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# Dependences of the divertor and midplane heat flux widths in NSTX

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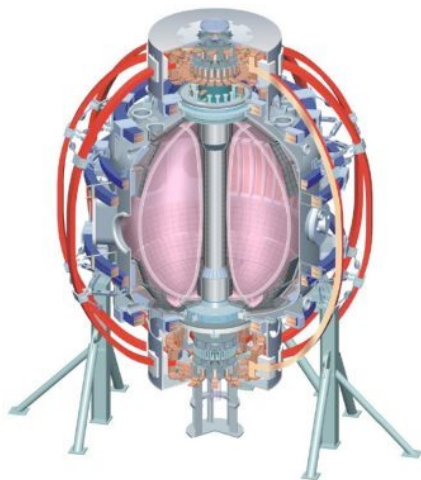
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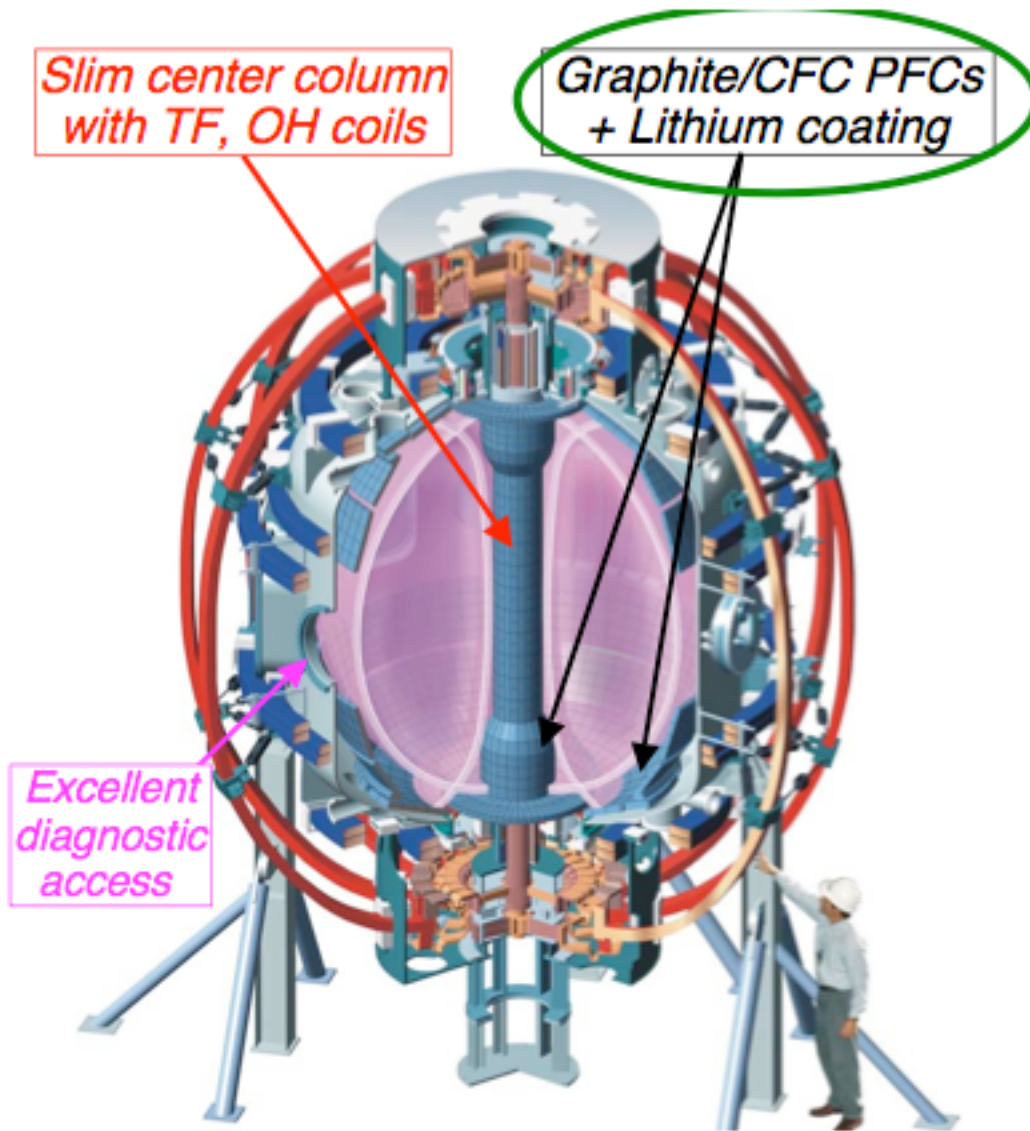
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## Introduction & Motivation

- Measurements of the divertor heat flux,  $q$  and the heat flux profile,  $\lambda_q$  are necessary for understanding thermal transport in the scrape-off layer of tokamak plasmas
- Heat loading on the divertor and plasma facing components (PFC) is also an engineering limit on the fusion reactor
  - High heat flux can also lead to PFC cracking, fatigue and subsequent impurity generation
  - Heat flux therefore limits PFC lifetime, and therefore reactor operational time between PFC replacement
- Spherical Tori (STs) are prone to large heat fluxes due to their compact design
- Part of the 2010 Joint Research Milestone (JRM) – Understanding thermal transport in tokamak scrape-off layer plasmas

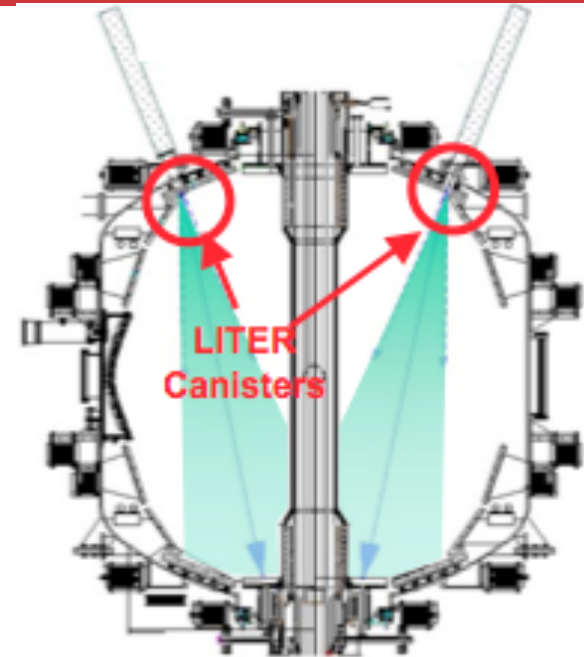
# Overview of the National Spherical Torus eXperiment



$R, a_{\max}$	0.8, 0.67 m
Aspect Ratio, $A$	1.27—1.6
Elongation, $\kappa$	1.6—3.0
Triangularity, $\delta$	0.3—0.8
Toroidal Field, $B_t$	0.3—0.55 T
Plasma Current, $I_p$	$\leq 1.5$ MA
Auxiliary Heating:	
NBI (100 kV)	$\leq 7.4$ MW
RF (30 MHz)	$\leq 6$ MW
Central Temperature	1—6 keV
Central Density	$\leq 1.2(10)^{20} \text{ m}^{-3}$

