

KSTAR Equilibrium Operating Space, H-mode Dynamics, and Projected Stabilization at High Normalized Beta^{*}

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NSTX Monday Physics Meeting

March 14th, 2011



Collaborative research on KSTAR equilibrium and global MHD stability

Scope of this collaborative research

- Support KSTAR experimental/theoretical equilibrium analysis
- Study on global MHD mode & rotation control physics for high beta operation regime
- Examine the edge localized mode (ELM) mitigation potential by resonant magnetic perturbations (RMP)

Research addressed in this talk

- □ Equilibrium reconstruction
 - EFIT code including theoretically estimated vessel current from VALEN-3D calculation
 - Equilibrium operating regimes of 2009 and 2010 KSTAR discharges
- Passive and active stabilization of resistive wall mode (RWM)
 - Kinetic modification of RWM stability by MISK calculation, which has been successfully used in NSTX
 - Passive stabilizing plate design to maximize RWM passive stabilization (finalized design applied to the passive stabilizing plates installed in 2010)
 - Power requirements for RWM active stabilization using IVCC including noise effect
- ELM suppression by RMP
 - TRIP3D calculations to evaluate vacuum island overlap created by RMP using a combination of all poloidal IVCC sectors with dominant n = 2 field spectrum
 - Appropriate RMP condition for 2011 XP in terms of coil parity and *q*-profile

EFIT model for reconstruction of 2009-10 KSTAR discharges



KSTAR configuration used in equilibrium reconstruction (12 vessel current groups are indicated by regions of different colors)

EFIT setup/input

- 14 PF currents, 67 (57) magnetic probes, 5 flux loop voltage monitors, 0 (5) flux loops,1 Rogowski coil are used as constraints *Numbers in parenthesis are for 2010 reconstruction
- Simple plasma basis function model is used for reliable reconstruction with lack of internal measurements

Vessel current estimation in EFIT

- Vessel current is represented as 12 independent current carrying groups
- Effective vessel group resistances from a VALEN-3D code startup calculation are used to estimate vessel currents



Vessel currents in VALEN-3D startup calculation

Allowance for ferromagnetic Incoloy effect in reconstruction

EFIT vacuum field reconstruction for shot 1845 by using different PF errors (low error : σ_{rel} = 0.5%, high error : as shown in table below) 2500 PF1U Current (A/turn) - · - Measured Current (A/turn) --- Measured 2000 2000 EFIT with low PF error EFIT with low PF error EFIT with high PF error EFIT with high PF error 1500 1500 1000 1000 500 PF2U (500 PF1U PF2U n -0.2 0.0 0.2 -0.4 0.2 0.4 0.6 -0.4 -0.2 0.0 0.4 0.6 3500 3500 (A/turn) (A/turn) 3000 --- Measured 3000 --- Measured EFIT with low PF error EFIT with low PF error 2500 2500 EFIT with high PF error EFIT with high PF error 2000 Current Current 2000 1500 1500 1000 1000 PF3U PF4U PF4U PF3U 500 500 0 0 0.0 0.2 0.4 0.6 -0.2 0.0 0.2 -0.4 -0.2 -0.4 04 0.6 1000 200 Total Vessel Current (kA) 175 PF5U Current (A/turn) --- Measured - - - Measured 750 EFIT with low PF error 150 EFIT with low PF error EFIT with high PF error EFIT with high PF error 125 500 100 250 75 Vessel PF5U 50 ma current 25 -250 0 0.0 -0.4 -0.2 0.2 0.4 0.6 -0.2 0.0 0.2 -0.4 04 0.6 0 50 MP4P18R B-field (G) B-field (G) — · — Measured — • — Measured -50 EFIT with low PF error EFIT with low PF error -50 EFIT with high PF error EFIT with high PF error -100 -100 -150 MP4P20Z -150 -200 **MP4P20Z** -200 **//P4P18**R -250 -250 -300 -0.4 -0.2 0.0 0.2 0.4 0.6 -0.4 -0.2 0.0 0.2 0.4 0.6 Time (s) Time (s)

Incoloy materials in KSTAR coils

- Conduit conductor of TF and some of PF coils (PF1-5) include ferromagnetic Incoloy material (magnetic permeability ≈ 10)
- Magnetic nonlinearity causes certain inconsistencies between measured and reconstructed signals

Increased PF error reasonably allows for Incoloy effect

- PF1-2 are found to carry most of the compensating currents
- The discrepancies in vessel current and MPs are mostly balanced by this change

PF1UL	PF2UL	PF3UL	PF4UL	PF5UL	PF6UL	PF7UL
8%	10%	4%	3%	1.5%	1%	1%

Relative errors set on PF coils for reasonable allowance for paramagnetic Incoloy effect

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Reconstruction result: shot 2048 reached maximum W_{tot} in 2009

Shot 2048 reached plasma stored energy, W_{tot} = 54 kJ, which is the maximum value among the 2009 discharges



Fast framing camera image and reconstructed equilibrium flux surfaces at t = 2.3 sec for shot 2048

