

Divertor Heat Flux Mitigation in High-Performance H-mode Discharges in NSTX

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Abstract and Acknowledgments

Abstract. Experiments conducted in high-performance 1.0-1.2 MA 6 MW NBI-heated H-mode plasmas with a high flux expansion radiative divertor in NSTX demonstrate that significant divertor peak heat flux reduction and access to detachment may be facilitated naturally in a highly-shaped spherical torus (ST) configuration. Improved plasma performance with high $\beta_p = 15 - 25 \%$, a high bootstrap current fraction $f_{BS} = 45 - 50 \%$, longer plasma pulses, and an H-mode regime with smaller ELMs has been achieved in the lower single null configuration with higher-end elongation 2.2-2.4 and triangularity 0.6-0.8. Divertor peak heat fluxes were reduced from 6-12 MW/m² to 0.5-2 MW/m² in ELMy H-mode discharges using high magnetic flux expansion and partial detachment of the outer strike point at several D₂ injection rates, while good core confinement and pedestal characteristics were maintained. The partially detached divertor regime was characterized by a 30-60 % increase in divertor plasma radiation, a peak heat flux reduction by up to 70 %, measured in a 10 cm radial zone, a five-fold increase in divertor neutral pressure, and a significant volume recombination rate increase.

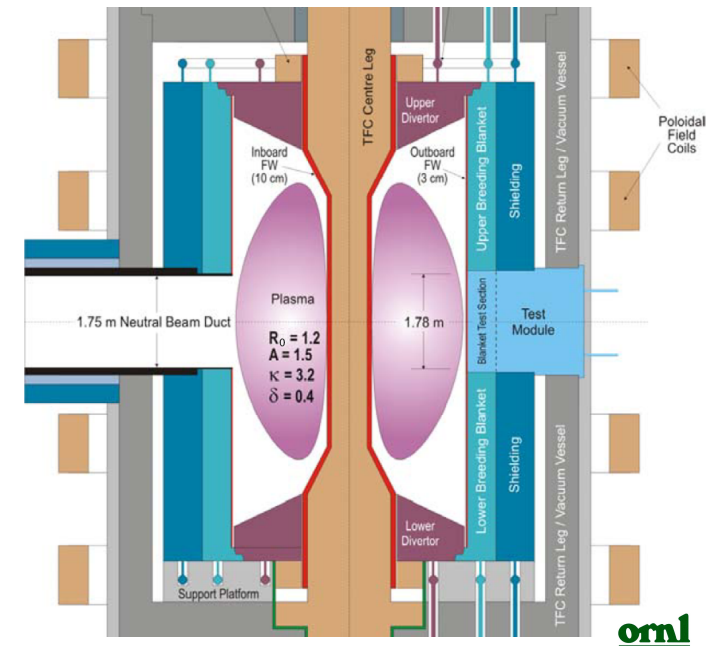
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Conclusions

- Significant divertor **peak heat flux reduction** has been demonstrated in highly shaped high-performance H-mode plasmas in NSTX using **divertor magnetic flux expansion and radiative divertor** simultaneously with **high core plasma performance**
 - Good synergy of high performance H-mode regime with partially detached divertor
- Detachment characteristics in NSTX
 - Steady-state PDD regime achieved only with additional gas injection into a high flux expansion divertor
 - High divertor radiated power, neutral pressure, volume recombination rate measured
 - PDD properties appear to be similar to those observed in tokamak
 - SOL geometry limits radiated power and momentum losses to the separatrix region

Divertor heat flux mitigation is key for present and future fusion plasma devices

- **Radiative divertor** is envisioned for present and future devices (e.g. ITER) as the **steady-state** heat flux mitigation solution
 - Divertor $q_{peak} < 10 \text{ MW/m}^2$
 - Large radiated power fractions ($f_{rad} = 0.50 - 0.80$)
 - Integration with pedestal and core
 - Partially detached divertor (**PDD**) is the most promising regime

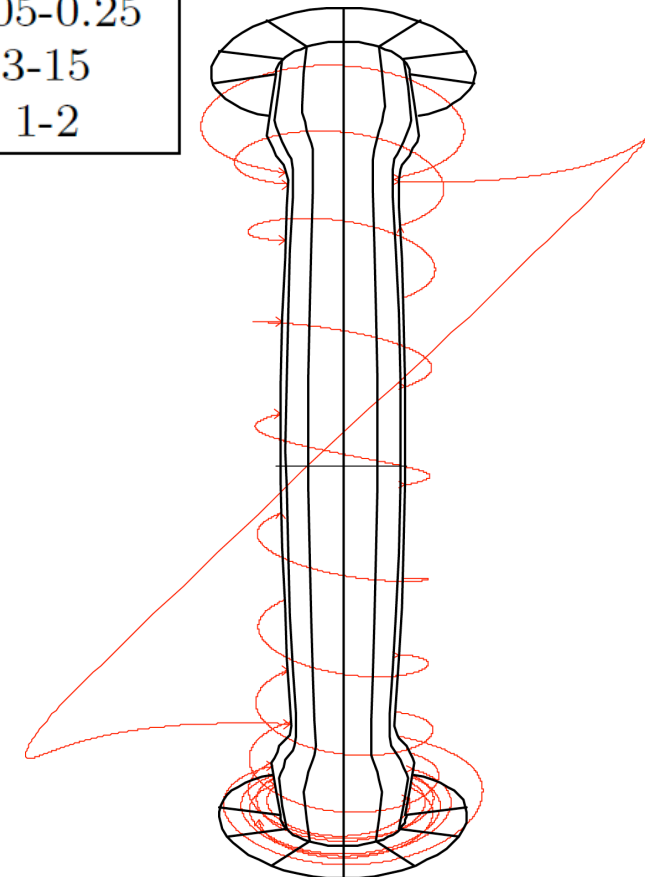
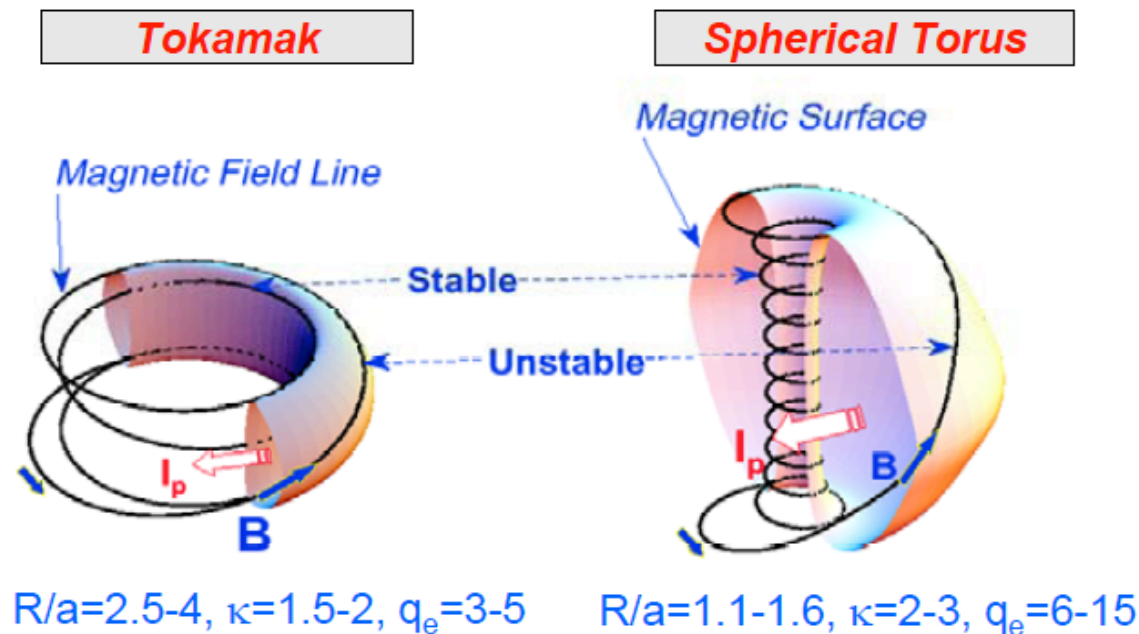


Peng et al, PPCF 47, B263 (2005)

- Radiative divertor in NSTX
 - Does radiative divertor work in a spherical torus (ST) with a compact high $q_{||}$ divertor? What are the limitations?
 - Experimental basis for radiative divertor optimization and projections to ST-CTF

