

Outline & status for: “Progress in understanding error-field physics in NSTX spherical torus plasmas” (red items remain to be done)

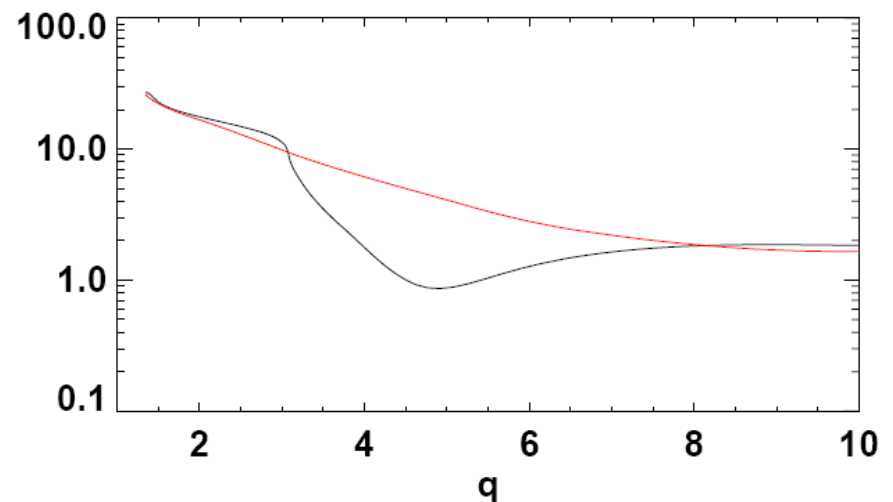
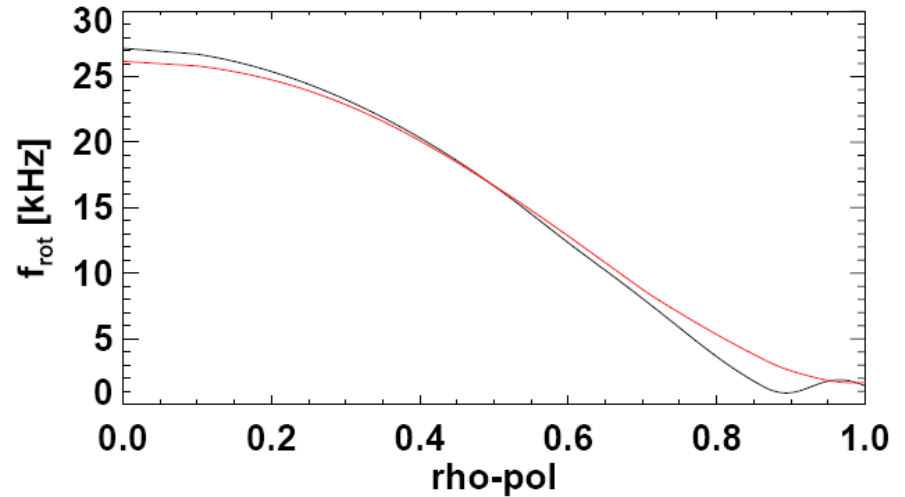
0. THEME: low-A and low-B of NSTX provide additional insight into EF physics
1. NSTX locked modes
 1. Discussion of sensor array
 1. Analyze error fields (EFs), sources of $n=1$ EF
 2. Threshold scaling
 1. linear scaling with plasma density, a weak dependence on BT, and a positive scaling with q shear
 2. Discussion of dependence on choice of q -shear variable, **compare to tokamak & Cole PRL**
 3. Results extrapolate to a favorable threshold $\delta B_{21}/BT > 1 \times 10^{-4}$ for ITER, size scaling implications
 4. IPEC
 1. discussion of code physics
 2. plasma response must be included to explain the empirically determined optimal correction
 3. Importance of poloidal mode coupling – apparent in LM scaling data
 4. best fits to data suggest we are optimizing correction of 3/1 or 4/1 rather than 2/1
 5. **Perform MSE reconstructions, include in fits and IPEC analysis**
 6. Discussion of pert. Helical flux vs. perturbed B_{norm} – how it changes spectrum, consistency w/ IPEC
2. $n \geq 1$ EF correction and performance – sensors used to measure EFA, RWM in real-time
 1. Optimized $n=1$ DEFC using externally applied $n=1$ pulse + gain & phase optimization
 2. Asymmetry in plasma response to $n=3$ EF polarity
 1. **Determine source of $n=3$ EF – suspect PF5 – need to analyze coil shape data**
 3. Demonstration of pulse-length extension and edge rotation maintenance using $n=3$ + $n=1$ DEFC
3. Implications for RWM critical rotation physics
 1. $n=3$ EF studies show important role of rotation at ($\rho = 0.6$ to 0.95 , $q=3$ to 8)
 2. Study role of toroidicity in kinetic-damping
 1. trapped-particle bounce times strongly modified by low-A – should impact RFA, DEFC, and critical rotation
 3. **Implement work of A. Egan into MARS-F calculations – compare theory to data**
 1. Summer 2007 - developed parametric fit to bounce/transit times vs local ε and $\mu B_{min}/E$

Both shots have $n=3$ applied – but with opposite polarities
Discharge with lower rotation near $\rho=0.9$ survives

Discharge with higher rotation there suffers RWM collapse

Perhaps rotation shear
change/reversal near edge is just
as important as magnitude of
rotation?

Y. Liu – last IPTA that rotation
profile shape is very important in
semi-kinetic damping model



- Above no-wall limit, DEFC system responds to amplified error field
- Amplification determined by RWM damping rate
- (semi-kinetic) damping rate predicted to depend on $\tau_{\text{pass}}, \tau_{\text{bounce}}$

τ_{pass} and τ_{bounce} decrease by almost factor of 2 near boundary at low-A

Impacts damping and RFA predictions – will compare to NSTX DEFC data

Line = numerical orbit time
Diamonds = MARS-F analytic

Improved analytic fits to the full numerical orbit times have been developed for implementation in MARS-F

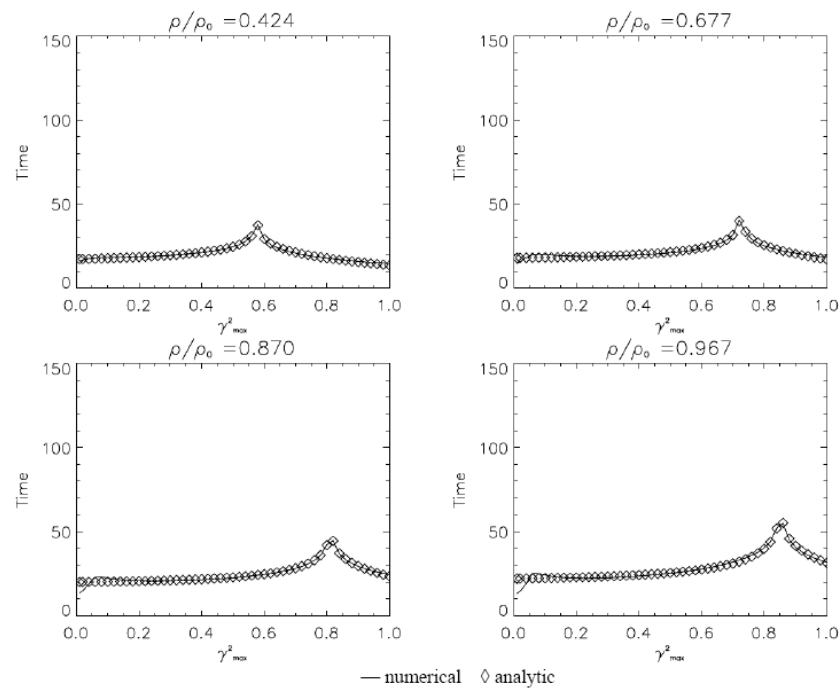
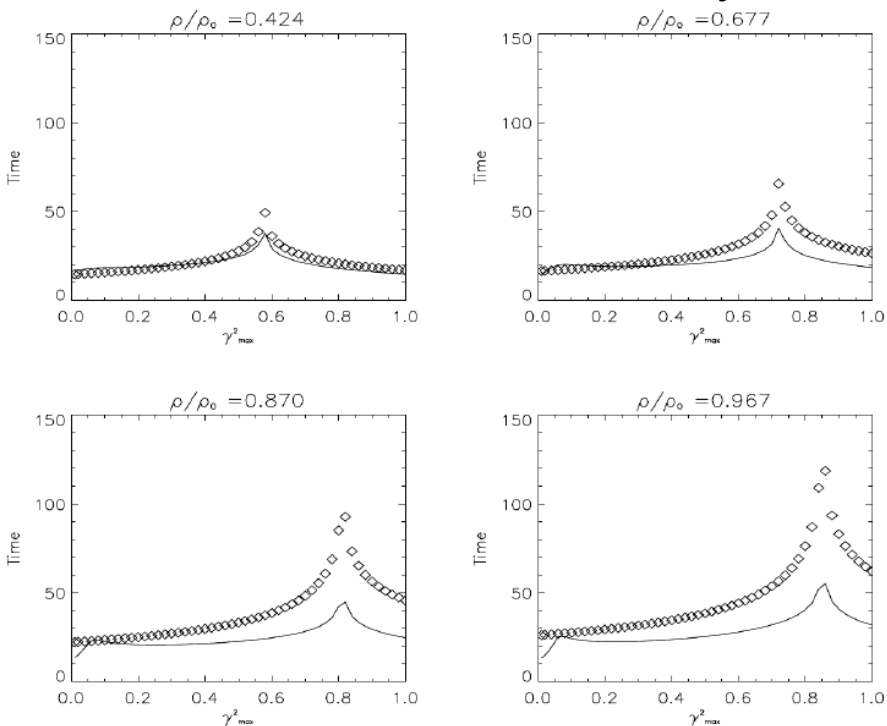


