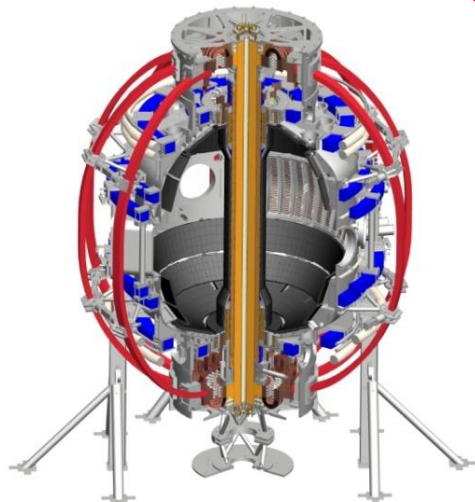


# 5 Year Review Panel Questions – Day 1

*Coll of Wm & Mary*  
*Columbia U*  
*CompX*  
*General Atomics*  
*FIU*  
*INL*  
*Johns Hopkins U*  
*LANL*  
*LLNL*  
*Lodestar*  
*MIT*  
*Lehigh U*  
*Nova Photonics*  
*ORNL*  
*PPPL*  
*Princeton U*  
*Purdue U*  
*SNL*  
*Think Tank, Inc.*  
*UC Davis*  
*UC Irvine*  
*UCLA*  
*UCSD*  
*U Colorado*  
*U Illinois*  
*U Maryland*  
*U Rochester*  
*U Tennessee*  
*U Tulsa*  
*U Washington*  
*U Wisconsin*  
*X Science LLC*

## NSTX-U Team

**NSTX-U 5 Year Plan Review**  
**LSB B318, PPPL**  
**May 21-23, 2013**



*Culham Sci Ctr*  
*York U*  
*Chubu U*  
*Fukui U*  
*Hiroshima U*  
*Hyogo U*  
*Kyoto U*  
*Kyushu U*  
*Kyushu Tokai U*  
*NIFS*  
*Niigata U*  
*U Tokyo*  
*JAEA*  
*Inst for Nucl Res, Kiev*  
*Ioffe Inst*  
*TRINITY*  
*Chonbuk Natl U*  
*NFRI*  
*KAIST*  
*POSTECH*  
*Seoul Natl U*  
*ASIPP*  
*CIEMAT*  
*FOM Inst DIFFER*  
*ENEA, Frascati*  
*CEA, Cadarache*  
*IPP, Jülich*  
*IPP, Garching*  
*ASCR, Czech Rep*

# Questions from Panel – 1-4 of 7

1. Compare and contrast the MAST and NSTX-U capabilities and plans
  - What are the complementary research objectives?
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  - What are possibilities for confirmatory experiments?

➤ Addressed by J. Menard
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  - How do things fit together to inform FNSF after the end of 5-year plan?

➤ R. Raman covered first question in his presentation

➤ Informing FNSF: Addressed by J. Menard
3. What are your priorities that are for the upgrades included in the base program? Addressed by J. Menard
4. Please provide the FTEs for scientific staff, including collaborators
  - Addressed by M. Ono

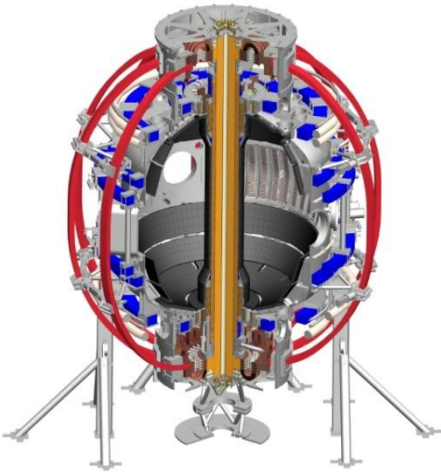
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  - NBI cryo – Addressed by: R. Raman / S. Gerhardt

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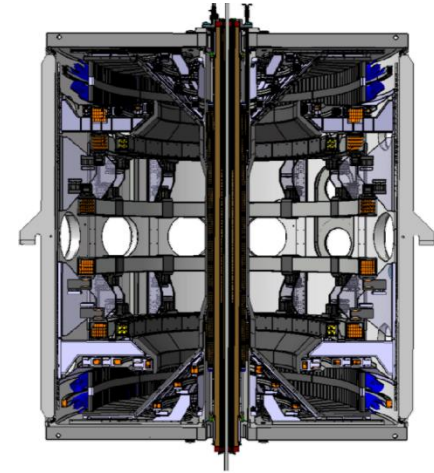
# NSTX-U and MAST-U share common mission elements with complementary physics capabilities



## NSTX-U

### Mission elements:

- Establish knowledge-base for an ST-based FNSF
- Extend physics understanding of tokamak, ITER
- Develop innovative PMI solutions for next-steps



## MAST-U

- High  $\beta$  up to ideal-wall limit at low  $v^*$
- BES, high-k, polarimetry for e & i-transport
- HHFW electron heating and CD
- High  $f_{BS}$  + co-NBI for high  $f_{NI}$
- CHI/plasma gun, ECH, HHFW, NBI ramp-up
- LiTER+paced ELMs for ion control (until cryo)
- Snowflake, detachment, Li vapor shielding
- J(r) control via large  $R_{tan}$  co-NBI
- Long-term: transition to high-Z + flowing LM

- MHD studies near no-wall limit at low  $v^*$
- BES, high-res Thomson for NTM, boundary
- EBW electron heating and CD
- High co-NBI CD fraction + BS for high  $f_{NI}$
- Merging-compression, EBW for ramp-up
- Divertor cryo-panels for D pumping
- Long line-length Super-X divertor, detachment
- Vertically-shifted off-axis co-NBI
- Graphite PFCs

# NSTX-U and MAST-U devices have similar current and field capability goals, but target complementary scenarios

## NSTX → NSTX-U

- $I_p$  = 1MA (1.4MA max) → 2MA
- $B_T$  = 0.55 → 1T
- $\tau_{\text{pulse}}$  = 1s → 5s
- $P_{\text{NBI}}$  = 5, 7.5MW → 10,15MW (5s,1.5s)

## MAST → MAST-U

- $I_p$  = 1MA (1.2MA max) → 2MA
- $B_T$  = 0.55 → 0.84T
- $\tau_{\text{pulse}}$  = 1s → 4s
- $P_{\text{NBI}}$  = 5MW → 7.5MW (4s) (Phase 1)

**NSTX-U will have leading PMI capability: ITER-level P/R, P/S up to 24MW/m, 0.5MW/m<sup>2</sup> from 15+6=21MW NBI+FW vs. MAST-U 7.5MW**

## Passive structure + MHD control differences motivate complementary scenarios:

- **Conformal close-fitting Cu plates**
- Mid-plane coils for RMP and **active RWM/EF control** (unless/until NCC)

- **Far conducting wall**
- Mid + off-mid-plane EF/RMP coils (MAST-U may not have off-midplane coils – TBD)

### • Impact on elongation and beta

- NSTX-U: w/ wall-stabilization →  $\kappa = 2.5-3$ ,  $\beta_N = 4.5-6$  →  $f_{\text{BS}} = 60-80\%$  → access lower  $I_i$  → higher  $\kappa$
- MAST-U: w/o wall stabilization →  $\kappa = 2-2.5$ ,  $\beta_N = 3-4.5$  →  $f_{\text{BS}} = 30-50\%$

### • 100% non-inductive sustainment

- NSTX-U: Moderate-to-high  $f_{\text{GW}} = 0.4-1.0$  → 20-40% NBI-CD → J(r) controllability challenging?
- MAST-U: Low to moderate  $f_{\text{GW}} = 0.25-0.5$  → 50-75% NBI-CD → AE, low-n kink stability problematic?