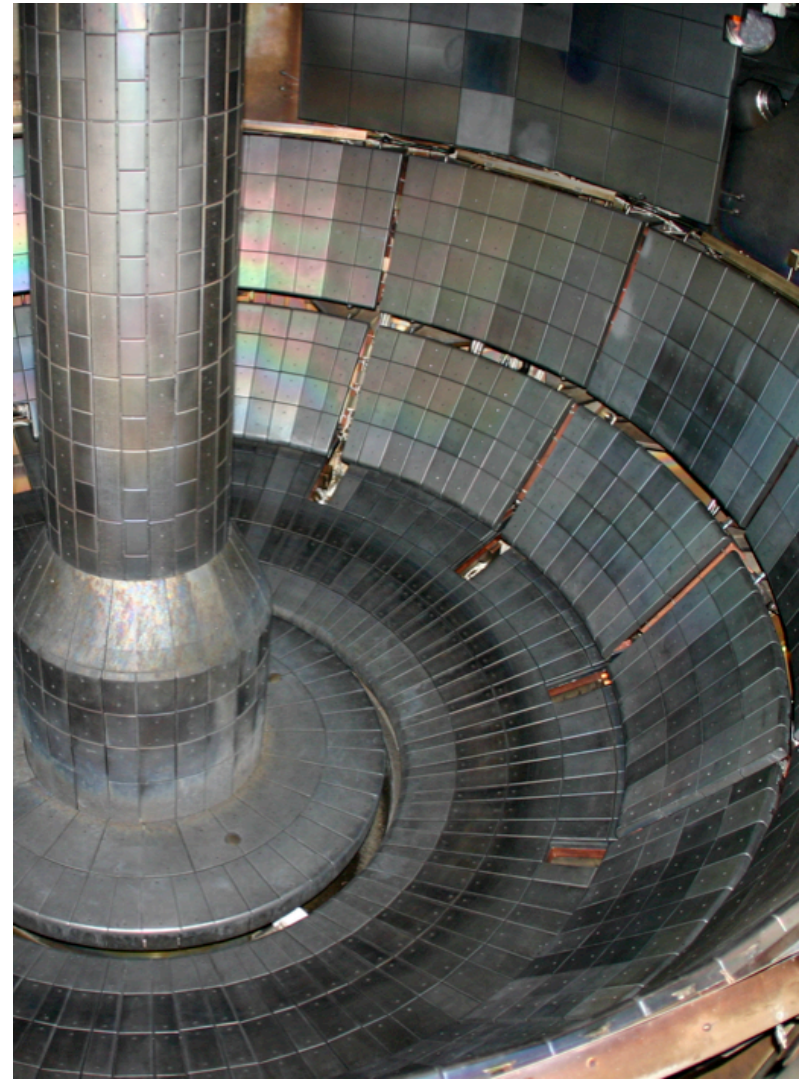
SOL / divertor geometric properties are different in spherical tori and large aspect ratio tokamaks

Quantity	NSTX	Tokamak
Aspect ratio	1.4-1.5	2.7
In-out plasma boundary area ratio	1:3	2:3
Midplane to target connection length L_c (m)	8-10	30-80
X-point to target parallel length L_x (m)	5-7	10-20
X-point to target poloidal length L_p (m)	0.05-0.15	0.05-0.25
Poloidal magnetic flux expansion f_m at OSP	16-24	3-15
Magnetic field angle at target (degree)	2-5	1-2



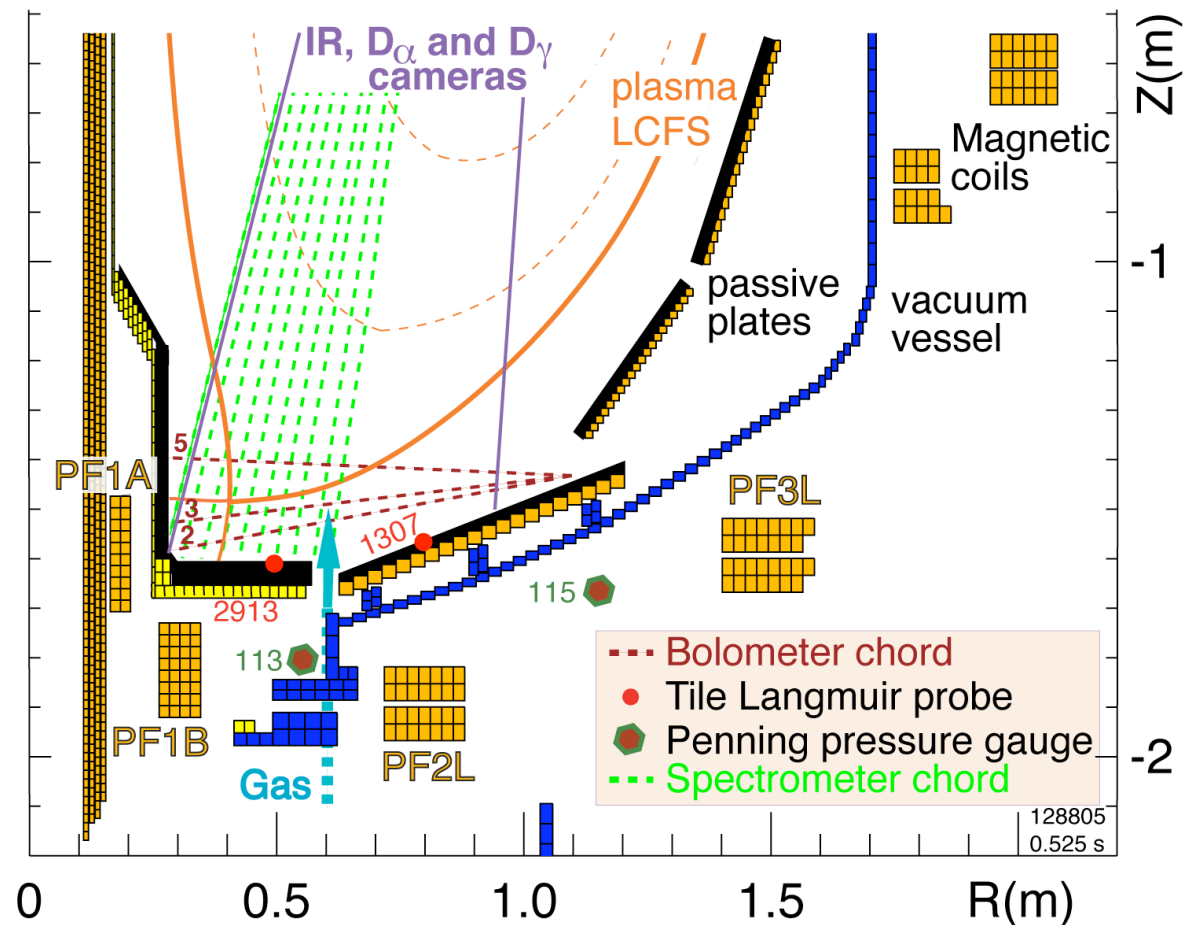
Open geometry NSTX divertor enables flexibility in plasma shaping

- Plasma facing components
 - ATJ and CFC tiles
 - Carbon - erosion, sputtering
 - Max P_{rad} fraction limited by carbon radiation efficiency
 - Typical divertor tile temperature in 1 s pulses $T < 500$ C
($q_{peak} \leq 10$ MW/m²)
- No active divertor pumping
 - Experiments with lithium coatings for reduced recycling (see Kaita et al., EX/P4-9)

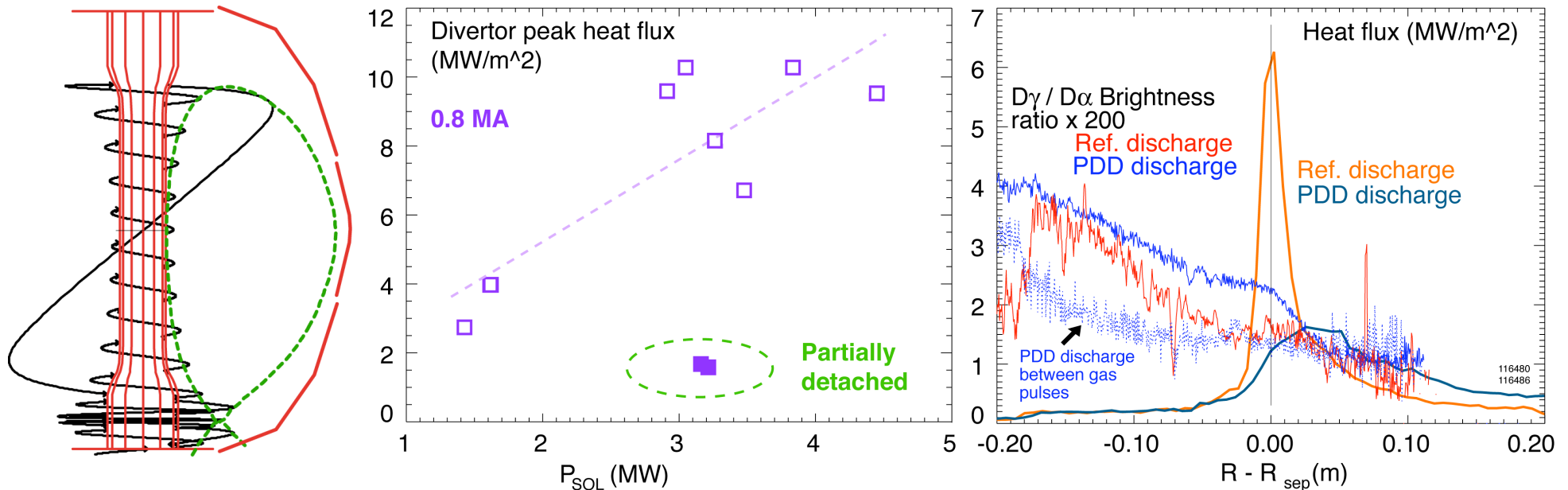


Multiple diagnostic measurements are analyzed to elucidate on radiative divertor physics in NSTX