Figure 3: For the low-A, strongly shaped case, the analytic formulae (8) produces orbit time profiles which deviate significantly from the numerical profiles.

Figure 5: For the low-A, strongly shaped case, the improved analytic formulae (16) produce orbit time profiles which strongly agree with the numerical profiles. Because (16) reduces to (8) for $c_0 = c_1 = 0$, the large-A, circular cross section case will show agreement very similar to that seen in Figure 2.

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Results from MHD XP's 701, 702, 703

Presented by:
J.E. Menard, PPPL

w/ contributions from
S. Gerhardt and S. Sabbagh

NSTX Results Review

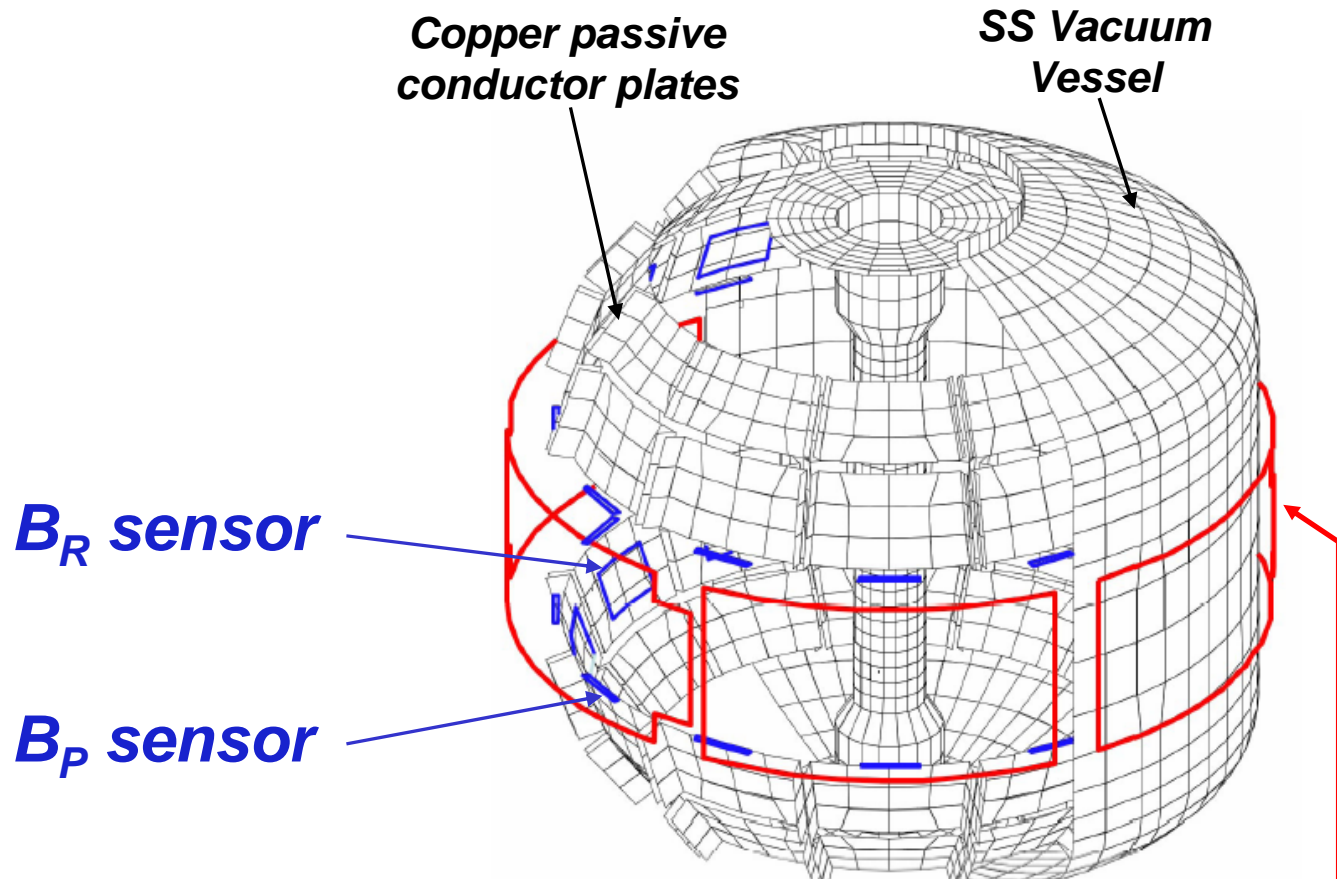
July 23-24, 2007

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The NSTX RWM/EF coil and sensor system

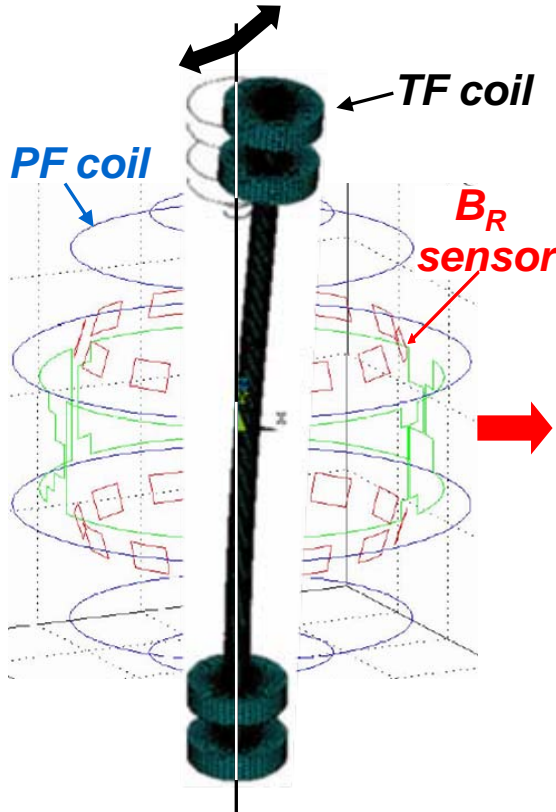


VALEN Model of NSTX (Columbia Univ.)