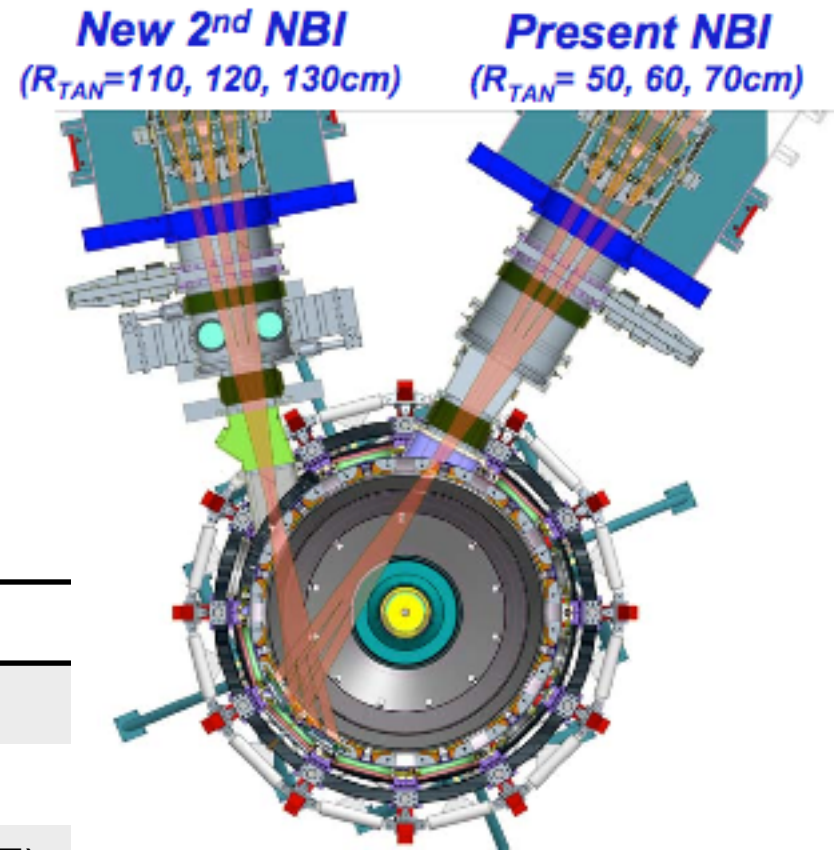
## NSTX utilizes evaporative lithium position on Graphite tiles as the primary plasma facing surface

- NSTX began the FY10 run campaign April 1<sup>st</sup>, 2010
- Lithium is applied between shots via high temperature lithium evaporators (LiTERs) onto graphite PFCs
  - No Boronization (starting with the FY10 run campaign)
  - No glow discharge cleaning (GDC) between shots
  - Deposit between 200 – 800 mg / shot
    - 200 mg is typical
- Addition of a toroidal, liquid lithium divertor (LLD) in FY10



## Upgraded NSTX is expected to be online in FY2014

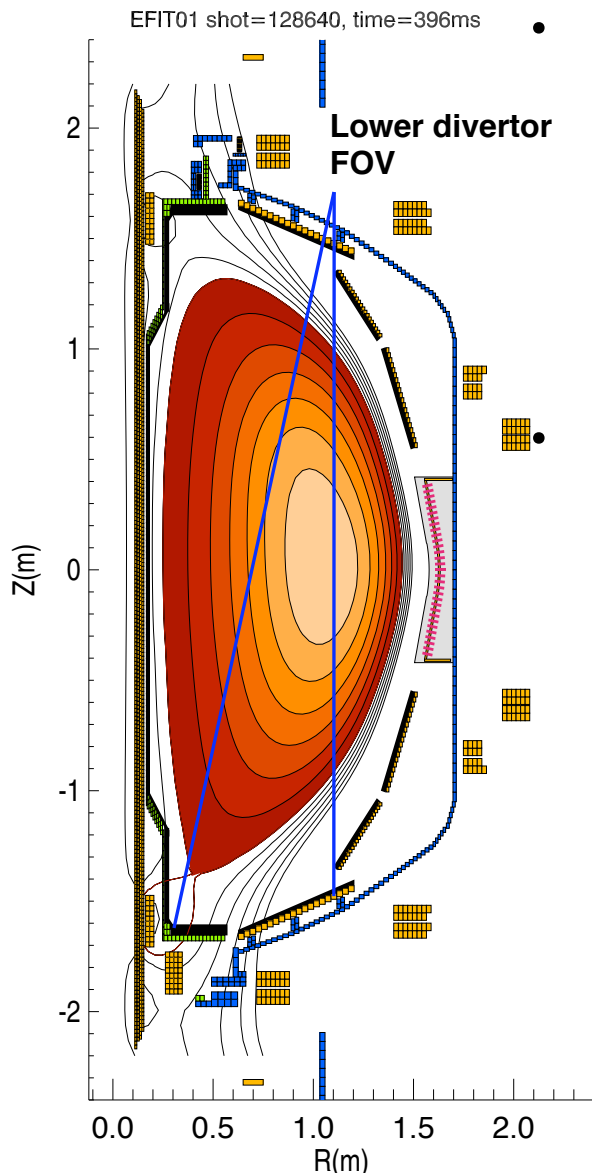
- Doubling of neutral beam heating power to 15 MW
- Will represent a significant increase in expected power deposited onto the divertor
- Techniques to handle the high power densities in NSTX-U are required



### NSTX-U Operating Parameters

Plasma Current, $I_p$	$\leq 2 \text{ MA}$
Toroidal Field, $B_t$	$\leq 1 \text{ T}$
Heating Power, $P_{\text{heat}}$	15 MW (NBI) 5 MW (RF)
Pulse Length	$\leq 5 \text{ s}$
P/R, R/A	20 MW/m, 0.4 MW/m <sup>2</sup>