- Diagnostic set for divertor studies:
 - IR cameras
 - Bolometers
 - Neutral pressure gauges
 - Tile Langmuir probes
 - D_α , D_γ filtered CCD arrays
 - UV-VIS spectrometer (10 divertor chords)
- Midplane Thomson scattering and CHERS systems
- Divertor gas injector
 - $\Gamma_{gas} = 20\text{-}200 \text{ Torr l / s}$



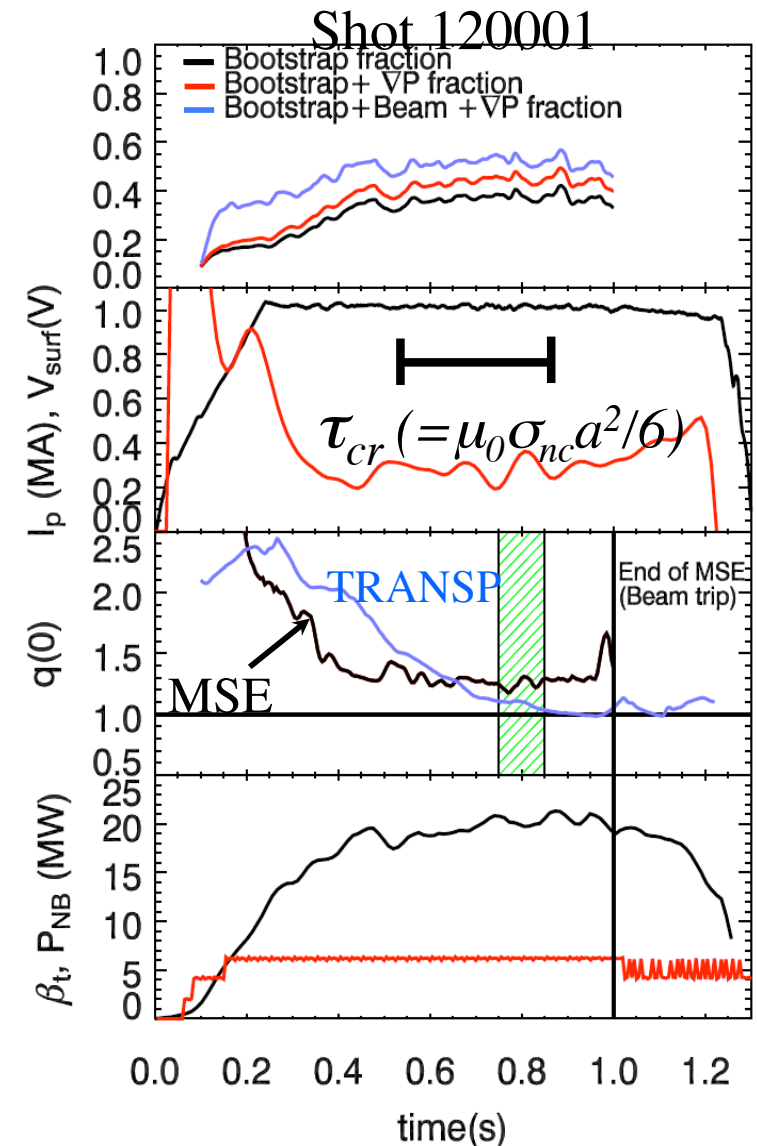
In low κ , δ configuration with rad. divertor, q_{peak} reduced albeit with confinement degradation



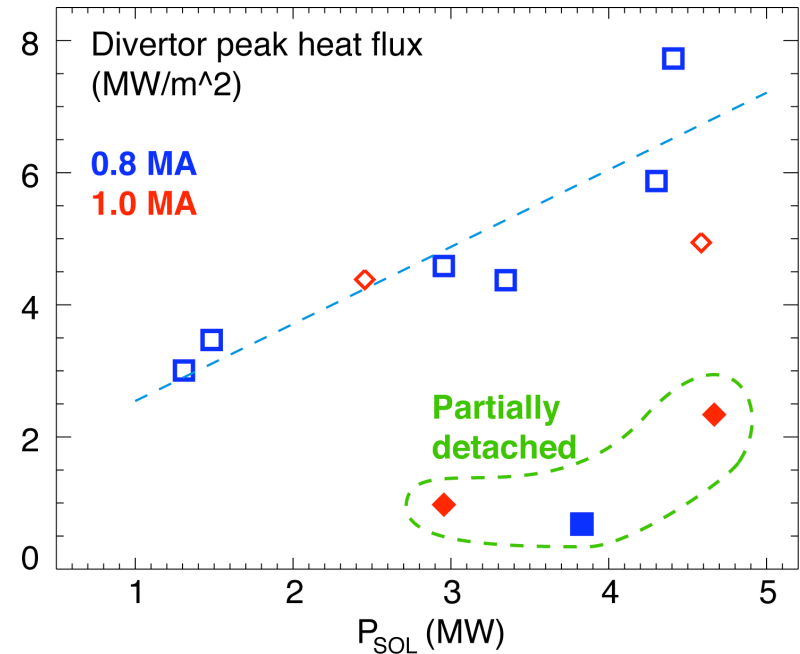
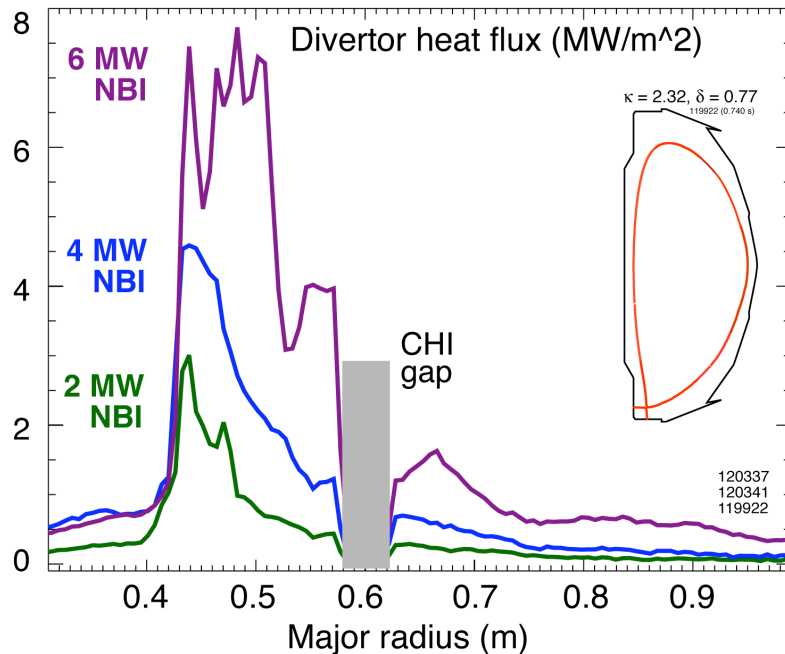
- Peak heat flux in outer divertor (**Maingi JNM 363-365, 196 (2007)**):
 - ITER-level $q_{out} < 10 \text{ MW/m}^2$
 - Scaling of q_{peak} : linear with P_{sol} (P_{NBI}), linear-monotonic with I_p
 - Large q_{peak} asymmetry - 2-10; inner divertor always detached
- Experiments using D₂ injection (**Soukhanovskii IAEA 2006**):
 - q_{peak} reduced by up to 60 % in transient PDD regime
 - X-point MARFE degraded confinement within $2-3 \times \tau_E$

High plasma performance and reduced q_{pk} are attained in highly shaped plasmas

- High performance H-mode
(Gates APS 2005, Maingi APS 2005, Menard IAEA 2006)
 - $\kappa = 2.2-2.3$, $\delta = 0.65-0.75$, $drsep \sim 5-10$ mm
 - H89P ~ 2.0
 - $\beta_t = 15 - 25$ %
 - $f_{bs} = 45 - 50$ %
 - longer pulses $\sim 50 \times \tau_E$
 - smaller ELMs
- Divertor in highly shaped plasmas
 - High flux expansion, area expansion ($q_{peak} \downarrow$)
 - Higher isothermal SOL volume ($P_{rad} \uparrow$)
 - Lower L_p (neutral penetration \uparrow)
 - Neutrals recycle toward separatrix



