



# First time realization of a detached, stable, efficient particle and heat exhaust regime in the island divertor of Wendelstein 7-X

**Oliver Schmitz**<sup>1</sup>, Y. Feng<sup>2</sup>, M. Jakubowski<sup>2</sup>, R. Koenig<sup>2</sup>, M. Krychowiak<sup>2</sup>, M. Otte<sup>2</sup>, F. Reimold<sup>2</sup>, G. Anda<sup>3</sup>, T. Barbu<sup>1</sup>, C. Biedermann<sup>2</sup>, S. Bozhenkov<sup>2</sup>, S. Brezinsek<sup>4</sup>, B. Buttenschon<sup>2</sup>, K.J. Brunner<sup>2</sup>, P. Drewelow<sup>2</sup>, F. Effenberg<sup>1</sup>, D. A. Ennis<sup>5</sup>, T. Estrada<sup>4</sup>, E. Flom<sup>1</sup>, H. Frerichs<sup>1</sup>, O. Ford<sup>2</sup>, G. Fuchert<sup>2</sup>, Y. Gao<sup>4</sup>, D. Gradic<sup>2</sup>, O. Grulke<sup>2</sup>, K. C. Hammond<sup>2</sup>, U. Hergenhan<sup>2</sup>, U. Höfel<sup>2</sup>, J. Knauer<sup>2</sup>, P. Kornejew<sup>2</sup>, G. Kocsis<sup>3</sup>, T. Kremeyer<sup>1</sup>, S. Kwak<sup>2</sup>, H. Niemann<sup>2</sup>, E. Pasch<sup>2</sup>, A. Pavone<sup>2</sup>, V. Perseo<sup>2</sup>, L. Rudischhauser<sup>2</sup>, G. Schlisio<sup>2</sup>, T. Sunn Pedersen<sup>2</sup>, J. Svensson<sup>2</sup>, T. Szepesi<sup>3</sup>, U. Wenzel<sup>2</sup>, V. Winters<sup>1</sup>, G.A. Wurden<sup>6</sup>, D. Zhang<sup>2</sup>, S. Zoletnik<sup>3</sup> and the W7-X experiment team

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**Acknowledgement:** This work was funded in part by the U.S. Department of Energy under grant DE-SC00014210 and DE-SC00013911 and has been carried out within the framework of the EUROfusion Consortium with funding from the Euratom research and training program 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.

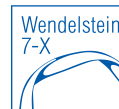
**Princeton Plasma Physics Laboratory**

**FES seminar**

**December 10, 2019**



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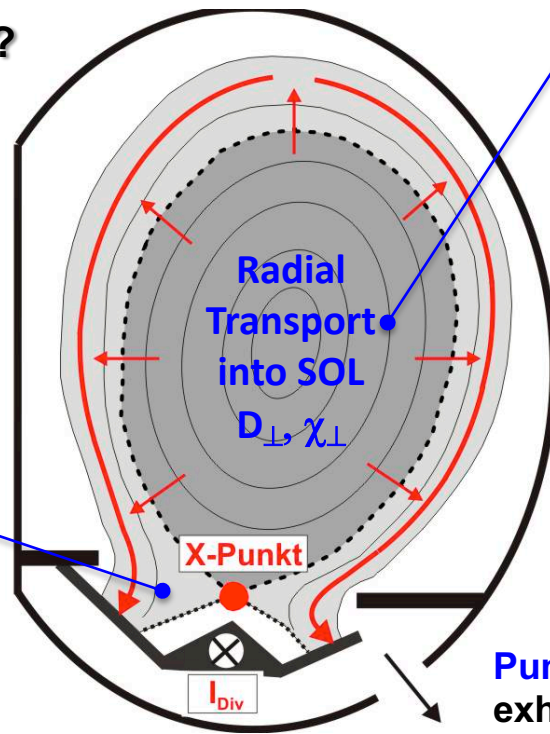
# Heat flux detachment and a low level of eroding particle fluxes need to be combined with sufficient particle exhaust in a successful divertor concept



- **What's a divertor supposed to do?**

**Divertor plasma** defines plasma wall interface

- Heat and particle flux handling within technical limits
- Power dissipation
- Neutral compression
- Impurity retention



**Plasma core** performance is to be maximized

- Stable density control
- Low impurity influx ( $Z_{\text{eff}}$ )
- Helium exhaust ( $\tau_{p,\text{He}}^*/\tau_E$ )

**Pumping system:** stable particle exhaust needs sufficient  $p_n$

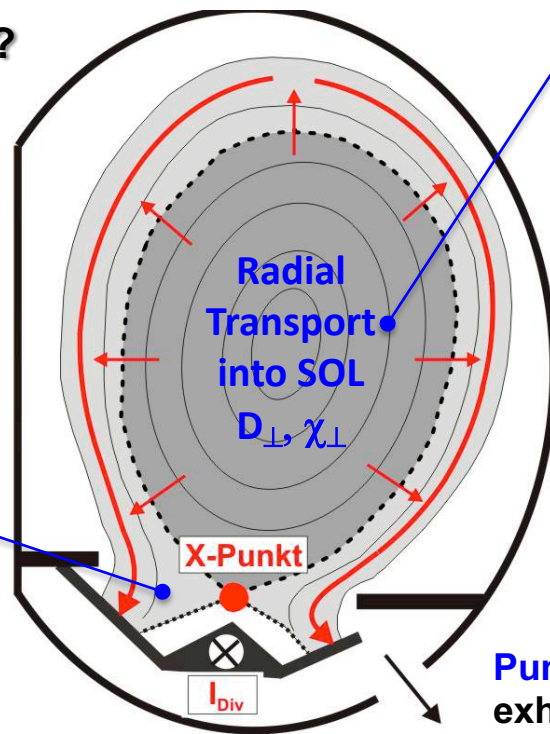
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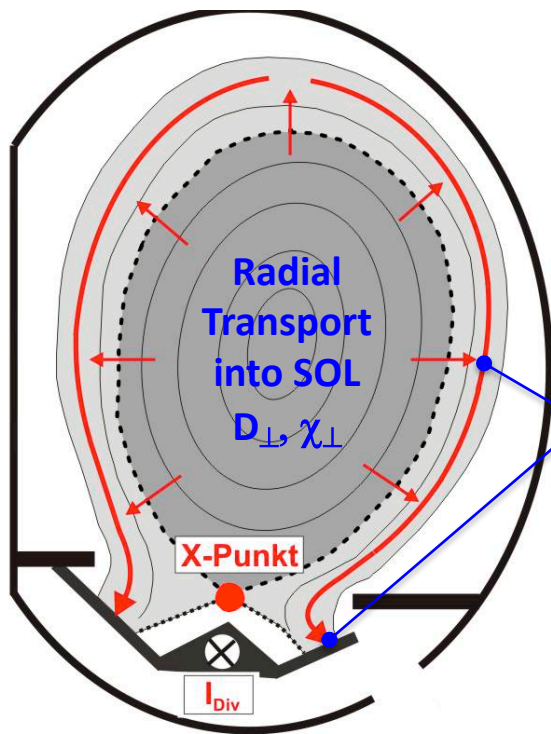
**Upstream**  
where particle and heat flux come from (separatrix region)

**Pumping system:** stable particle exhaust needs sufficient  $p_n$

**Downstream**  
where particle and heat flux go to (divertor targets)

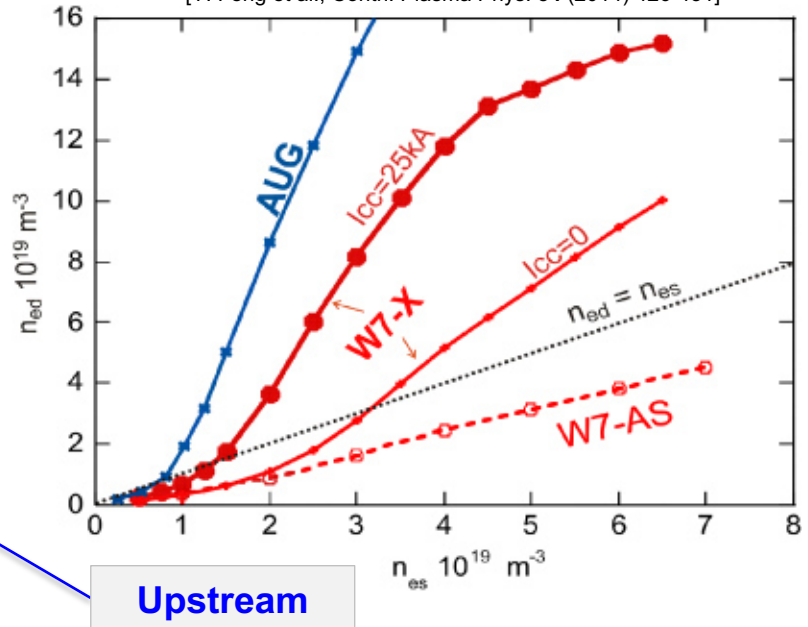


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[Y. Feng et al., Contri. Plasma Phys. **54** (2014) 426-431]

Downstream

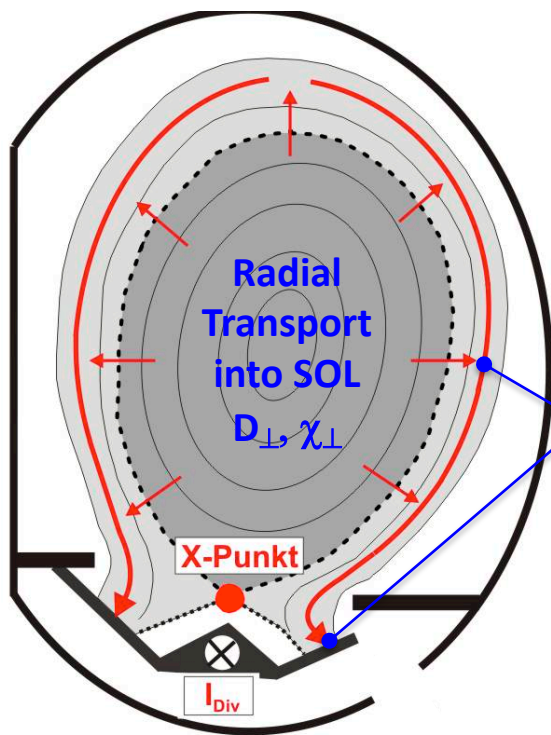


Upstream

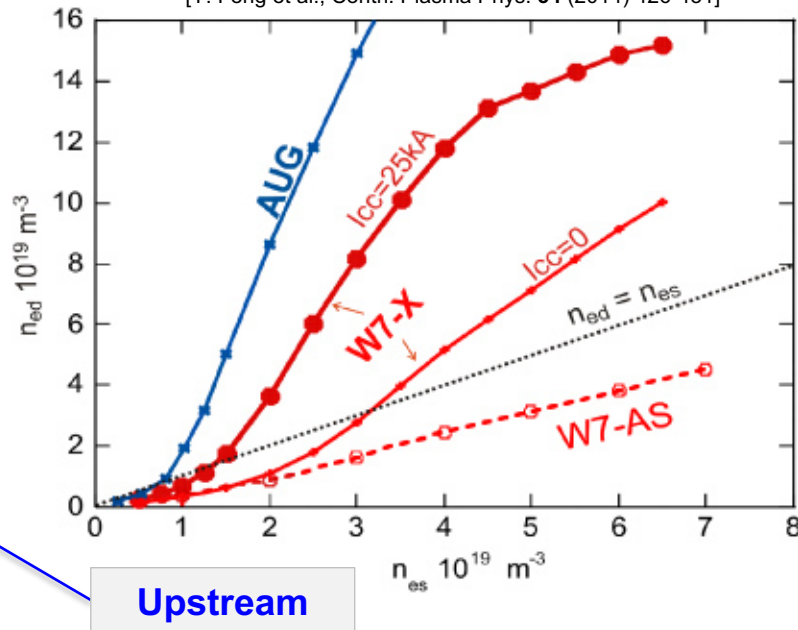
Importance of high  $n_{ed} == \text{high } \Gamma_d ?$



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Ionization energy loss

Energy loss by impurity radiation

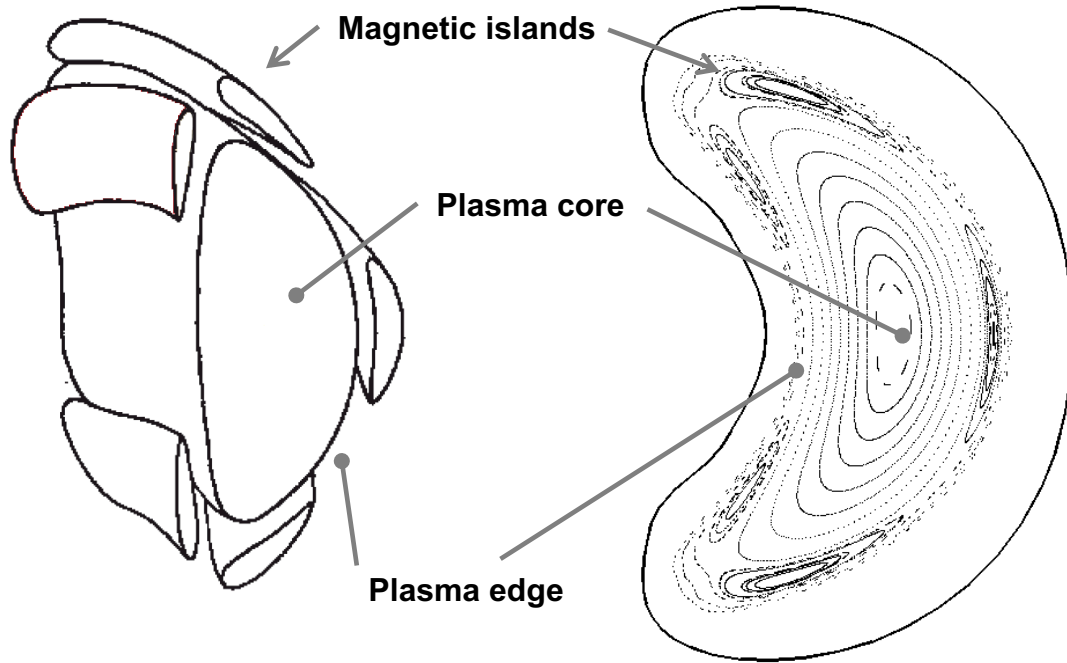
Rapid ionization



# The island divertor at Wendelstein 7-X is a promising helical resonant divertor<sup>1</sup> concept for stellarators



- A low order resonance placed in the plasma edge defines the divertor structure



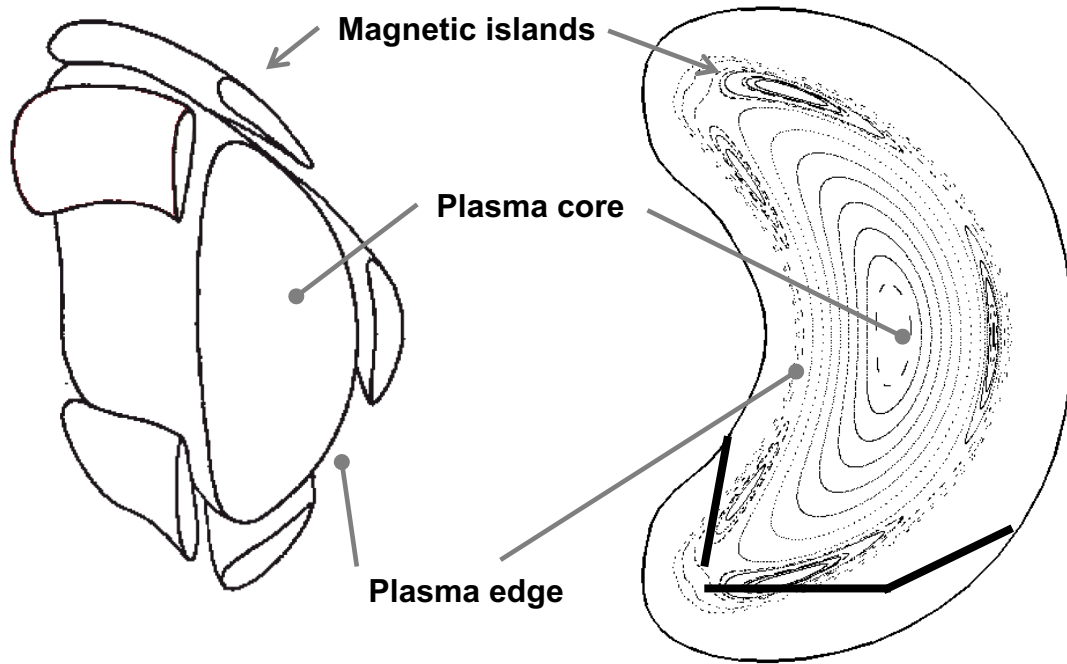
[X. Bonin et al., Nuclear Fusion **45** (2005) 22-29]



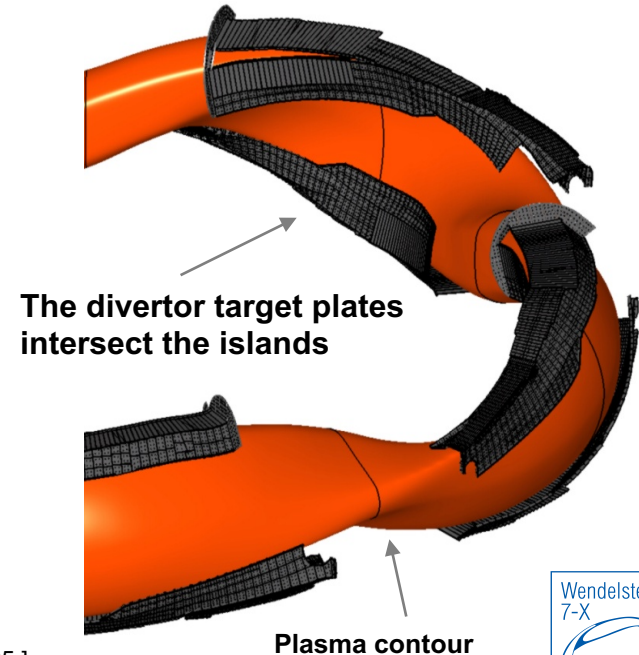
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The Island Divertor is a modular divertor