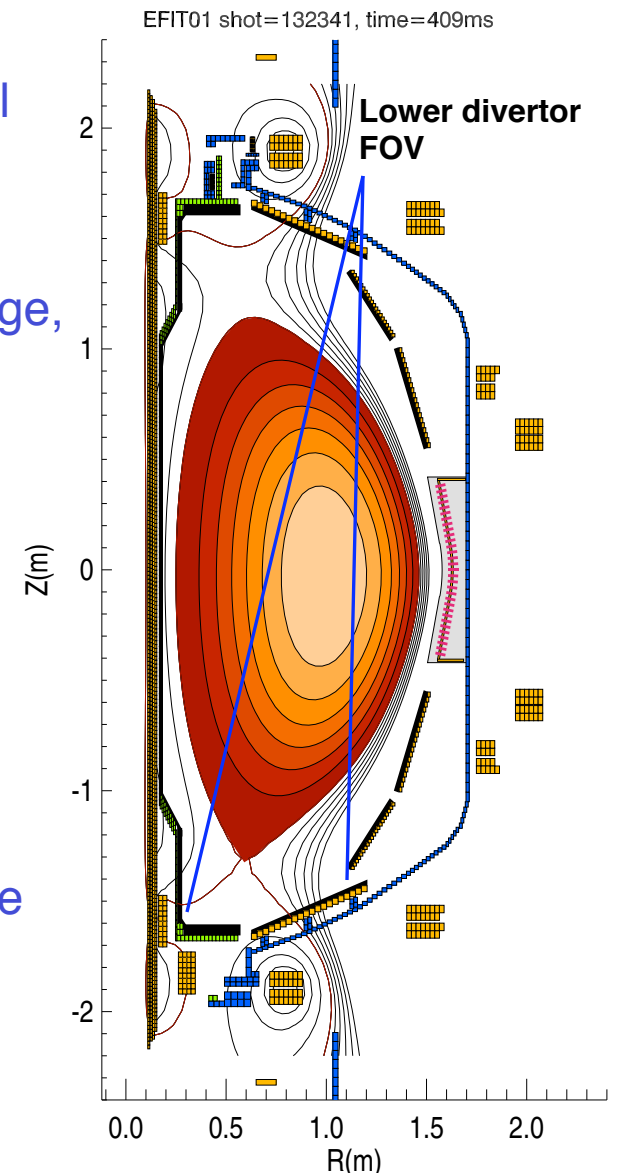
# ORNL IR Cameras currently installed on NSTX



- Two slow (30 Hz) IR cameras
  - Indigo Omega, 160x128 pixel
  - uncooled microbolometer
  - 15° FOV of lower divertor
  - 7-13  $\mu\text{m}$ , 12-bit, 0-700°C range, ZnSe window

## • One fast (1.6-7.0 kHz) IR camera

- Santa Barbara Focal Plane, 128x128 pixel
- LN<sub>2</sub>-cooled
- 15.5° FOV of lower divertor (Bay H)
- 2 color system designed to be less sensitive to emissivity changes
  - MWIR: 4–6  $\mu\text{m}$  and
  - LWIR: 7 – 10  $\mu\text{m}$



## Determine dependence of $\lambda_q^{mid}$ on external parameters from NSTX data

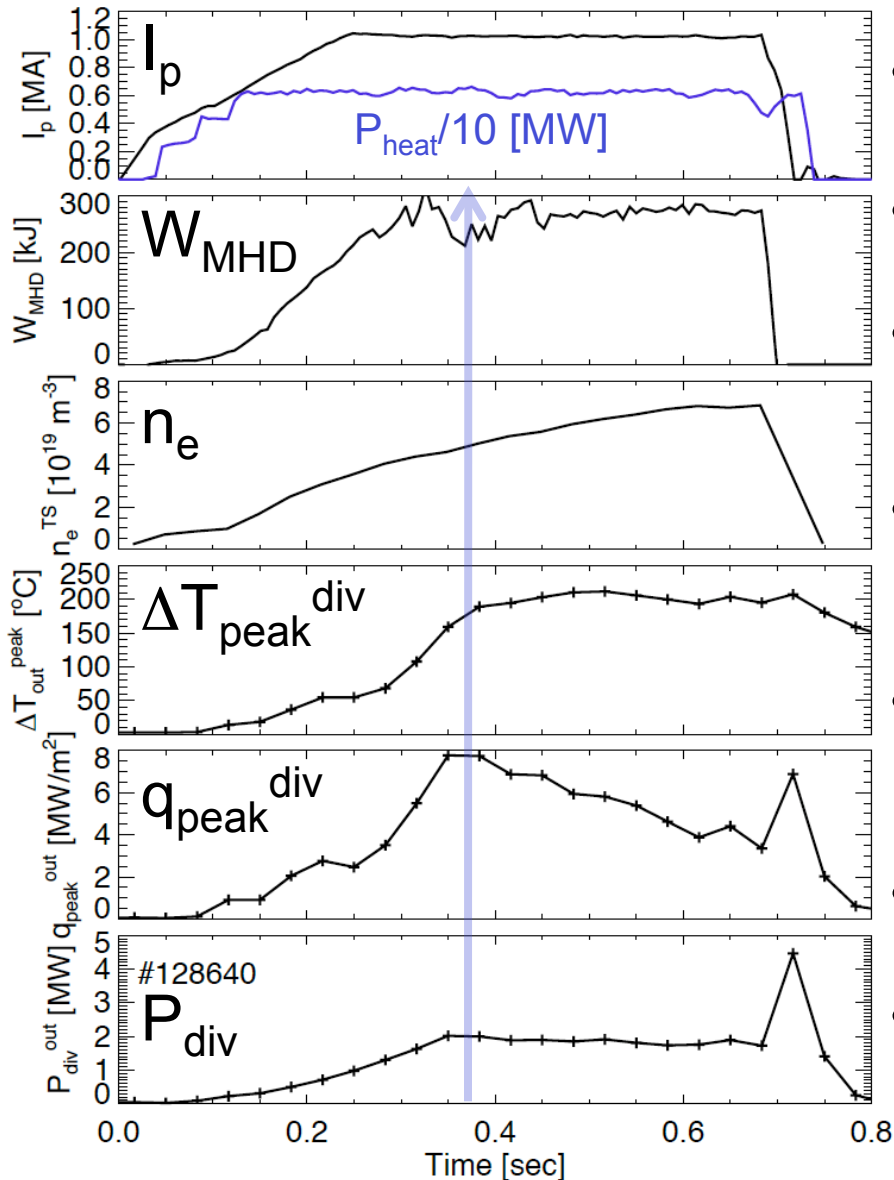
- All data is time averaged over ELMs and before lithium coatings were applied
- IR thermography measures surface temperature, which is used to estimate heat flux profile  $q_{div}^{out}(r,t)$  and calculate divertor power loading: 
$$P_{div}^{out} = \int_{R_{min}}^{R_{max}} 2\pi R_{div}^{out} q_{div}^{out} dr$$

- Define characteristic divertor heat flux scale length,  $\lambda_{q,div}^{out}$  [Loarte 1999]: 
$$\lambda_{q,div}^{out} = P_{div}^{out} / (2\pi R_{div,peak}^{out} q_{div,peak}^{out})$$
- Assume  $\lambda_{q,div}^{out}$  related to characteristic midplane scale length through flux expansion,  $f_{exp}$  such that:

$$\lambda_q^{mid} = \lambda_{q,div}^{out} / f_{exp}, \text{ where } f_{exp} \equiv \frac{R_{mid} B_{\theta}^{mid}}{R_{div} B_{\theta}^{div}}$$

$$\therefore q_{div,peak}^{out} = P_{div}^{out} / (2\pi R_{div,peak}^{out} f_{exp} \lambda_q^{mid}) \text{ with } \lambda_q^{mid} = f(I_p, P_{loss}, B_t, f_{exp})$$