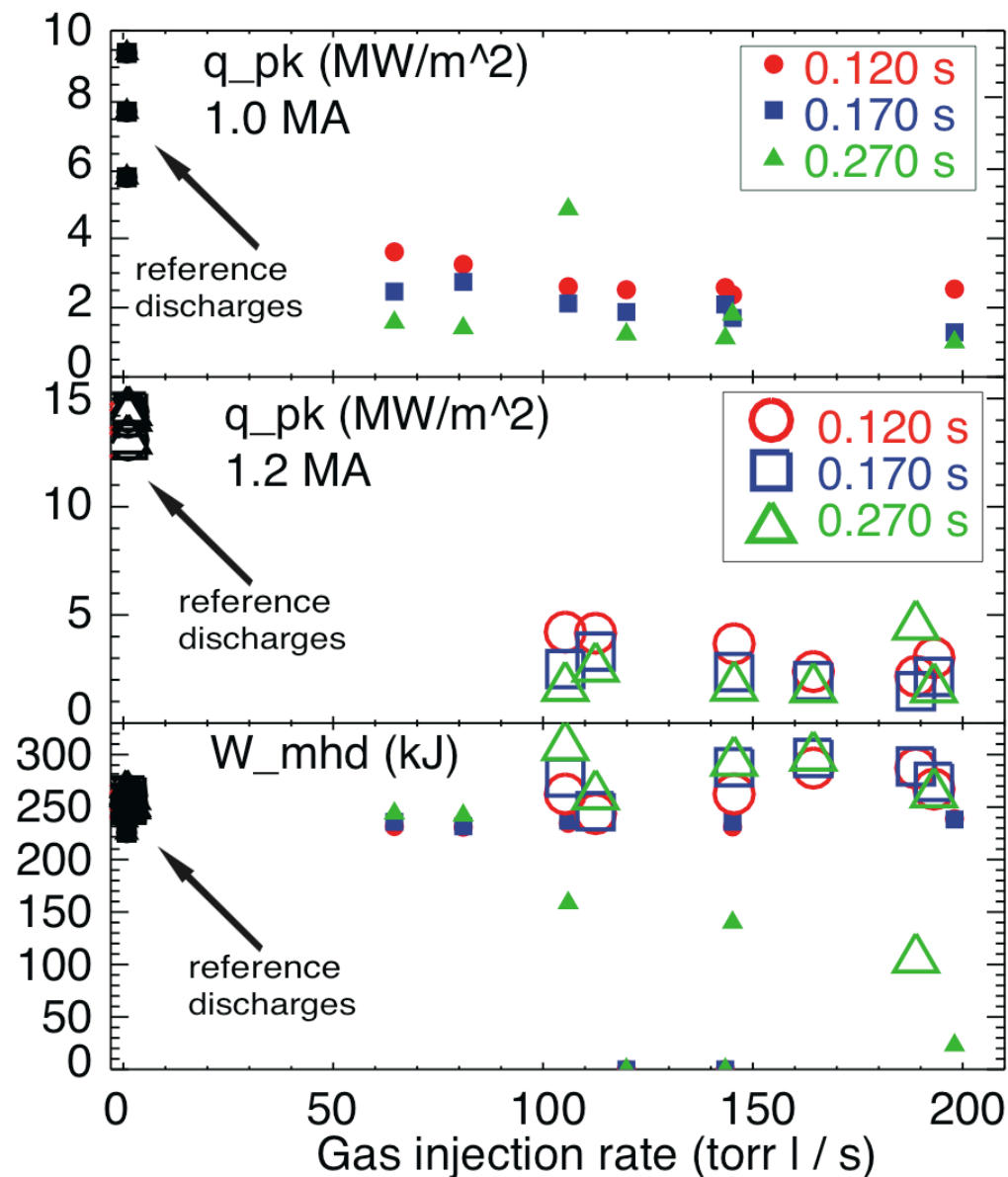
Good core plasma performance and significant q_{peak} reduction with PDD obtained at high κ , δ



- Experiments conducted in 0.8-1.0 MA 4-6 MW NBI discharges with $\kappa=2.2-2.3$, $\delta=0.6-0.75$ (**Soukhanovskii APS 2007**)
- Obtained partially detached divertor (PDD) outer strike point using divertor D₂ injection, however, P_{rad} due to intrinsic carbon and helium
- q_{peak} reduced by 60 - 80 % in PDD phase with min. confinement degradation

Radiative divertor conditions were optimized in 1.0 MA and 1.2 MA 6 MW H-mode discharges

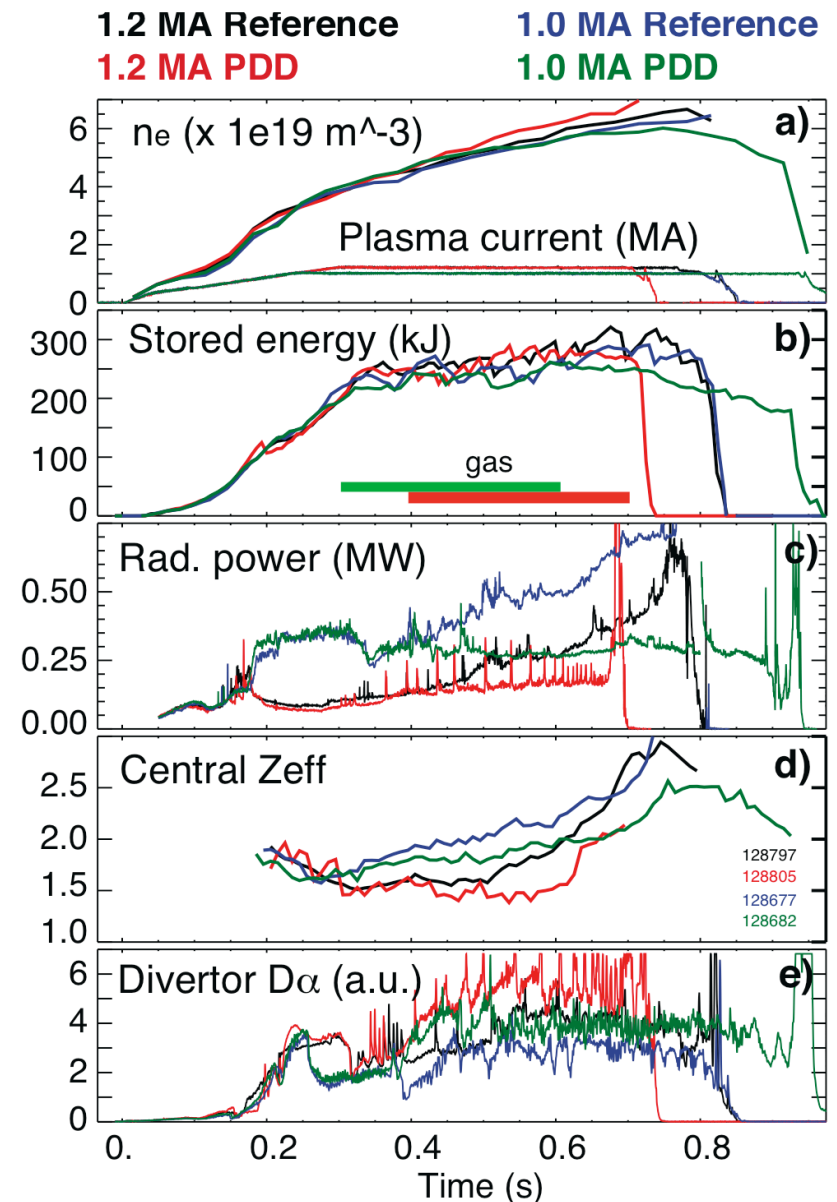
- Criteria of optimization - find gas injection rate to obtain PDD with minimal confinement degradation
- $q_{||}$ was higher in 1.2 MA discharges thus more gas was needed to reduce q_{pk}
- After 0.250-0.270 ms peak heat flux reached low steady-state level
- Optimal gas injection found (used 300 ms pulses)
 - 50-100 Torr I /s for 1.0 MA discharges
 - 110-160 Torr I /s for 1.2 MA discharges