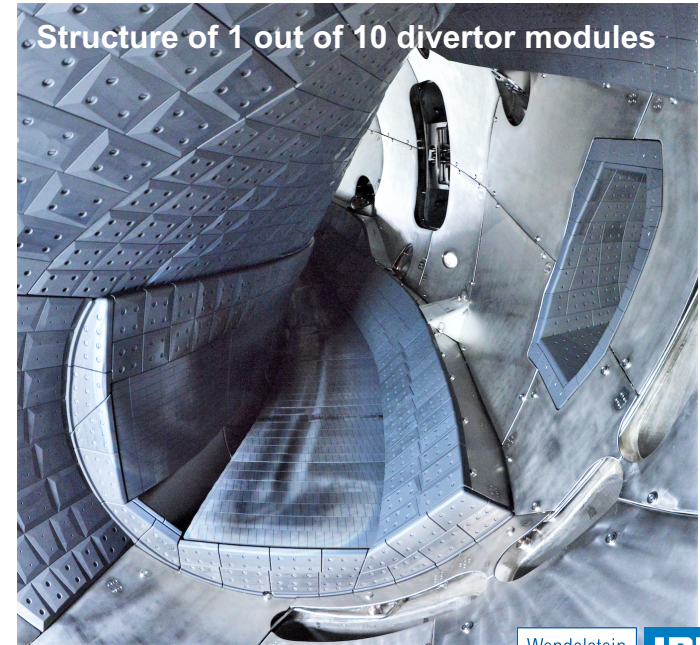
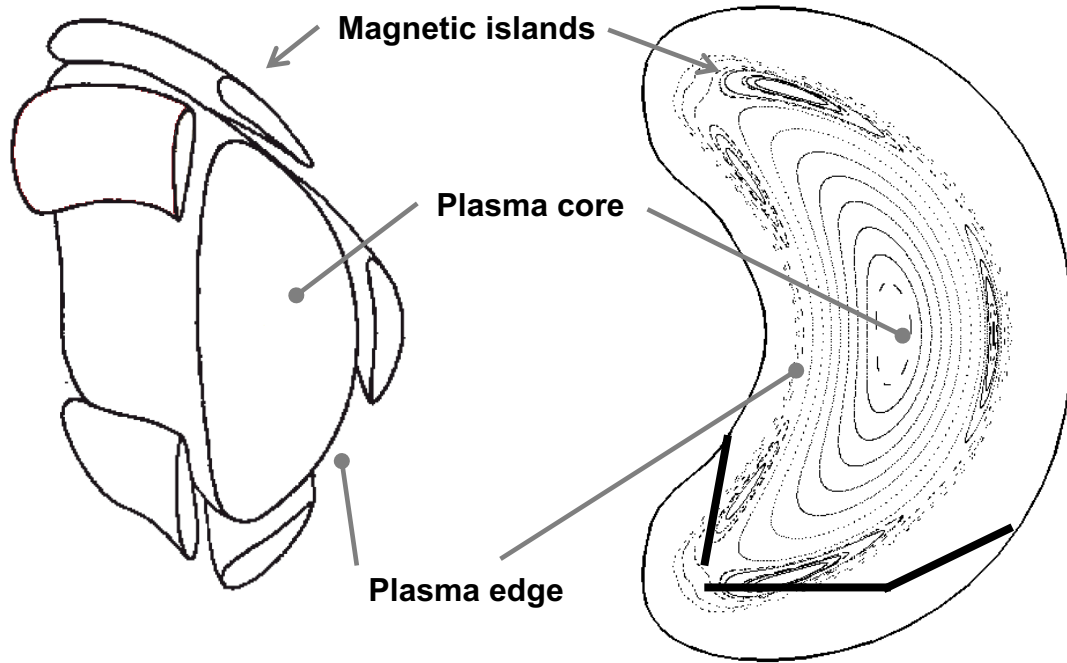
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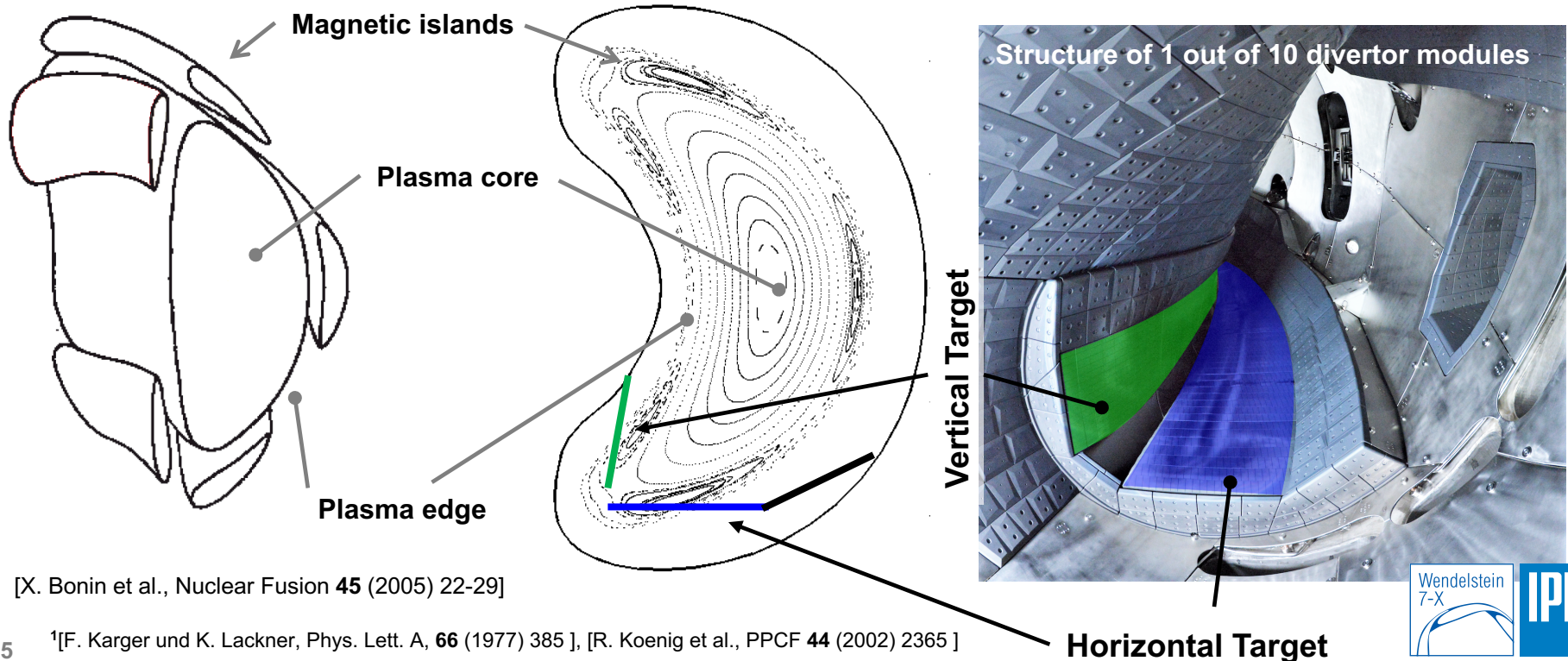
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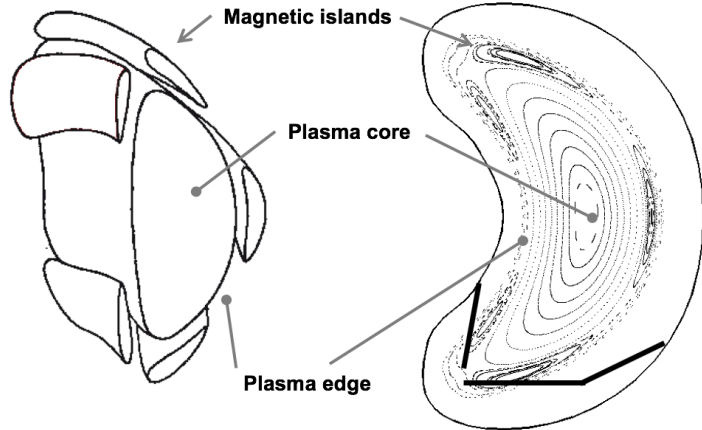
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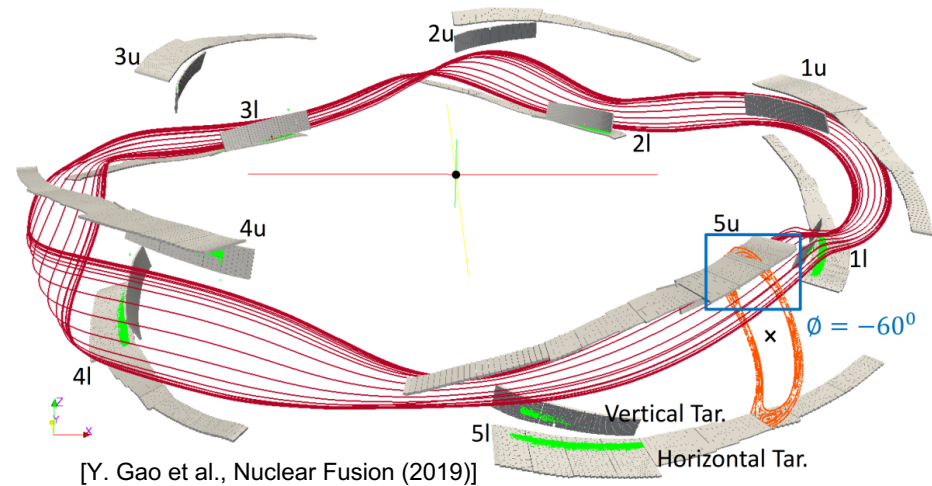
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[Y. Gao et al., Nuclear Fusion (2019)]

**Standard divertor configuration (SDC): pairs of modules 180 degree apart toroidally are connected by magnetic flux tubes**



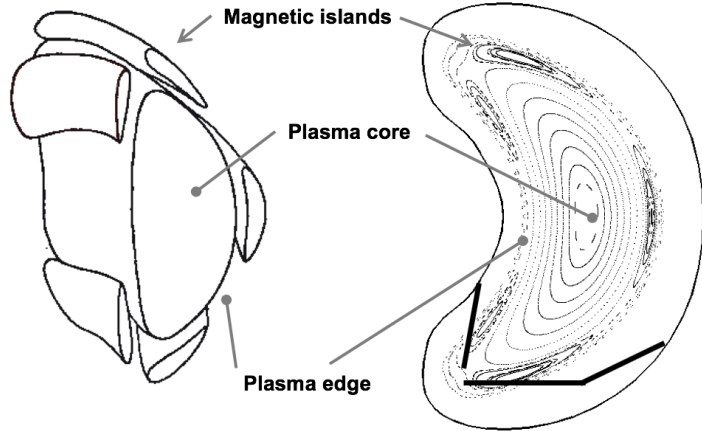
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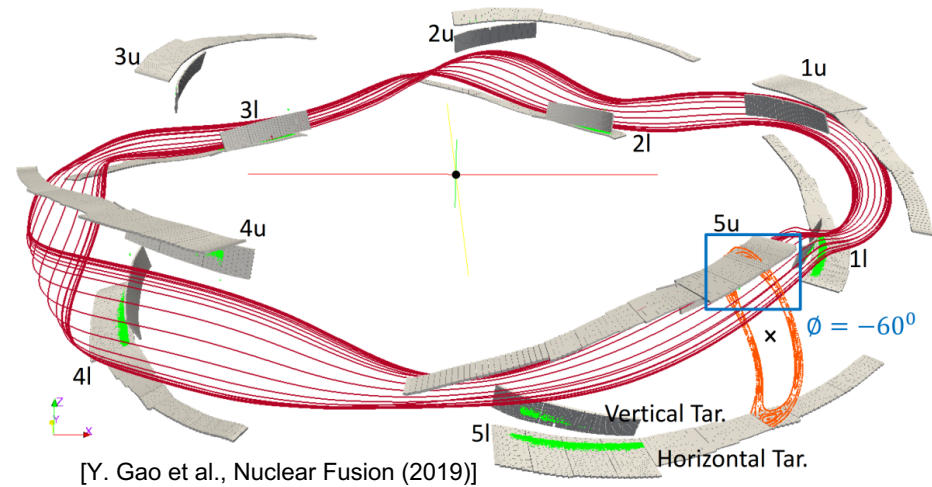
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This divertor concept was tested at W7-AS and now needs to be qualified as a viable stellarator system component for steady state plasma operation.



- A **stable, thermally fully detached island divertor regime with small divertor particle fluxes** but still **sufficient divertor neutral pressures** was shown for the first time.
- This detached island divertor regime is **reached with minimal feedback control in a reliable fashion** and **the divertor operational point is defined through sufficient radiative losses at a given input power.**

The **geometry of the magnetic islands** forming the divertor allow to **fine tune the divertor neutral distribution** for **maximized neutral pressure** in the detached state.

- This island divertor regime is **compatible with steady state particle exhaust** for the upcoming high-performance campaign of W7-X.

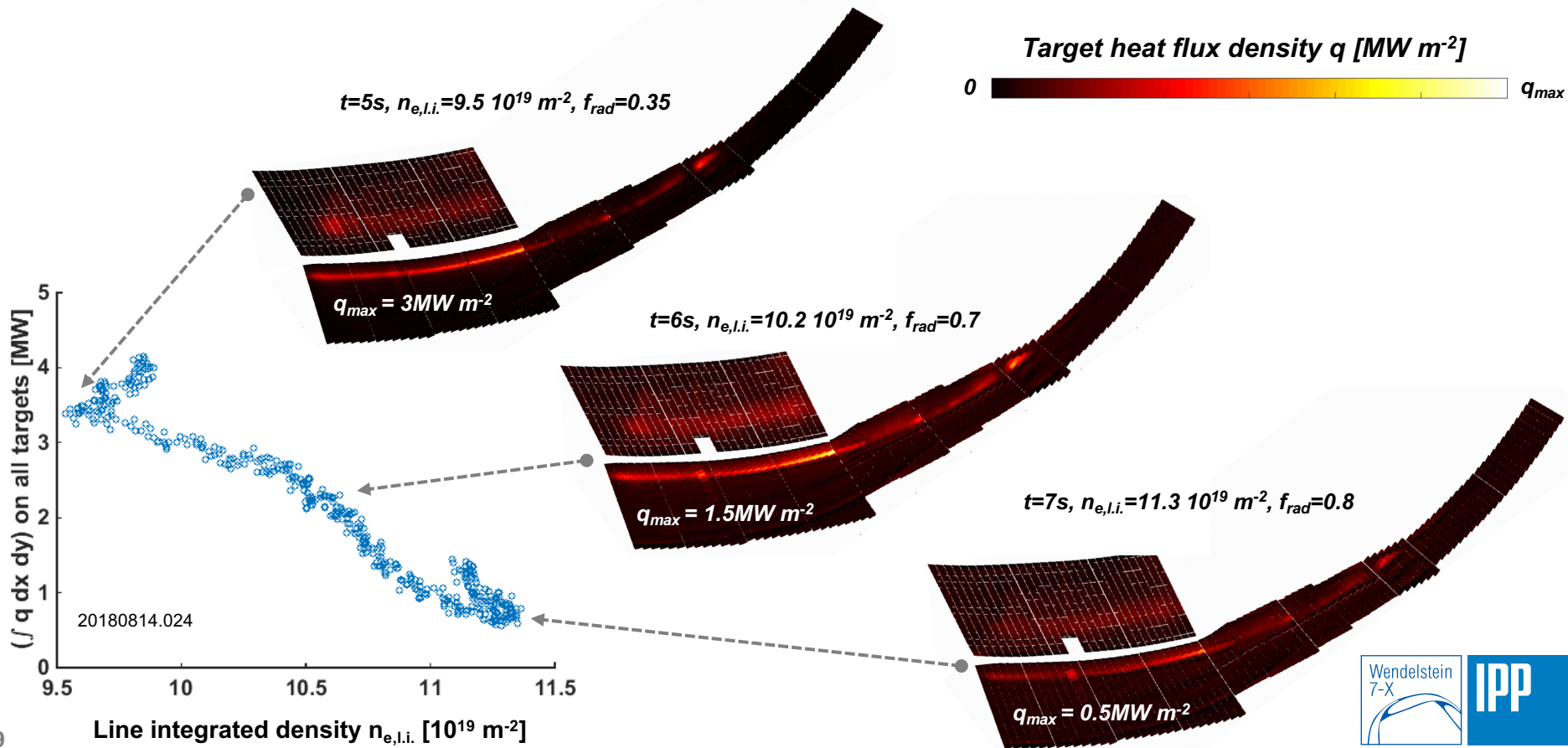


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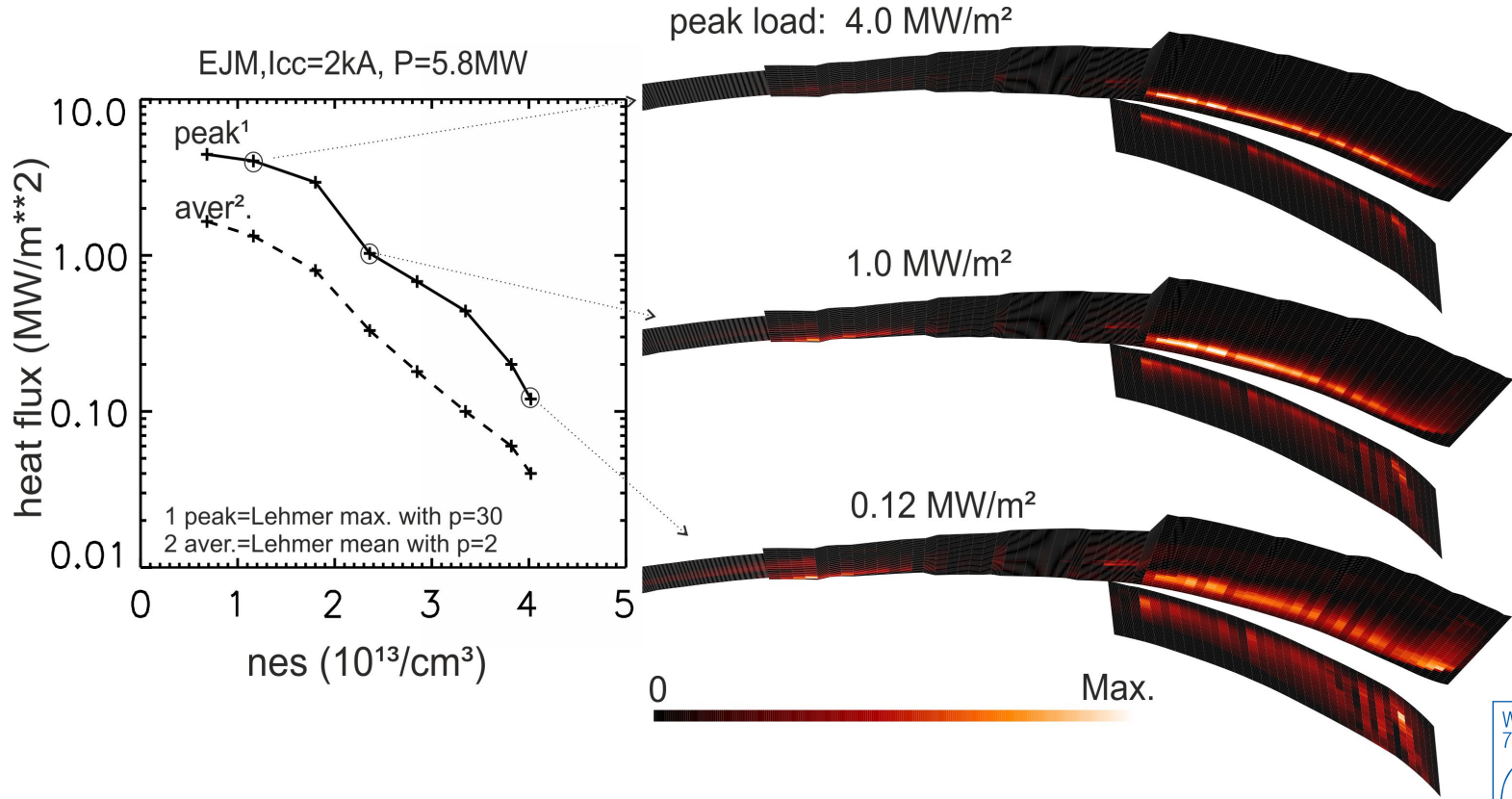
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# Full and homogeneous thermal detachment was obtained during a gradual density increase by just 20% - a reliable access scenario due to $f_{\text{rad}}$ dependence