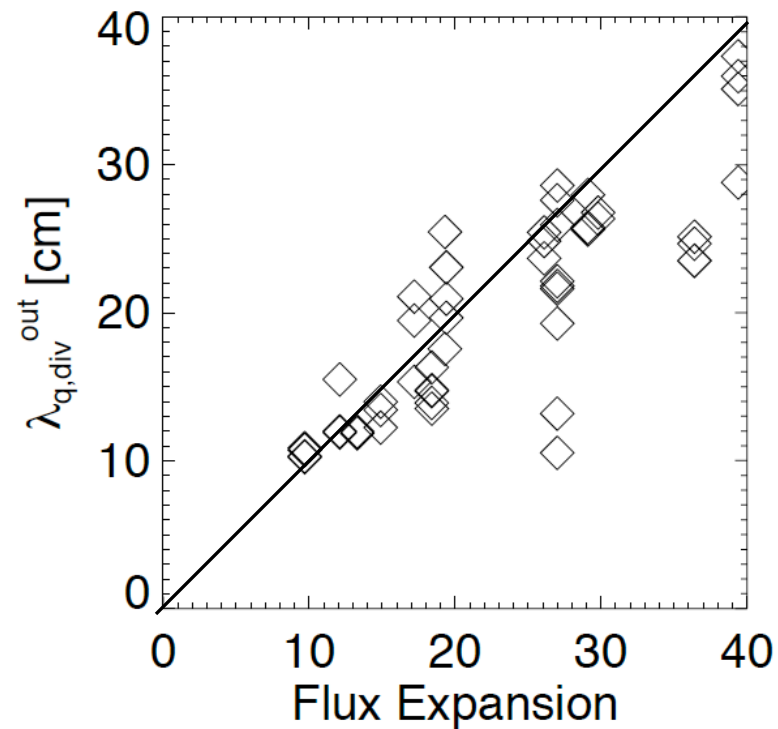
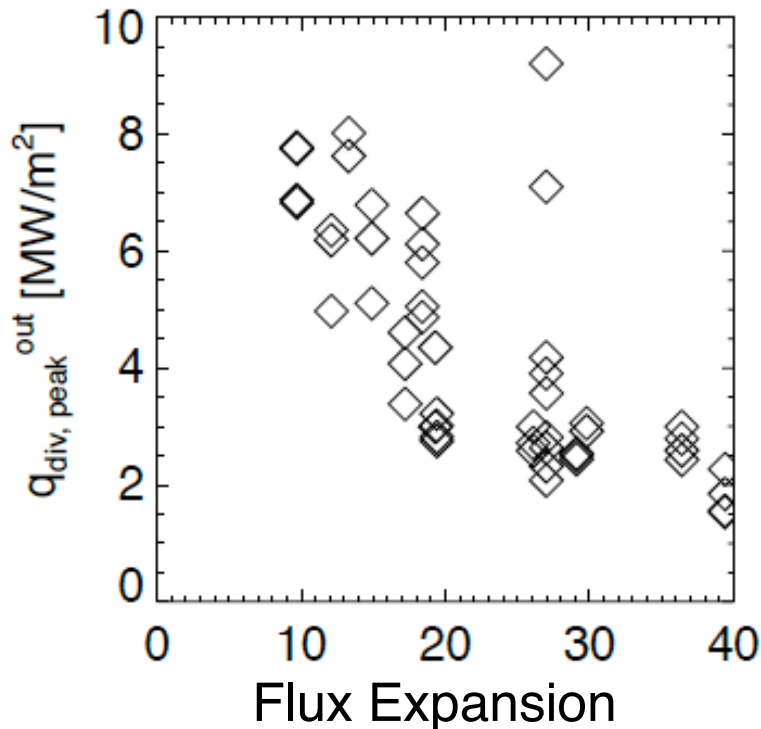
# Divertor peak heat flux evolves during a discharge



- $I_p$  flat-top at 0.25 sec
  - L-H transition at 0.13 sec
- Stored energy usually flat-tops after  $I_p$  flat-top
- Density ramps throughout the discharge (large  $d_r^{\text{sep}}$ , small ELMs)
- Outer divertor heat flux peaks when  $W_{\text{MHD}}$  flat-tops
  - $q_{\text{div}}$  rolls over as density rises
- Total outer divertor power is relatively constant
  - Heat flux profile broadens
- Data is taken over 100–200 ms after  $W_{\text{MHD}}$  flattens
- Should be a conservative projection for NSTX-U

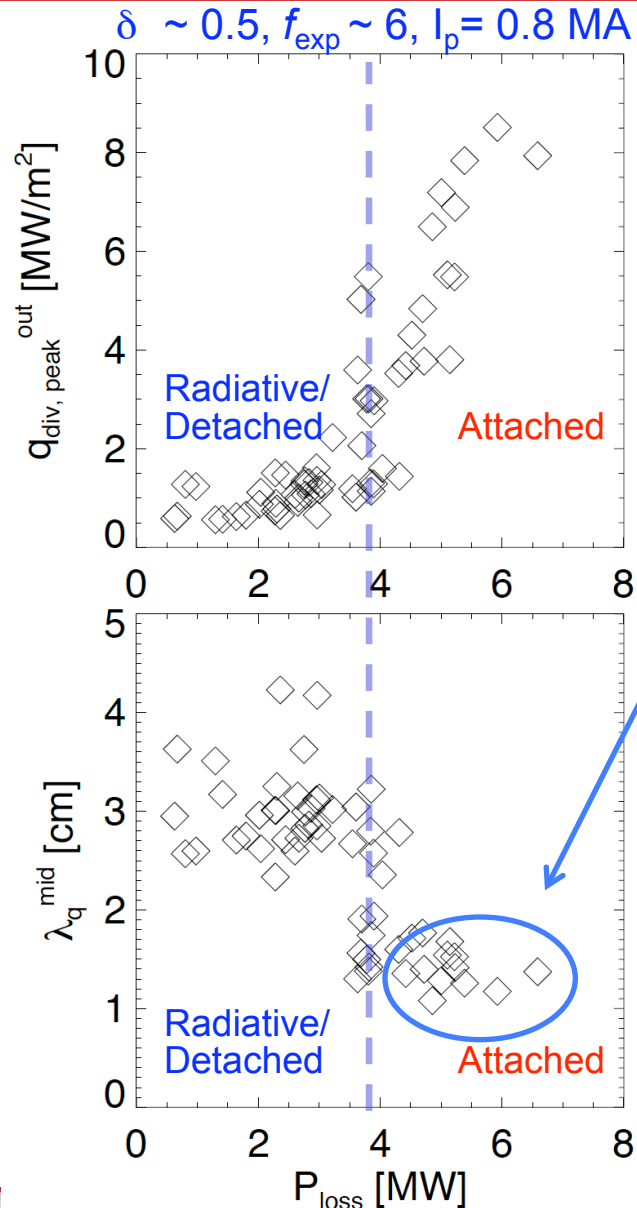


## Peak heat flux decreases inversely with flux expansion with roughly constant $\lambda_q^{mid}$



- $q_{div, peak}$  decreases as flux expansion increases
- $\lambda_q^{div}$  broadens with flux expansion
  - Effectively increasing the plasma wetted area of the divertor
- $\lambda_q^{mid}$  stays approximately constant during the scan
  - Decreases by 20% over a factor 4—5 scan of  $f_{exp}$