# NSTX-U researchers will be playing active role in MAST 2013 run campaign

Number	Title	Person in charge
FPP-001	Time-resolved measurements of DD fusion products using proton detector & neutron camera/fission chamber during short timescale MHD activity & NBI blips	D. Darrow M. Cecconello
FPP-006	Identification & study of TAE avalanches	E. Fredrickson
MHD-011	Effect of $I_p$ and $\beta_p$ on pedestal	A. Diallo
TC-014	Measure perturbative particle transport in MAST	Y. Ren
TC-011	Momentum transport	W. Guttenfelder

- Thanks to MAST team for strong outreach/accomodation to NSTX team
- Gary Taylor assisting coordination of NSTX collaboration on MAST
- Experiments to start very soon - will benefit MAST/MAST-U and NSTX-U

**NSTX-U will accommodate MAST researchers during MAST-U outage**



# Expected joint research, confirmatory experiments

Nucl. Fusion 51 (2011) 073045

MAST

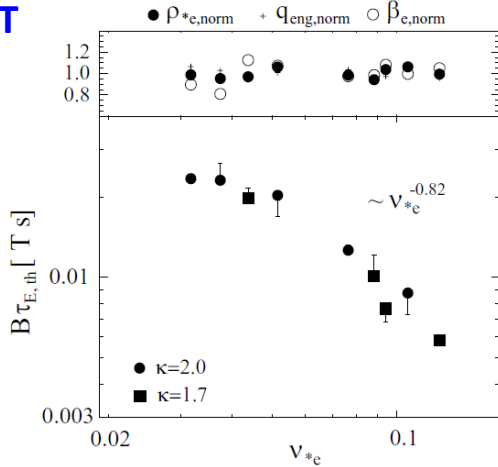
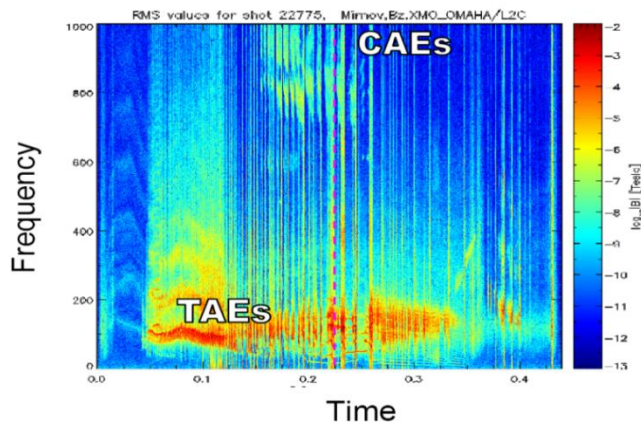


Figure 3. Collisionality scan of thermal energy confinement time. Vertical bars show the size of the correction due to variations in  $\rho_{*e}$ , assuming gyro-Bohm scaling,  $\nu_{*e} \propto \bar{n}_e(T_e)^{-2}R$ .

- Underlying physics of collisionality scaling of thermal confinement

- NSTX + MAST observation of  $1/\nu$  scaling of confinement confirmed scaling as ST trend rather than device-specific trend
- Confinement scaling critical issue for projecting to next-step STs – data from both devices will be essential

MAST



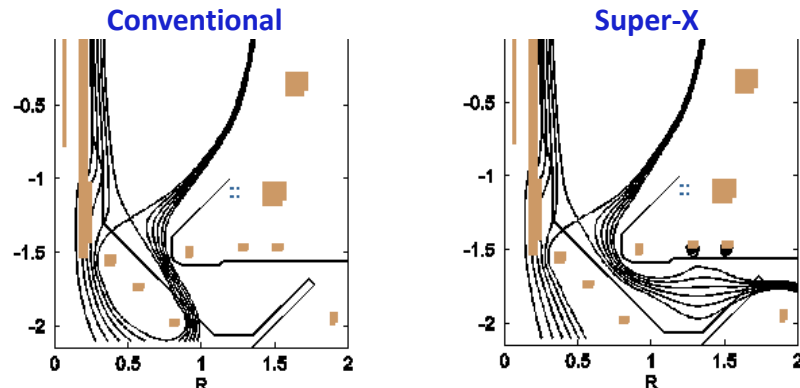
- Physics & impact of fast-ion instabilities

- Chirping/bursting TAE/EPM modes
- EP-induced modes
- Exploitation of active MHD spectroscopy (AE antenna) in ST geometry
- Fast-ion transport from \*AE critical issue for NBI-CD in NSTX-U, MAST-U, FNSF

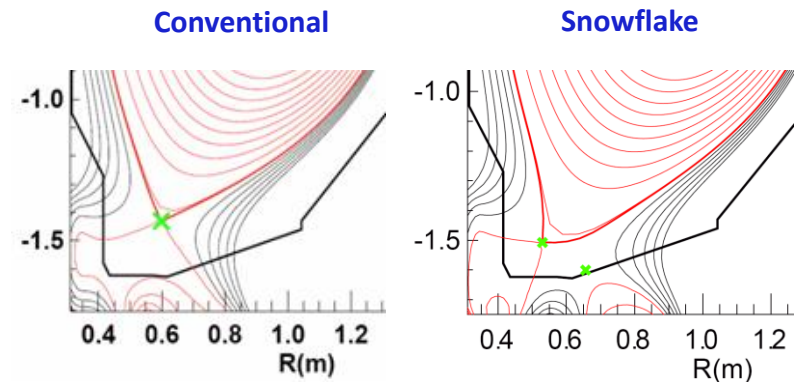


# Expect substantial joint research on advanced divertors

## MAST Upgrade



## NSTX Upgrade



- **MAST-U: Super-X + cryos**
- **NSTX-U: snowflake + lithium**
- Both will access high flux expansion, variation of line-length, pumping
- Complementary: open vs. closed divertor, different pumping techniques
- Both will require advanced boundary control
  - **Example: control of multiple X-points/flux expansion**
- Divertor requirements and optimization are critical issues for FNSF