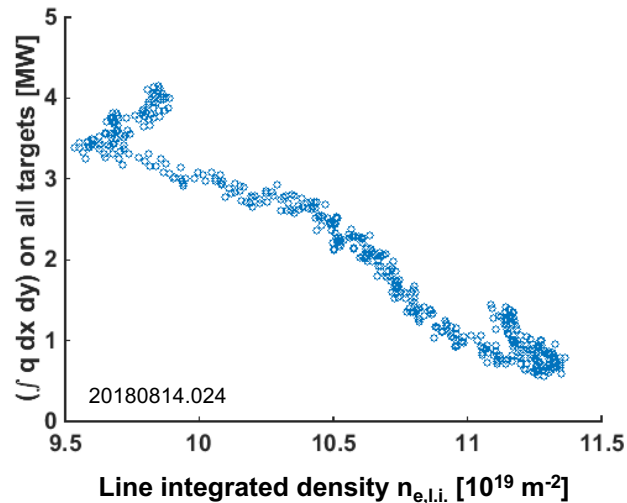
# The homogeneous dissipation of the divertor power load during the density increase is reproduced in EMC3-EIRENE modeling



# The heat flux reduction is driven by a density scaling of $f_{\text{rad}}$ and a complete thermal detachment is combined with significant neutral pressures



**Integral heat flux to targets  
vanishes with increasing density**

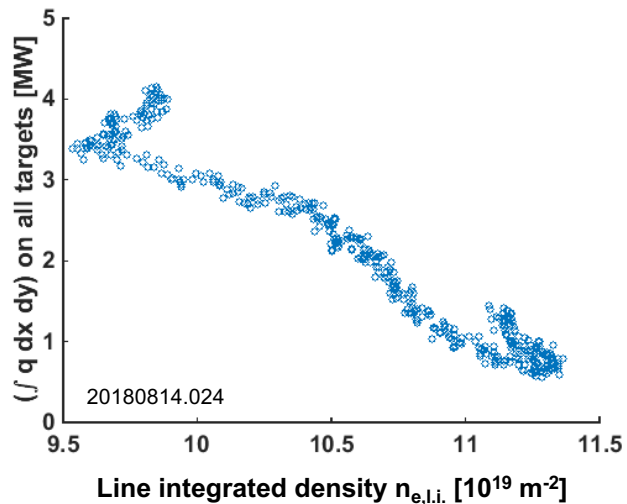




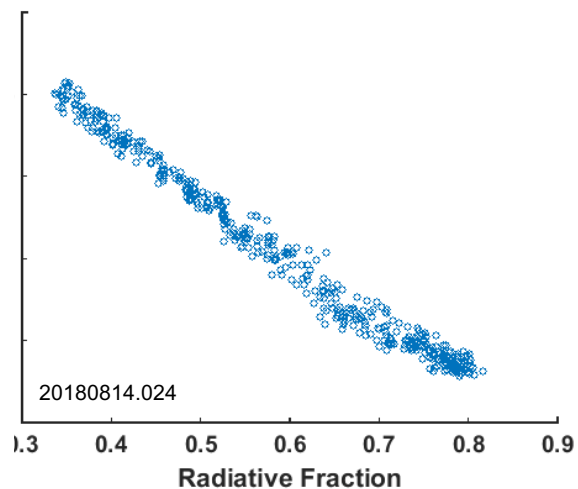
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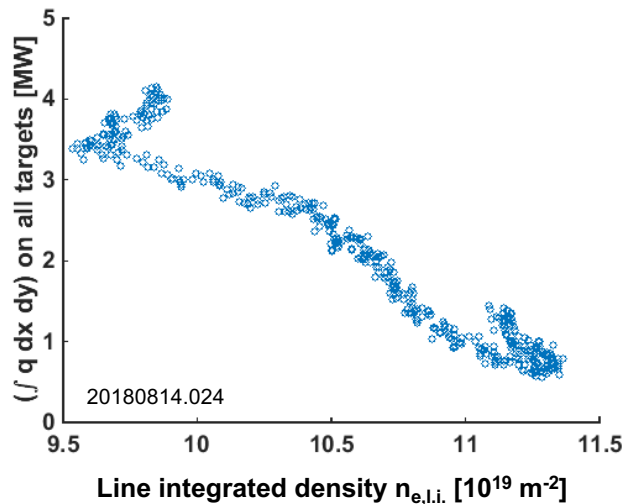
**Radiative fraction drives heat flux dissipation into detached regime**



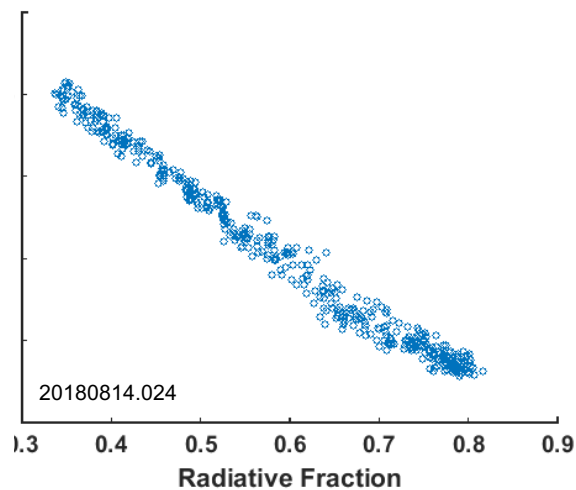
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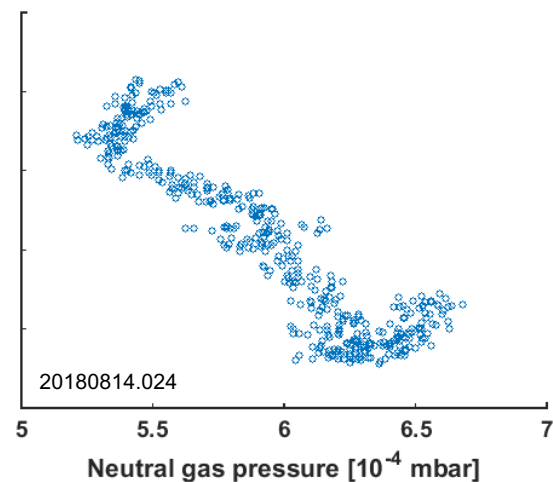
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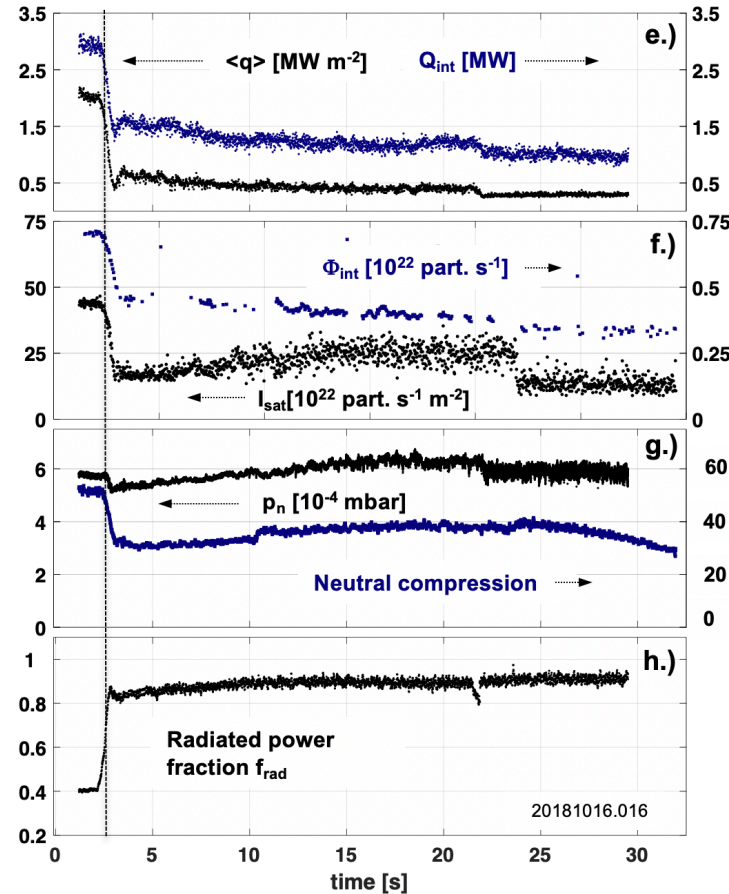
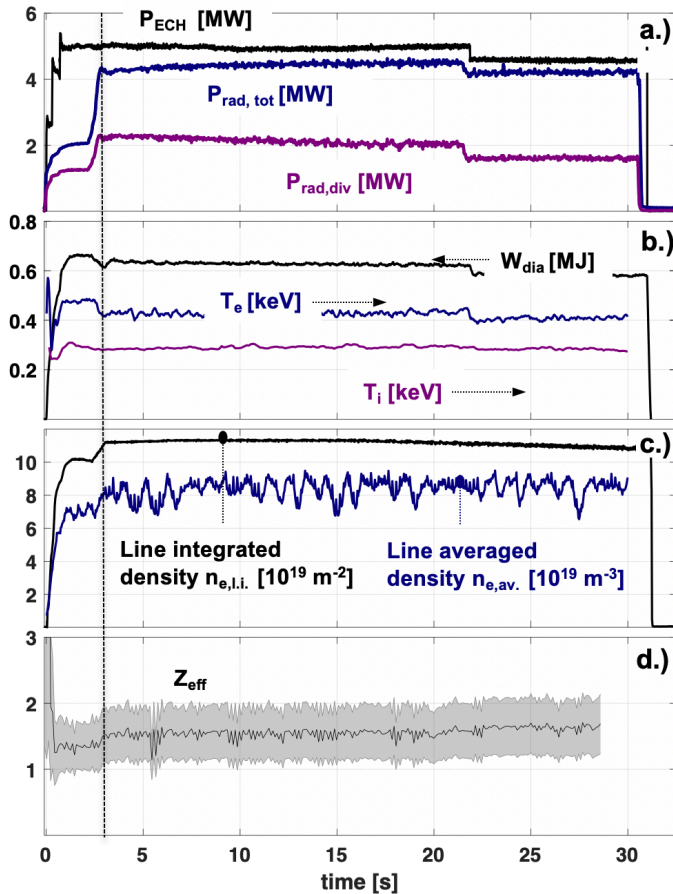


Small heat flux can be combined with significant neutral pressures



A regime of small integral heat flux ( $<0.5 \text{ MW}$ ) and small peak ( $<0.2 \text{ MW m}^{-2}$ ) has been accomplished at up to  $0.05\text{-}0.1 \text{ Pa}$  ( $10^{-3} \text{ mbar}$ ) neutral pressure levels

# This stable detachment was obtained with high divertor neutral pressures for up to 30s only limited by input energy limits in the uncooled divertor phase



# Outline of this talk in form of an executive summary



- A **stable, thermally fully detached island divertor regime with small divertor particle fluxes** but still **sufficient divertor neutral pressures** was shown for the first time.
- This detached island divertor regime is **reached with minimal feedback control in a reliable fashion** and **the divertor operational point is defined through sufficient radiative losses at a given input power.**

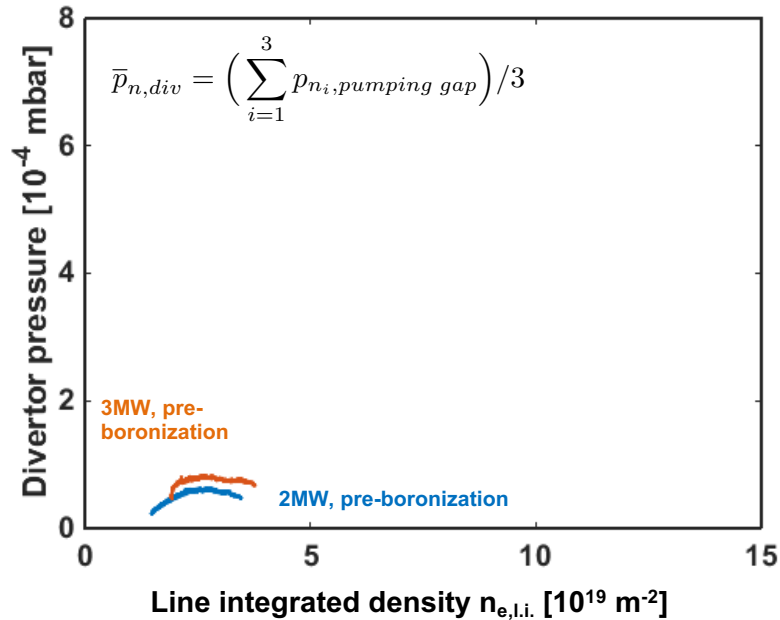
The **geometry of the magnetic islands** forming the divertor allow to **fine tune the divertor neutral distribution** for **maximized neutral pressure** in the detached state.

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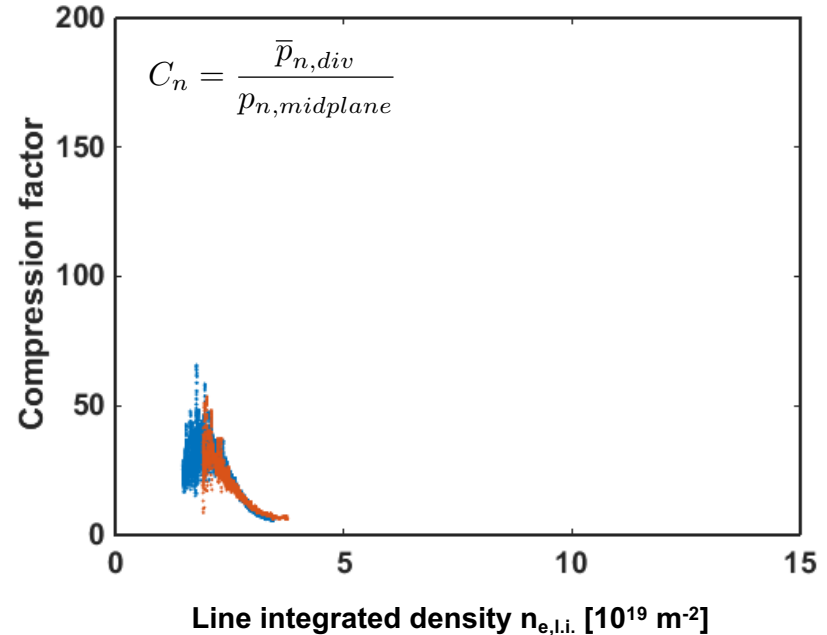
# Moderate divertor neutral pressures within a quite limited density range was seen at W7-X without a boronization