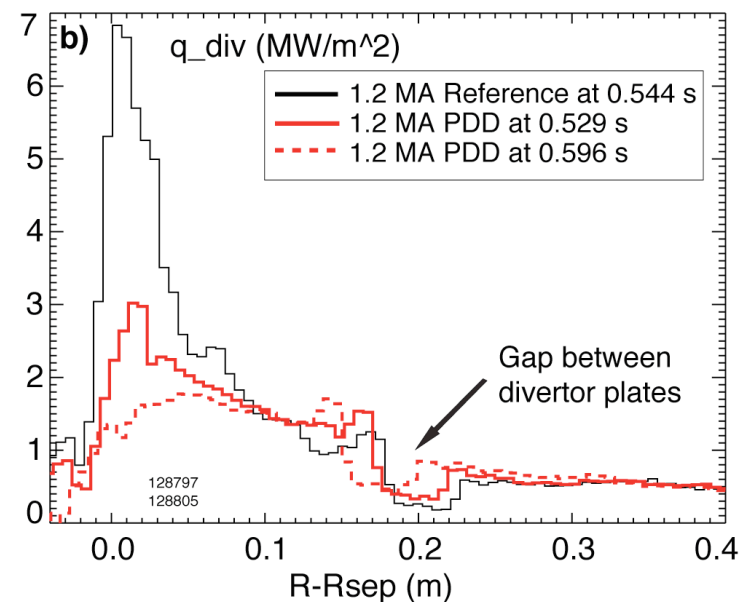
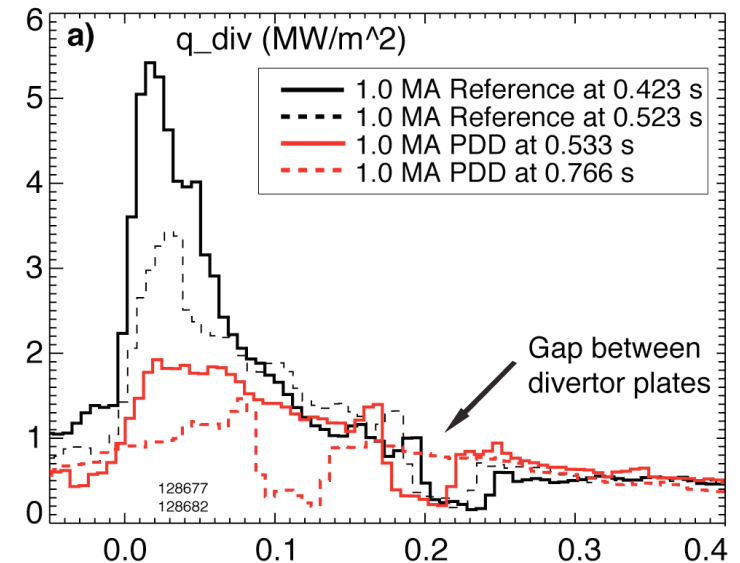
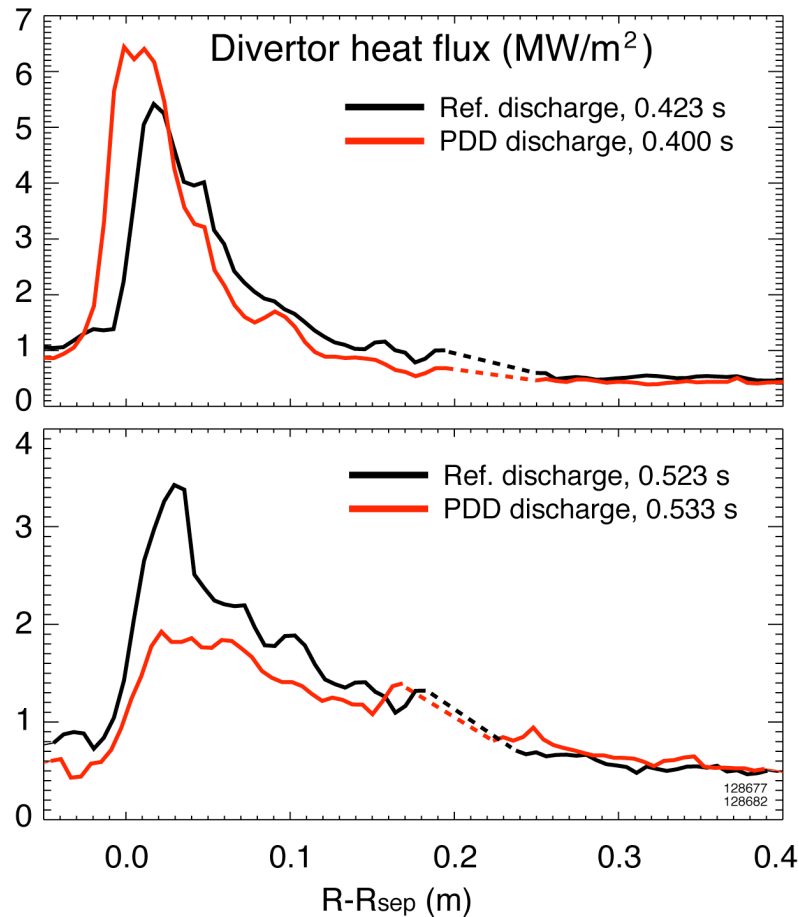
High core and pedestal plasma performance during PDD is achieved in high κ , δ configuration

- These experiments
 - $I_p = 1.0-1.2$ MA
 - $P_{NBI} = 6$ MW
 - $n_e = (0.7-0.8) \times n_G$
 - D₂ injection in divertor
 - $q_{||} = P_{SOL} / (4\pi R (B_p / B_{tot}) \lambda_q) = 50-80$ MW/m²
 - **Carbon is main impurity**

- High core plasma performance during PDD phase
 - Minimal effect on W_{MHD} or pedestal
 - Core P_{rad} and n_c decreased
 - Small ELMs ($\Delta W_{MHD} / W_{MHD} \leq 1\%$) and mixed ELMs

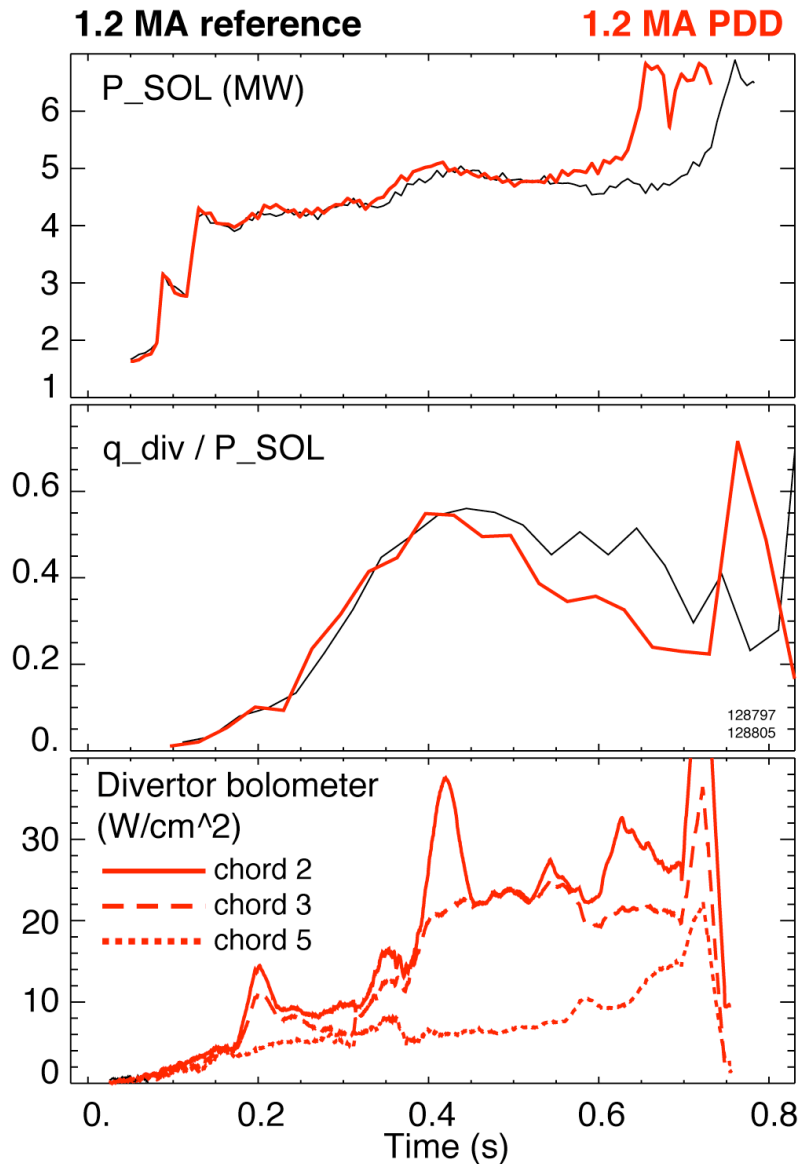


Peak heat flux reduced by up to 60 % as a result of outer strike point partial detachment



- λ_q changed from 5-10 cm to 10-15 cm
- PDD zone 10-15 cm
- No q reduction outside of PDD zone

Divertor heat flux reduction was attributed in part to divertor radiated power loss



- Total $P_{SOL} = 4.5 - 5$ MW
- $Q_{out.div.} = 2-3$ MW (reference discharge)
- $Q_{out.div.} = 1-2$ MW (PDD discharge)
- Outer leg radiated power estimate:
 - $V=0.1$ m³
 - Total $P_{rad}=0.5$ MW

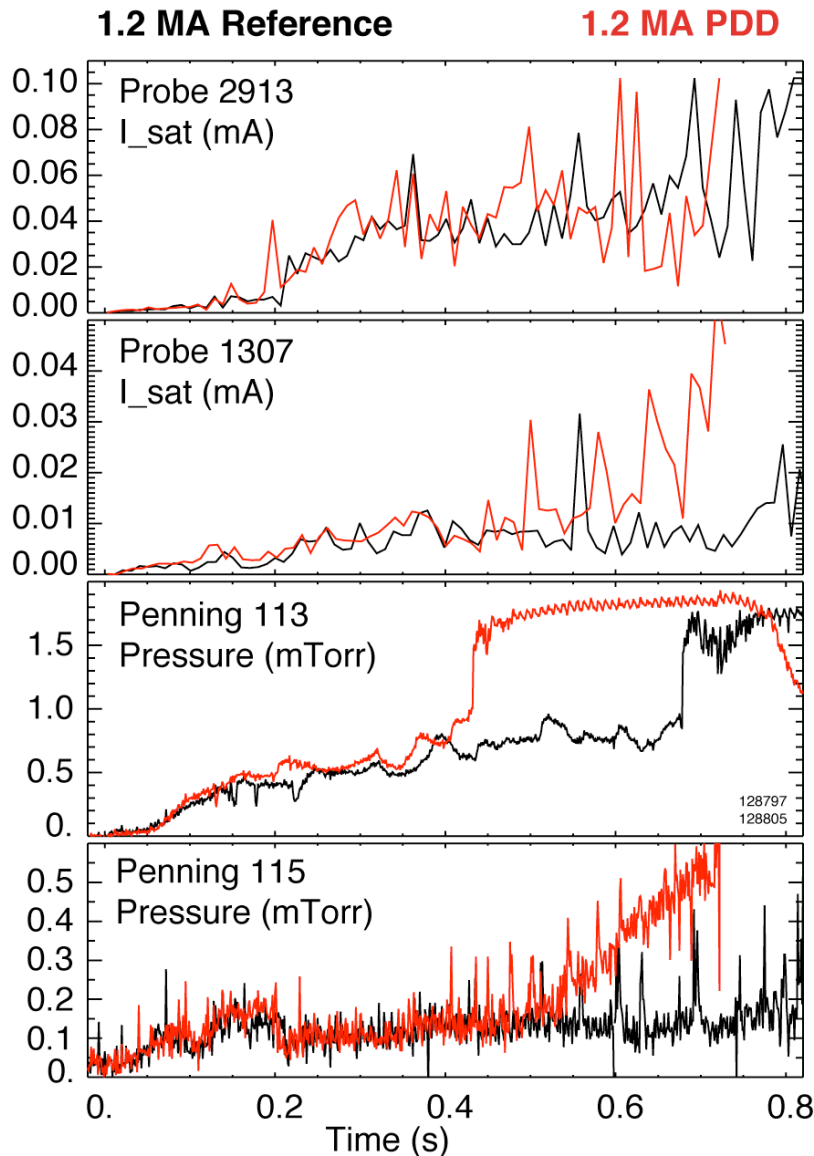
$$\frac{\partial(nv)}{\partial x} = n(n_n \langle \sigma v \rangle_i - n \langle \sigma v \rangle_{rec}) + S_{\perp}$$