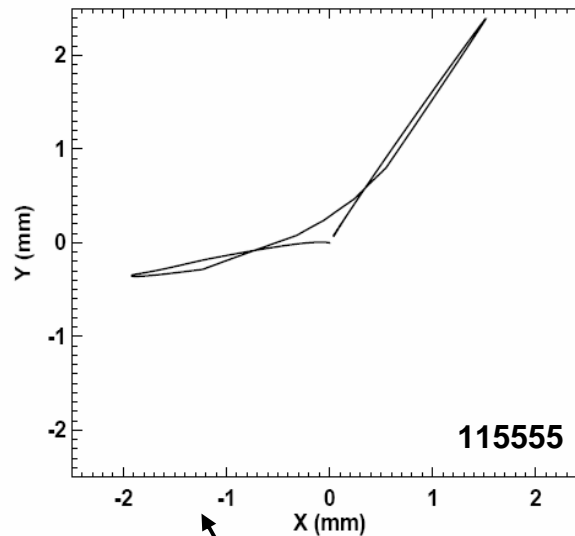
6 ex-vessel midplane control coils

Error field source identification and compensation in NSTX

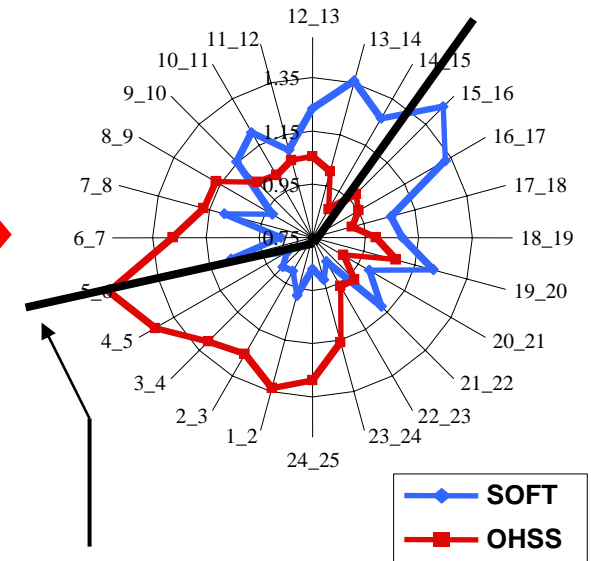
- Some scenarios with lower κ , δ exhibit Ω_ϕ and β_N collapse when $\beta_N > \beta_N$ (no-wall)
- Measure 2-3 Gauss $B_\perp^{2/1}$ EF in LM experiments... what is EF source?
- **Present picture of EF Source:** EF from/near OH leads at top of machine induces TF coil motion relative to B_R sensors (plates, vessel) and thus **the PF coils**



TF coil shift at mid-plane
inferred from B_R sensors
during OH+TF vacuum shot



Normalized TF bottom joint voltage drop from OH+TF test



TF flag-joint voltage variation direction
consistent with magnetics

Shim between TF bundle and OH tension tube added before 2007 run to reduce motion

XP701 - Assessment of intrinsic error fields after TF centering

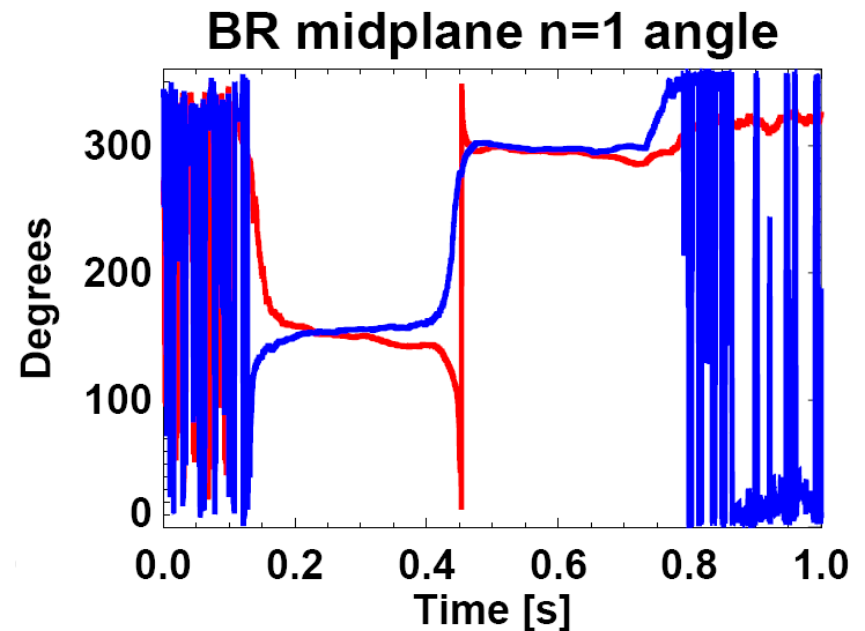
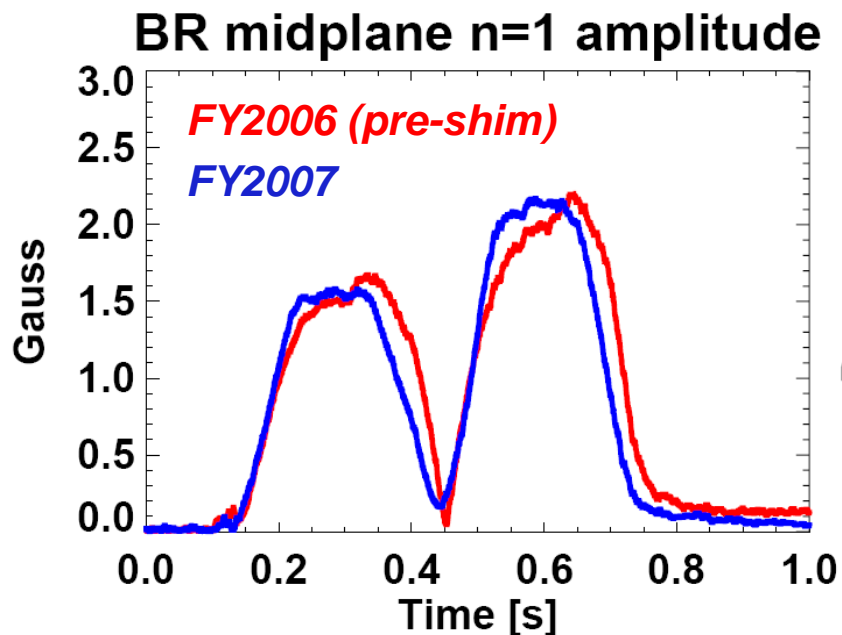
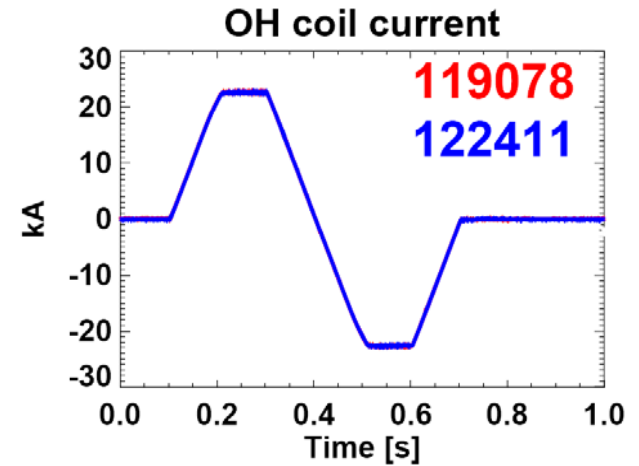


- Assessed modifications to TF coil centering w.r.t. intrinsic EF
 - Intrinsic EF very similar to 2006 for LM ohmic shots
 - Larger difference for long-pulse – lower EF after $I_{OH}=0$ crossing
- Verified rotation response asymmetry to $n=1$ applied field
- Could not reproduce 2006 reference discharge for OHxTF EFC algorithm optimization (rotation collapse not observed)
 - Used externally applied $n=1$ pulses instead in XP702
- NEW: Measured plasma response asymmetry to $n=3$
 - Pulse-length increases with “corrective” $n=3$
 - Rotation increases with “corrective” $n=3$

