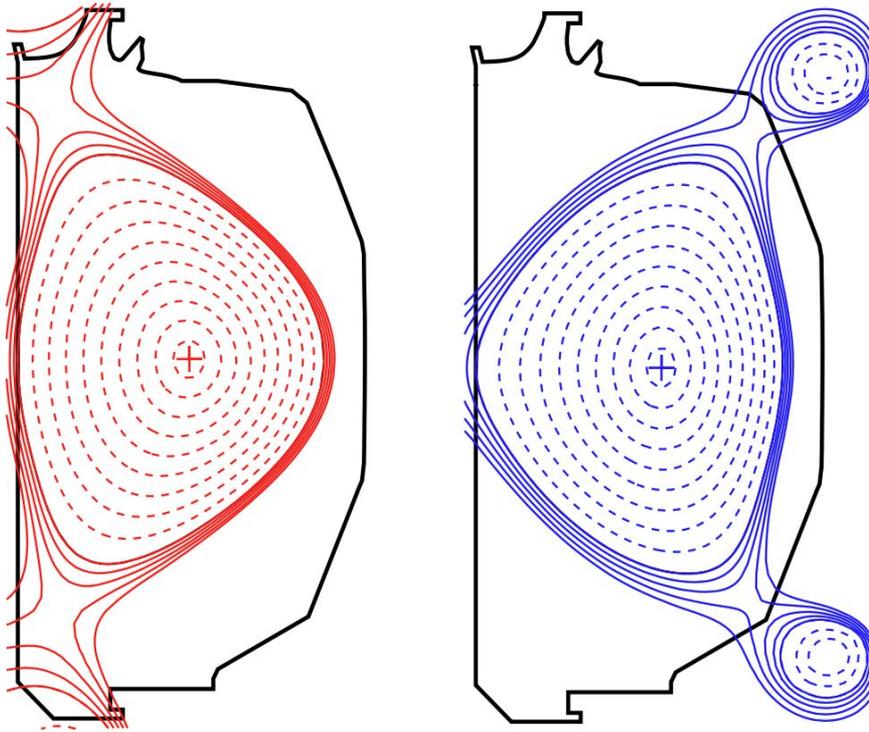


# Second Stability Access in Neg-D Reactors

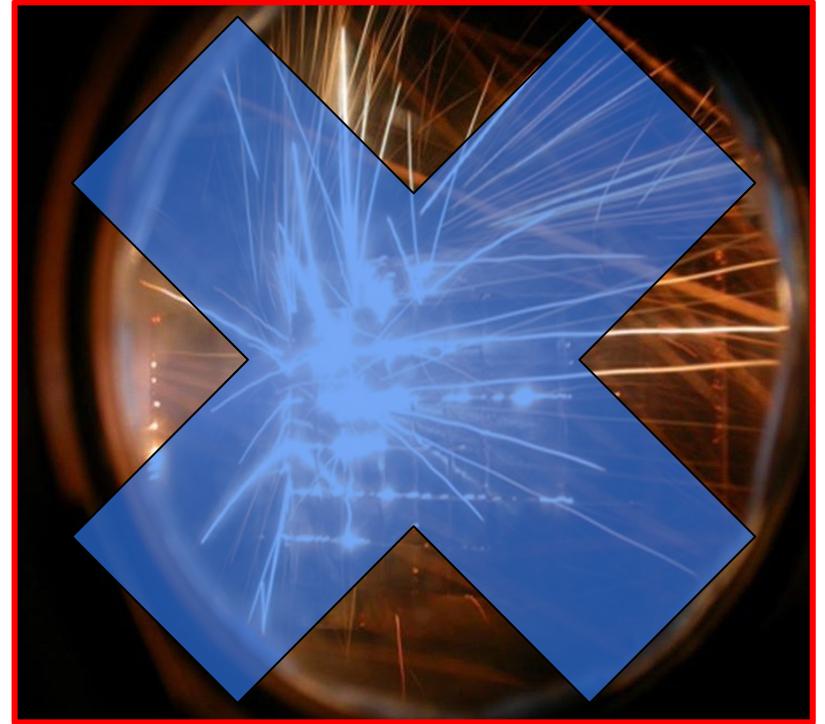
**A. O. Nelson**  
with C. Paz-Soldan and S. Saarelma