$$\frac{\partial(mnv^2 + 2nT)}{\partial x} = -mnv(n_n \langle \sigma v \rangle_{cx+el} + n \langle \sigma v \rangle_{rec})$$

$$\frac{\partial}{\partial x} \left(-\kappa_0 T^{5/2} + \frac{1}{2} mnv^3 + 5nTv \right) =$$

$$-n^2 f_Z L_Z - \frac{3}{2} T n n_n \langle \sigma v \rangle_{cx+el} - n E_{ion} \langle \sigma v \rangle_i + Q_{\perp}$$

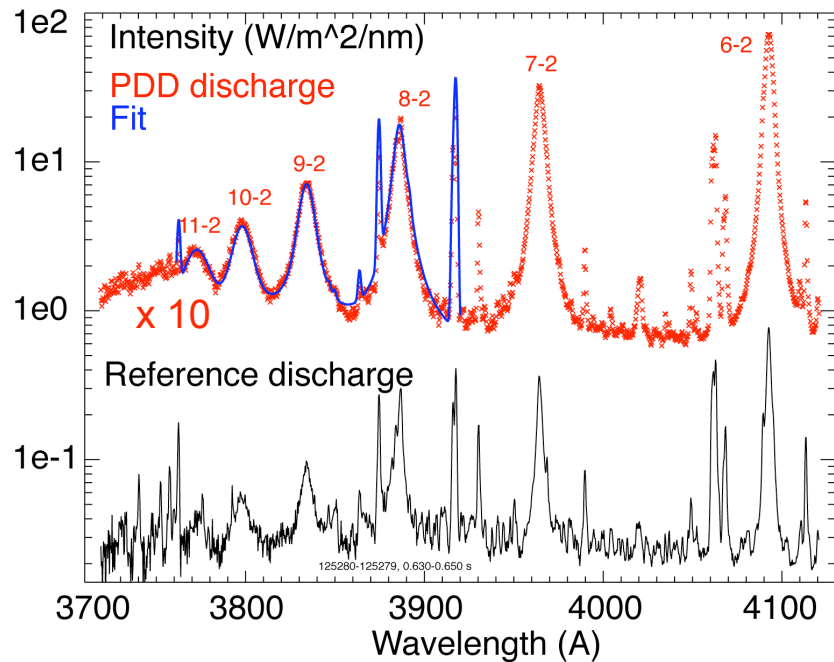
Momentum loss was evidenced by divertor neutral pressure increase and particle flux decrease



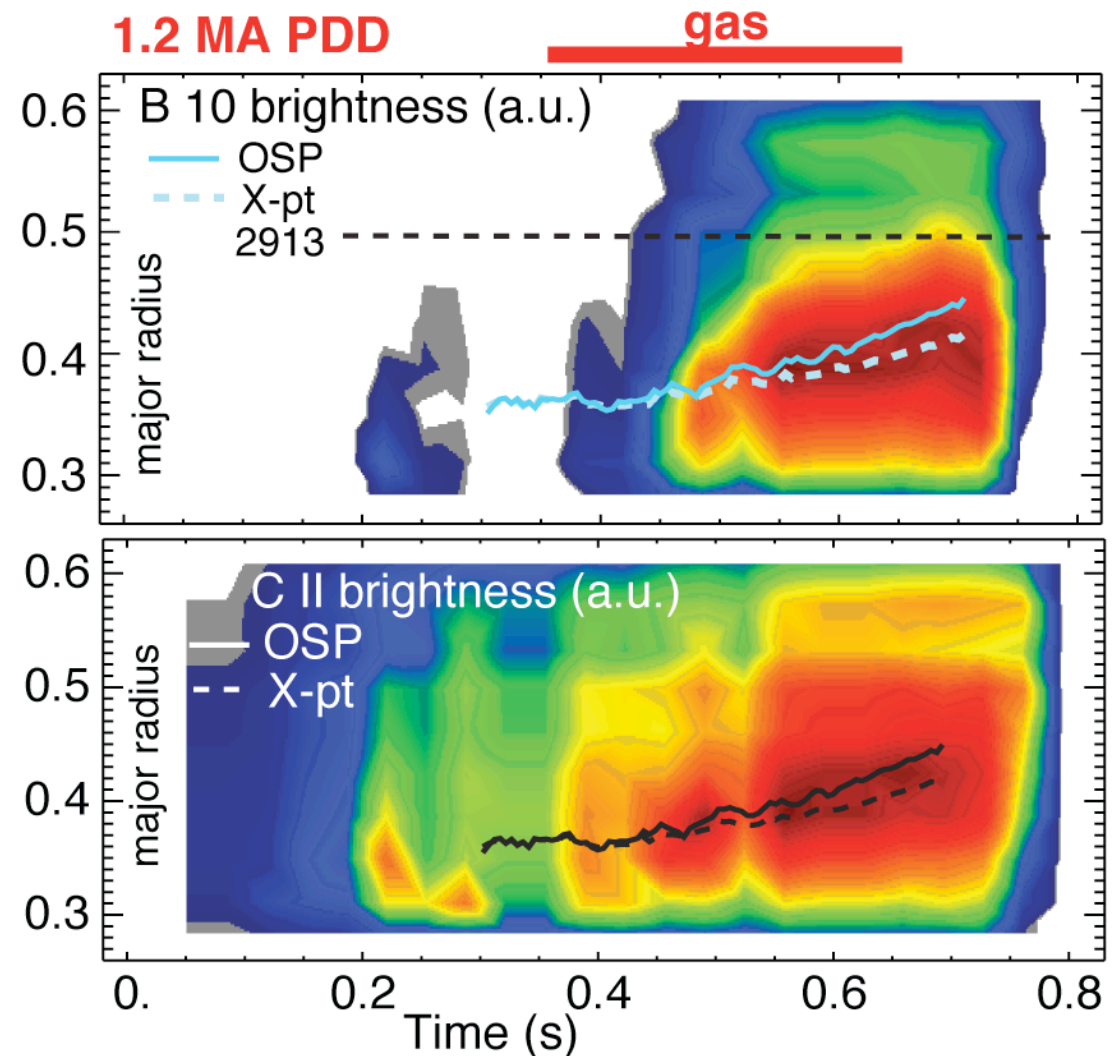
- Langmuir probe in PDD zone showed particle flux decrease during gas puff
- Langmuir probe outside of PDD zone showed particle flux increase during gas puff – as expected in high-recy. regime
- Neutral pressure increased in outer div. region from 0.5 to 2-3 mTorr
- Neutral pressure of 2-3 mTorr is required to explain plasma pressure drop of $dp/dx = 9-10 \text{ Pa/m}$

$$\frac{dp}{dx} = m\Gamma_i n_n \langle \sigma v \rangle_{cx+el} + mn^2 \langle \sigma v \rangle_{rec}$$

Carbon radiation and ion recombination rates increased in divertor detachment phase



- Increase in recombination rate
- D I Balmer spectra (8...11 - 2) indicate
 - $T_e < 0.7\text{-}1.2$ eV (from line intensity ratio according to Saha-Boltzman formula)
 - $n_e \sim 2\text{-}6 \times 10^{20} \text{ m}^{-3}$ (from Stark broadening and MMM calculations)