Error field from fast OH variation largely unchanged



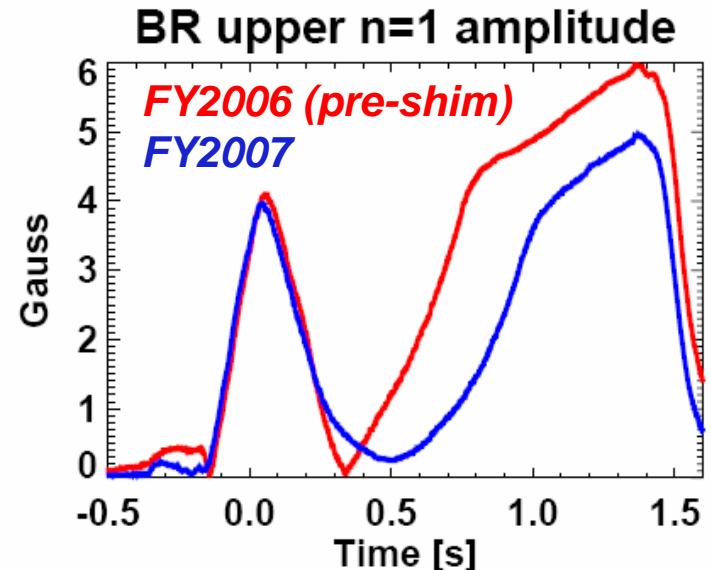
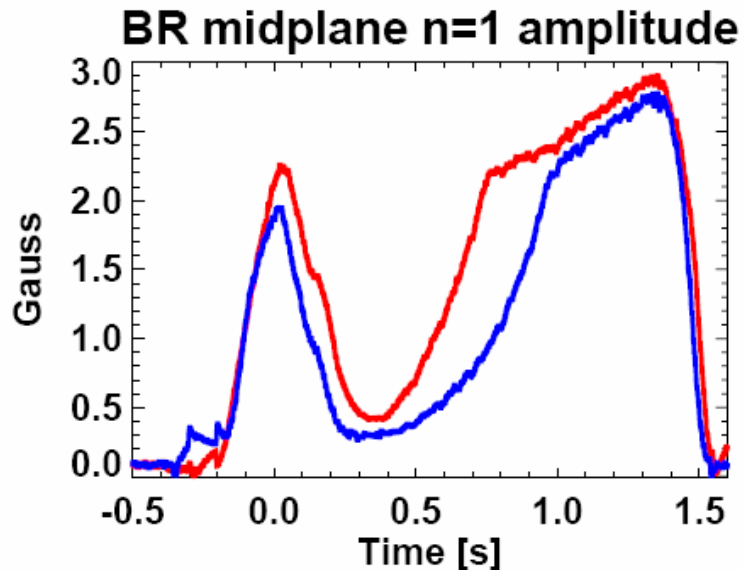
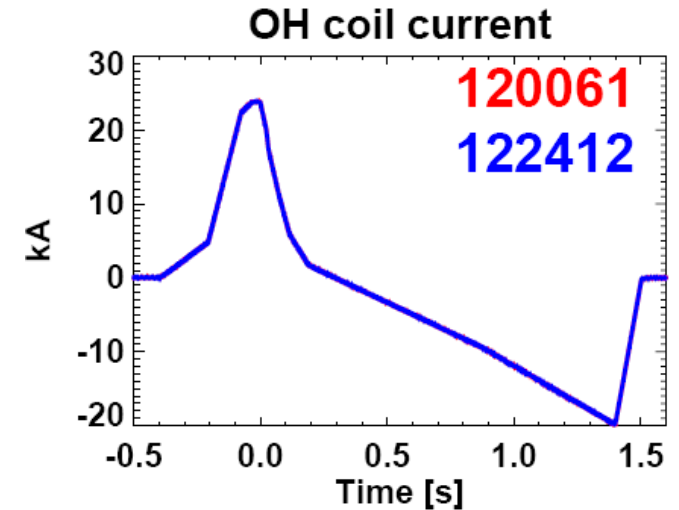
- OH waveform similar to that in ohmic discharges used for locked-mode experiments



EF from slow OH variation different after $I_{OH}=0$ crossing



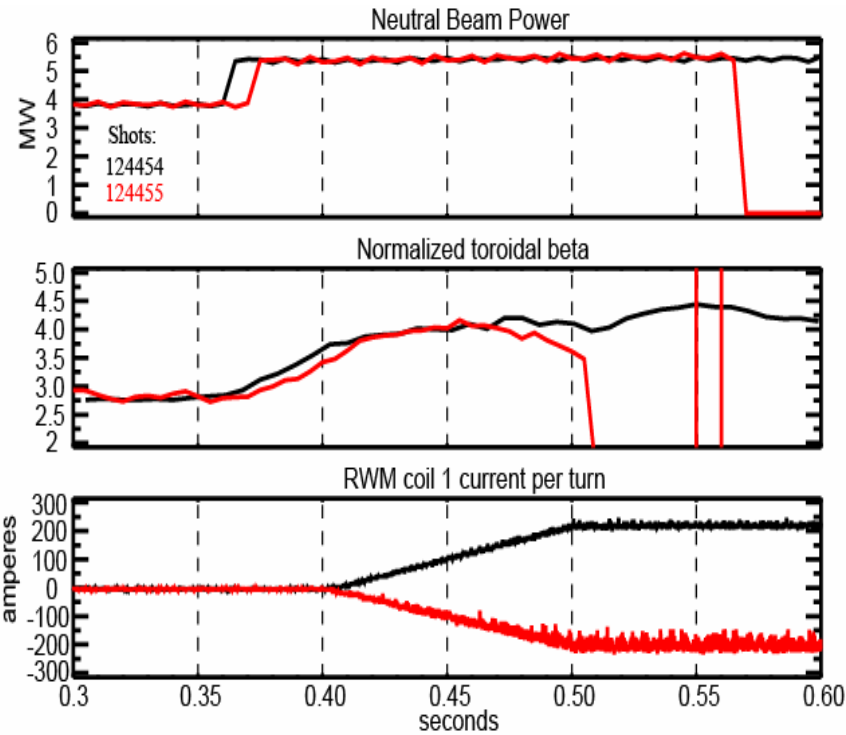
- OH waveform similar to that for NBI H-mode long-pulse
- EF increase is delayed after I_{OH} crossing, but eventually reaches similar amplitude and slope
- Midplane EF amplitude similar, upper EF amplitude reduced late in shot



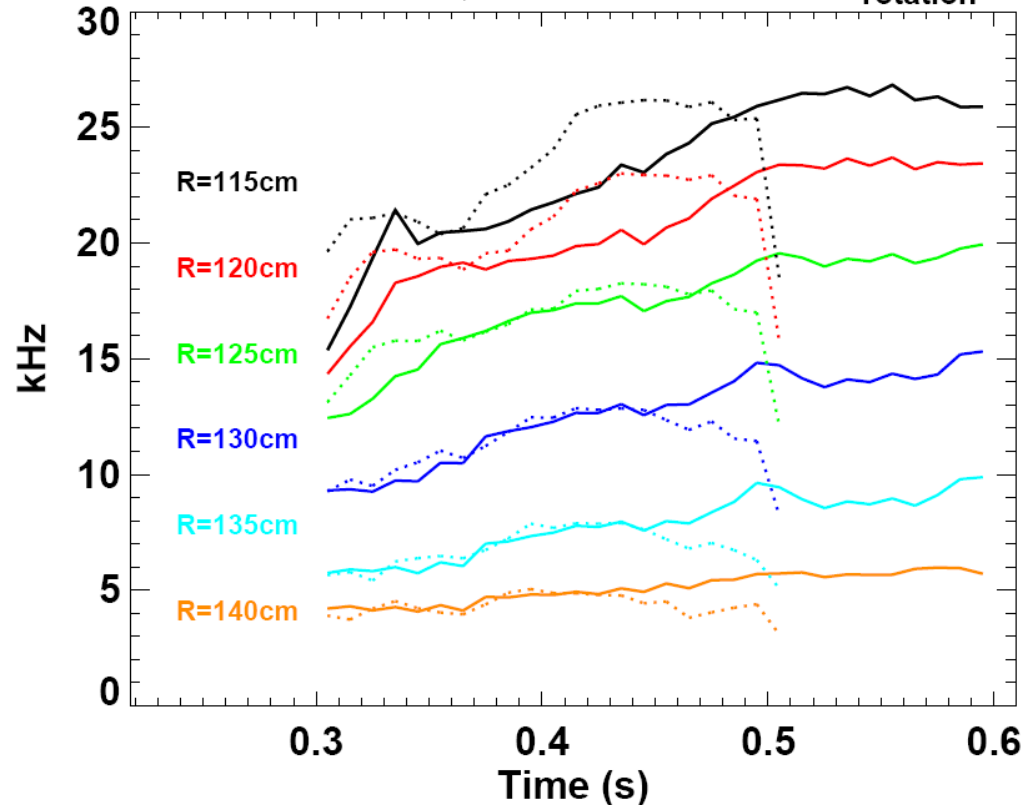
Plasma still exhibits asymmetric response to phase of applied $n=1$ field



- Rotation collapse begins at $t=0.45\text{s}$, and is most clearly evident for radial positions $R > 1.25\text{m}$