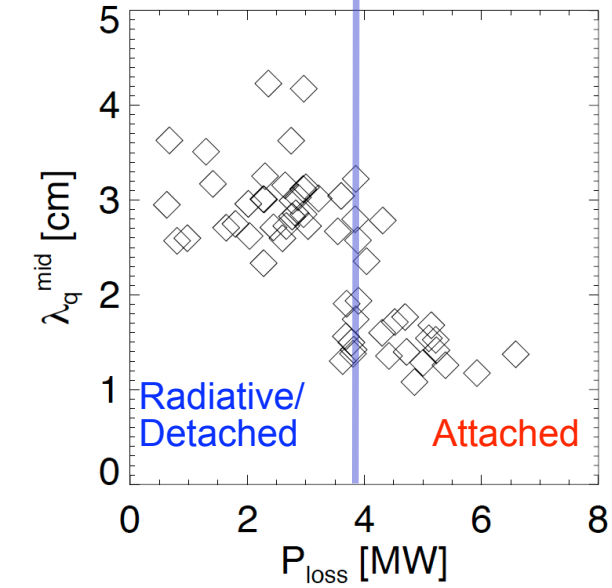
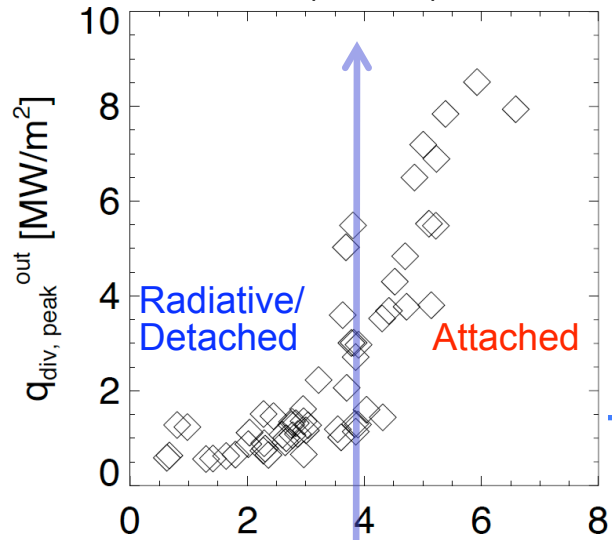
# Heat flux width $\lambda_q^{mid}$ is largely independent of $P_{loss}$ for attached plasmas



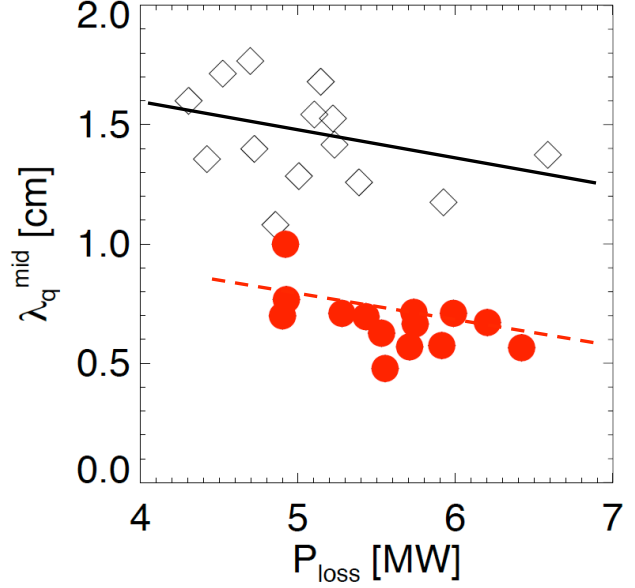
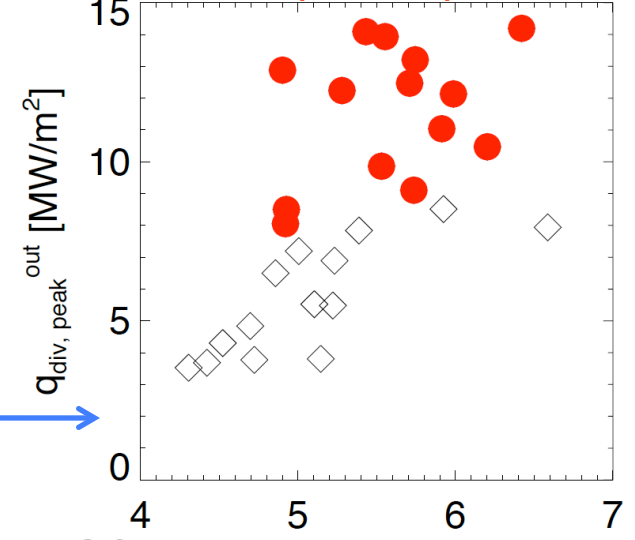
- Peak divertor heat flux increases with  $P_{loss}$
- Apparent change in slope near  $P_{loss} = 4$  MW in these conditions
  - Divertor transitions from a radiative/detached divertor to an attached divertor
  - Similar to previous experiments suggesting a radiative detached divertor at low  $P_{loss}$  [Maingi 2007]
- $\lambda_q^{mid}$  relatively independent of  $P_{loss}$  in high heat flux/attached regime
  - $P_{loss} > 4$  MW