Joint super-X and snowflake research on MAST-U, NSTX-U, DIII-D, TCV recently proposed by H. Wilson (University of York + many others) – unfortunately this proposal was not funded by UK EPSRC

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# Aim to demonstrate and understand integrated non-inductive start-up and ramp-up for ST-FNSF near end of 5 year plan

	2015	2016	2017	2018	2019
Maximum $B_T$ [T] and $I_p$ [MA]	0.8, 1.6	1, 2			
Structural force and coil heating limit fractions	0.5, 0.5	1.0, 0.75	1.0, 1.0		
Nominal $\tau_{\text{pulse}}$ [s]	1 – 2	2 – 4	4 – 5		
Sustained $\beta_N$	3 – 5	4 – 6	NCC	5 – 6	
$v^* / v^*$ (NSTX)	0.6	0.4	Cryo	0.3 – 0.2	0.2 – 0.1
Non-inductive fraction ( $\Delta t \geq \tau_{\text{CR}}$ )	70 – 90%	80 – 110%		90 – 120%	100 – 140%
CHI closed-flux current [MA]	0.15 – 0.2	0.2 – 0.3		0.3 – 0.5	0.4 – 0.6
HHFW +BS non-inductive $I_p$ [MA]	0.15– 0.25	0.2 – 0.3	ECH	0.3 – 0.4	0.3 – 0.5
NBI+BS $I_p$ ramp-up: initial $\rightarrow$ final [MA]		0.6 $\rightarrow$ 0.8	0.5 $\rightarrow$ 0.9	0.4 $\rightarrow$ 1.0	

Ability to integrate will be highly dependent on physics, resources, run-time

Integrated non-inductive start-up, ramp-up, and sustainment

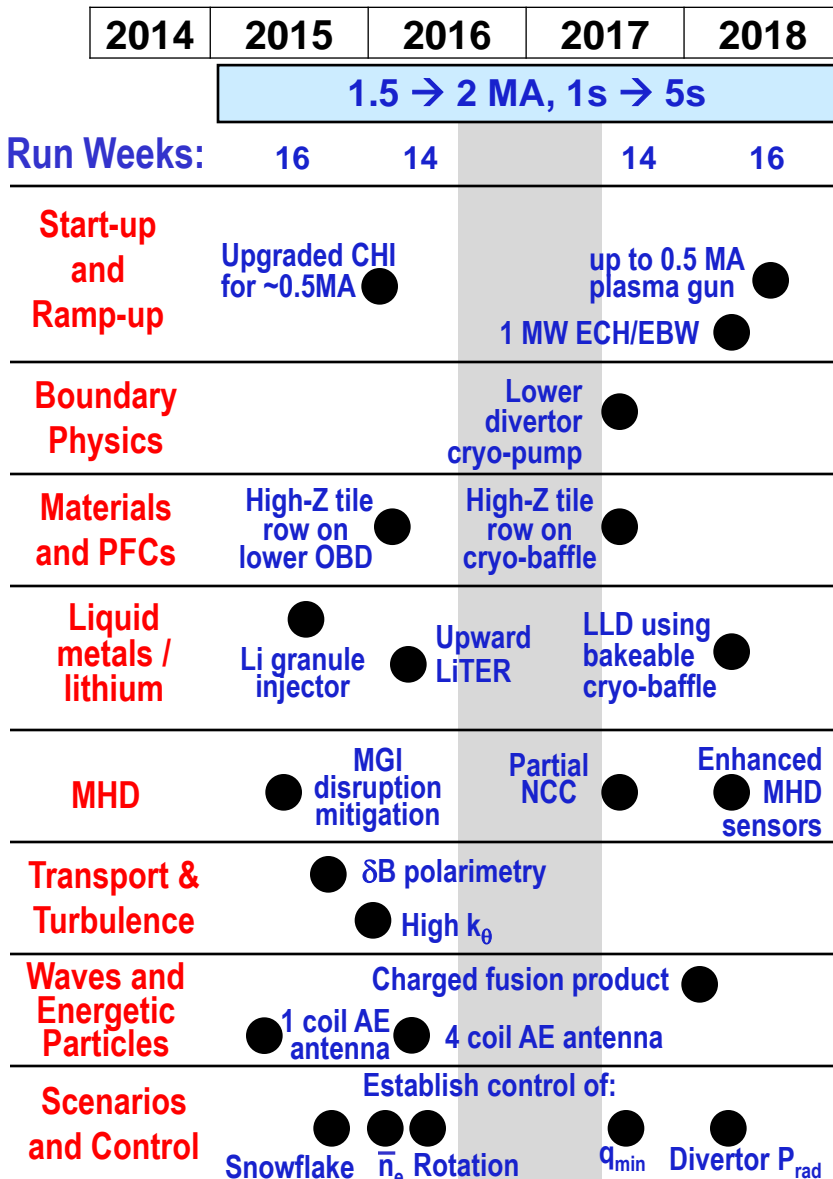
- Model, interpret, understand in NSTX-U with TSC, TRANSP, NIMROD, NOVA-K, AORSA, GENRAY, ...
- Extend models to FNSF  $\rightarrow$  assess implications for FNSF design: coils, NBI, ECH/EBW, FW, ...

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# Prioritization of 5 year plan tools with 5YP base funding

## Ranked according to programmatic impact, cross-TSG linkages, cost



- Plasma control development
  - Highly cross-cutting, modest cost
- Density control, access to low  $v^*$  and  $Z_{eff}$  cross-cutting for all 5YP goals
  - Modest cost: upward LiTER, LGI
  - Higher cost: divertor cryo-pump
- Turbulence diagnostics (high-k,  $\delta B$ ) critical for understanding transport at low  $v$ , high  $b$ 
  - Modest cost, collaborator supported
- Start-up/ramp-up critical ST issue
  - Upgraded CHI: high impact, modest cost
- \*AE important for sustainment, ramp-up
  - AE antenna, charged FPD: low/modest cost
- MHD tools vital for high  $\beta$ , FNSF control
  - MHD sensors, MGI/EPI - modest cost
  - NCC: cross-cutting, but higher cost
- FNSF start-up: bridging  $T_e$  gap important
  - ECH: higher cost, a bit less cross-cutting
  - Plasma guns: moderate cost, technically ready?
- Begin high-Z studies, cryo-baffle LLD
  - Longer-term goal, modest/moderate cost

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# NSTX-U Research Manpower Summary

(#s are based on the recent count)

## PPPL Science / Operations FTEs

	NSTX	NSTX-U Construction		NSTX-U	
	FY 2010	FY2014		FY 2015-2018	
	Actual	Base	Incrementals	Base	Incrementals
Run Weeks	15	0	0	14 - 16	16 - 20
Science	36.2	31.3	31.3	36.8	39.3
Operations	71.1	42.3	42.3	72.2	74.2
Total FTEs	107.3	73.6	73.6	109	113.5

- NSTX-U research and operations staffing level is similar to that of NSTX. Incremental funding will enable research staff enhancement to support increased research output.
- Collaborating FTE#s are not accurately known since the grant is managed directly by OFES. We estimate that 16.6 FTE non-lab collaborators and 5.4 lab collaborators are directly supported by the NSTX-U collaboration grant.
- There are other sources of funding for our collaborating researchers including advanced diagnostic initiative and theory related funding.
- International collaborators are generally funded by home institutions.
- 17 NSTX-U collaborating researchers are presently residing at PPPL.
- In addition, there are 33 students presently associated with NSTX-U research program.