Shot 124454, 124455 carbon f_{rotation}

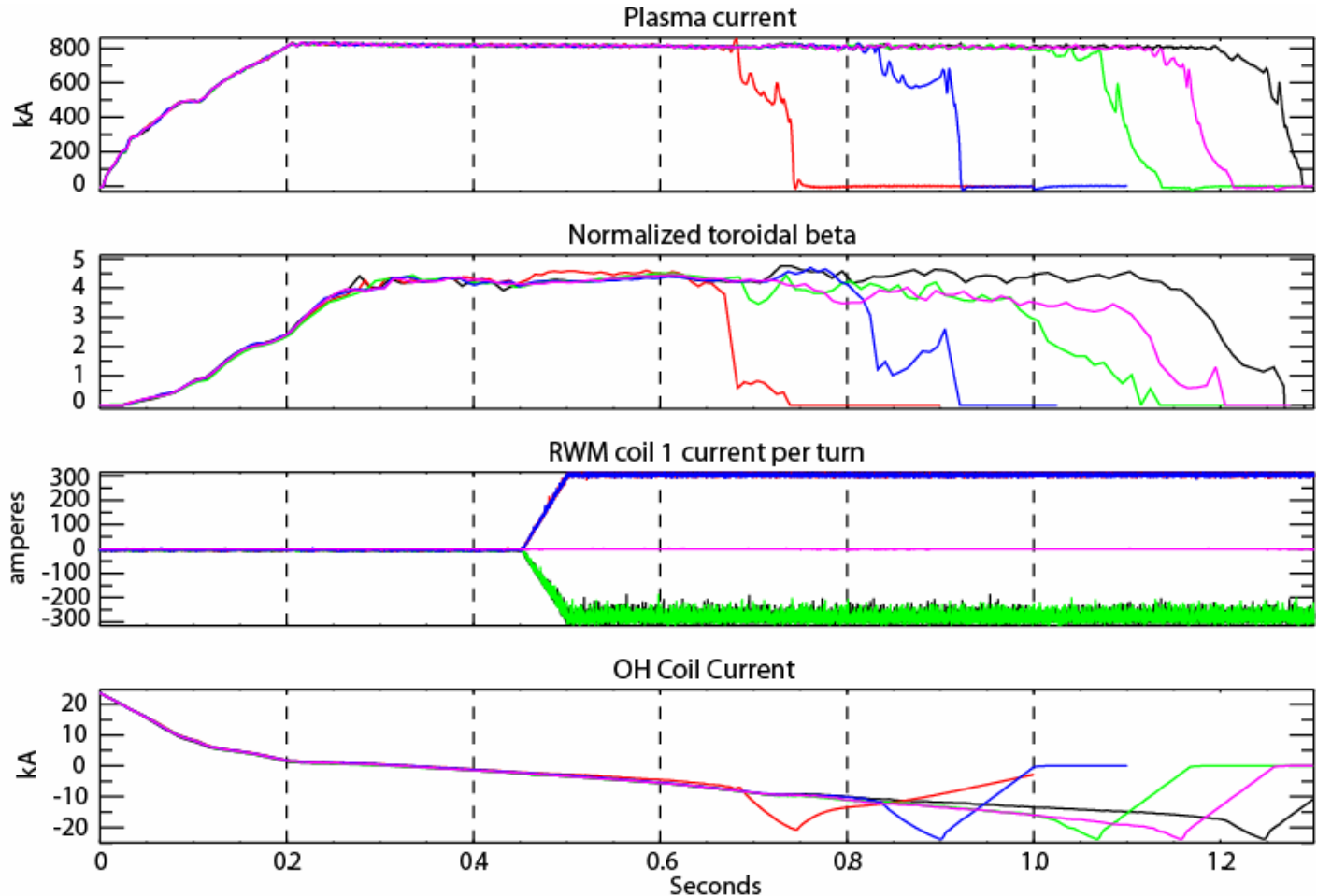


NEW: Plasma exhibits asymmetric response to applied $n=3$ field



- Pulse-length depends on polarity of applied $n=3$ field

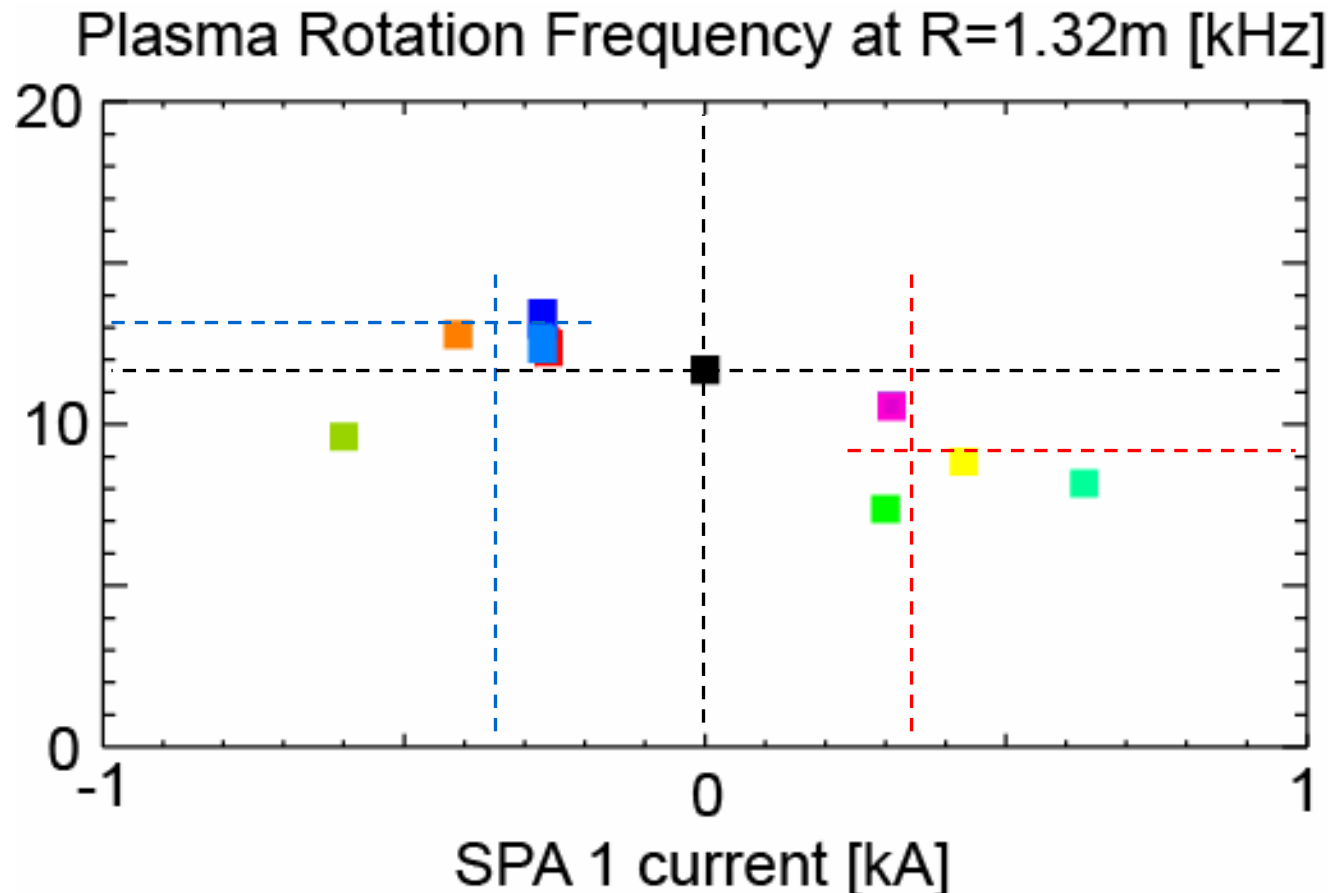
Shots:
124428
124429
124430
124432
124411



Outboard Ω_ϕ changes by 30-40% with n=3 polarity flip



- Optimal n=3 current magnitude = 300-400A
- PF5 coil shape data from 2004 → PF5 is source of n=3 EF
 - Need to assess if this is consistent with empirical correction below