# Heat flux width $\lambda_q^{mid}$ largely independent of $P_{loss}$ in attached plasmas

$\delta \sim 0.5, f_{exp} \sim 6, I_p = 0.8$  MA



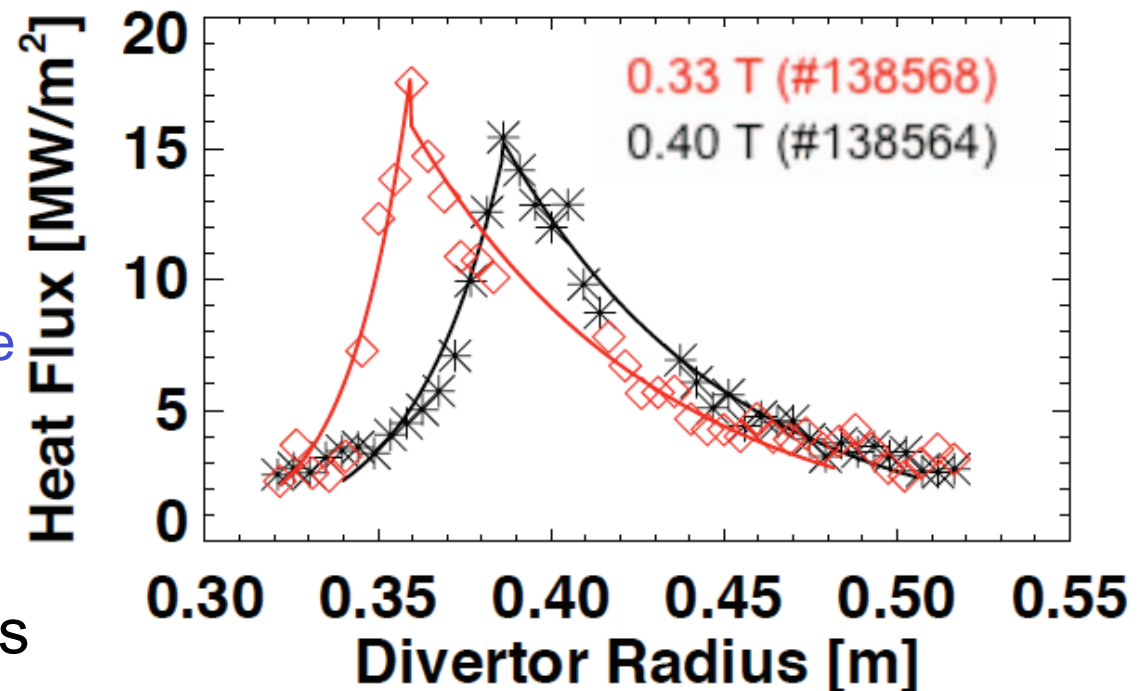
$\delta \sim 0.7, f_{exp} \sim 16, I_p = 1.2$  MA



- Add in **high  $\delta$  data**
- Narrow  $P_{loss}$  plot range
- Apparent  $I_p$  or  $q_{95}$  effect at higher triangularity
- $\lambda_q^{mid}$  is reduced for higher  $\delta$ , higher  $I_p$  discharges

## Changes in $B_t(0)$ don't appear to effect divertor heat flux profiles

- Preliminary measurements from a scan of toroidal magnetic field,  $B_t(0)$  appear to have minimal impact on the heat flux footprint
  - All other parameters were kept constant
  - Limited ranges of  $B_t$  are accessible in NSTX
- Suggestions that  $L_{||}$  does not have a large impact on the divertor profiles



## Heat flux width, $\lambda_q^{\text{mid}}$ contracts with $I_p$

- Combined data from dedicated  $I_p$  scans in low  $\delta$  and **high  $\delta$**  discharges

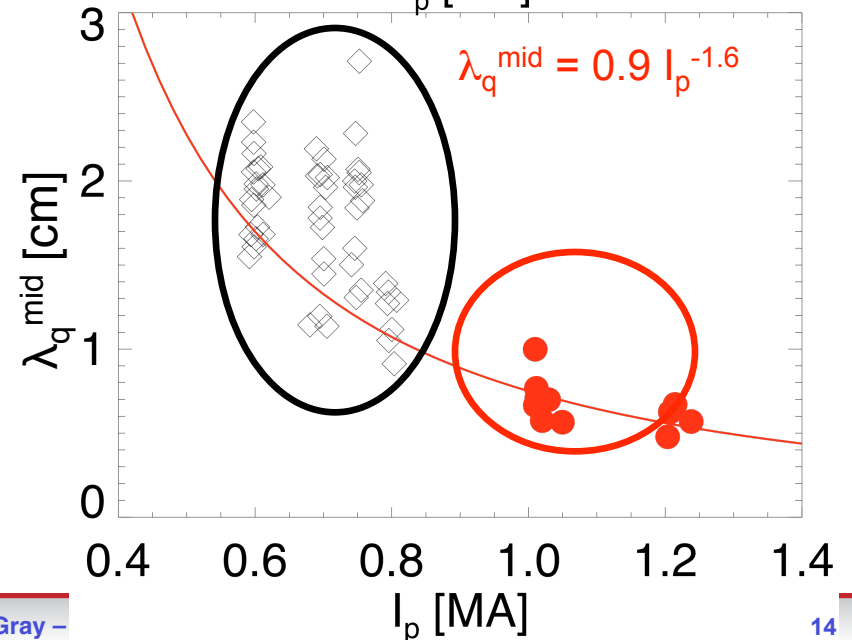
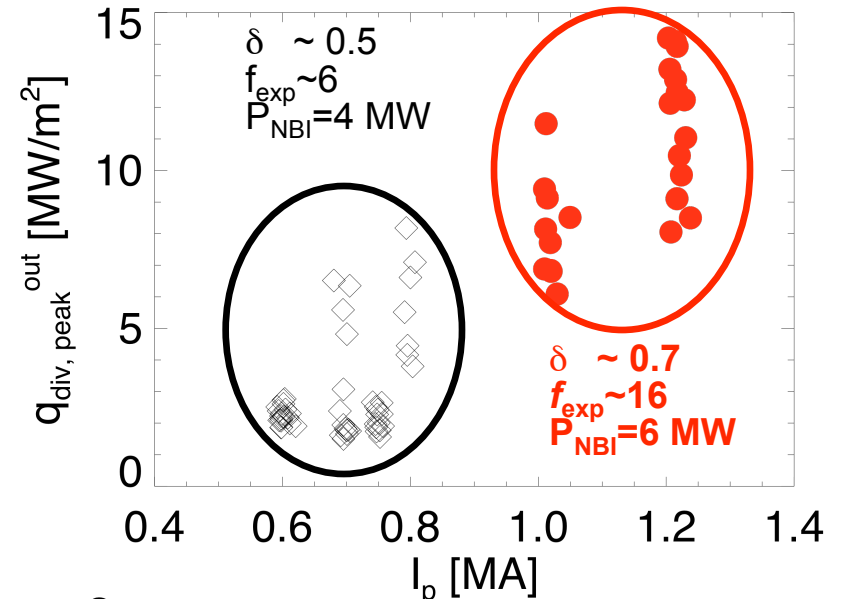
- Different  $P_{\text{NBI}}$  and  $f_{\text{exp}}$ , but previous slides shows no  $P_{\text{loss}}$  or  $f_{\text{exp}}$  effect on  $\lambda_q^{\text{mid}}$
- $I_p$  dependence also in DIII-D, JET
- $q_{95}$ ,  $L_{\parallel}$  re varied (constant  $B_T$ )