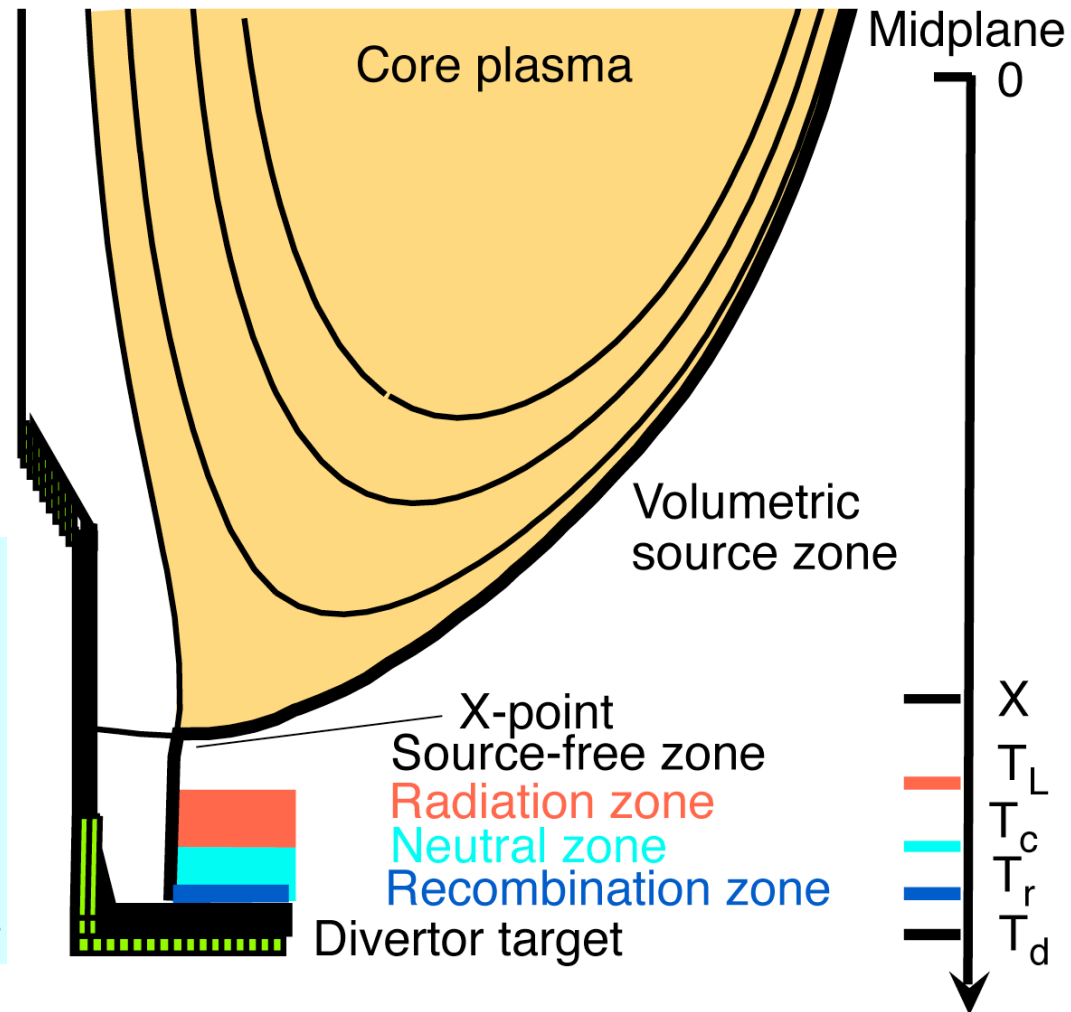
Six-zone 1D analytic SOL / divertor model captures essential features of detachment

- **Goswami PoP 8, 857 (2001)**
- Zone locations defined by temperature of process
- Sources and sinks Q_{\perp} , S_{\perp} , Γ_{i-div} , f_{rad} , R_{rec} , v_{i-n} as input

Continuity: $\frac{d}{dx}(nv) = S_n$

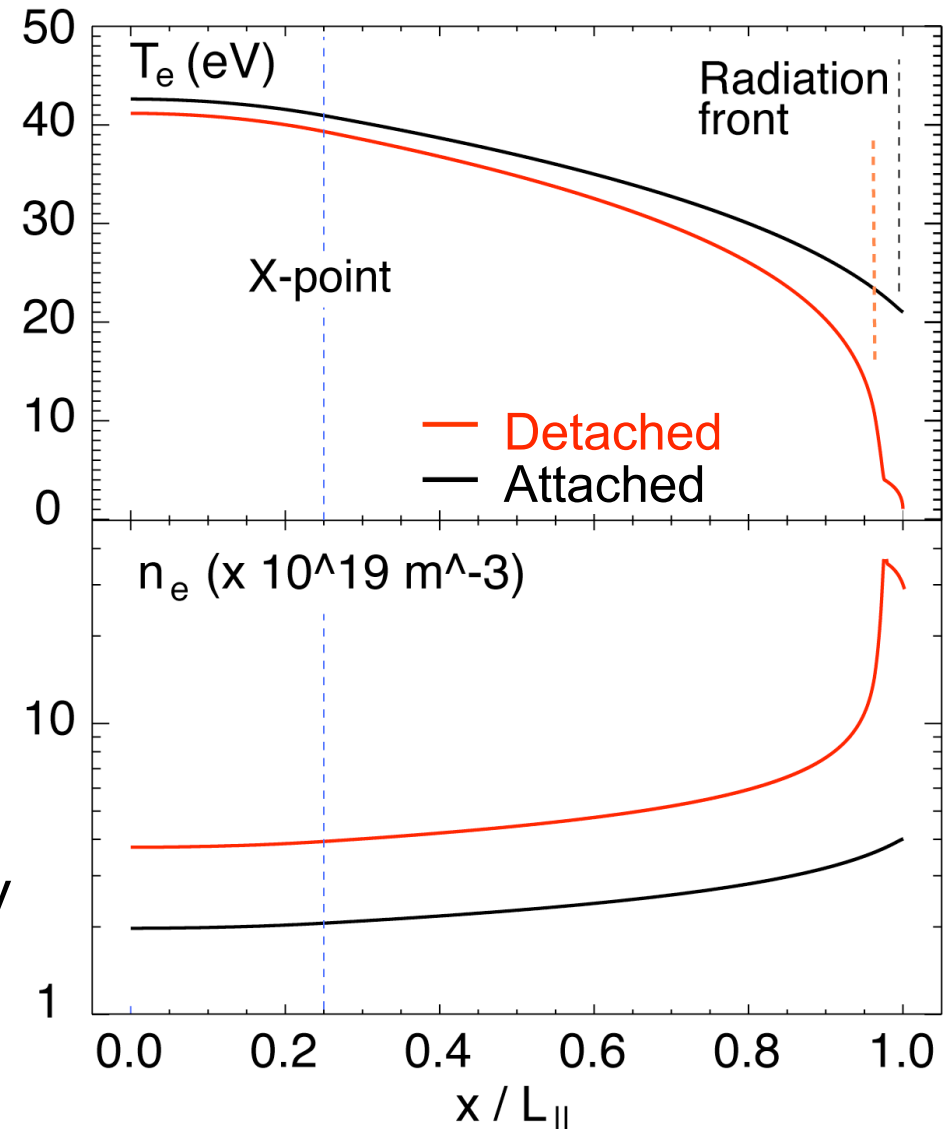
Momentum: $\frac{dp}{dx} = S_p$

Energy: $\frac{d}{dx}(\kappa_0 T_e^{5/2} \frac{dT_e}{dx}) = S_q$



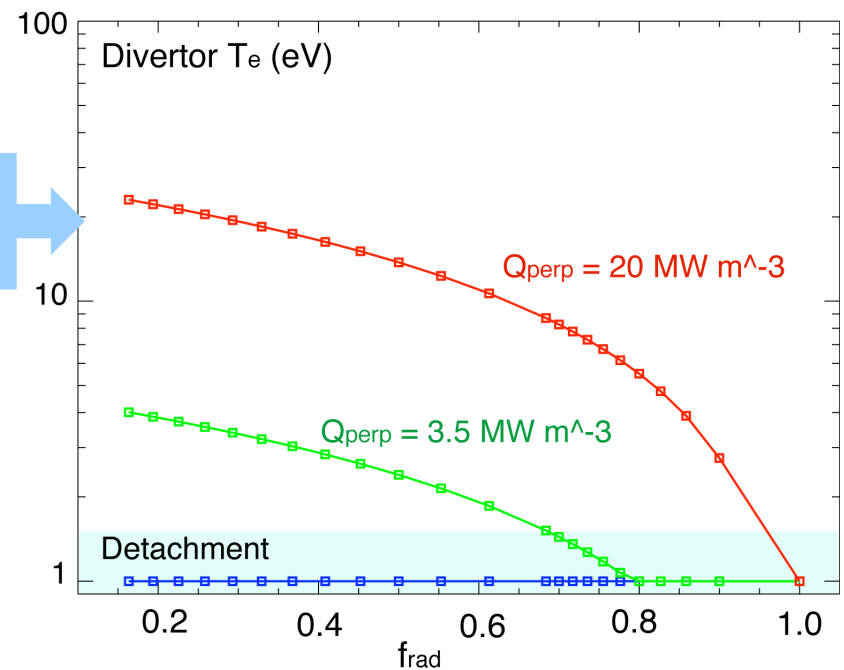
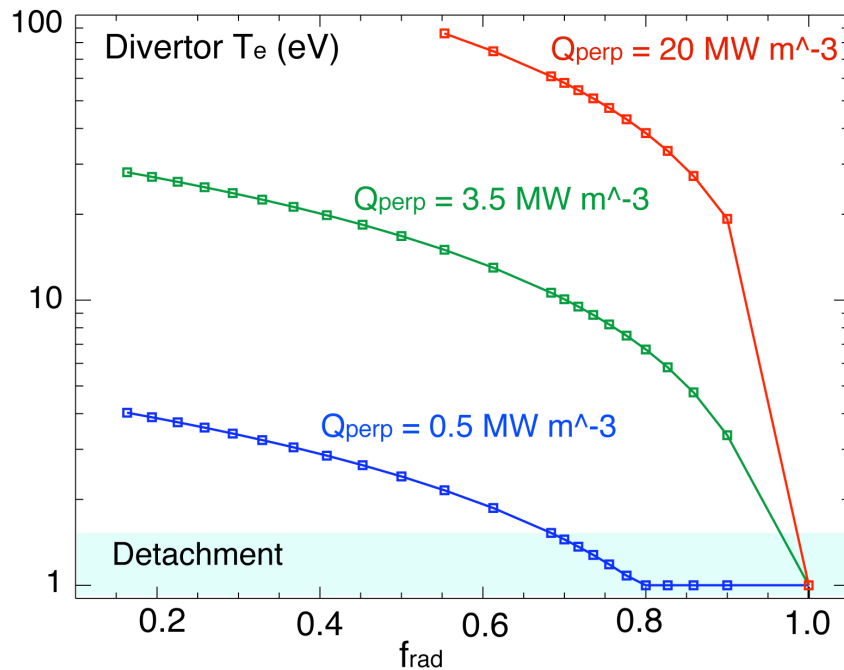
Model predictions consistent with experiment within NSTX range of SOL parameters