# Questions from Panel – 5-7 of 7

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# NSTX Rep. Rates and NSTX-U TF Limitations

- NSTX Rep. Rates:
  - W/ boronization and He glow, 15-20 minutes was standard for high performance plasmas.
  - W/ Lithium conditioning, 10 minutes was possible (though borderline too fast: ~4 minutes for data to arrive + 2 minutes to set up shot left only 4 minutes for thinking.)
- NSTX-U: TF  $I^2t$  increased a factor of 20, OH increased a factor of 3.5.
- Basic spec. for NSTX-U is a  $\tau_p=2400$  s rep rate at full field and current, upgradable to  $\tau_p=1200$  s.
  - Key point: CS systems themselves are qualified at  $\tau_p=1200$  s @ full performance
- Key Constraint: TF bus work is presently sized for  $\tau_p=2400$  s, with an equivalent square wave of  $\tau_{ESW}=7$  seconds @  $I_{TF}=130$  kA, ( $I_{RMS}=7$  kA).
  - Year 1 max:  $\tau_{ESW}=4.5$  s @  $I_{TF}=100$  kA, then rep. rate is 15 minutes.
  - Year 2 max:  $\tau_{ESW}=5.5$  s @  $I_{TF}=125$  kA, then rep. rate is 30 minutes.
  - Year 3 max:  $\tau_{ESW}=7.0$  s @  $I_{TF}=125$  kA, then rep. rate is ~ 38 minutes.
- 1200 s upgrade for the TF involves increasing the cable runs between the rectifiers and the TF coils, increasing the RMS current to 10 kA:
  - Year 3 max:  $\tau_{ESW}=7.0$  s @  $I_{TF}=125$  kA, then rep. rate is 16 minutes.

# Other Coils Will Not Be Near As Limiting

Solenoid and Vertical Field Coil Already Designed for 1200 s at full capability (24 kA on VF coil).

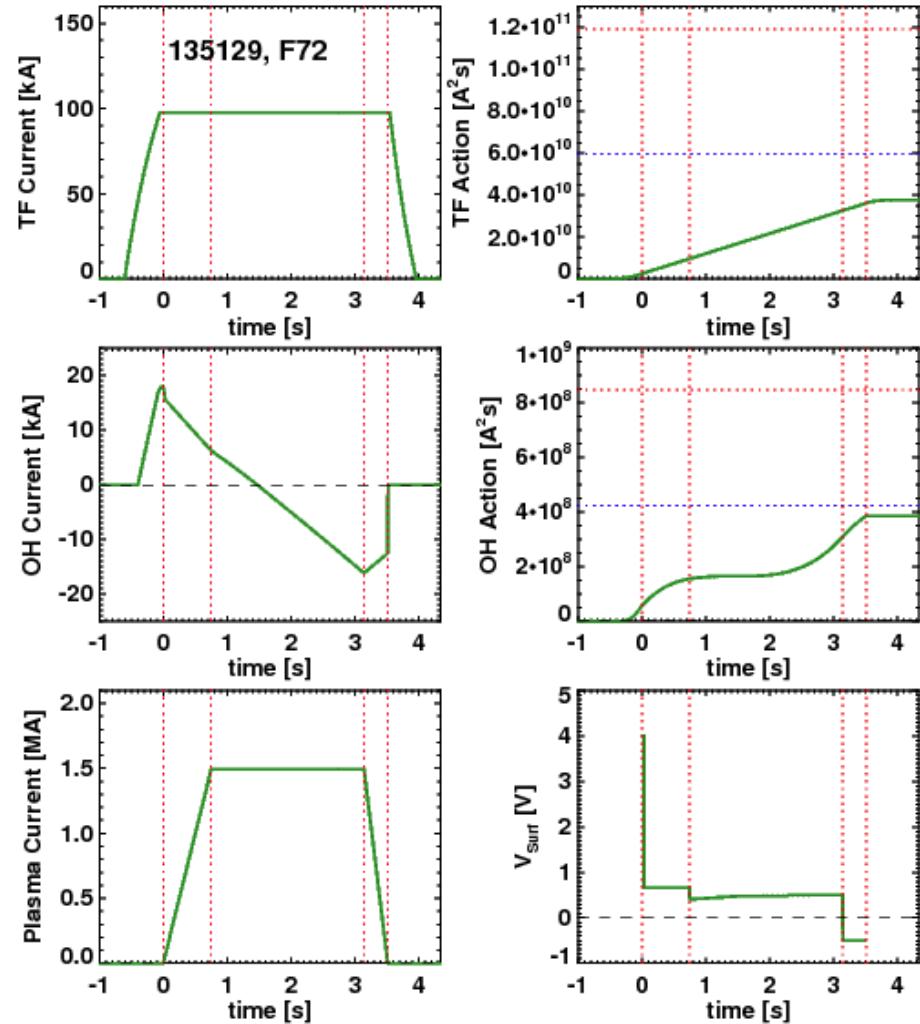
Example Year 1 Scenario at 1.5 MA and 0.75 T

- Use OH pre-charge that causes the OH coils to maximize the time near zero.

- Proper pre-charge will be a function of the target plasma current and non-inductive level.
- In general, OH heating likely to provide pulse duration constraint in year 1 of NSTX-U (limiting heating to  $\frac{1}{2}$  the design point).

- For year 1 example with 19 kA pre-charge with  $I_{RMS}=0.9$  kA (1200 sec configuration), OH rep rate is 9 minutes.

- TF cools in 15 minutes for this case.
- Even most aggressive year 1 scenarios will not have cycle times longer than NSTX standards.



# Anticipated Pulse Spectrum of NSTX-U Limits the Number of Full Field Long Pulse

- For engineering design purposes, a distribution of pulses was assumed in the General Requirements Document.
  - Based on the distribution of NSTX discharges
  - 20000 pulses = 10 years x 16 weeks x 5 days x 25 shots
    - This implies a 20 minute rep rate for an 8.5 hour day.
- Limited number of 1 T, 5 second discharges anticipated.
  - Majority of research program anticipated to be ~0.75 T -> 23 minute rep rate for 7.0 second TF flat-tops.
  - Limitation to 500-1000 shots **very** conservative with regard important fatigue limits.
- Other mitigating effects:
  - New PCS code that automates the TF rampdown after a disruption eliminates wasted TF heating/lifetime.
  - Will monitor the TF RMS current to stay near, but beneath, the limits.