- $\lambda_q^{\text{mid}}$  found to scale accordingly:

$$\lambda_q^{\text{mid}} \approx 0.9 I_p^{-1.6}$$

- Suggests that for NSTX-U, with  $I_p = 2$  MA and  $P_{\text{NBI}} = 10$  MW:

$$\lambda_q^{\text{mid}} = 3 \pm 0.5 \text{ mm}$$



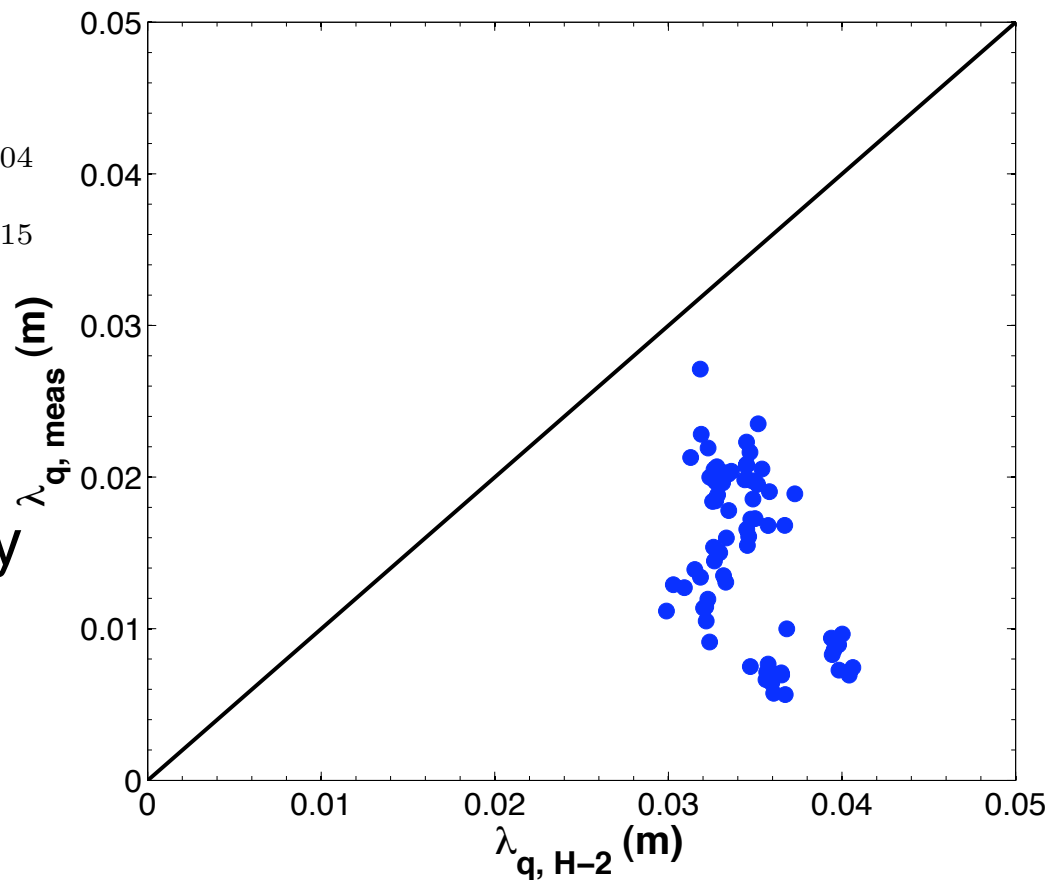
# Previous H-mode scalings over predict the measured $\lambda_q^{\text{mid}}$

- H-2 scaling [Loarte 1999]

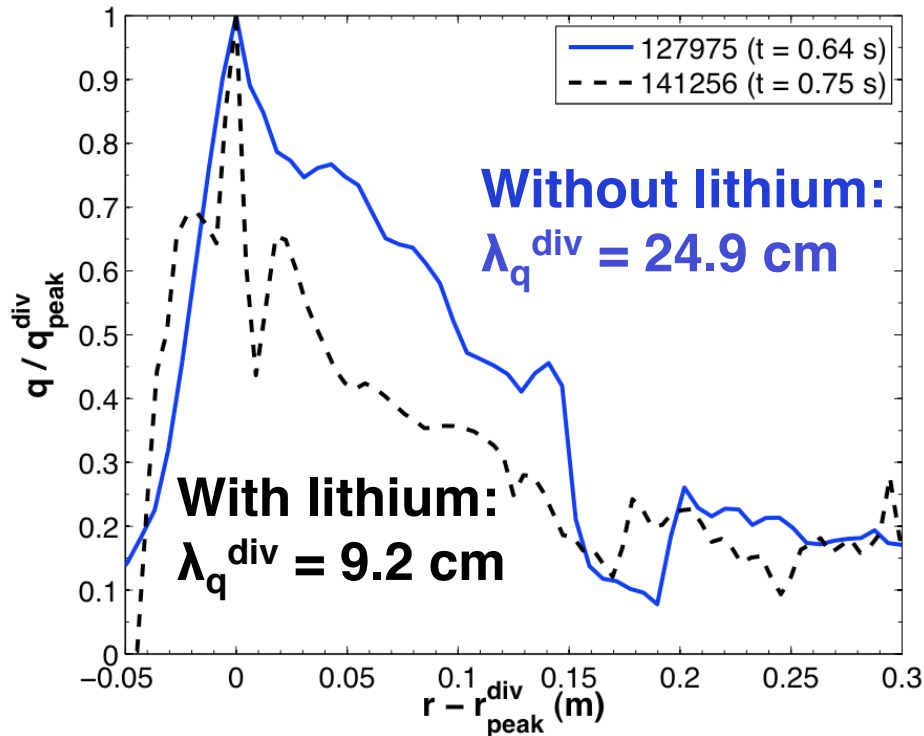
- Used AUG, DIII-D and JT-60U data

$$\lambda_q^{H-2}[\text{m}] = (5.3 \pm 1.4)10^{-3}P_{\text{TOT}}[\text{MW}]^{0.38 \pm 0.04} B[\text{T}]^{-0.71 \pm 0.08} q_{95}^{0.30 \pm 0.15}$$

- Over predicts the magnitude of  $\lambda_q^{\text{mid}}$
- Under predicts the severity of the contraction with  $I_p$ 
  - $\lambda_q^{H-2} \sim I_p^{-1}$
- Possibly due to the different aspect ratio



# Resultant divertor heat flux profile is narrowed with use of lithium coatings



## Under similar discharge conditions:

- $\lambda_{q,\text{non-lithium}} \sim 2 \lambda_{q,\text{lithium}}$
- High  $\delta$ , 1 MA, 4 MW NBI,  $f_{\text{exp}} \sim 18$
- Appears consistent across  $I_p$  and  $P_{\text{NBI}}$  scans

- For the discharge with lithium, the fast, 2 color IR camera is used
  - Frames are averaged together to yield a similar integration time as the slow, single color IR camera
- Narrowing of the heat flux profile appears with 2 color IRTV camera
  - Confirms earlier trends with single color, IRTV system [Gray 2010]
  - Not simply an effect of changing surface emissivity
  - Believed due to the elimination of small type V ELMs

## Experiments on NSTX have successfully mapped out the behavior of the divertor heat flux with many engineering parameters

- By magnetically mapping the divertor heat flux profile,  $\lambda_q^{\text{div}}$  to the midplane, it's dependencies on heating power and flux expansion are eliminated
  - Yielding only  $\lambda_q^{\text{mid}} \approx f(I_p)$
- $\lambda_q^{\text{mid}}$  contracts strongly with increasing plasma current
  - This has been observed on DIII-D and JET as well
- Magnetic flux expansion appears to be a viable method to spread the heat flux out on the divertor
- Implications for NSTX-U at full design capabilities of  $I_p = 2$  MA and  $P_{\text{heat}} = 10$  MW are:
  - $q_{\text{div, peak}} = 24$  MW/m<sup>2</sup>,  $\lambda_q^{\text{mid}} \sim 3$  mm with  $f_{\text{exp}} = 30$
  - Operations with a large magnetic flux expansion will be necessary to mitigate the expected large heat fluxes
  - Or operating with a detached divertor via divertor gas puffing will be necessary
- The full effect of thin lithium coatings is still being explored, but initial results show a further contraction of  $\lambda_q^{\text{div}}$  that is not yet understood