### Averaged neutral particle pressure at pumping gap



### Neutral particle compression in divertor

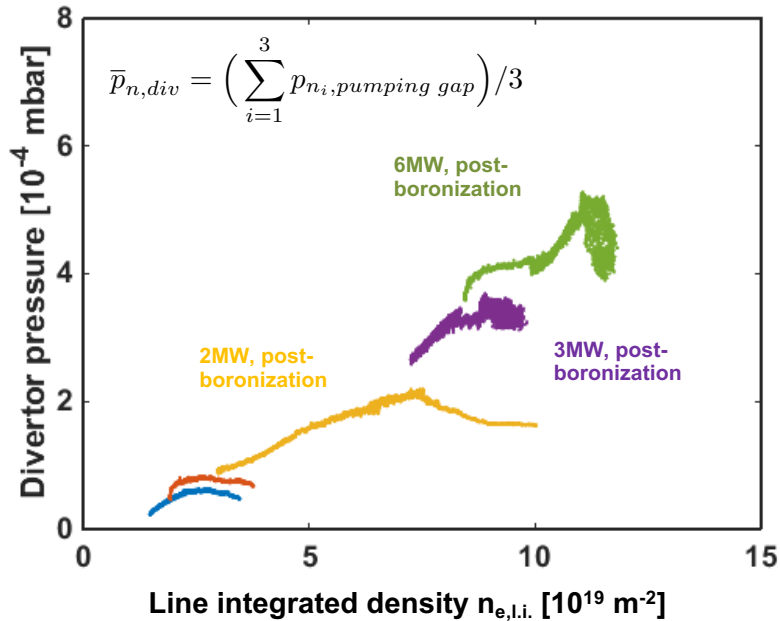


Before boronization: oxygen and carbon were the dominant impurities

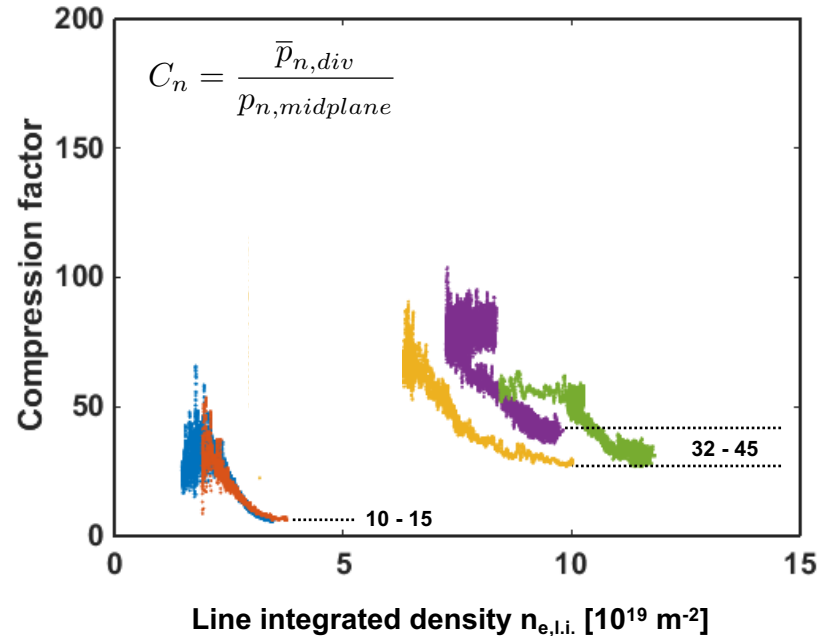
# Boronization of W7-X yielded build up of substantial divertor neutral pressure at largely increased density limits



### Averaged neutral particle pressure at pumping gap



### Neutral particle compression in divertor



After boronization: oxygen content was reduced by up to a factor of 20

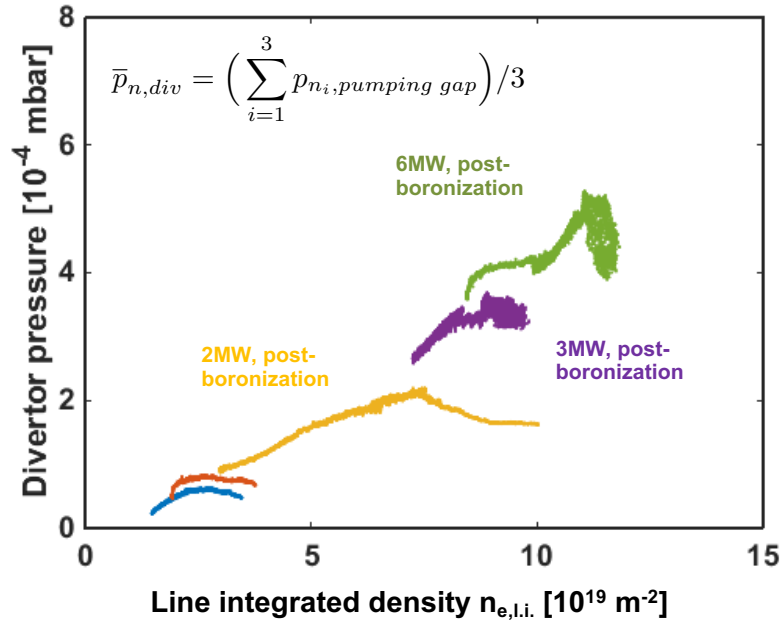




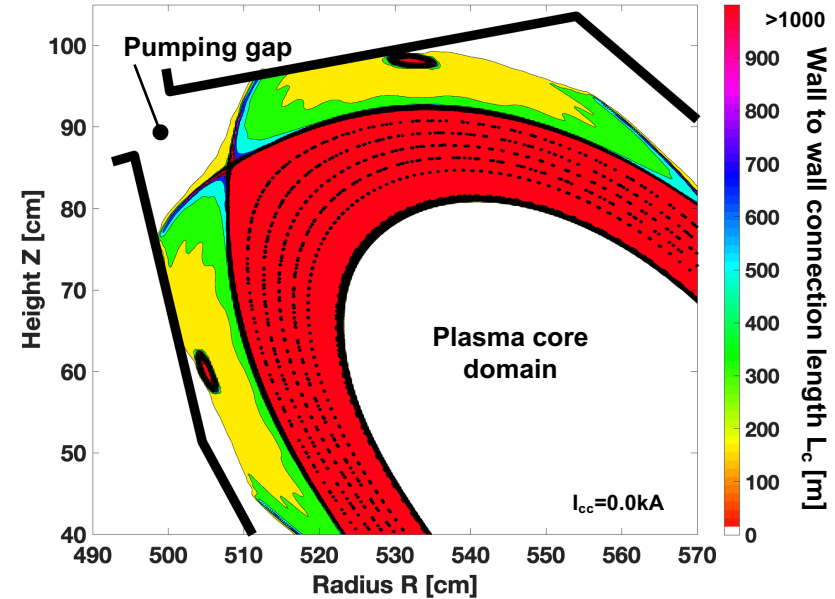
This attractive scenario could be fine tuned by adjustment of the structure of the magnetic island that form the divertor



Averaged neutral particle pressure at pumping gap



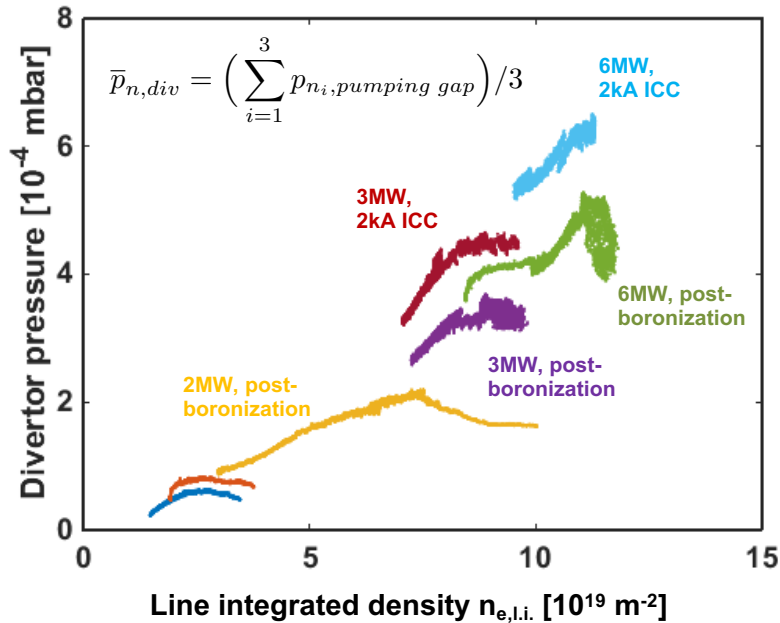
Structure of the magnetic island



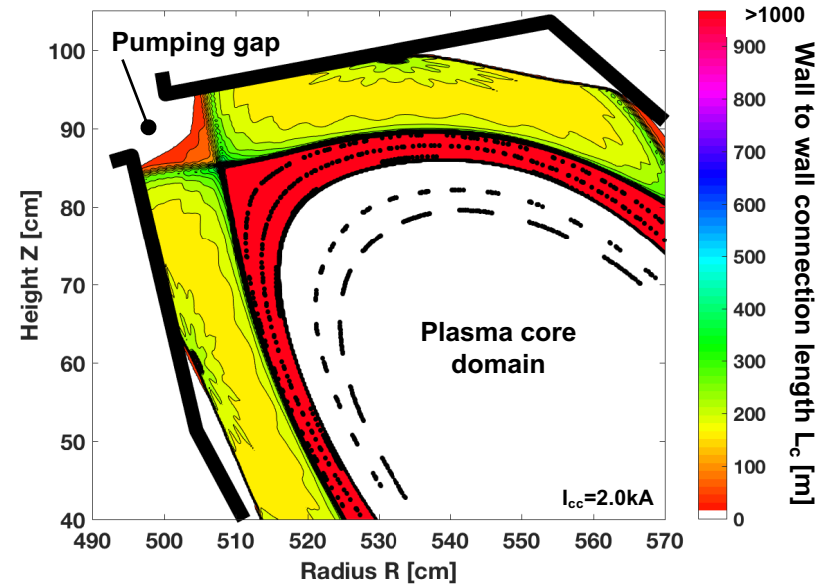
# Applying a stationary divertor control current allows to increase the divertor neutral pressure by up to 50%



## Averaged neutral particle pressure at pumping gap

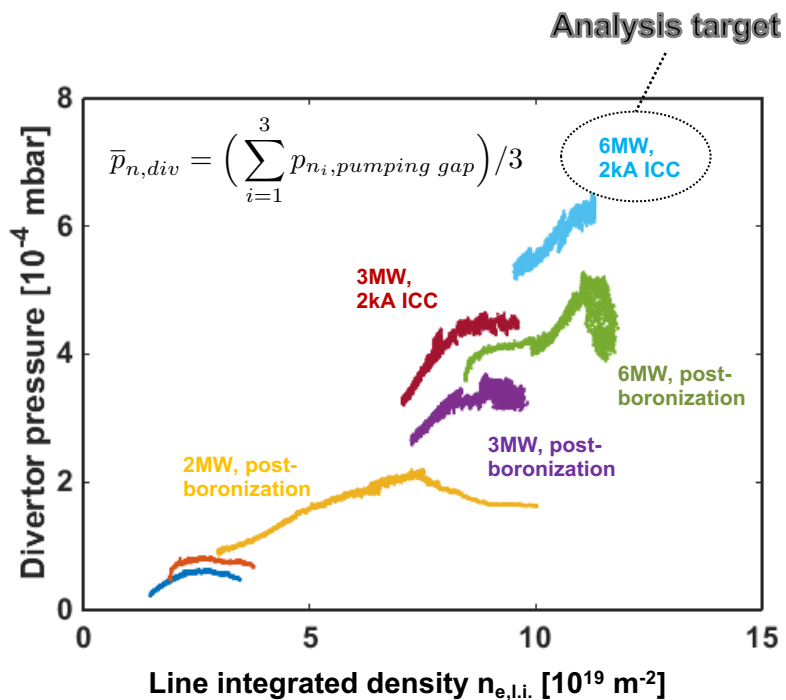


## Change of island structure with divertor control coil current $I_{cc}$

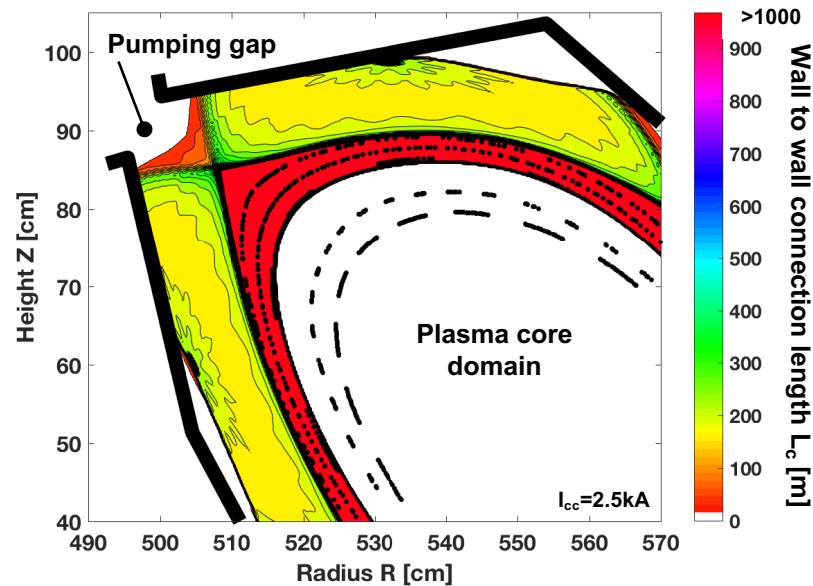


- Island widening, closure of outer gap
- Strike point moves towards gap
- Connection length  $L_c$  reduced

# Increasing the divertor island size allows to increase the divertor neutral pressure by up to 50% compared to small island configuration

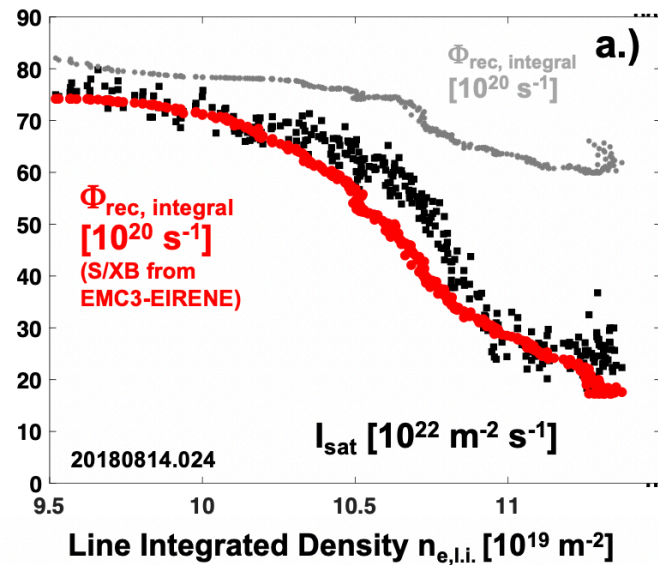


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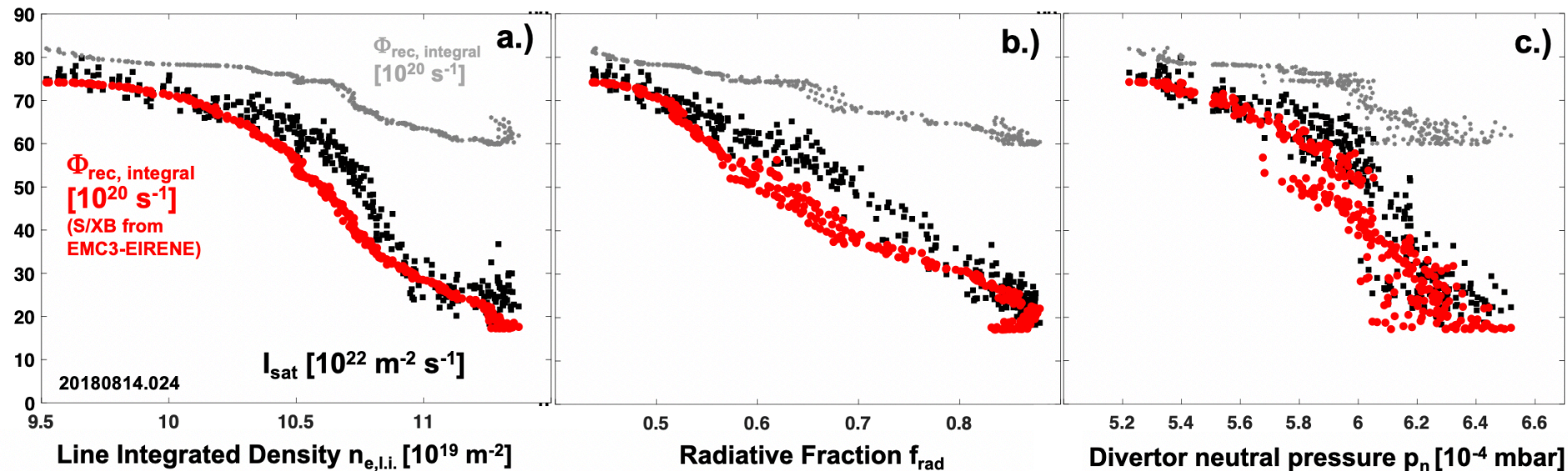


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# Particle flux detachment develops together with power detachment and pressure build up due to increasing radiation

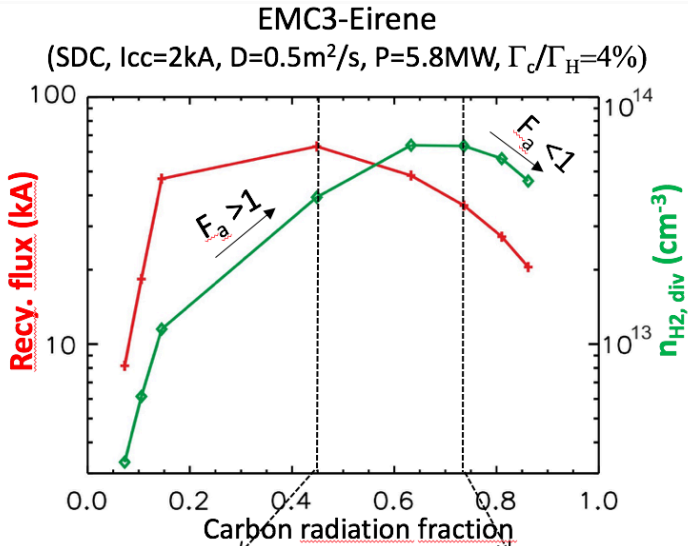


# Particle flux detachment develops together with power detachment and pressure build up due to increasing radiation



Both, heat and also particle fluxes are detached but still a high neutral pressure of up to  $6.5 \cdot 10^{-4} \text{ mbar}$  are reached! **What is behind this interesting feature?**

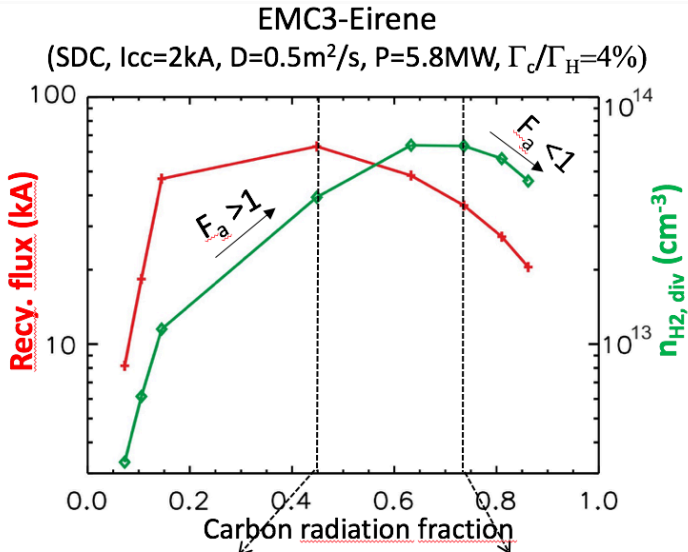
# Particle flux detachment can be combined with sustainment of neutral particle exhaust under power detachment in the island divertor



Distribution of neutrals in island divertor module defines neutral influx  $\Gamma_{\text{in}, \text{H}_0}$  into pumping domain.