- NSTX SOL / divertor parameters
 - $Q_{\perp} = 0.5 - 20 \text{ MW m}^{-3}$ (high)
 - $S_{\perp} = 0.01-3 \times 10^{23} \text{ s}^{-1} \text{ m}^{-3}$
 - $L_x = 5-10 \text{ m}$ (low)
 - $R_{rec} = 10^{23} \text{ s}^{-1} \text{ m}^{-3}$
- Example calculation
 - $Q_{\perp} = 10 \text{ MW m}^{-3}$
 - $S_{\perp} = 6 \times 10^{22} \text{ s}^{-1} \text{ m}^{-3}$
 - $f_{rad} = 0.3$ (attached)
 - $f_{rad} = 0.9$ (detached)
- Recombination onset at $T_e < 1.5 \text{ eV}$
- Detachment at $T_e < 1.0 \text{ eV}$



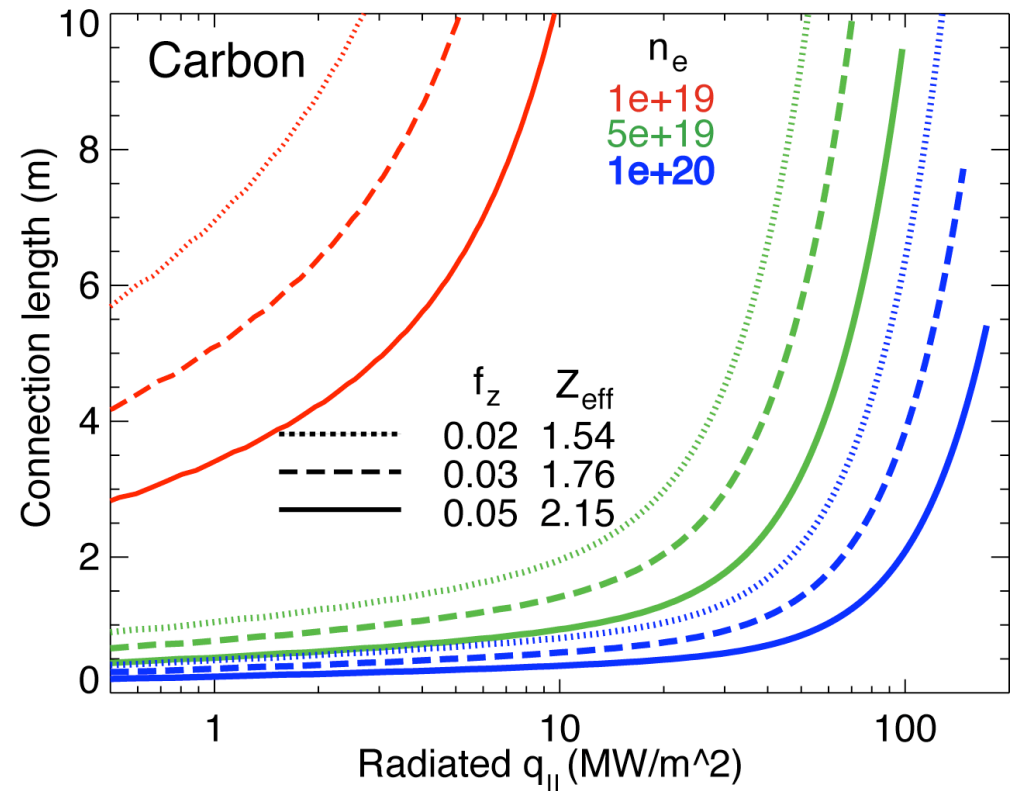
All routes to detachment predicted by model involve high f_{rad}

- Detachment at NSTX-range of Q_{\perp} , S_{\perp} can be achieved in model by
 - increasing f_{rad} (shown)
 - increasing Γ_{i-div} (gas puff)
 - increasing S_{\perp} (not shown)



High f_{rad} can be achieved with carbon in NSTX divertor at high n_e and n_z

- Hulse-Post non-coronal radiative cooling curves for low Z impurities for n_0/n_e , $n_e\tau_{recy}$
- Calculate max $q_{||}$ that can be radiated
- Express max $q_{||}$ as function of distance from heat source for range of f_z
(Post JNM 220-222, 1014 (1995))
- Power losses due to deuterium P_{rad} and ionization not considered
- For NSTX, use $n_0 = 0.1\%$ and $n_e\tau_{recy} = n_e \times 1e-3$ s



$$q_{||} = -\kappa_0 T_e^{5/2} \frac{\partial T_e}{\partial x}$$

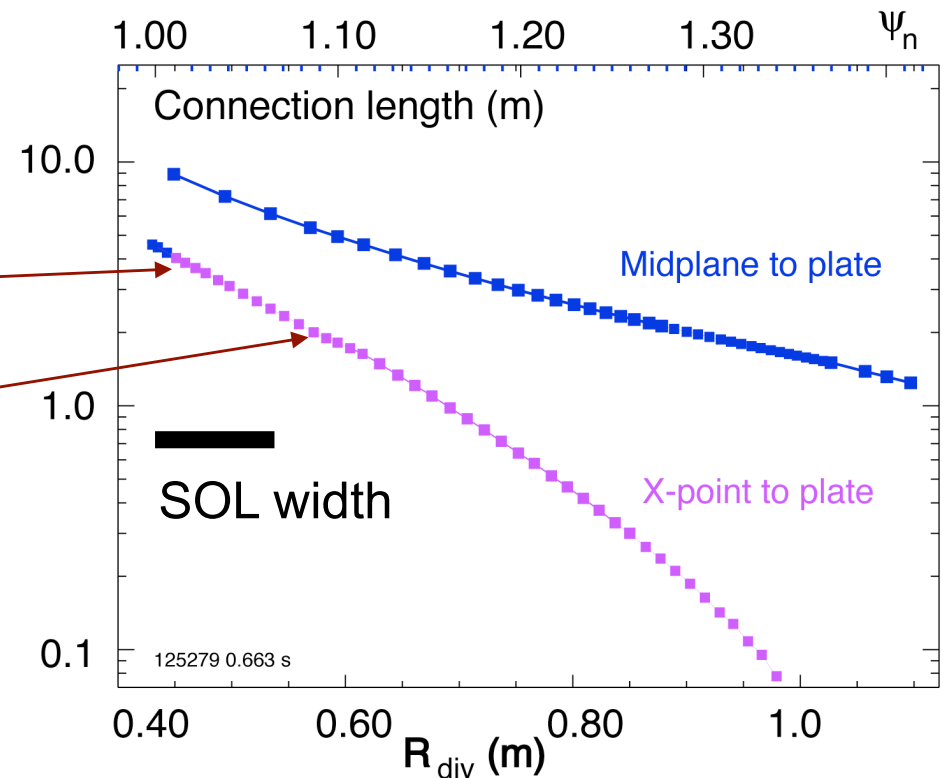
$$\frac{\partial q_{||}}{\partial x} = -n_e n_z L_Z(T_e)$$

Volumetric power and momentum losses are limited by L_x (R) at high magnetic field shear

- Fraction of $q_{||}$ to be radiated is a function of L_x for given impurity
 - high f_{rad} only where L_x longest
- Electron-ion recombination rate depends on divertor ion residence time
 - Ion recombination time: $\tau_{ion} \sim 1-10$ ms at $T_e = 1.3$ eV
 - Ion residence time: $\tau_{ion} \leq 1$ ms

possible to detach
 $L_x \sim 5-6$ m

difficult (impossible)
 to detach $L_x \sim 1-2$ m



Discussion

- PDD regime with reduced q_{pk} and good core confinement demonstrated in open geometry un-pumped divertor in a high power spherical torus
- In an ST, modest $q_{||}$ can yield high divertor q_{pk}
 - in NSTX, $q_{||} = 50\text{-}80 \text{ MW/m}^2$ and $q_{pk} = 6\text{-}12 \text{ MW/m}^2$
 - Large radiated power and momentum losses are needed to reduce $q_{||}$
- In NSTX density ramp discharges do not necessarily lead to PDD
 - n_{sep} weakly coupled with n -bar
- In NSTX, PDD regime is accessible only
 - in highly-shaped plasma configuration with high flux expansion divertor (high plasma plugging efficiency, reduced $q_{||}$)
 - modest divertor D_2 injection still needed
- ST SOL geometric effects appear to play dominant role in the above