Plasma is downshifted in most of the reconstructed equilibria, which may due to additional current flowing in the bottom of cryostat (S.W. Yoon, IAEA 2010, EXS/5-1)



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View of KSTAR in-vessel structure completed in 2010



Equilibrium configurations were mostly LSN in 2010

- Equilibria in 2010 were mostly in LSN configuration and DN was transiently achieved during vertical movement of plasma
- Reconstructed boundaries from EFIT are very consistent with fast camera image



Fast framing camera image and reconstructed equilibrium flux surfaces at t = 1.73 sec for shot 4358 (time of maximum W_{tot} in 2010)



Fast framing camera image and reconstructed equilibrium flux surfaces at t = 1.66 sec for shot 4202 (time of maximum transient kappa in 2010)

Reconstruction of H-mode discharges in 2010



Equilibrium operating space of 2009-10 discharges

2011 XP



Equilibrium operating regime drawn in (I_{i}, β_N) space explored by 2009-10 discharges

- black : 2009 ohmic circular discharges (18 shots)
- red : 2010 ELMy H-mode discharges (24 shots)
- green : 2010 ELM-less discharges (9 shots)



Plasma elongation vs. internal inductance of elongated equilibria in 2010 (27 shots)

Summary of equilibrium records for 2009-10 discharges

	2136	2074	2048	1924	2155
I_P	361 kA	285 kA	337 kA	139 kA	290 kA
β_N	0.62	0.99*	0.73	0.32	0.68
l_i	0.84	0.92	0.89	0.84	0.85
W_{tot}	48 kJ	44 kJ	54 kJ	9.5 kJ	35 kJ
К	1.04	1.03	1.03	1.08	1.03
t_{pulse}	3.69 s	3.63 s	3.62 s	1.50 s	4.05 s

Shot number

2009 near-circular, ohmic discharges



	4340	4358	4202	4445
I_P	693 kA	587 kA	575 kA	332 kA
β_N	0.44	1.34	1.09	0.41
l_i	1.02	1.11	1.10	1.18
W_{tot}	72 kJ	258 kJ	228 kJ	63 kJ
K	1.83	1.79	1.85	1.78
t _{nulse}	3.62 s	3.21 s	1.83 s	6.69 s

2010 elongated, beam-driven discharges

<u>Those are representative values during current flattop.</u> *The higher β_{N} of shot 2074 is due to the steady I_P decrease around t = 2.3 s.

Kinetic stabilization of RWM in KSTAR being analyzed using a physics model successfully used in NSTX



- Stability modification depends on
 - Integrated ω_{ϕ} profile: resonances in δW_K (e.g. ion precession drifts)
 - Particle collisionality
- Plasma is stable when rotation is in resonance
 - \Box *l* = 0 harmonic : resonance with precession drift frequency
 - \square *l* = -1 harmonic : resonance with bounce frequency

 $\omega_{E} + \langle \omega_{D} \rangle = 0$ $\omega_{E} - \omega_{b} = 0$ key resonances

MISK calculation for KSTAR theoretical equilibrium

- MISK (Modification of Ideal Stability by Kinetic theory) code is used to calculate kinetic modification of RWM stability in KSTAR
- □ Target KSTAR equilibrium:
 - A theoretical equilibrium with $\beta_N = 4.0$, $l_i = 0.7$ and H-mode pressure profile ($n_e = n_i$, $T_e = T_i$)
 - Rotation profile similar to NSTX (all co-directed beams)
- Results:
 - □ The steep edge gradient of the target equilibrium causes a large ion diamagnetic frequency and a large negative *ExB* frequency near the edge
 - □ For the chosen profile ($\omega_{\phi 0}$ = 10 kHz), the trapped thermal ion precession drift resonance is insufficient in the outer surface where the RWM eigenfunction is large



RWM stability diagrams for KSTAR and NSTX



(a) Stability diagram for theoretical $\beta_N = 4.0$ KSTAR equilibrium with varied rotation profiles with $\omega_{\phi 0}$ from 0~60 kHz and (b) for NSTX shot 121083 at t = 0.475 s. The experimental point labeled "32.0" is close to marginal stability

- Stability diagram: contours of constant $\gamma \tau_w$ for varying rotation profile magnitude
- Compared to NSTX, KSTAR requires higher rotation for kinetic stabilization of RWM
 - Due to the lack of resonance in the outer region of the plasma, relatively large rotation $\omega_{\phi 0} \sim 42$ kHz is required for stability with $T_0 =$ 13 keV, $n_0 = 1.3 \times 10^{20}$ m⁻³ and $\omega_{\phi 0} \sim 34$ kHz with $T_0 = 10$ keV, $n_0 = 1.7 \times 10^{20}$ m⁻³



KSTAR passive stabilizing plate design was finalized to maximize RWM passive stabilization

- Passive stabilizing plate design was finalized and installed in 2010 after considering the impact of materials (SS vs. Cu) and electrical connections on RWM growth rates
 - The final design utilizes Cu plates, each having 4 toroidal high resistance breaks and current bridges were eliminated due to the increased potential for error fields
 - Copper plates reduce the RWM growth rate by a factor of 15 compared to SS at $\beta_N = 4.5$