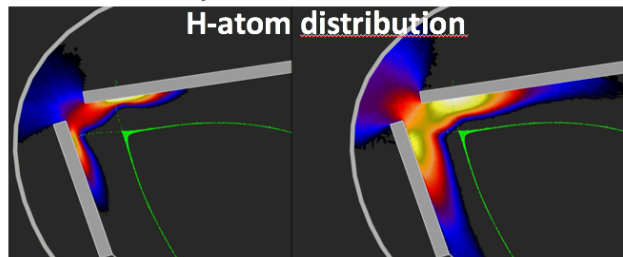
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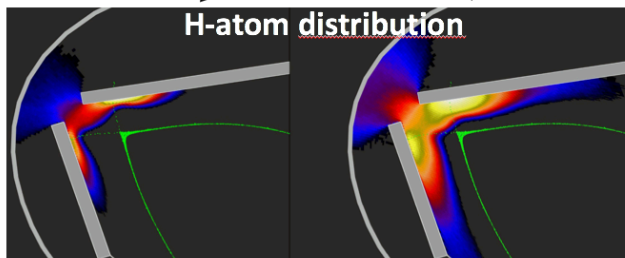
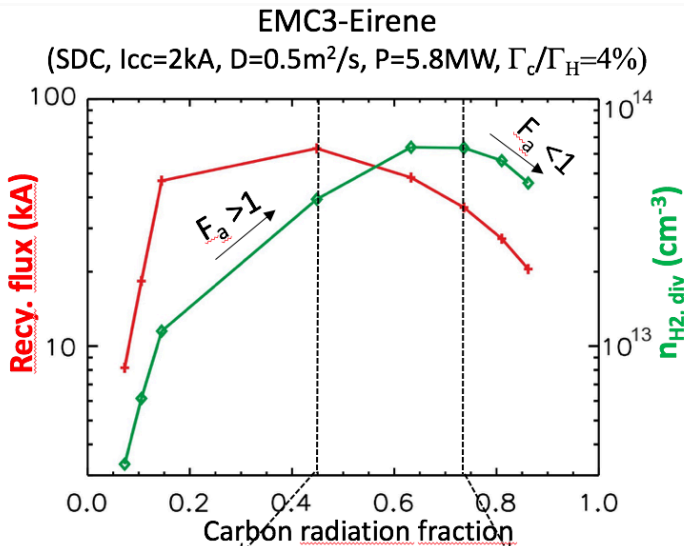
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**Intuitive model:** [Y. Feng et al., W7-X workshop, 2017]  
[Y. Feng et al., Nuclear Fusion **56** (2016) 126011]

- Neutral distribution is defined by local plasma parameters in island
- Mean free ionization  $\lambda_{\text{io}}$  lengths vs. mean distance to pump entrance  $l_p$  defines  $p_n$
- Increasing  $f_{\text{rad}}$  reduces  $T_e$  and hence increases ionization length scale  $\lambda_{\text{io}}$ , also  $n_{e, \text{target}}$  is reduced
- More neutrals can enter the pumping domain



# 3D modeling predicts that $f_{\text{rad}}$ moderates the neutral ionization distribution such that an increase of $\lambda_{\text{io}}$ yields increasing $p_n$ with reduced $\Phi_{\text{target}}$



Distribution of neutrals in island divertor module defines neutral influx  $\Gamma_{\text{in}, H_0}$  into pumping domain.

Intuitive model: [Y. Feng et al., W7-X workshop, 2016]

$$\Gamma_{\text{in}}^{H_0} \propto \Gamma_{\text{ef}}^{H+} \cdot \exp(-F_a)$$

$$F_a = \bar{l}_{\text{gap}} / \bar{\lambda}_{\text{ion}} \quad \text{attenuation factor}$$

$$\Gamma_{\text{ef}}^{H+} \quad \text{recycling flux}$$

$$\bar{l}_{\text{gap}} \quad \text{mean distance to pumping gap}$$

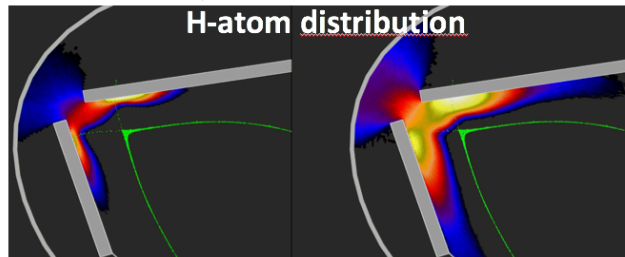
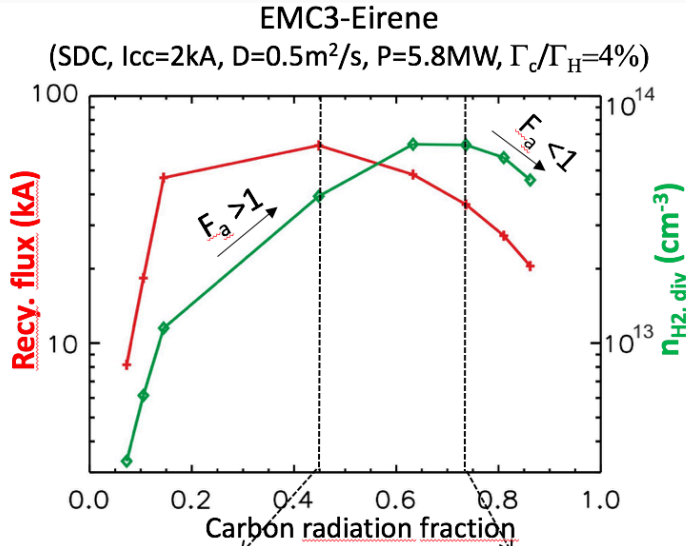
$$\bar{\lambda}_{\text{ion}} \quad \text{mean ionization length scale}$$

Key plasma parameter

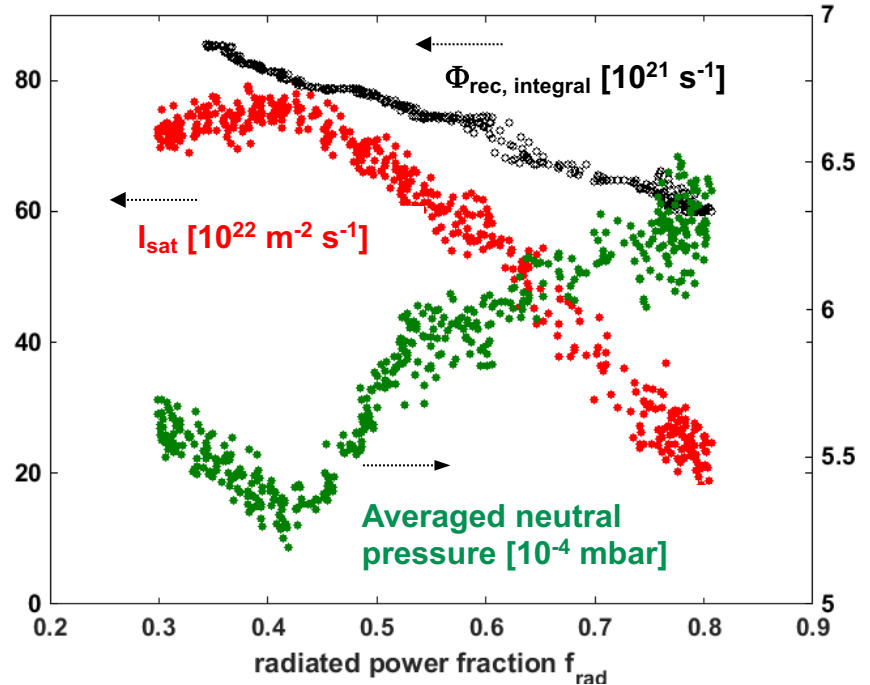
$$\lambda_{\text{io}} = \frac{v_n}{n_e \langle \sigma v \rangle (T_e)}$$

Regulated through  $f_{\text{rad}}$

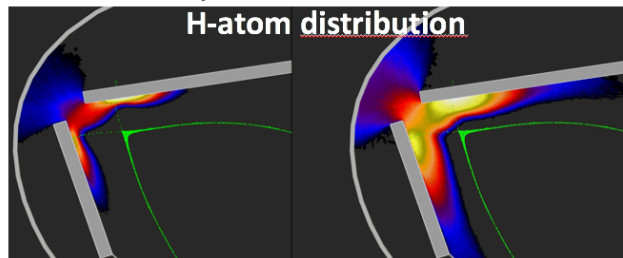
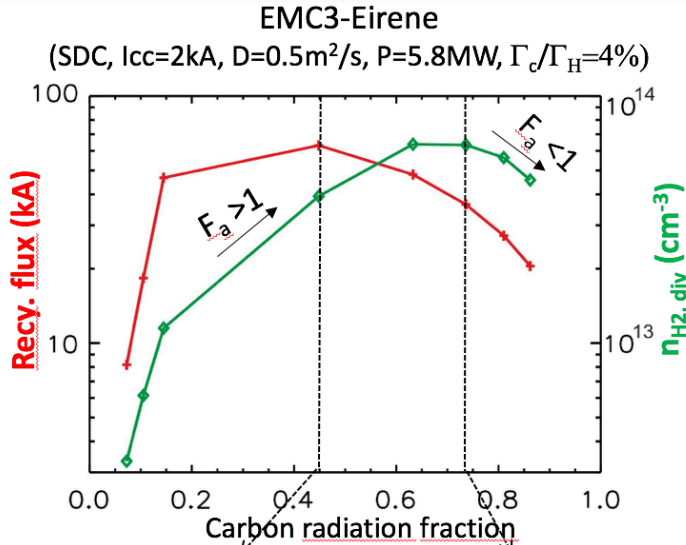
# Particle flux detachment can be combined with sustainment of neutral particle exhaust under power detachment in the island divertor



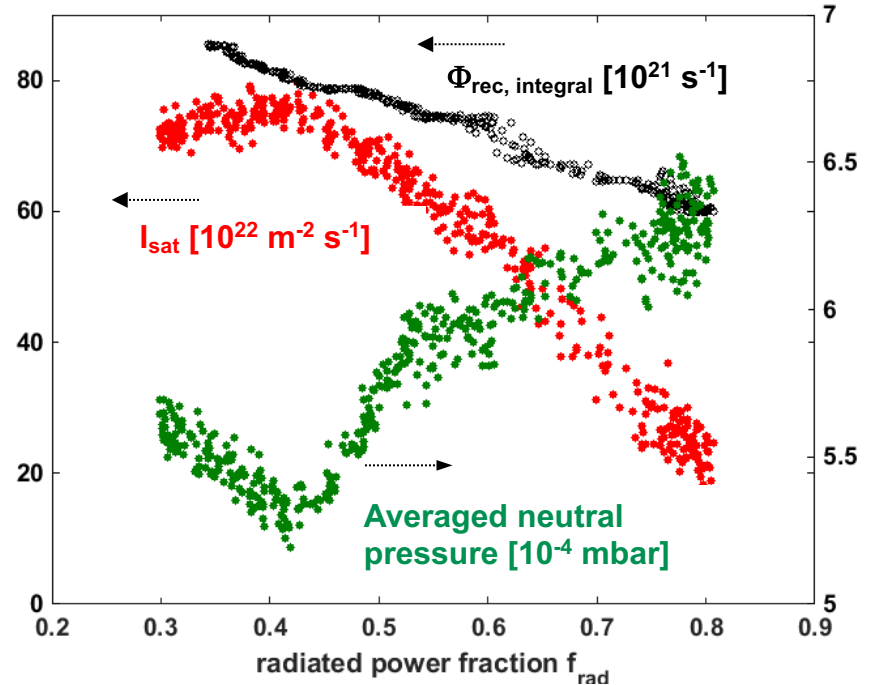
## Experimental data support this intuitive model



# Particle flux detachment can be combined with sustainment of neutral particle exhaust under power detachment in the island divertor

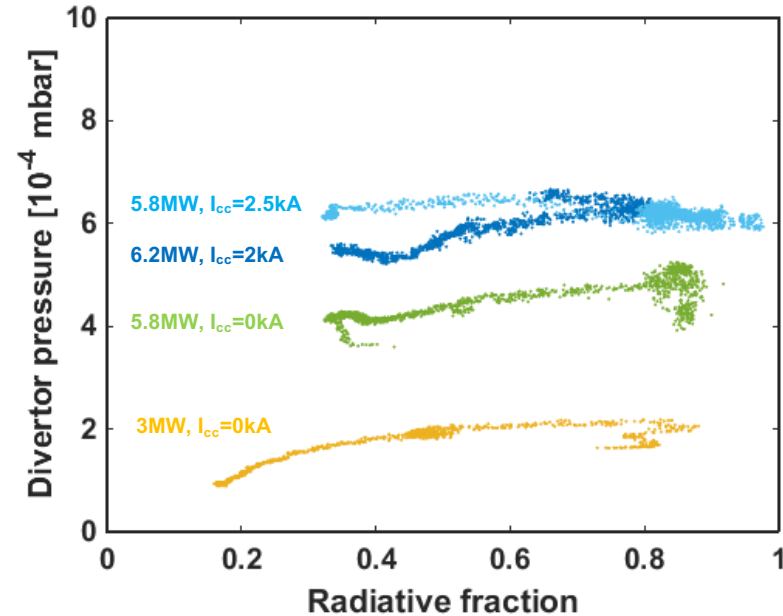
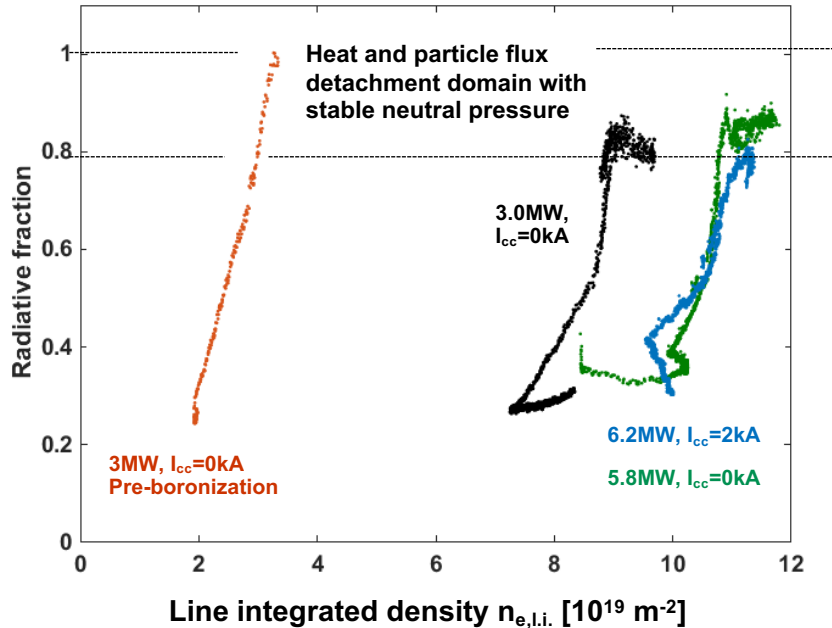


## Experimental data support this intuitive model



No  $p_n$  roll-over is observed in the experiment due to  $f_{\text{rad}}$  limit from ECH heating scenario

The radiation fraction is dependent of the heating power for a given density range – this is the basis for the regulation of divertor temperature in the island

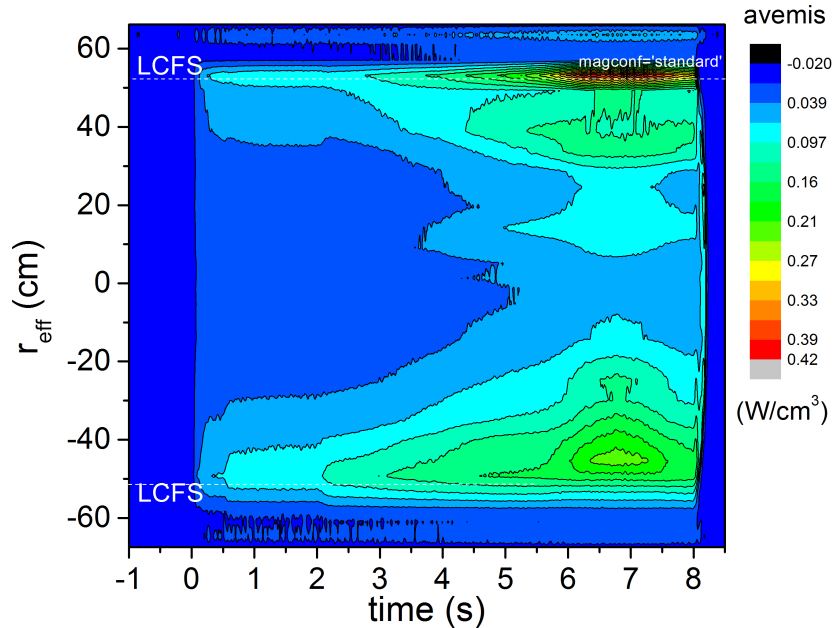


The radiated fraction depends on density which in turn is defined by the available heating power through ECRH – this sets the stage for the detached regime.