Table 2-4 - NSTX CSU Pulse Spectrum

Performance	60%	75%	90%	100%	
$B_t$	0.6	0.75	0.9	1	T
$I_p$	1.2	1.5	1.8	2	MA
$T_{pulse} = T_{flat} - I_p$ (sec)					Total pulses
3	200	1800	1200	1000	4200
3.5	200	1800	1200	1000	4200
4	200	1800	1200	1000	4200
4.5	200	1800	1200	500	3700
5	200	1800	1200	500	3700
					Total
					20000

~18 min w/o upgrade

~26 min. w/o upgrade

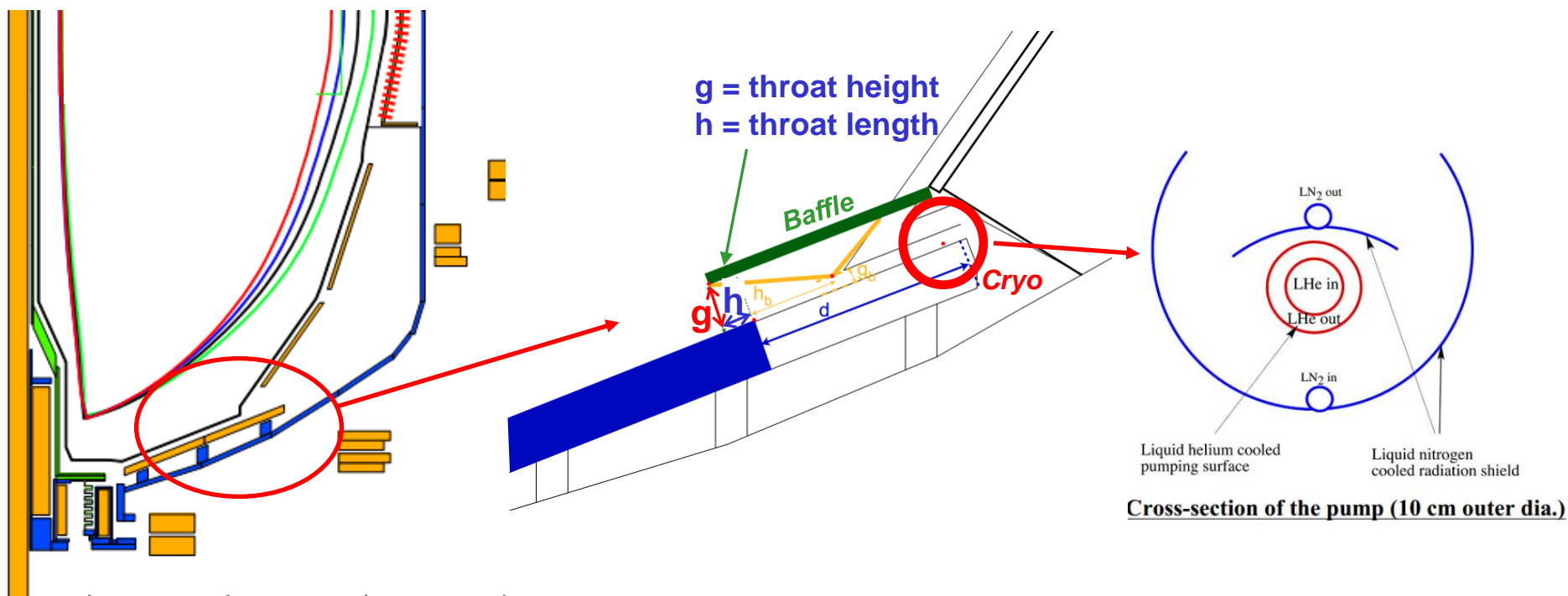
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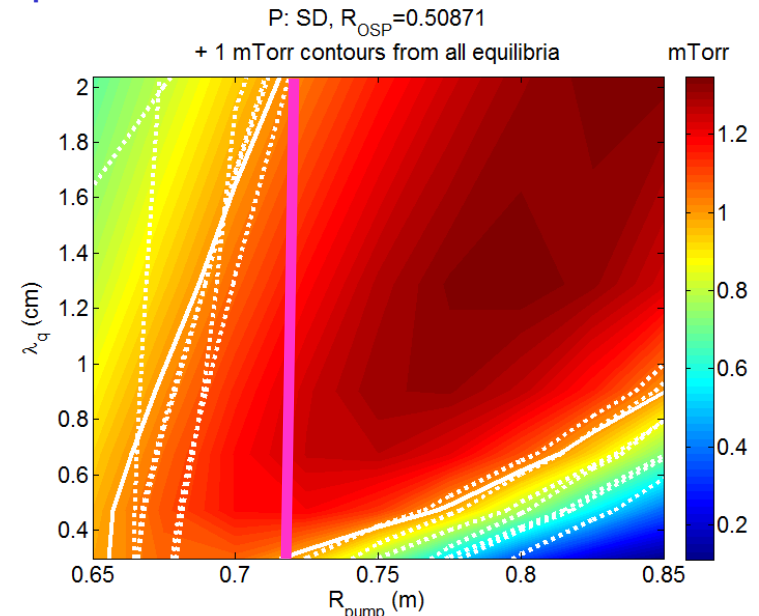
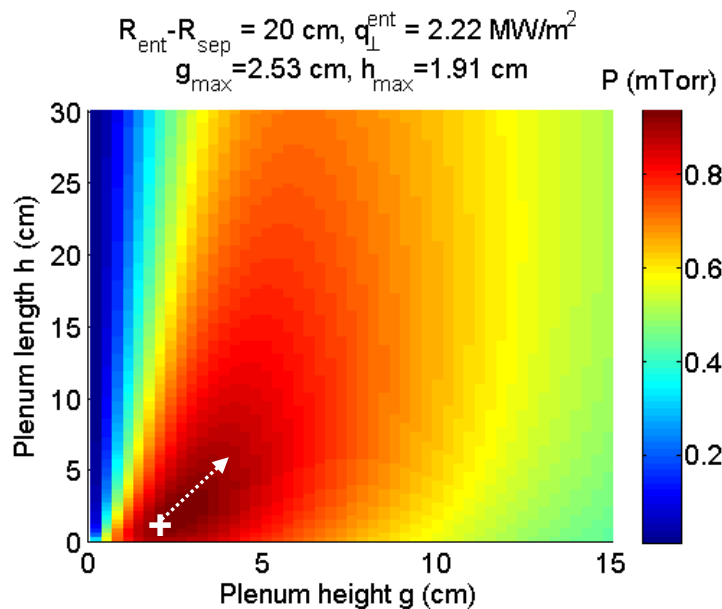
# NSTX-U cryo-pumping design based on DIII-D system

