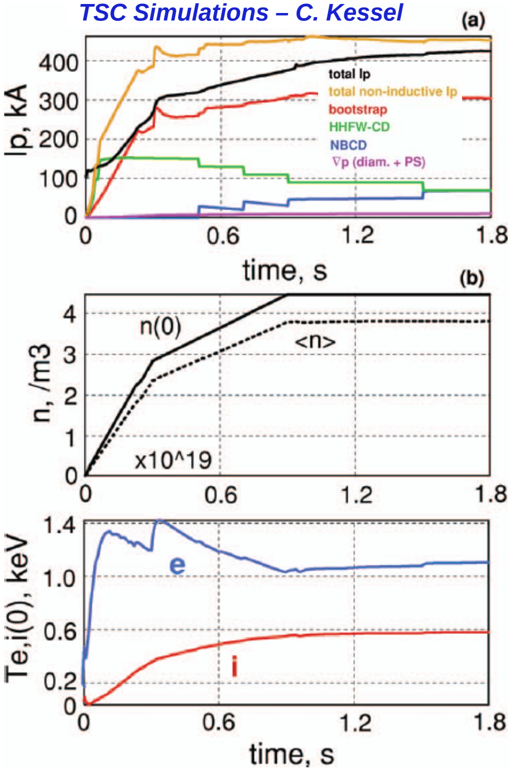
Ramp to ~0.4MA with fast wave heating:

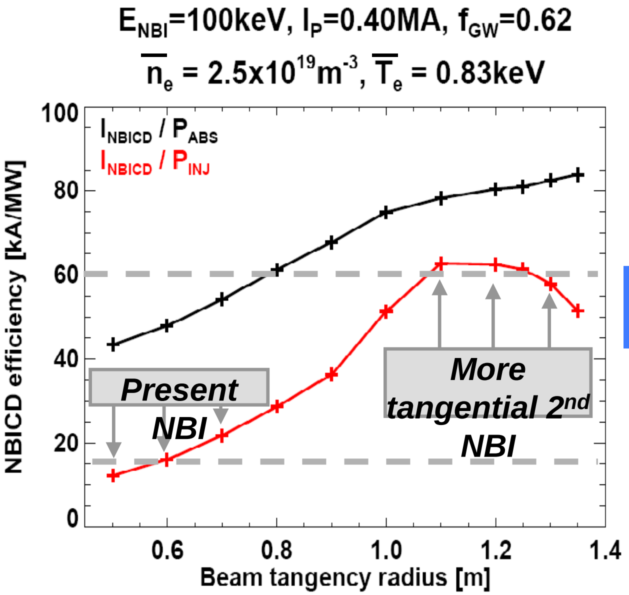
- High field ≥ 0.5T needed for efficient RF heating
- ~2s duration needed for ramp-up equilibration
- Higher field 0.5→1T projected to increase electron temperature and bootstrap current fraction

Extend ramp to 0.8-1MA with 2nd NBI:

- Benefits of more tangential injection:
  - Increased NBI absorption = 40→80% at low I_P
  - Current drive efficiency increases: ×1.5-2
- New CS needed for ~3-5s for ramp-up equilibration
  - Higher field 0.5→1T also projected to increase electron temperature and NBI-CD efficiency

TSC Simulations – C. Kessel



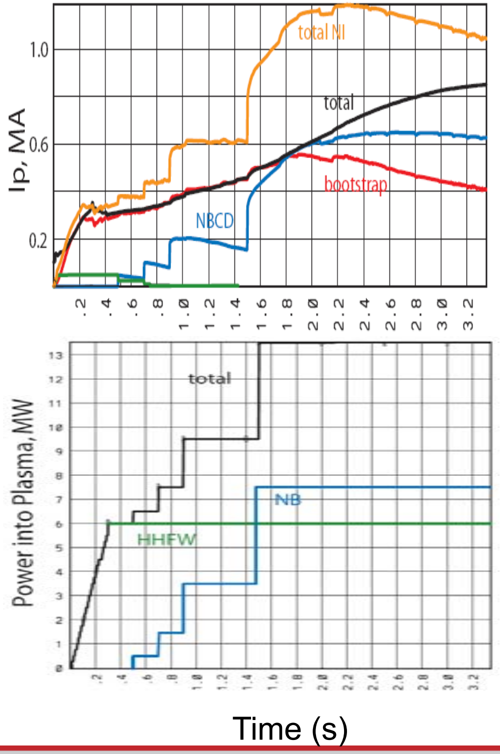


E_{NBI}=100keV, I_P=0.40MA, f_{GW}=0.62

$\overline{n}_e$ = 2.5x10^{19}m^{-3}, $\overline{T}_e$ = 0.83keV

Present NBI

More tangential 2nd NBI



Summary

- Free-boundary equilibrium calculations have been performed to determine the coil currents to support B_T = 1T, I_P = 2MA, high β_N – **largest change is for VF**
- **Additional divertor PF coils** have been optimized and incorporated to provide **enhanced power exhaust flexibility** - including high flux expansion
- TRANSP calculations indicate NB injection at **large tangency radius** is favorable for **increased current drive efficiency**, especially at reduced I_P
- Summary of physics and performance enabled by NSTX Upgrade:
  - New CS with B_T = 1T, I_P = 2MA (with induction), $t_{flat\text{-}top}$ = 5s to provide:
    - Extended range of field, current, β, collisionality to obtain unique data to aid development of first-principles understanding of turbulent transport
    - Longer pulse to assess RF ramp-up, 100% non-inductive sustainment at ~1MA
    - Higher field to stably accept high power for edge heat/particle transport studies
  - More tangential 2nd NBI to provide:
    - Up to 2 times higher CD efficiency, J profile control, tests of NBI ramp-up to ~1MA
    - World-leading capabilities for plasma boundary physics at high heat flux
    - Increased heating power to access very high β at low collisionality – important for fundamental studies of transport and global stability