# Radiation in detached state is localized predominantly around separatrix – exact resolution so far very challenging due to limited resolution of bolometer



#20180814.024 Bolometer (HBC) chord-brightness

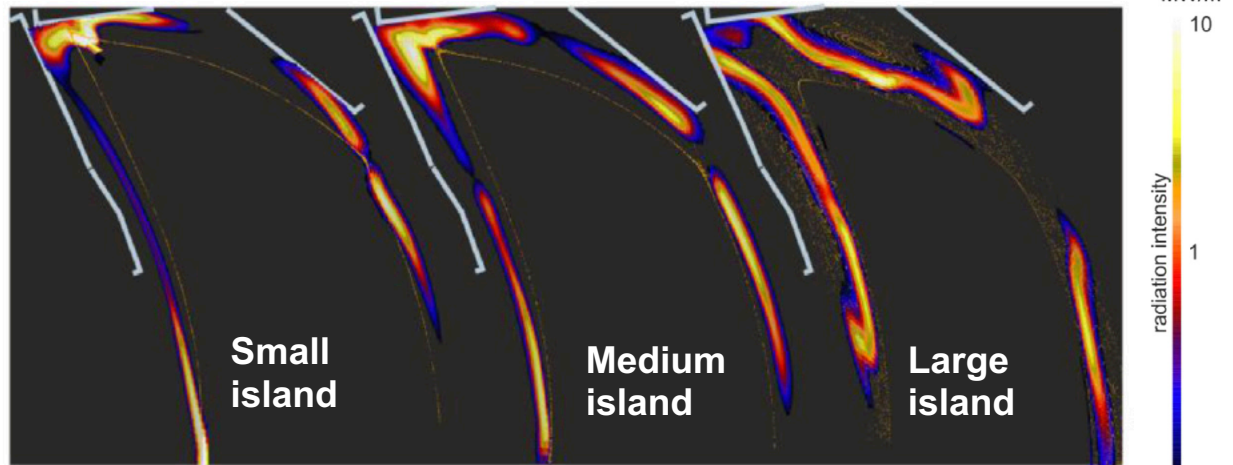
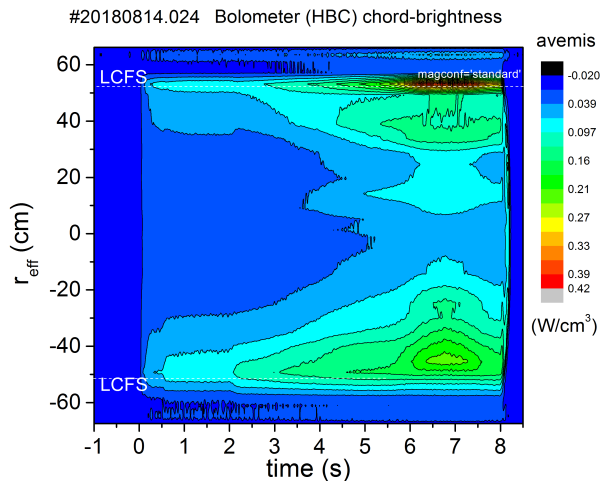


**Exact power balance in the plasma edge layer is a high priority topic to disentangle radiation contributions**

# Radiation in detached state is localized predominantly around separatrix – exact resolution so far very challenging due to limited resolution of bolometer



## Island size dependence of C radiation around islands at $f_{\text{rad}}=0.8$



Radiation localized at strike point

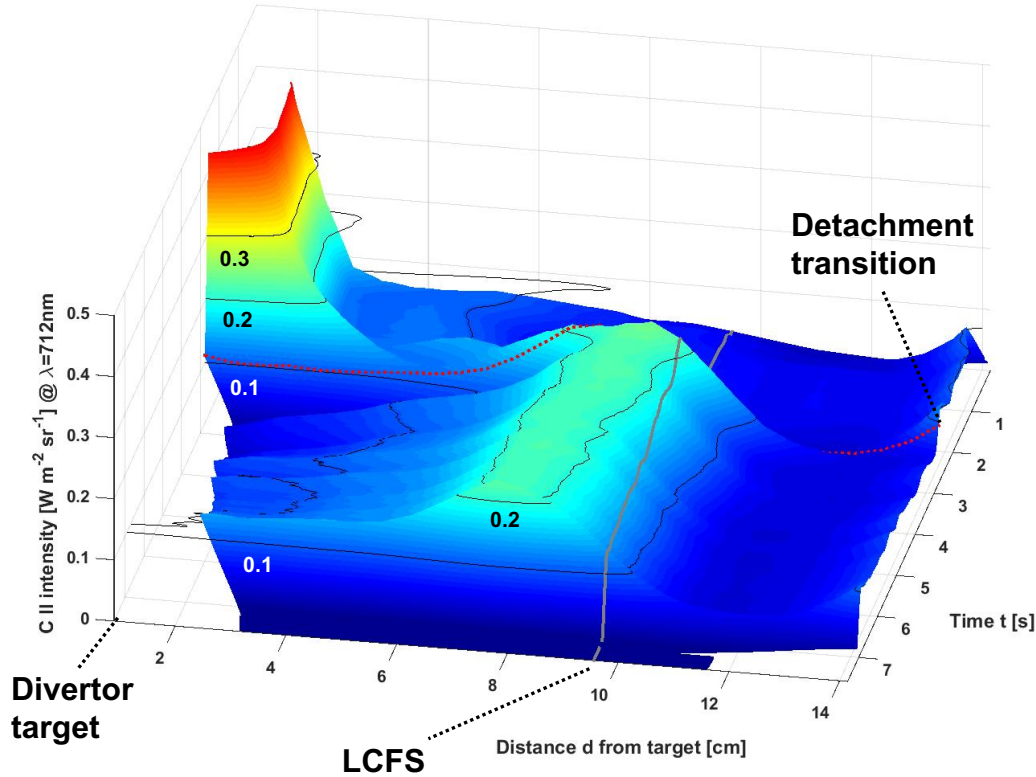
Radiation fills island domain

Radiation reaches separatrix

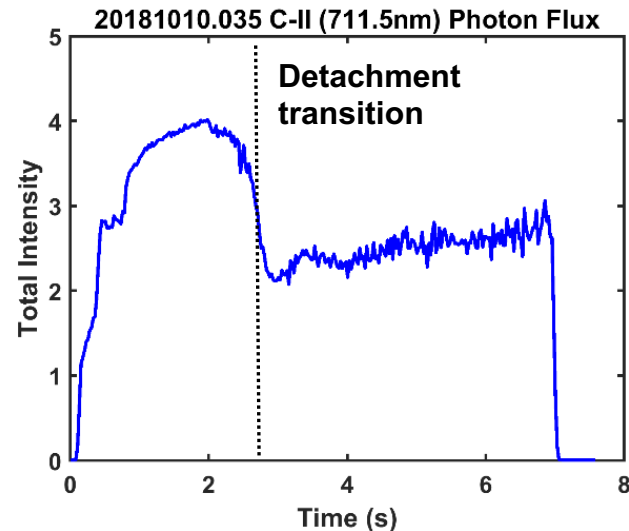
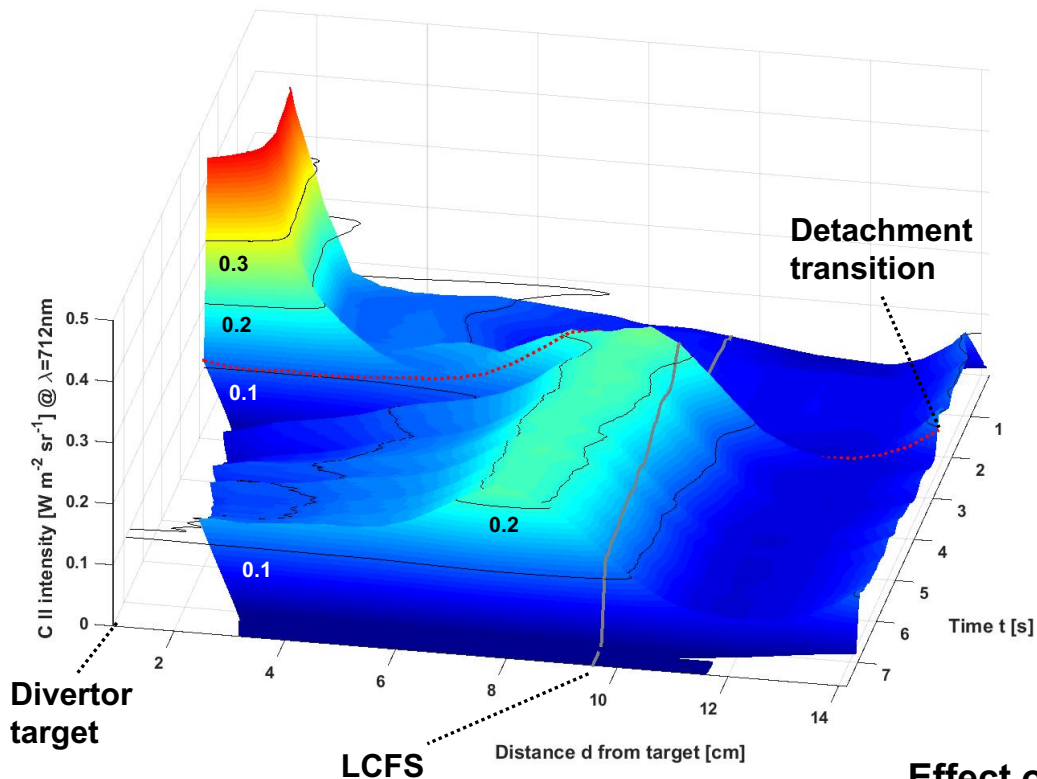
Exact power balance in the plasma edge layer is a high priority topic to disentangle radiation contributions – modeling suggests radiation inside SOL up to  $f_{\text{rad}} \sim 0.8$



# Carbon impurity source and C-II line emission define the local radiation equilibrium which detaches from surface



# Carbon impurity source and C-II line emission define the local radiation equilibrium which detaches from surface



The integrated C-II emission is reduced but the C-source estimated ( $10^{22} \text{ part. s}^{-1}$ ) shows almost no significant reduction.

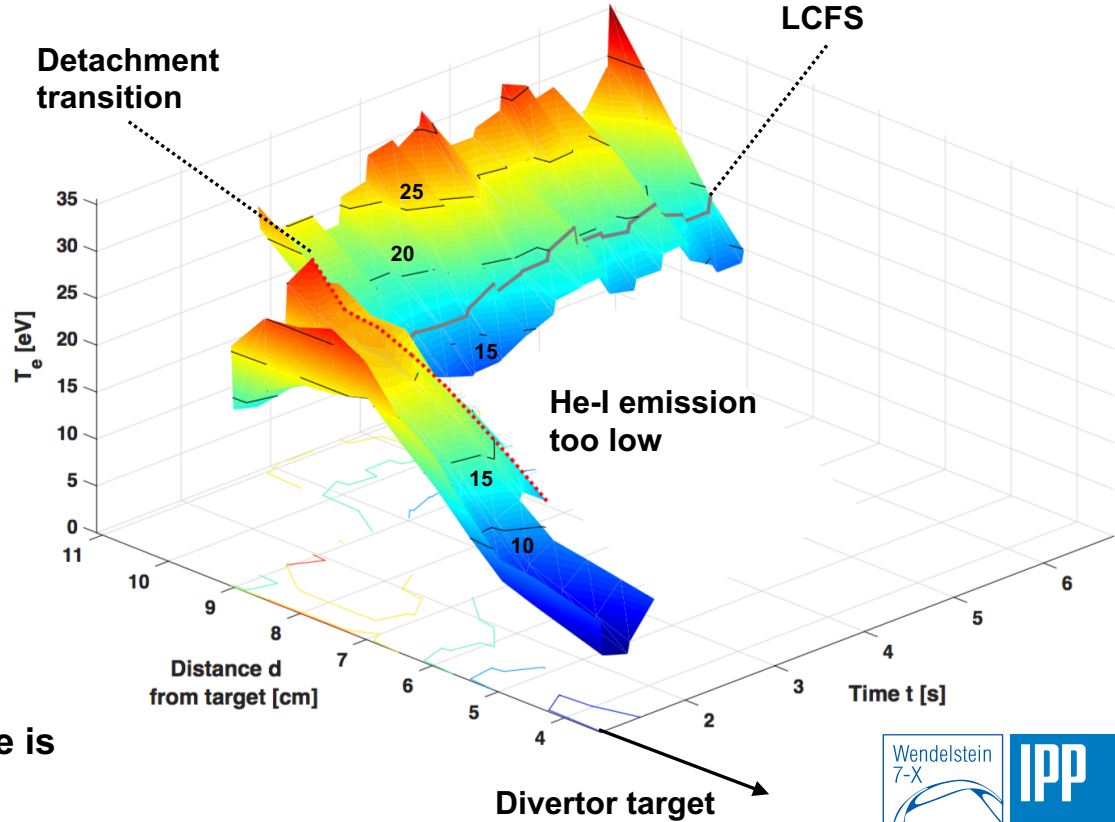
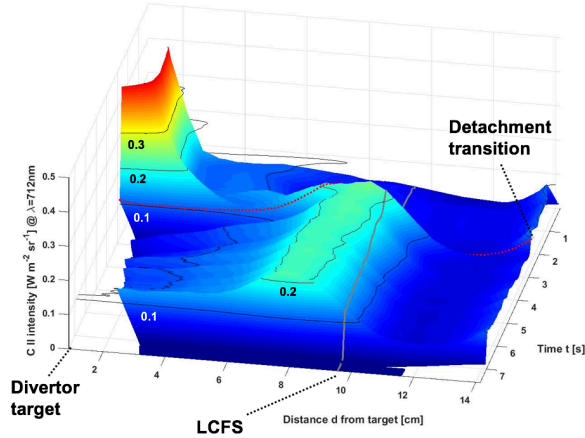
Effect of local plasma parameters!



# Carbon radiation distribution is followed by position of 15 eV isothermal surface in island divertor domain



Iso-thermal surface ( $T_e \sim 15$  eV) moves inward with radiation front.



Density at the position of this surface is almost constant ( $n_e \sim 5.0 \cdot 10^{19} \text{ m}^{-3}$ )

# Outline of this talk in form of an executive summary



- A **stable, thermally fully detached island divertor regime with small divertor particle fluxes** but still **sufficient divertor neutral pressures** was shown for the first time.
- This detached island divertor regime is **reached with minimal feedback control in a reliable fashion** and **the divertor operational point is defined through sufficient radiative losses at a given input power.**

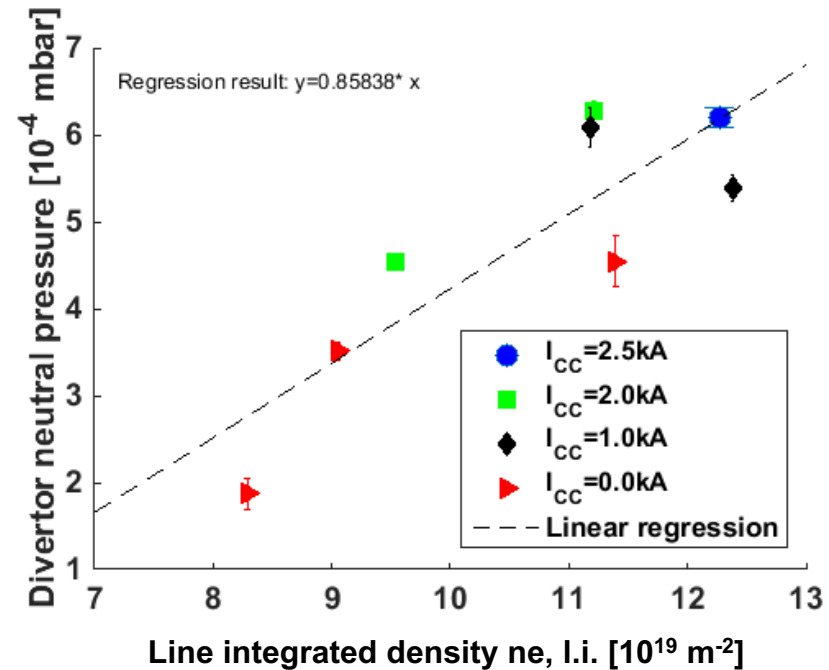
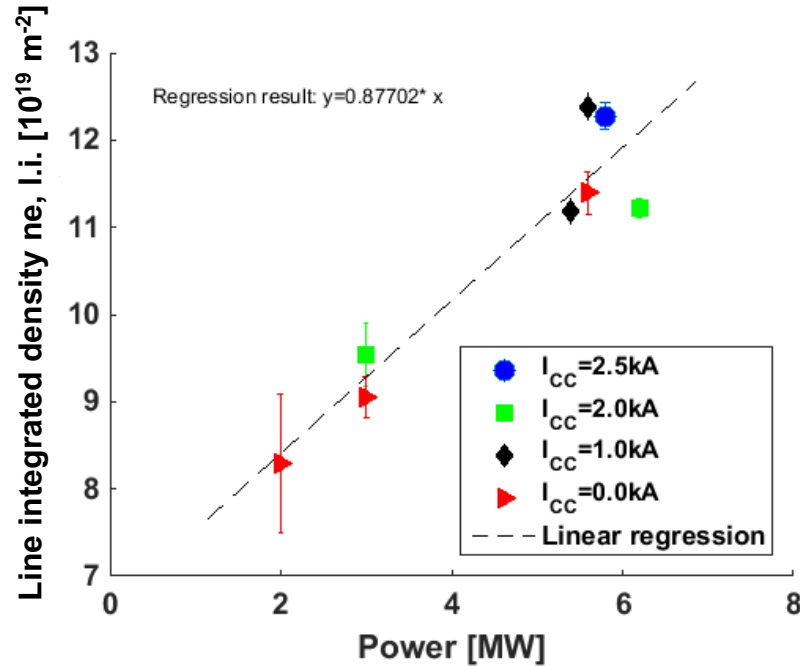
The **geometry of the magnetic islands** forming the divertor allow to **fine tune the divertor neutral distribution** for **maximized neutral pressure** in the detached state.