- Cryo-pump is proven technology for plasma density control
  - More conventional pumped ELMy H-mode scenario
- NSTX-U design is similar to DIII-D outer lower pump
  - Plenum located under new baffling structure near secondary passive plates
  - Pumping capacity of a toroidal liquid He cooled loop
    - $S=24,000$  l/s @  $R=1.2$ m (Menon, NSTX Ideas Forum 2002)
  - Need plenum pressure of 0.6 mTorr to pump beam input (TRANSP)



# Semi-analytic pumping model used to optimize plenum geometry

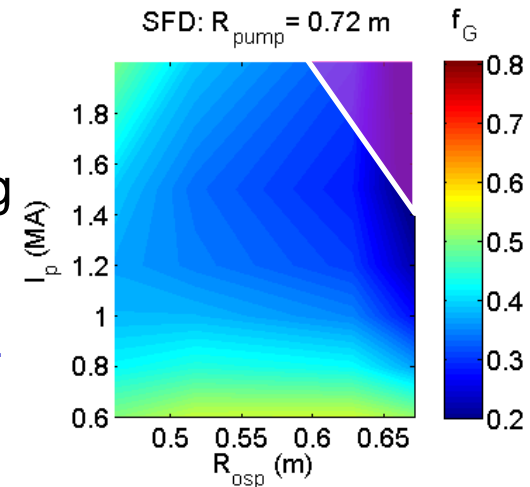
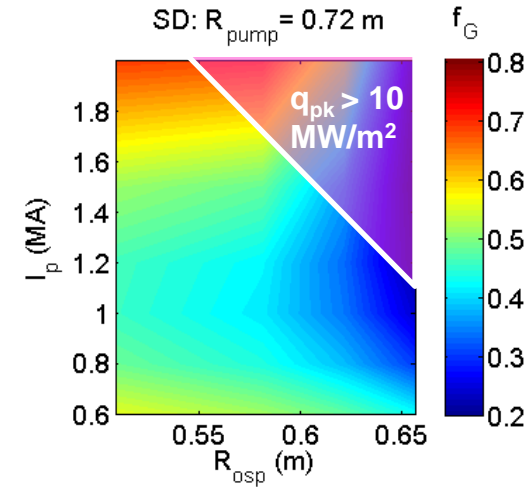
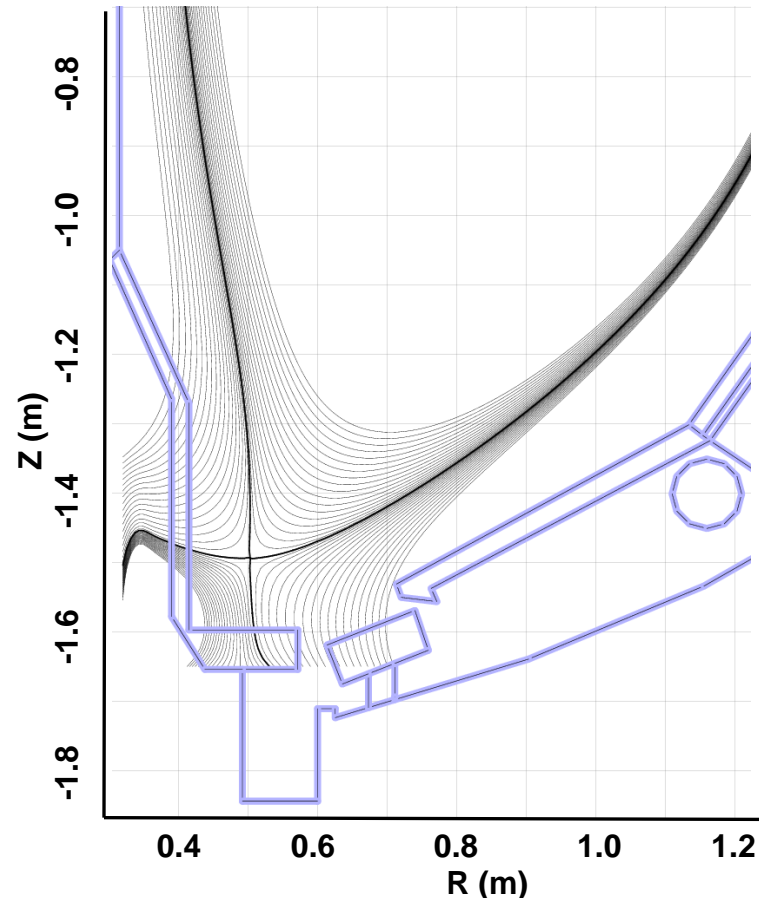
- Model developed for DIII-D pumping studies (Maingi, NF '99)
  - Predicts plenum pressure, validated with DIII-D data
  - Projected NSTX-U heat flux ( $I_p$  scaling) and divertor  $T_e$  ( $\sim 15$  eV) used as input
  - Uses first-flight neutral model (insufficient for detached divertor)
- Pressure is maximum for duct height  $g \sim 2.5$  cm, length  $h \sim 2$  cm
  - But is only weakly reduced if these are increased together
- With pump entrance at  $R=0.72$ m, pressures  $>1$  mTorr can be reached over wide range of plasma shapes and SOL widths
  - Comparable to pressures in DIII-D plenum
  - Well above that needed to pump NBI particle input



# Optimized plenum geometry can pump to low density for conventional and snowflake divertors over a range of $R_{OSP}$ , $I_p$

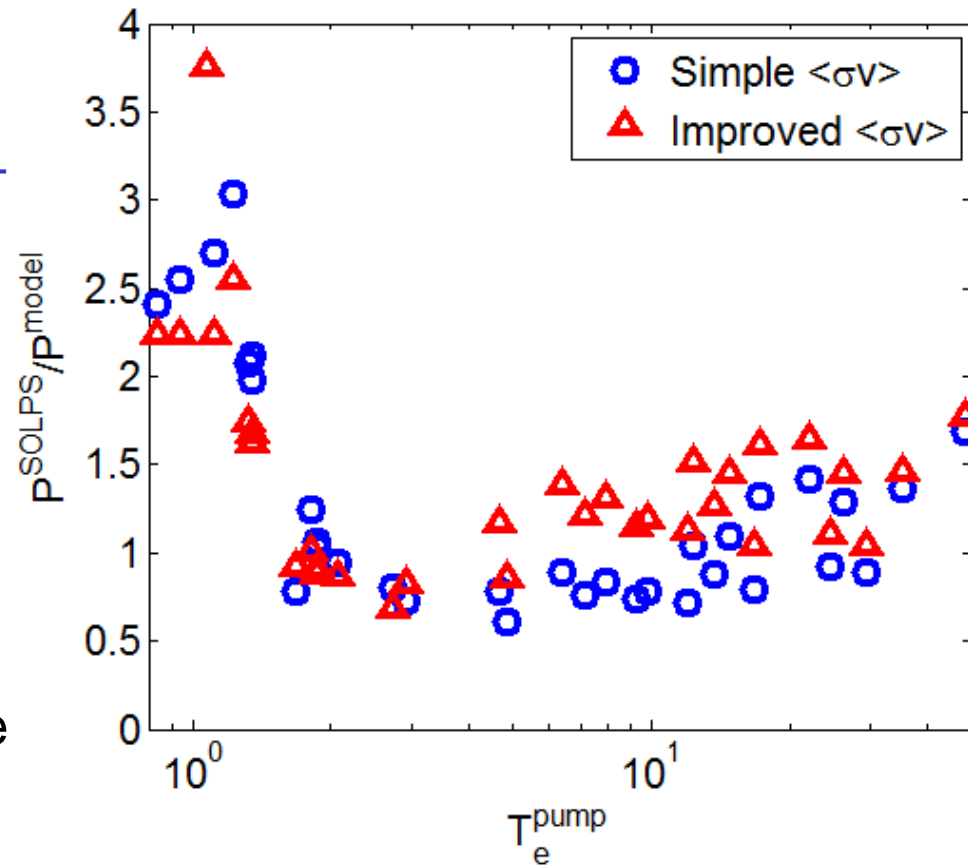
$R_{OSP}$ : outer strike point radius  
 $R_{pump}$ : plenum entrance radius  
 SD: standard divertor  
 SFD: snowflake divertor  
 $f_G$ :  $n_e/n_G$