## Future experiments and data analysis

- Measured  $I_p$ ,  $P_{\text{heat}}$ ,  $\delta_r^{\text{sep}}$ ,  $n_e$ ,  $B_t$  dependences on heat flux profile with lithium using the new 2 color IR Camera
  - More reliable estimate of heat flux with lithium thin films due to the low emissivity of lithium
  - Determine how  $\lambda_q^{\text{mid}}$  scales with  $I_p$  in lithiated discharges
- Further development of snowflake divertor and magnetic flux expansion to mitigate heat flux
  - see Poster EXD/3-32: V. Soukhanovskii, "Snowflake divertor configuration in NSTX" for more information
- Effect of 3D magnetic fields on the heat flux profile
  - See Poster EXD/P3-01: J-W Ahn, "Effect of non-axisymmetric magnetic perturbations on divertor heat and particle flux profiles"
- Assess replacing lower inboard divertor C tiles with Mo
  - Mo offers improved chemical compatibility with evaporative lithium coatings
  - Metal walls are more relevant to fusion reactor scenarios

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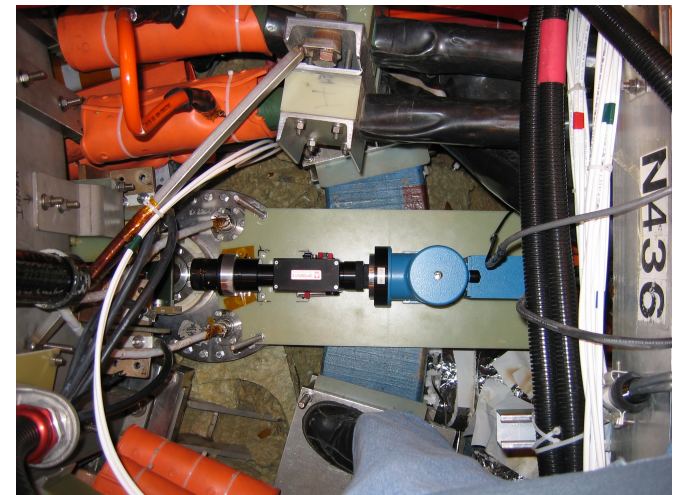
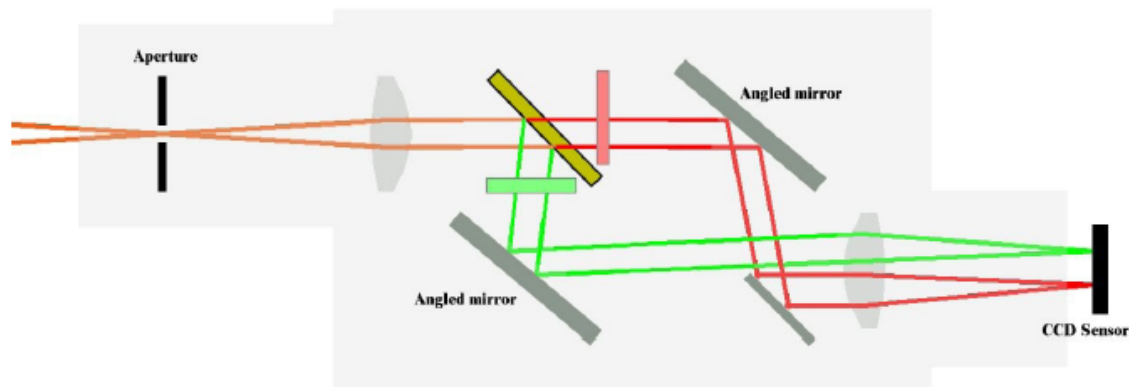
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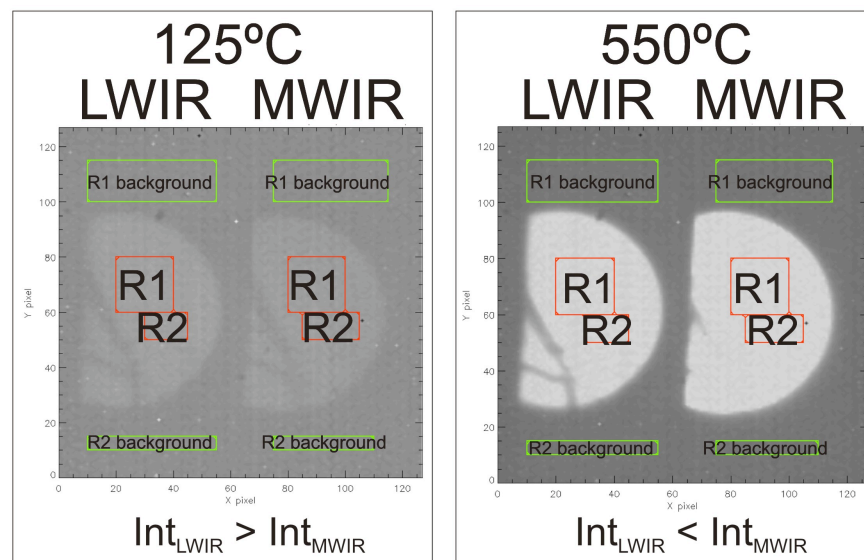
# A two-color infrared imaging adaptor for the fast IR camera on NSTX [6]

- Use of the LLD in NSTX will make assumptions of high surface emissivity (applicable to graphite) inaccurate
  - Complications include: Surface coating changes in real time during plasma shots, emissivity changes due to H-absorption in Li, reflections from Li surface, deposition of Li on C surfaces, erosion/transport of Li and C
- Two-color camera measures temperature based on the ratio of integrated IR emission in two IR bands, not single band intensity
- Image split into medium wavelength IR (4-6  $\mu\text{m}$ ) and long-wavelength IR (7-10  $\mu\text{m}$ ) using a dichroic beamsplitter, filtered with bandpass filters, projected side-by-side into the NSTX fast IR camera (1.6 kHz full frame)



# Calibration and physics application of two-color IR

- Calibration accomplished *ex-situ* using a 0-750°C blackbody source
  - Useful, low error LWIR/MWIR ratio from ~100-600°C
- Additional *in-situ* calibration during heating of LLD plates from 0-320°C
  - Shows extended useful range due to losses in MWIR channel
- True radial view of NSTX lower floor
  - View of inner divertor (graphite), CHI gap, and LLD plates



SBFP 2-color intensity ratio calibration, blackbody source, 22  $\mu$ s integration time