- This island divertor regime is **compatible with steady state particle exhaust** for the upcoming high-performance campaign of W7-X.

# Linear scaling of plasma density with input power enables build up of sufficient divertor neutral pressures and maximize by island size increase



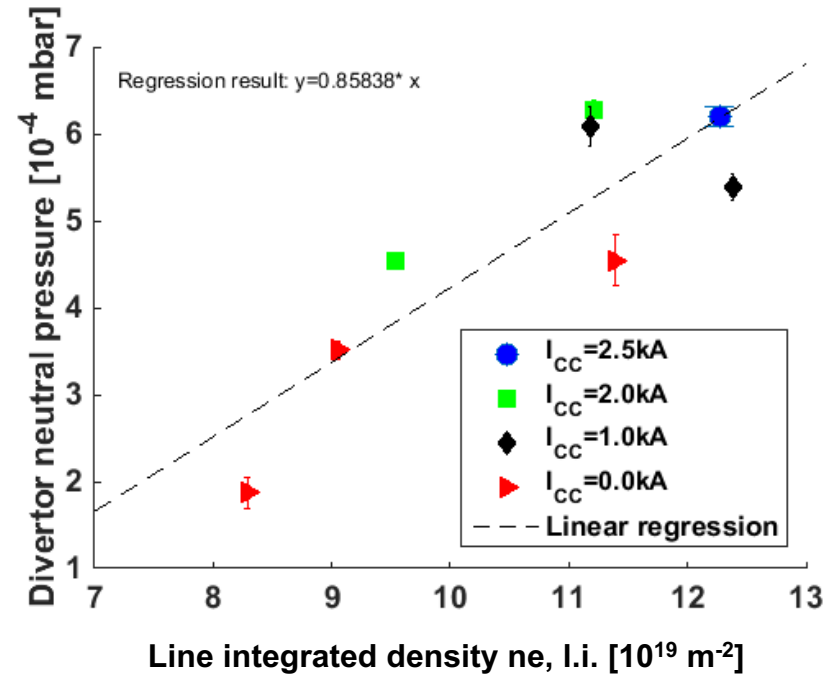
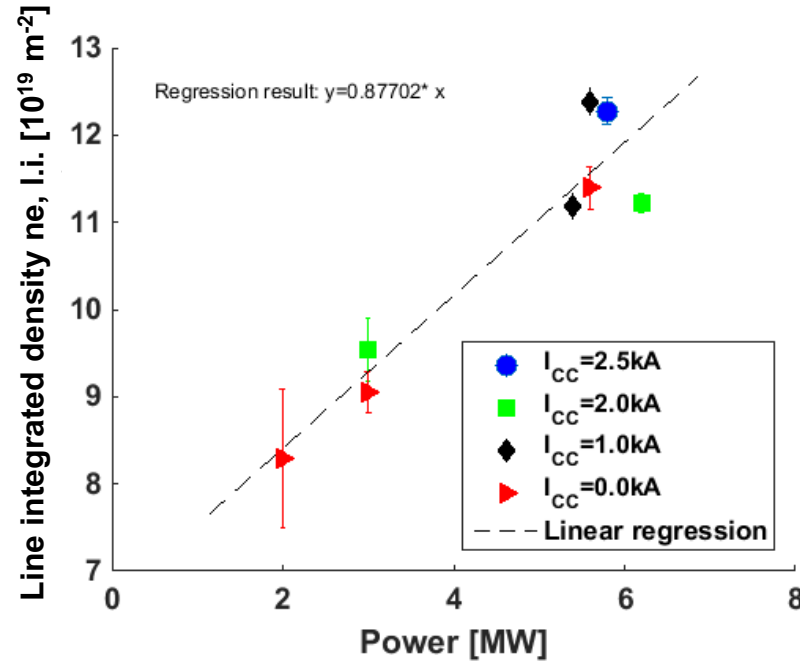
Data were averaged over stable detached windows for various experimental programs with  $[0.75 < f_{\text{rad}} < 0.9]$



# Linear scaling of plasma density with input power enables build up of sufficient divertor neutral pressures and maximize by island size increase



Data were averaged over stable detached windows for various experimental programs with  $[0.75 < f_{\text{rad}} < 0.9]$



The divertor neutral pressures obtained scale favorably towards steady state

# Pumping particle flux level reached under reliably detached conditions is compatible with exhaust requirements for steady state



- **Basic observation:** increase of neutral back pressures of  $<8.0 \cdot 10^{-4}$  mbar averaged across all available pump ducts for after Boronization from  $<5.0 \cdot 10^{-5}$  mbar before Boronization
- **Existing pumping capacity from Turbo-Pumps:**  $10 \times 3 \times 1250$  l/s = 37500 ltr. Hydrogen /s
- **Expected pumping capacity with Cryo-pump:** 70.000 ltr. Hydrogen /s

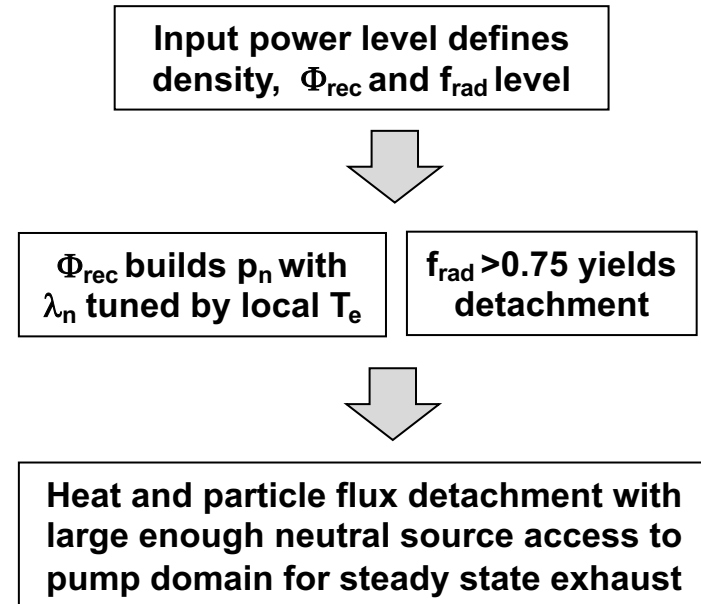
	Value	TMP scenario	Cryo scenario
OP1.2.b	<b>Pumped flux <math>\Gamma_{\text{pump}}</math></b>	<b><math>5.2 \cdot 10^{20}</math> H2/s</b>	<b><math>9.25 \cdot 10^{20}</math> H2/s</b>
	<b>Fueled flux <math>\Gamma_{\text{in}}</math></b>	<b><math>5.0 \cdot 10^{20} - 1.0 \cdot 10^{21}</math> H2/s</b>	<b><math>5.0 \cdot 10^{20} - 1.0 \cdot 10^{21}</math> H2/s</b>
Based on example 20180814.024 with <b><math>8.0 \cdot 10^{-4}</math> mbar</b> averaged divertor pressure			
OP1.2.a	<b>Pumped flux <math>\Gamma_{\text{pump}}</math></b>	$9.0 \cdot 10^{19}$ H2/s	$1.6 \cdot 10^{20}$ H2/s
	<b>Fueled flux <math>\Gamma_{\text{in}}</math></b>	$2.2 \cdot 10^{20} - 2.0 \cdot 10^{21}$ H2/s	Does not scale, low $n_e$
Executed based on example 20180801.039 and 20171207.024 with <b><math>5.0 \cdot 10^{-5}</math> mbar</b> averaged divertor pressure			





- The attractive detached island divertor regime was reached through intrinsic radiation scaling with density, which is defined by the input power.
- Magnetic island size, magnetic connection length and strike line position as actuators
- This regime was only limited by input energy limits, which will be overcome with the actively cooled High-Heat Flux (HHF) divertor.
- The results so far have laid ground for a promising outlook on the overall steady state compatibility of the island divertor concept.

## A possible hierarchy of the process



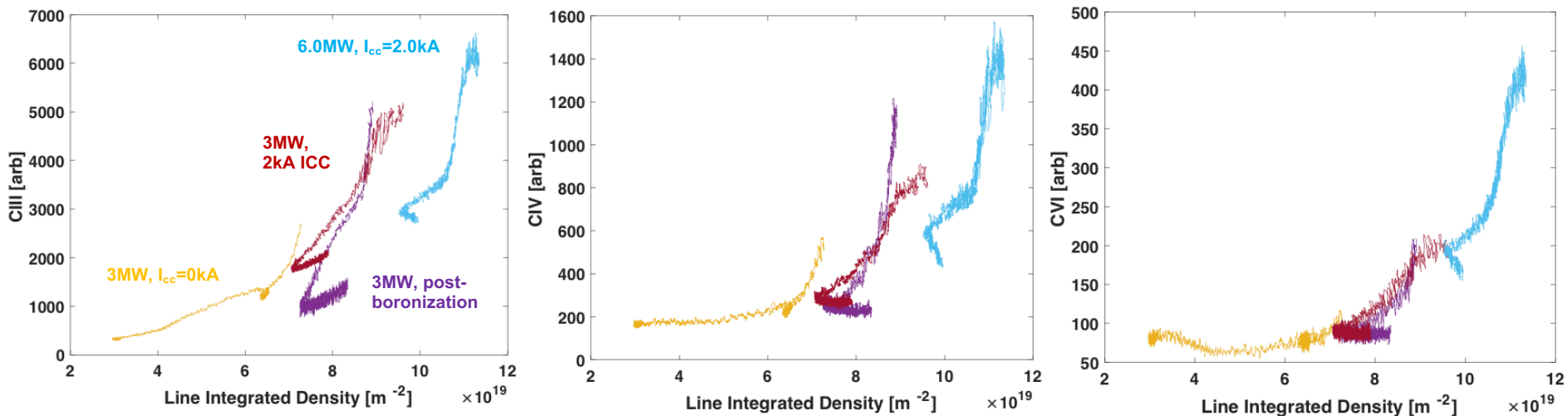


# Appendix

# Carbon charge states emit across the island divertor volume featuring a quadratic dependence on density which defines divertor $T_e$

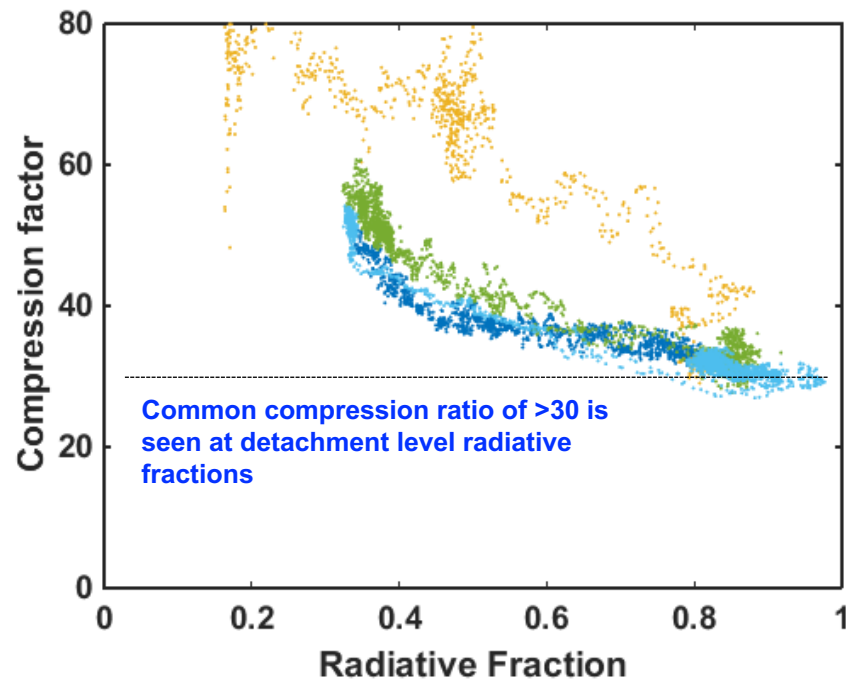
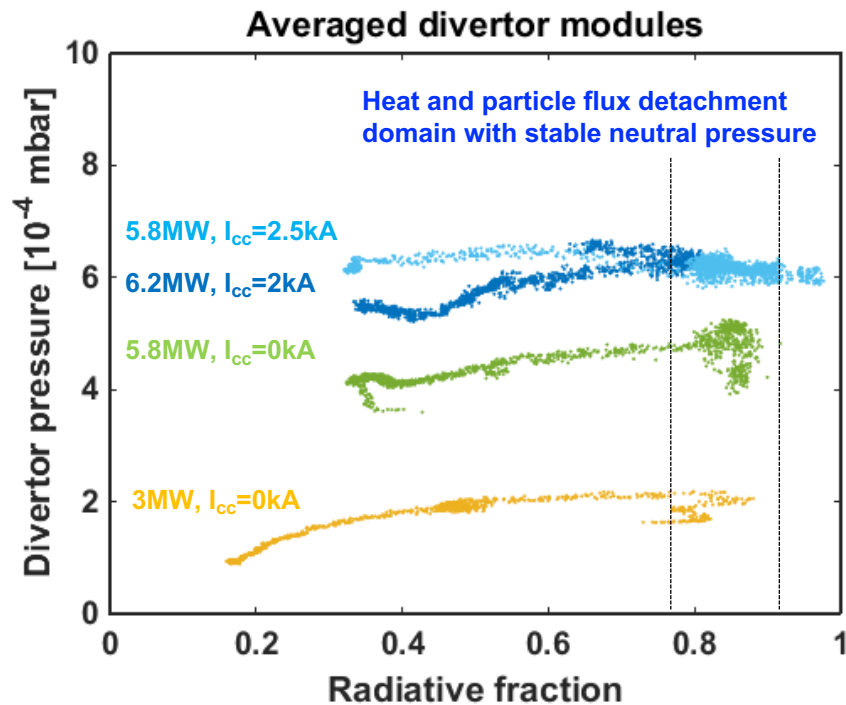


Quadratic rise of carbon line radiation close to the target (C-III), in the island domain (C-IV) and around separatrix (C-VI) supports facilitation of detachment by intrinsic impurity radiation



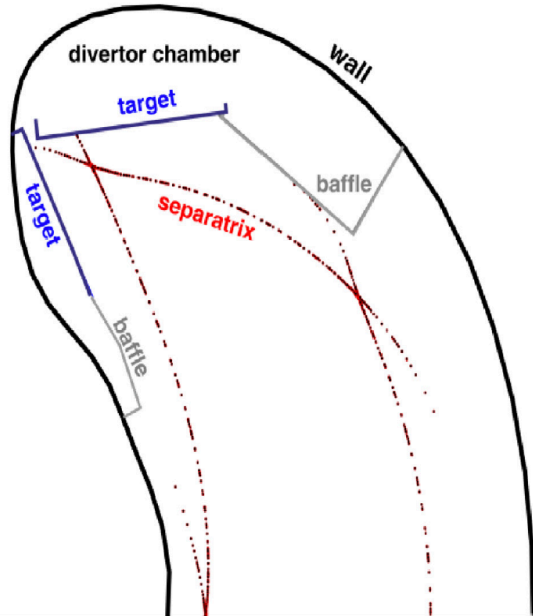
Carbon as intrinsic impurity supports the necessary radiative losses localized inside and in the close vicinity of the island domain.

# The divertor neutral pressure level depends on density scaling with increasing heating power – access to detachment for $f_{\text{rad}} > 0.75$

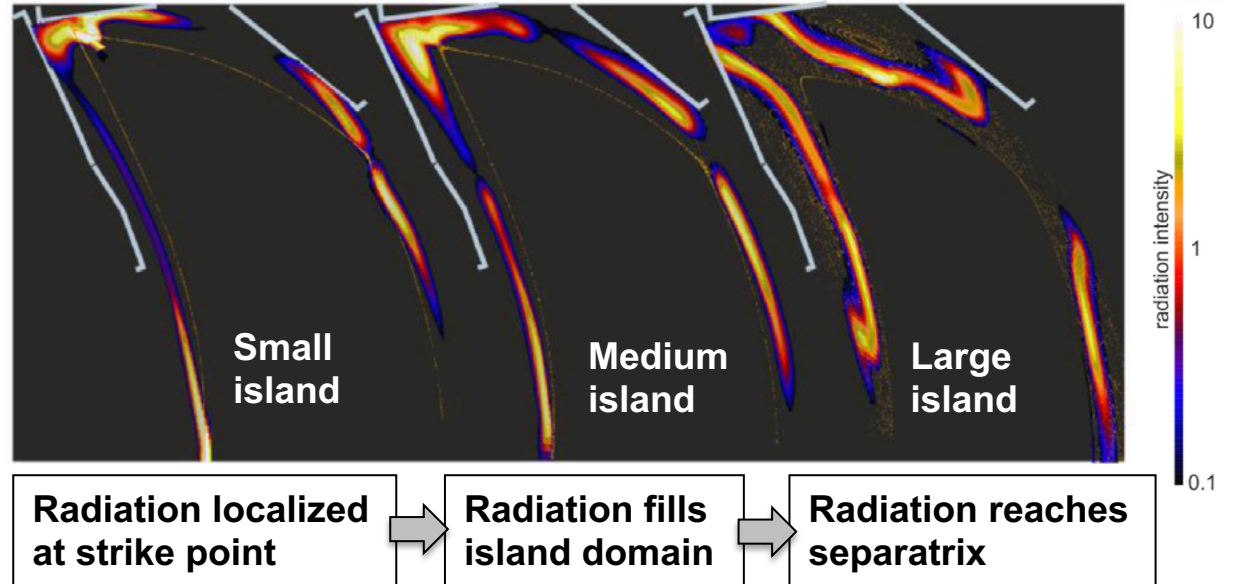


At a radiated fraction of  $0.75 < f_{\text{rad}} < 0.9$  a saturated neutral pressure  $p_n$  regime is seen with  $p_n$  being set by the plasma density

# The volume of the magnetic island is predicted to serve as a reliable interface layer with a beneficial radiation and ionization equilibrium



Island size dependence of C radiation around islands at  $f_{\text{rad}}=0.8$



[Y. Feng et al., Nuclear Fusion **56** (2016) 126011]

**Interplay of radiation distribution with power dissipation and divertor neutral capture is key to understand the island divertor!**