- Core density estimated assuming pumped flux=NBI input
  - 2-pt model used to estimate upstream density
  - Assume  $n_e/n_e^{sep} \sim 3$
- Can pump to  $f_G < 0.5$ 
  - $f_G \sim 0.7$  desirable for all scenarios, lower provides more flexibility
  - Moving  $R_{OSP}$  closer to pump allows lower  $n_e$ , but limited by power handling
- High flux expansion in SFD gives *better* pumping with SOL-side configuration
  - More plasma in far SOL near pump
  - More room to increase  $R_{OSP}$  at high  $I_p$



# SOLPS calculations confirm optimization approach based on analytic model

- SOLPS: 2D fluid plasma/neutral transport
  - Plasma transport classical parallel to B (+kinetic corrections), ad-hoc cross-field transport coefficients
  - Kinetic neutral transport using MC code EIRENE
    - More comprehensive treatment of neutral transport (beyond first-flight)
    - Can treat radiative/detached divertor
- Range of divertor conditions have been produced using standard and snowflake equilibria
- SOLPS-calculated plenum pressure agrees with analytic model for  $T_e^{\text{div}} > 2$  eV, factor of  $\sim 3$  higher in detached regimes



**$\Rightarrow$  Optimization of design presented here is conservative**  
**– Pumping likely to be stronger for realistic conditions**

# Questions from Panel – 5-7 of 7

5. What are the rep-rate limitations for high field operation?
  - What arises first, second, third?
  - How do you plan deal with them?
  - Addressed by S. Gerhardt
  
6. What is the physics basis for the cryopump and the expected particle exhaust rates as compared to lithium coatings?
  - Addressed by J. Canik
  
7. **Is the cryopump compatible with MGI or NB operation? (... but we will answer a slightly different question):**  
**Is MGI compatible with divertor cryopump and NB operation?**
  - **NBI cryo – Addressed by: S. Gerhardt / R. Raman**
  - **Divertor cryo – Addressed by J. Canik / R. Maingi**

# MGI Experiments on NSTX-Upgrade are Primarily For Scientific Purposes

- NSTX-U is designed to tolerate 2 MA disruptions.
  - MGI is not anticipated to be a machine protection system
- Experiments on other devices show that the leading edge of the gas front is most critical for mitigation
  - NSTX-U experiments will aim at understanding the minimum required gas loading by varying the poloidal injection location
  - Will use fast-opening electromagnetic valves of a design similar to JET and ITER, located close to the vessel, to minimize the gas input.
- Anticipated MGI levels are up to 500-700 torrL at most
  - D<sub>2</sub> or He, with smaller fractions of Ne or Ar.
  - Values are ~5000 torr @ ~100 cc-> 500 torrL.
  - Leads to ~6 mtorr vessel w/ one beam box, 4 mtorr w/ two beams boxes.
  - NSTX-U TMP systems significantly upgraded, will help with He pumping.
- **Beams:** Very desirable to use NBI + MGI to test penetration into H-mode pedestal.
- **Cryopump:** May very well be possible to run MGI experiments with divertor cryopump not at liquid He temp, as it is not needed for experiments



# Two Significant Issues Have Been Identified for NBI+MGI

- Beam Reionization: Beam is “reionized” in the duct by the higher pressure, bent to the duct wall as it enters the TF.
  - Can avalanche: sputtered/ejected material from beam strike can increase the duct pressure.
  - Solution: Interlocks and procedures will be implemented to turn beams off before MGI. Experiment would be conducted within the beam slowing time.
    - Updated Gas Injection PCS Spec. for NSTX-U has an explicit test of the beam power before firing MGI valves.
- Beamline Cryopump Regen
  - Helium provides a conduction path from panels to the hotter components.
  - NB Group does regenerations by applying 5 mtorr of He to a closed box.
- Experiments with NB valves open will need to maintain the pressure in the box beneath this level with some safety margin. 90 Torr.L He is acceptable (previously tested on NSTX)
  - 2015: 100 Torr.L D2, and gradually increase to 500-700 Torr.L D2 (understand assimilation efficiencies)
  - 2015: 500-700 Torr.L D2 + Neon
  - 2015: 500-700 Torr.L He + Neon (should be sufficient for full mitigation studies)
  - 2016: Determine minimum levels of He + Neon to achieve full mitigation
  - 2017: Determine minimum levels of He + Argon to achieve full mitigation

# Heat load on the divertor cryo-pump during MGI needs assessment

- As previously noted, beam cryo-pump already provides a significant constraint on the maximum He pressure for cases with beams:
  - Divertor cryopump will only be needed for long-pulse examples, all of which will require beams.
- Acceptable heat load on NSTX-U divertor cryo-pump has not yet been assessed
  - DIII-D design maximum cryo heat load was ~ 10 W
  - DIII-D tests were conducted with heat loads up to 25 W, with no spontaneous re-gen
  - DIII-D cryo can pump large amounts of *deuterium* gas > 2500 torr-I, without re-gen
- Reiterate: For scientific exploration of MGI physics, likely not necessary to utilize divertor cryo-pumps at all.