XP702 - RFA detection optimization during dynamic error field correction



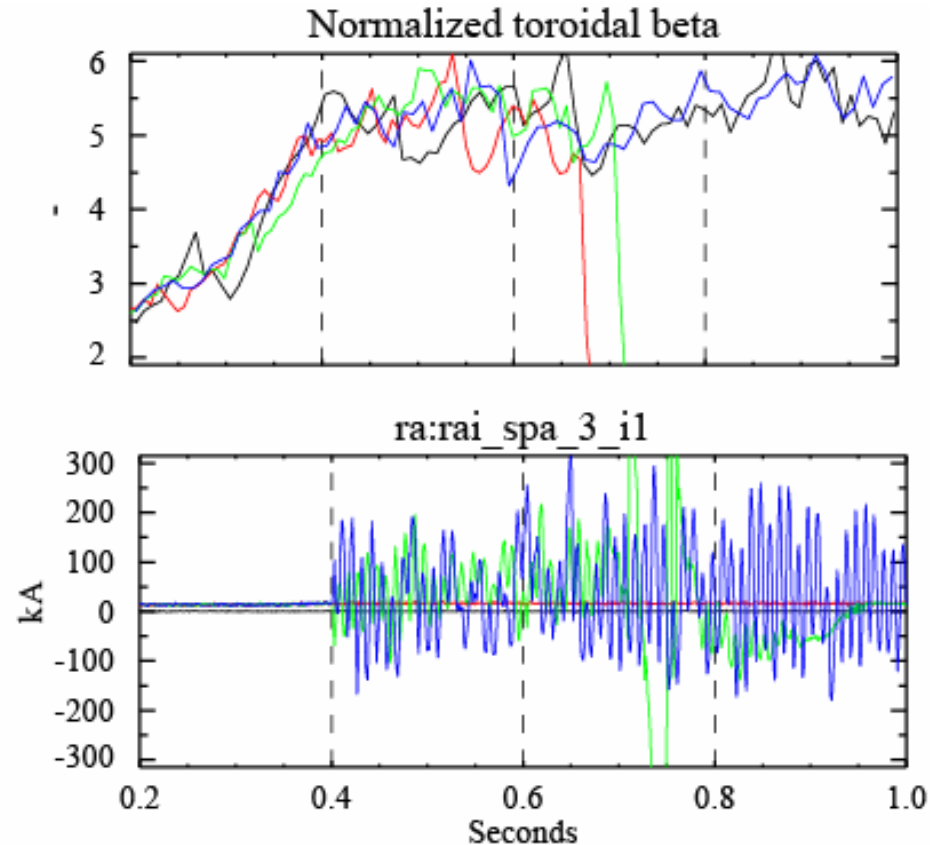
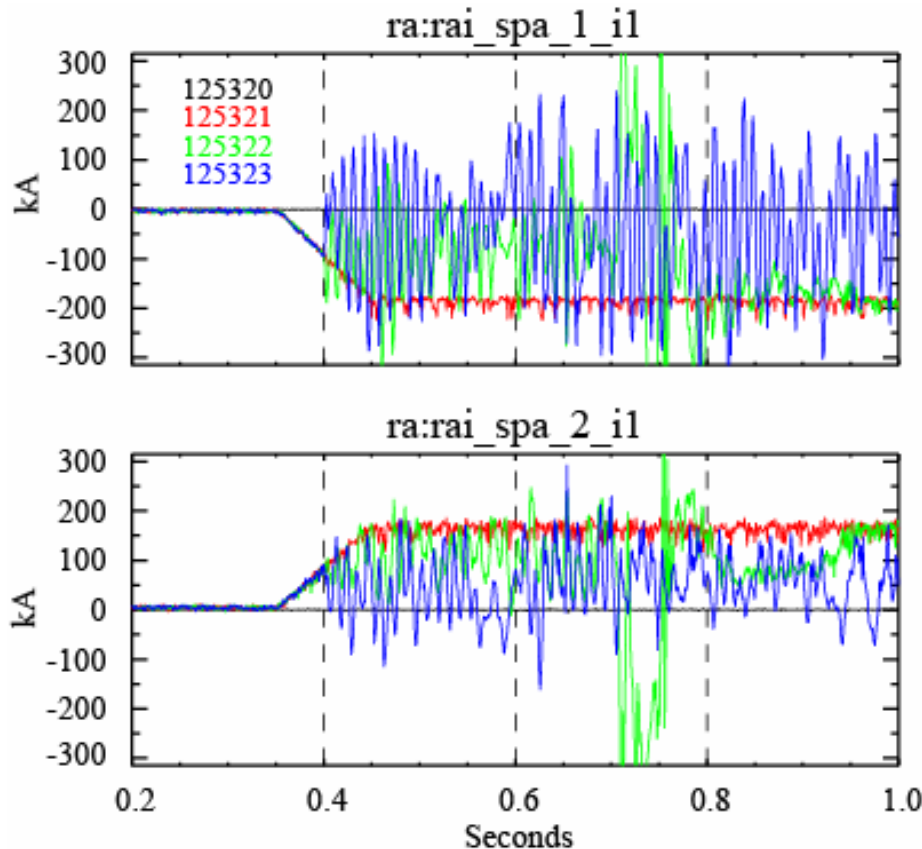
- Implemented real-time mode-ID using U+L B_p and B_R sensors
- Compared DEFC response using upper and lower B_p sensors vs. just using upper B_p sensors (as was used in 2006)
 - More robust mode-ID achieved (higher signal / baseline offset)
 - Higher proportional gain possible (0.7-0.8 vs. 0.5)
- Could not reproduce 2006 reference discharge which previously exhibited intrinsic rotation collapse →
 - Instead, applied $n=1$ EF pulse to induce collapse when OHxTF small
 - Scanned DEFC phase and gain until applied currents were nulled
 - **feedback system “trained” to eliminate EFA of known source**
- Combination of “trained” $n=1$ DEFC + $n=3$ EFC →
 - longest pulse of all shots in XP702
 - sustained plasma rotation

DEFC system trained to null RFA from externally applied/known n=1 error field source



- Optimal phase difference ($\delta=270^\circ$) between measured B_p (U/L avg) and applied B_R required to null n=1 EF pulse
- Sufficient feedback gain also required:

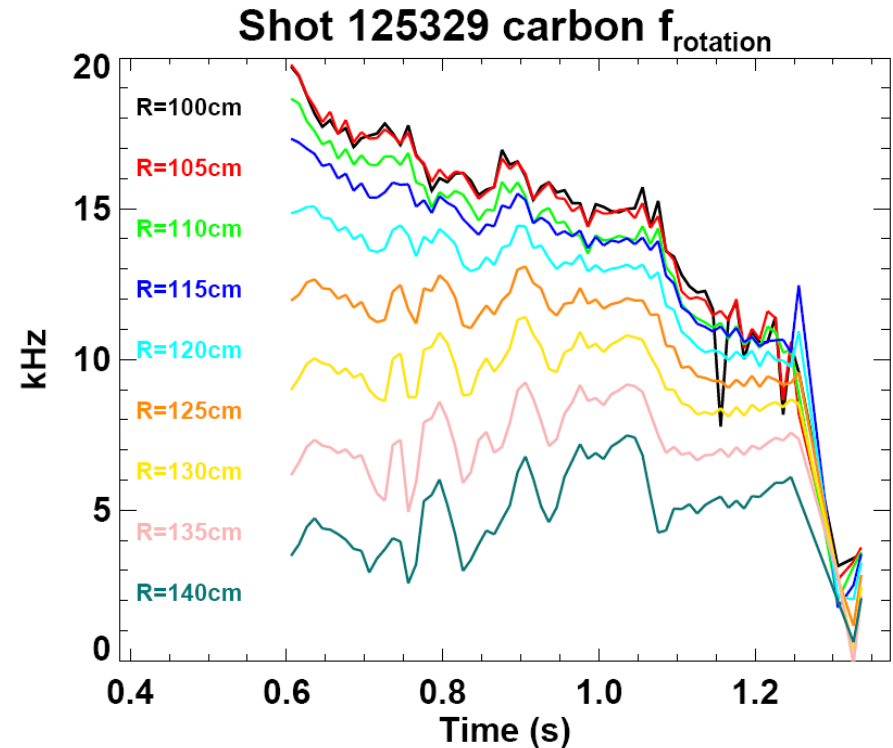
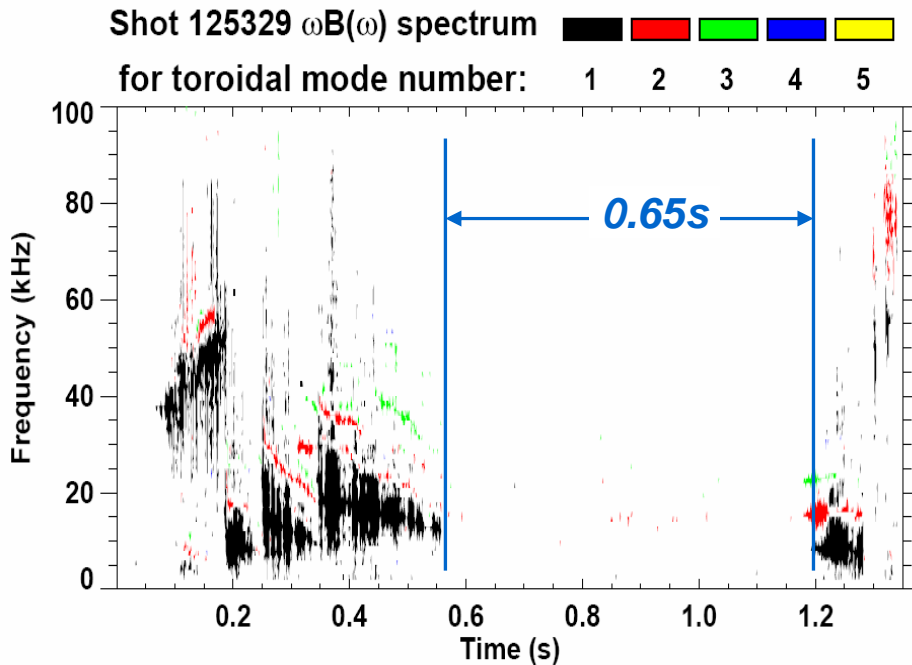
$G_p=0.0$ $G_p=0.5$ $G_p=0.7$



n=1 RFA feedback + n=3 EFC improves performance



- Long period free of core low-f MHD activity
 - Plasma rotation sustained over same period
 - Core rotation decreases with increasing $f_{GW} \rightarrow 0.75$, $P_{RAD} \rightarrow 3.5\text{MW}$
 - $R > 1.2\text{m}$ rotation slowly increases until $t=1.1\text{s}$ (large ELM?)
- Longest pulse at $I_p=900\text{kA}$