# The EMC3-EIRENE model in a nutshell

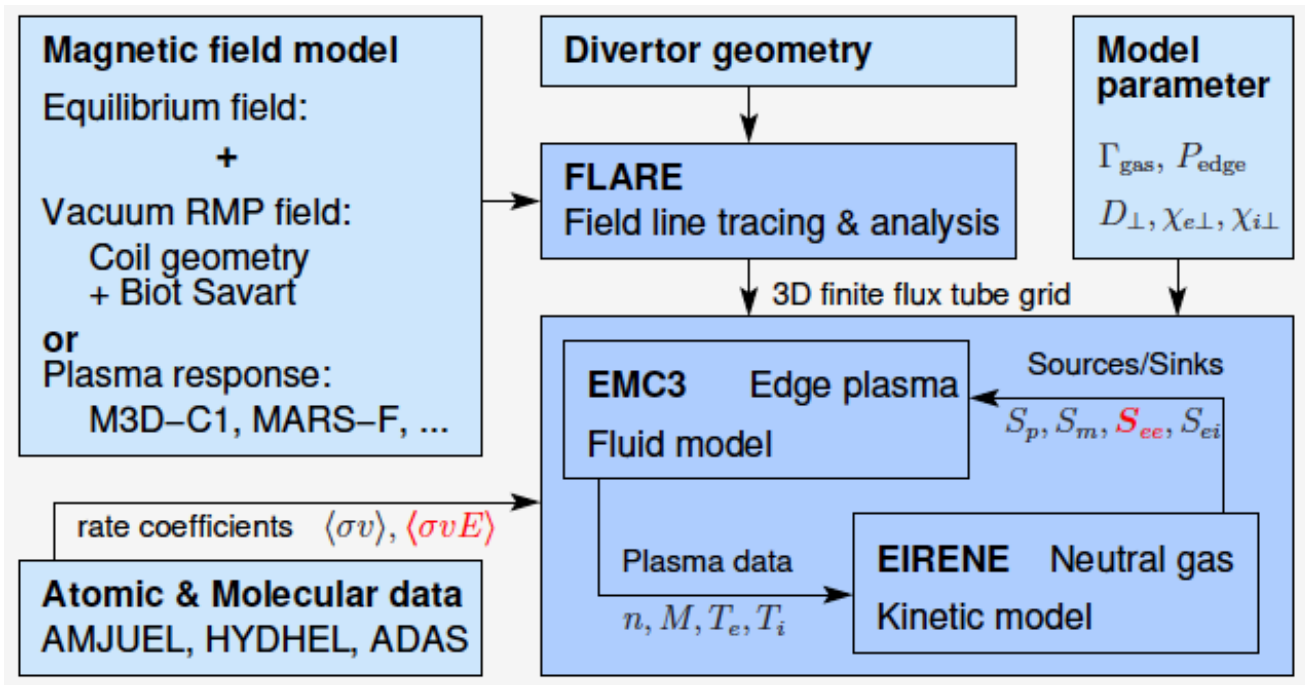


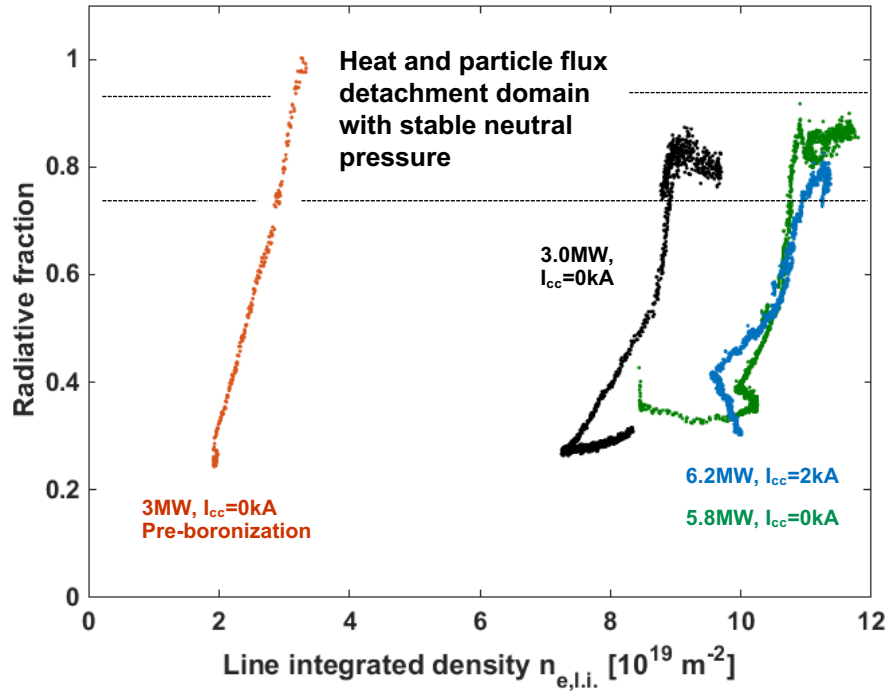
Figure courtesy of H. Frerichs

[Y. Feng et al., JNM **266-269** (1999) 812] [Y. Feng et al., PPCF **59** (2017) 034006]

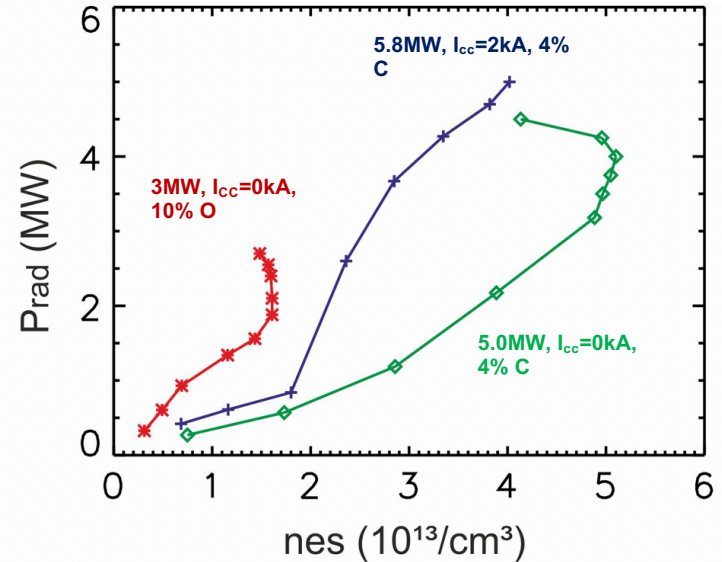
[Y. Feng et al., Contri. Plasma Phys. **54** (2014) 426-431]



The radiation fraction is dependent of the heating power for a given density range – this is the basis for the regulation of divertor temperature in the island



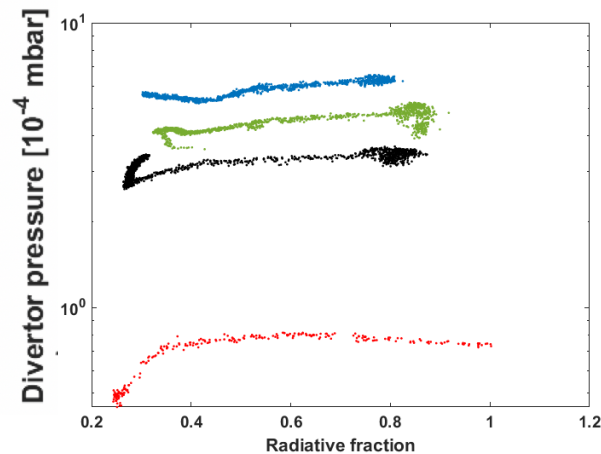
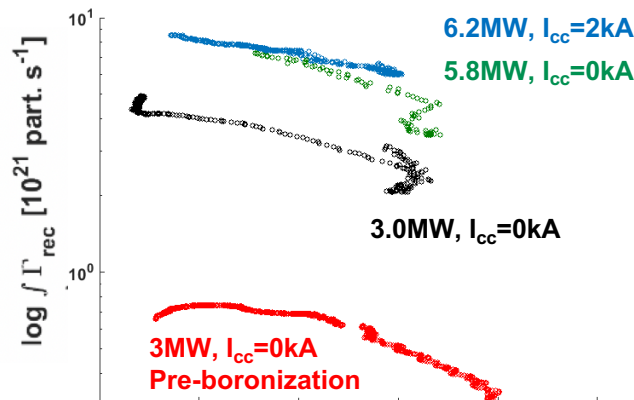
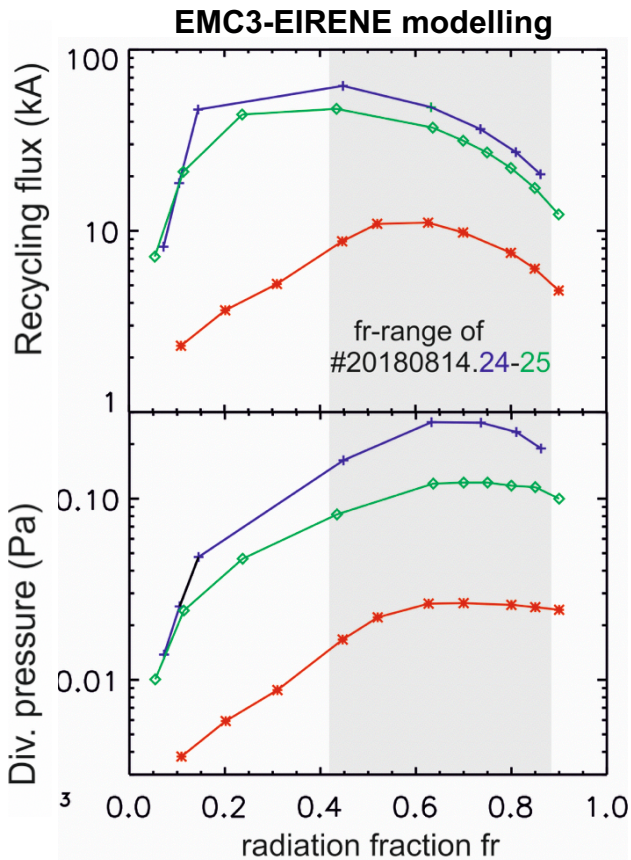
EMC3-EIRENE predicts comparable scaling of radiation in island with density



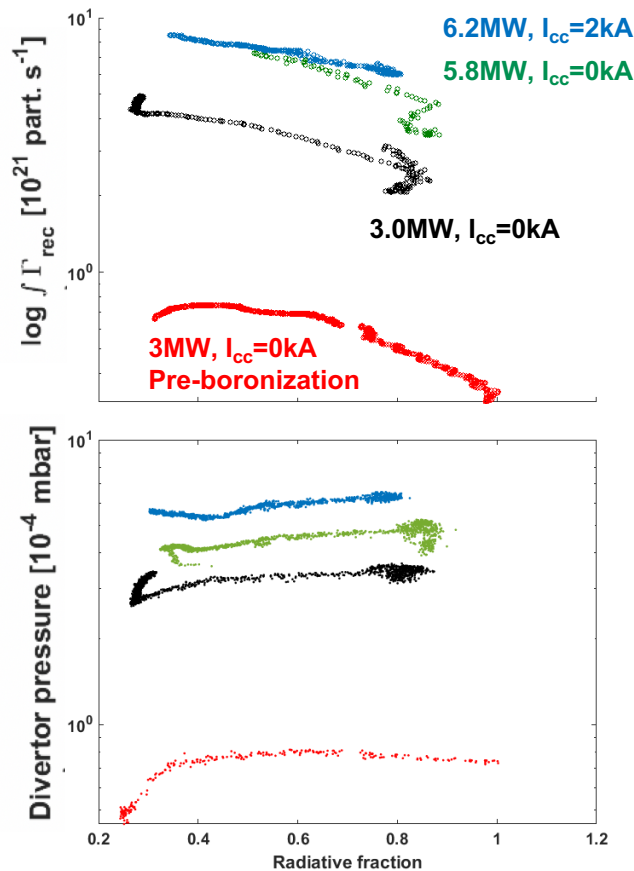
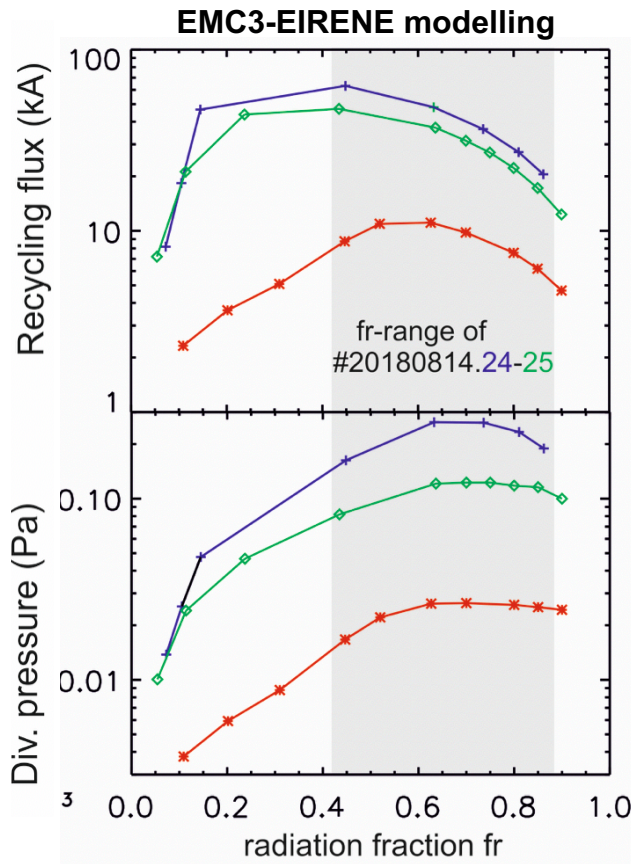
The radiated fraction depends on density which in turn is defined by the available heating power through ECRH – this sets the stage for the detached regime.



# Dependence of target parameters on $f_{\text{rad}}$ is consistent between experiment and EMC3 model, but a significantly weaker dependence is found in measurement

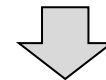


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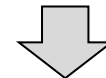


A possible hierarchy of the process

Power level defines density and hence  $\Phi_{\text{rec}}$

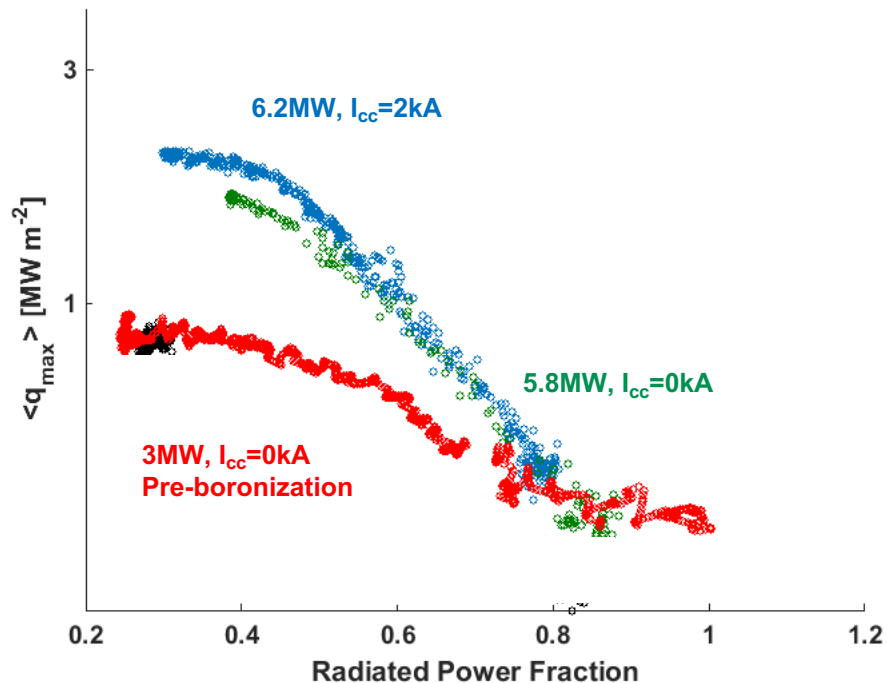
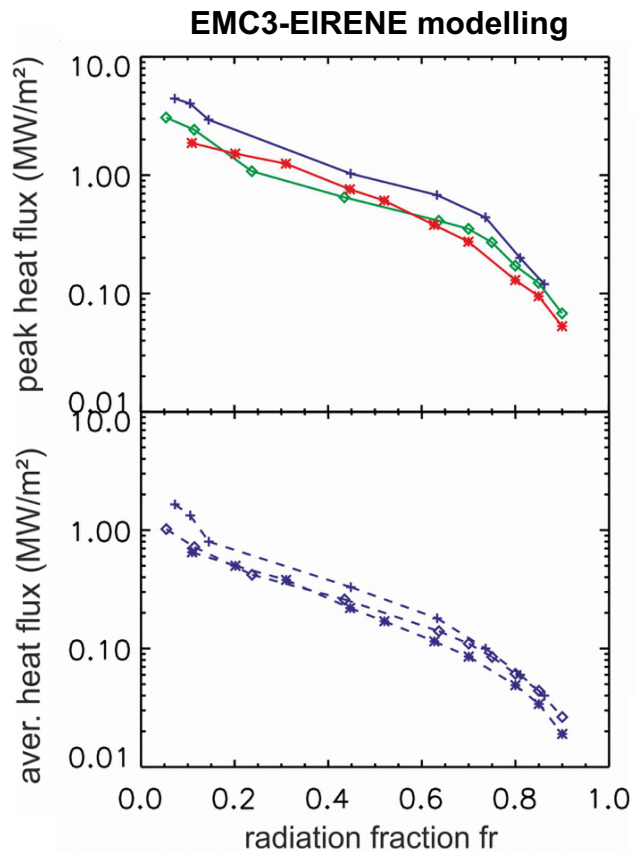


$\Phi_{\text{rec}}$  provides source for  $p_n$



Optimal neutral particle distribution for good pump access is defined by  $f_{\text{rad}}$

# Dependence of target parameters on $f_{\text{rad}}$ is consistent between experiment and EMC3 model, but a significantly weaker dependence is found in measurement



**Power dissipation due to radiation from intrinsic impurity yields thermal detachment**



# Particle flows are reduced at transition into detachment