# Backup

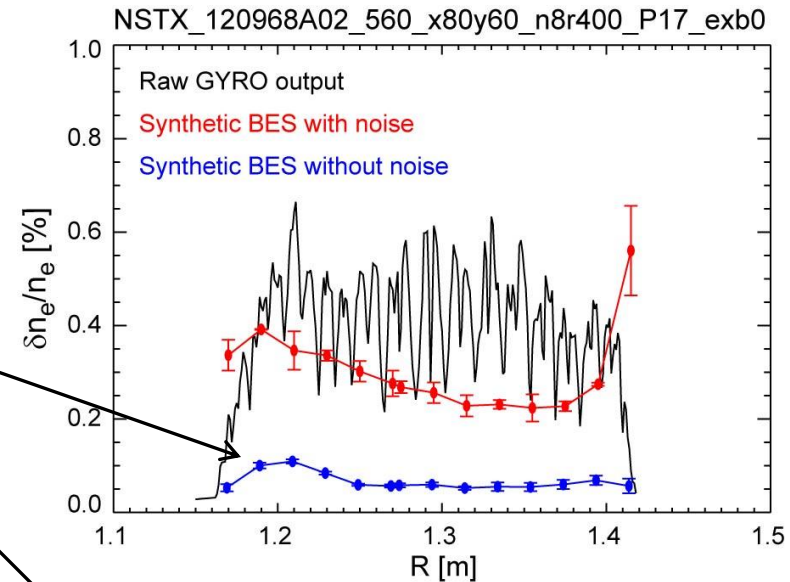
# MAST-NSTX collaboration testing sensitivity of BES to microtearing turbulence through synthetic diagnostics

- Using nonlinear NSTX microtearing simulations from GYRO with synthetic diagnostic for MAST BES
  - Difficult to detect MT with expected signal-to-noise ratio (uncorrelated noise dominates)
  - If S/N can be increased (e.g. significant time averaging) MT features may be measurable, such as:
    - detectable correlated fluctuation levels ( $\delta n/n \sim 0.1\%$ )
    - large poloidal correlation lengths ( $L_p \sim 15\text{-}20\text{ cm}$ )

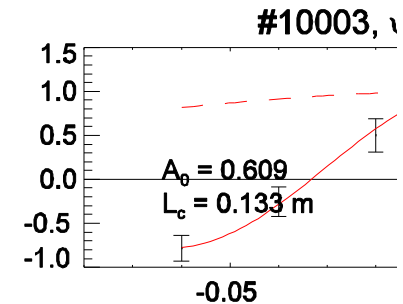
## Future plans:

- Pursue non-linear simulations for MAST discharges with available BES data
- Propose experiments for FY13 at next MAST research forum (Dec 2012) to focus on relationship between collisionality scaling and microtearing turbulence

Density fluctuation (rms)



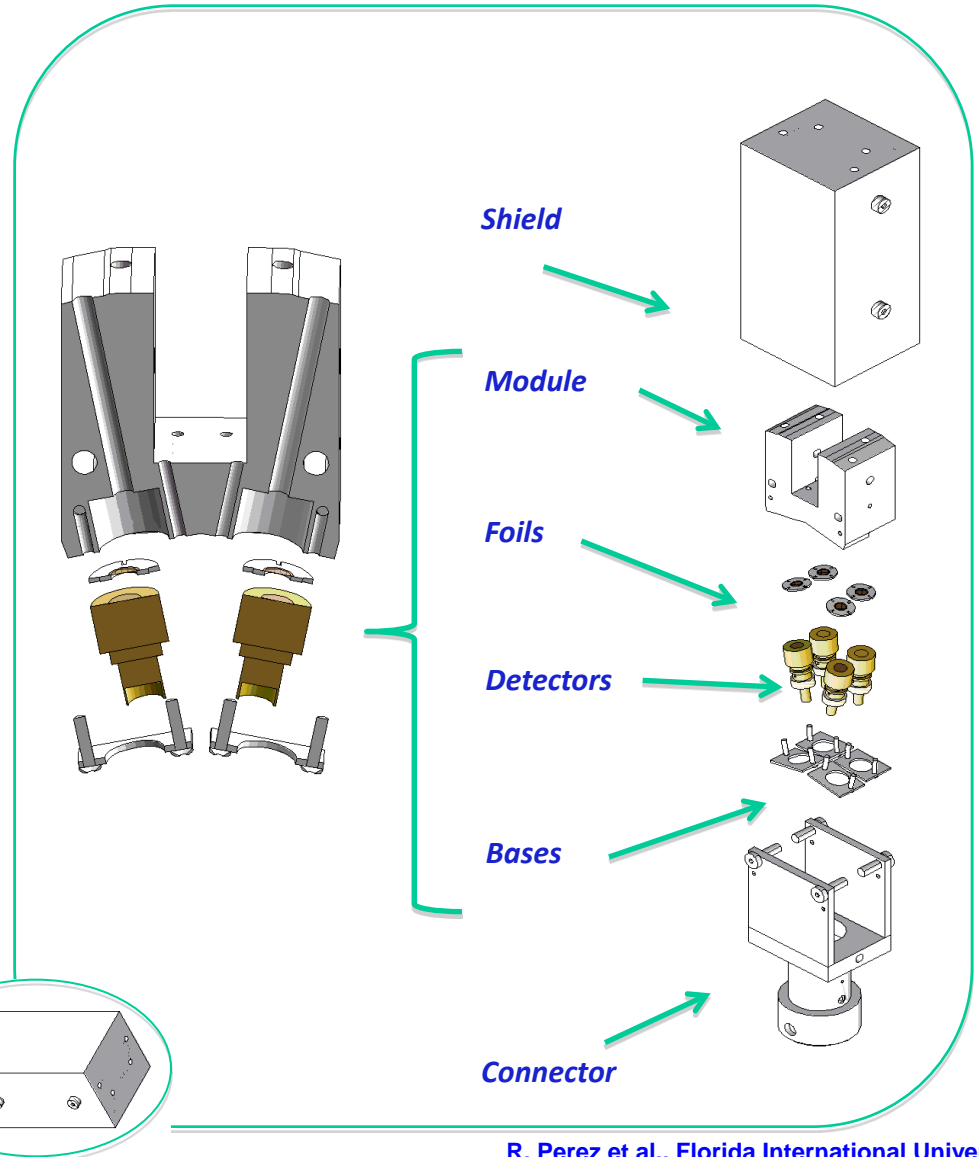
Poloidal correlation from synthetic diagnostic



# NSTX-U Charged Fusion Products Diagnostic on MAST

Provides fusion reactivity profile due to MHD and other phenomena

- Collaborators: FIU, MAST, PPPL
- MAST Installation: November 2012
- Objective: obtain time-dependent, precise information on the  $d(d,p)t$  fusion rate profile with the goal of determining the neutral beam ion density profile as a function of  $R$ ,  $z$ , and  $t$



R. Perez et al., Florida International University

# Data Acquisition Will Be Upgraded to Support Increased Data Load

- Extension of pulse length to 5 seconds increases the data load considerably, and steps have been taken to bring down the data transfer time.
  - Network upgrades
  - Elimination of CAMAC
- Expected times:
  - 3.5 minutes for MDS+ physics data.
  - 5 minutes for EPICS engineering data (mostly NB, MG, and rectifier signals)