XP703 - B and q scaling of low-density locked-mode threshold at low-A



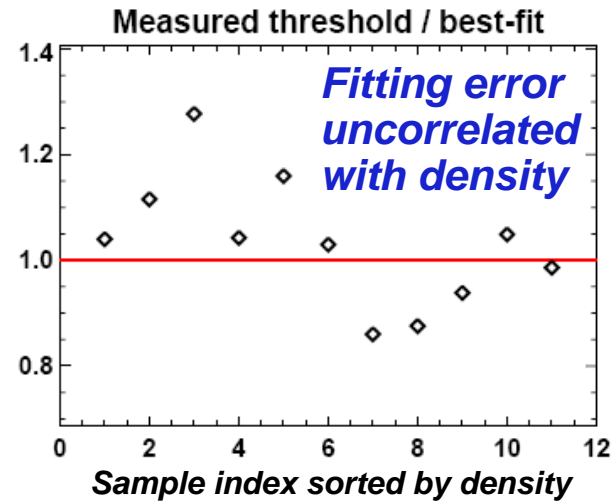
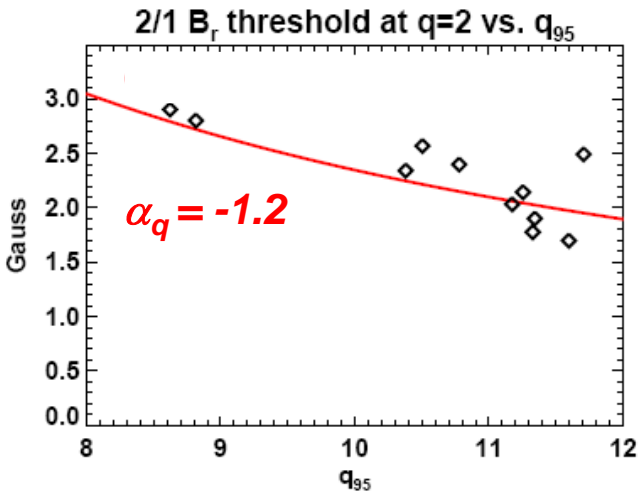
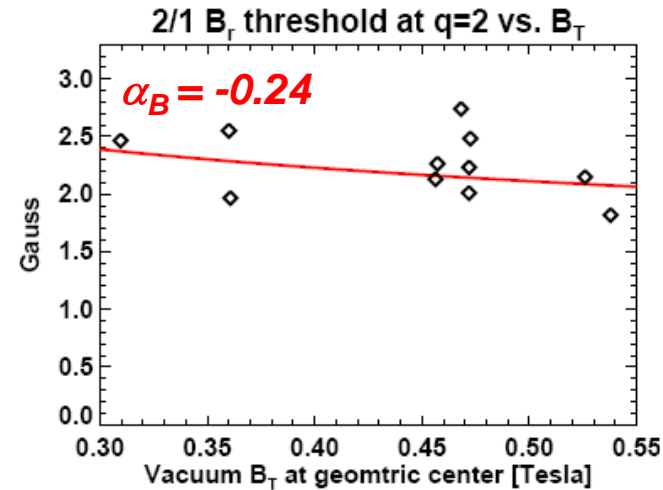
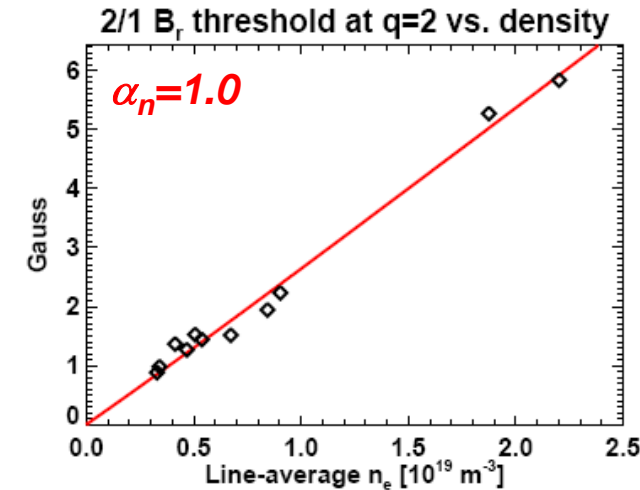
- Extended density range for threshold – now have factor of 4
- Performed B_T scan from 3kG to 5.5kG
- q_{95} scan difficult because high-q does not have $q=2$ in plasma
 - Found this out after MSE data was obtained
- Threshold increases with increased edge q-shear (w/o MSE)
 - Similarly - also increases with internal inductance
- Obtained MSE data for 4 scenarios of interest
 - $q=2$ surface is in plasma at time of locking, but NO $q=1$ surface
 - Core shear is often weakly reversed
 - Measured q profiles not yet included in analysis shown below!
- Locking threshold scaling favorable for ITER

NOTE: Scaling form used below: $B_{21}(\text{lock}) \propto n^{\alpha_n} B_T^{\alpha_B} q^{\alpha_q} R^{\alpha_R}$

NSTX locking data shows linear density scaling and weak B_T dependence, but unexpected inverse scaling with q_{95}



$2/1 B_r$

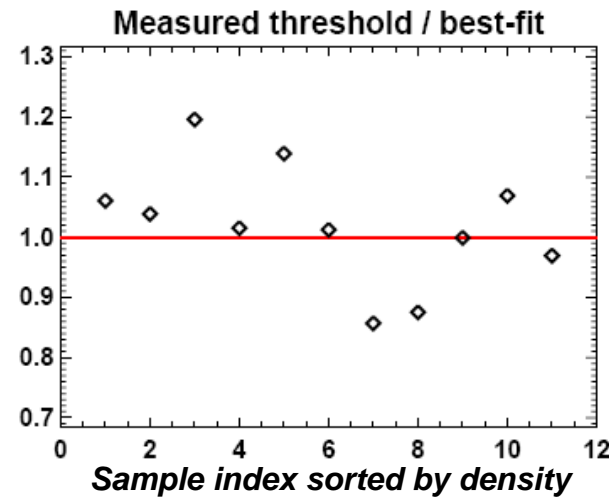
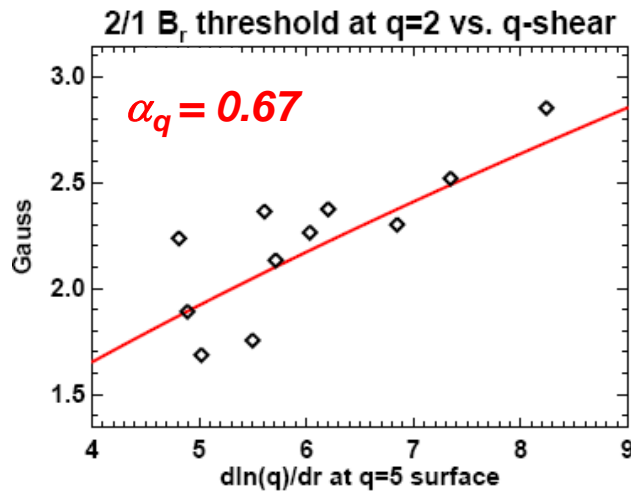
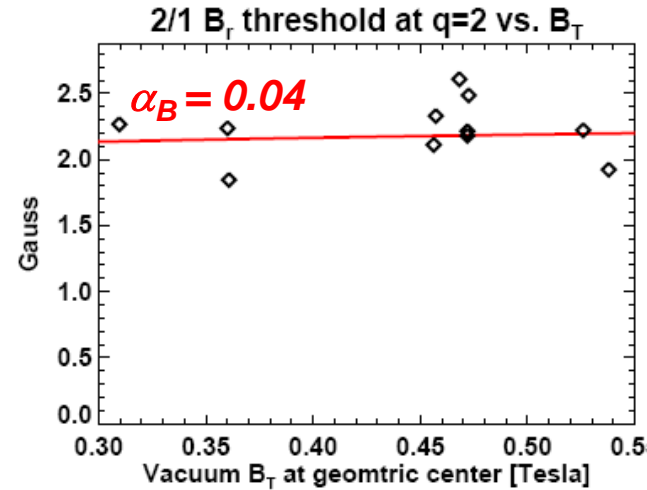
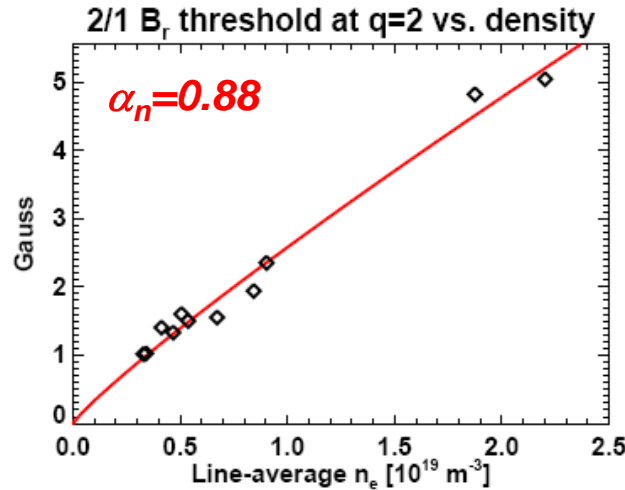