FECs) with surrounding conductive casing in VALEN model

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4 toroidal cuts (red)

RWM feedback phase scan and resulting mode growth rate with different feedback gains

- Unstable *n* = 1 eigenfunction from DCON for a theoretical equilibrium with $\beta_N = 5.0$, $l_i = 0.7$ and H-mode pressure profile is used in VALEN code growth rate calculations
- Middle-FEC coil with SS casing is used for RWM active stabilization



Variation of real and imaginary values of growth rate which denote amplitude and rotation of the mode, respectively vs. feedback phase

A stable feedback phase between B_p sensor set and control coil voltages is found



Mode growth rate vs. β_N with different feedback gains

- Plasma can be stabilized up to with-wall limit $(C_{\beta} = 99\%)$ predicted by DCON with controller gain $G_{\rho} = 2$ V/G and stable FB phase
- □ Conductive casing of IVCC shows a small degradation of control performance, which results in the reduction of C_β by ~5%

Time domain RWM active stabilization calculation for stable feedback phase

- Ideal control system without noise or time delay is assumed
- Stable feedback phase is used for an equilibrium having β_N = 4.8 (C_β = 98%) with G_p = 2 V/G
- Feedback starts when mode amplitude becomes 10 G
- RWM amplitude becomes less than 1 G and mode rotation is clockwise during feedback



RWM amplitude and phase during feedback stabilization with stable feedback phase

Polar plot of RWM behavior during feedback

Ideal power requirements for RWM active stabilization



3.7

387.5

3.7

 $R = 44 \text{ m}\Omega$ L/R = 1 ms

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 $P_{RMS}(W)$

387.5

Required feedback control power increases due to sensor noise, but remains at reasonable levels

Approach

- Allow passive growth of RWM to 10 G then start feedback with 10 kHz, 2 ~ 10 G white noise in mode detection sensors (8 midplane B_p sensors)
- Same RMS time interval: 20 x RWM growth times = 39 msec



Total RMS power of IVCC vs. sensor noise level 7.68 kW

4.41 kW

2.38 kW

8

3.11 kW

10

- Unloaded IVCC with 2 G white noise
- Feedback & noise start when mode becomes 10 G
- Direct experience of PS needs from NSTX and DIII-D
- Presently a key consideration for n = 1 feedback in ITER

Potential for ELM mitigation by RMP from IVCC: Even parity is more favorable for resonance pitch alignment

- The TRIP3D code is used to calculate RMP spectrum pitch alignment with a theoretical equilibrium having q_{95} = 3.6 and β_N = 2.5 with an experimental H-mode pressure profile
- A combination of all poloidal IVCC sectors (top, middle, bottom IVCCs) is used

Odd parity (top, middle, bottom IVCCs) = (+12, 0, -12) kA



Even parity (+8, -8, +8) kA

- Odd parity has relatively lower *m*-spectrum caused by utilizing only 2 poloidal IVCC sectors
- □ The perturbation is not efficiently coupled to *q*-profile and perturbs more into the core
- Resonant field spectrum is localized around the plasma edge, higher *m*-spectrum aligns better with *q*-profile

Poloidal Mode Number (m)

- The amount of middle-FEC current can change the applied *m*-spectrum
- □ Favorable to make a pitch alignment with elevated *q*-profiles

Island overlap created by the odd and even parity RMPs



Even parity fulfills the vacuum Chirikov criterion for equilibria expected in 2011 XP

- □ Use theoretical equilibria having $B_T = 2.0$ T, $\beta_N = 1.5$, $I_i = 1.0$ with different I_P to vary the *q*-profile
- The maximum allowable currents in 2011 XP (4 kAt) are applied to all poloidal IVCC sectors



□ Only even parity fulfills the Chirikov criterion for the target equilibria spanning $B_T = 2$ T and 0.8 < I_P (MA) < 1.1 by using the planned IVCC current in 2011

Conclusions

- Experimental equilibria of 2009-10 discharges were reconstructed using the EFIT code, including theoretically estimated vessel current and reasonable allowance for Incoloy effect.
- Equilibrium operating space much broadened in 2010 and reconstruction of achieved H-mode gave us useful guidance to understand underlying dynamics.
- Kinetic modification of MHD stability calculated by the MISK code indicates that significant rotation may be required to obtain RWM stability. Further analysis of profile variations, use of measured kinetic and rotation profiles will be made.
- A design of the passive stabilizing plates was finalized to have maximum RWM passive stabilization, and a time dependent RWM control simulation showed the mode can be stabilized with reasonable levels of feedback control power and increased power demands caused by sensor noise were also confirmed.
- The ELM mitigation potential is analyzed using the TRIP3D code, and higher mspectrum from up-down even parity configuration would be better to obtain favorable pitch alignment for 2011 XP.

Backup Slides

Structure/Connection of KSTAR IVCC