MSE data (not used for scaling above) shows variation in q_{min} when q_{95} is varied. $q(0)$ does not = 1 as for other experiments \rightarrow q_{95} not good proxy for q -shear for NSTX.

NSTX locking data shows nearly linear density scaling and very weak B_T dependence, and expected positive scaling with edge q-shear



$2/1 B_r$

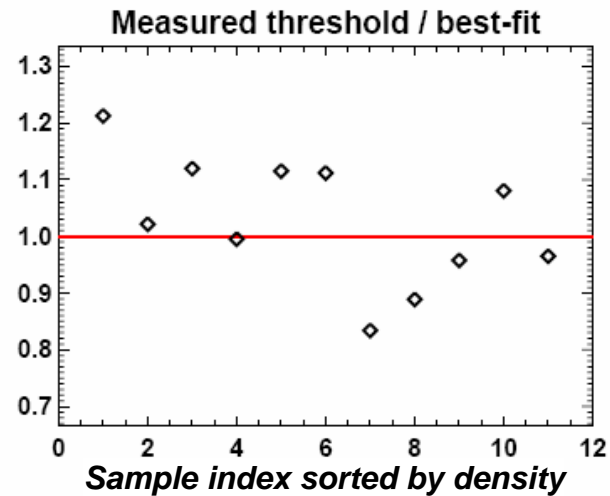
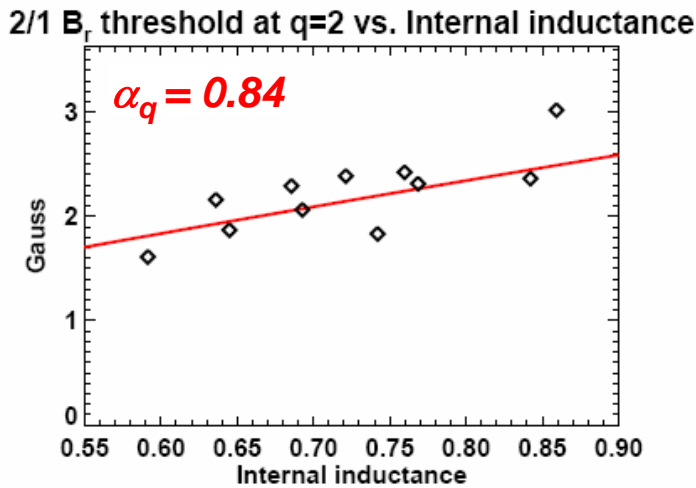
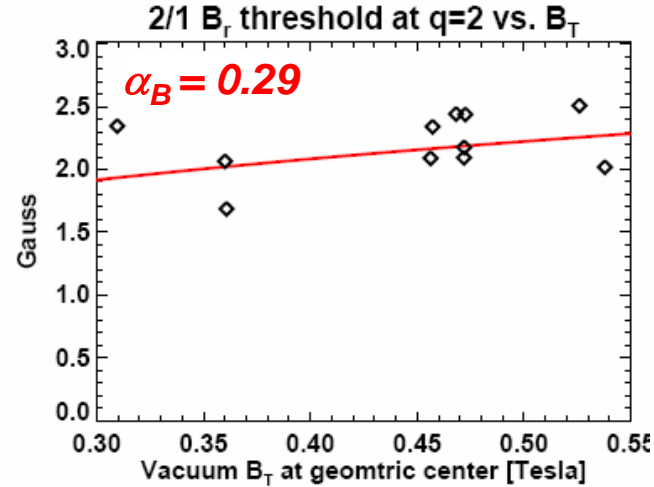
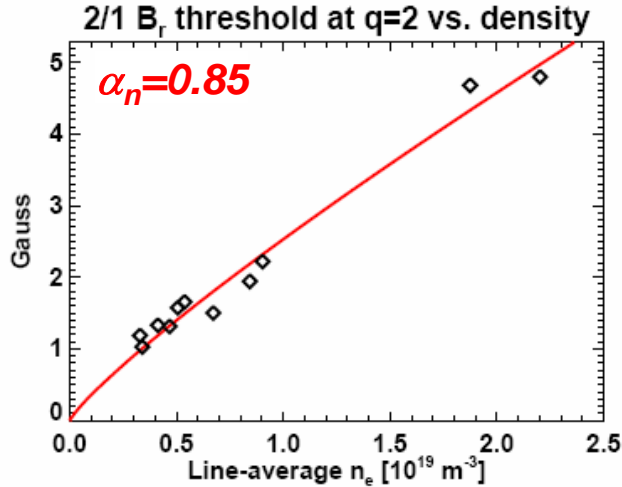


Density and B-field scalings are sensitive to choice of q-scaling variable, but, assuming size scaling coefficient $\alpha_R = 2\alpha_n + 1.25(\alpha_B - 1) \rightarrow$ NSTX $\alpha_R = 0.45$ to 0.56

NSTX locking data shows nearly linear density scaling, weak positive B_T dependence, and nearly linear scaling with internal inductance



$2/1 B_r$



Density and B-field scalings are sensitive to choice of q -scaling variable:
 Range in NSTX: $\alpha_R = 0.45$ (q_{95}), $\alpha_R = 0.56$ (q' at $q=5$), $\alpha_R = 0.8$ (I_i)

Large extrapolation from NSTX to ITER, but here it is...



For NSTX q_{95} scaling with:

$$n_e = 10^{19} \text{m}^{-3}, B_T = 5.7 \text{T}, R_0 = 6 \text{m}, \alpha_R = 0.45, q_{95} = 3$$

$$\text{ITER } B_{21} \rightarrow 14 \text{G}, \text{ or } B_{21}/B_T = 2.5 \times 10^{-4}$$

For NSTX I_i scaling with:

$$n_e = 10^{19} \text{m}^{-3}, B_T = 5.7 \text{T}, R_0 = 6 \text{m}, \alpha_R = 0.8, I_i = 1.0$$

$$\text{ITER } B_{21} \rightarrow 30 \text{G}, \text{ or } B_{21}/B_T = 5.2 \times 10^{-4}$$

Caution – no $q=1$ surface in NSTX plasmas which could lower thresholds in ITER (and NSTX)

Also need to propagate uncertainties through analysis properly...

IPEC analysis not yet systematically included in scalings



- IPEC analysis shows that total B_{\perp}^{mn} (including plasma response) on resonant surfaces differs significantly from vacuum external B_{\perp}^{mn}
 - So how did we account for intrinsic error field in NSTX if plasma response is important, and we didn't include it?
- Empirically find that different normalization for B_{\perp}^{mn} can improve accounting for EF using only vacuum fields:

– Instead use perturbed helical flux:
$$\delta\psi_{mn}^h = \sigma \left[R^3 \left| \frac{q}{F} \right| (B_Z \delta B_R - B_R \delta B_Z) \right]_{mn}$$

Where σ is a polarity and phase factor and $F = B_{\phi} R$

– $\delta\psi^h$ scales as $R^2 |\nabla\psi| q/F B_{\perp}^{mn}$

R^2 scaling of $\delta\psi^h$ apparently provides better geometric representation of fields that generate singular currents, torques, and mode locking

ALL NSTX DATA SHOWN ABOVE USES RENORMALIZED VACUUM $\delta\psi^h$ to compute $\delta B_{2/1}$