**April 11<sup>th</sup>, 2022**  
**NSTX-U / Magnetic Fusion Science Meeting**

# Neg-D: L-modes with H-mode like confinement



Austin, et. al. PRL (2019)



<https://www.iter.org/newsline/166/628>

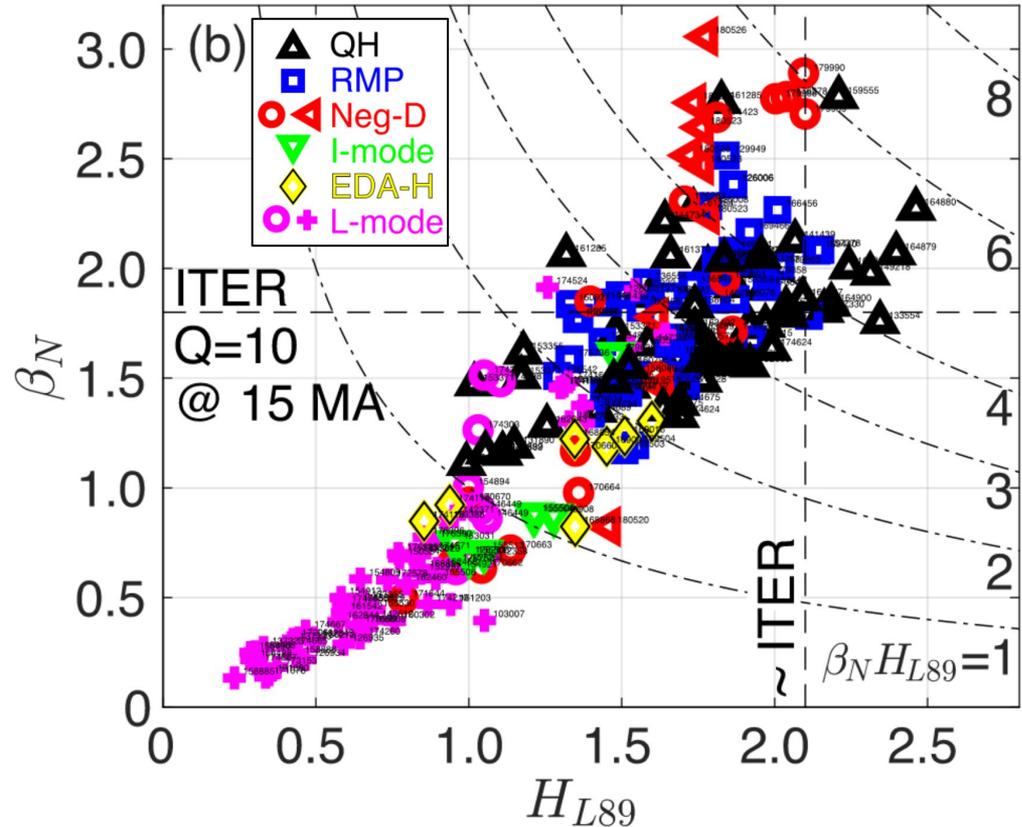
# Neg-D compares well with other no-ELM scenarios

## Core:

- High pressure and confinement due to turbulence reduction
- Stability is generally worse

## Edge:

- Exhaust integration could be alleviated
- H-mode and ELMs avoided through MHD?

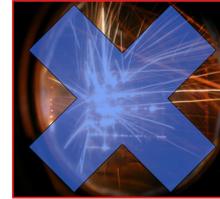


Paz-Soldan, PFCF (2021)

# Outline

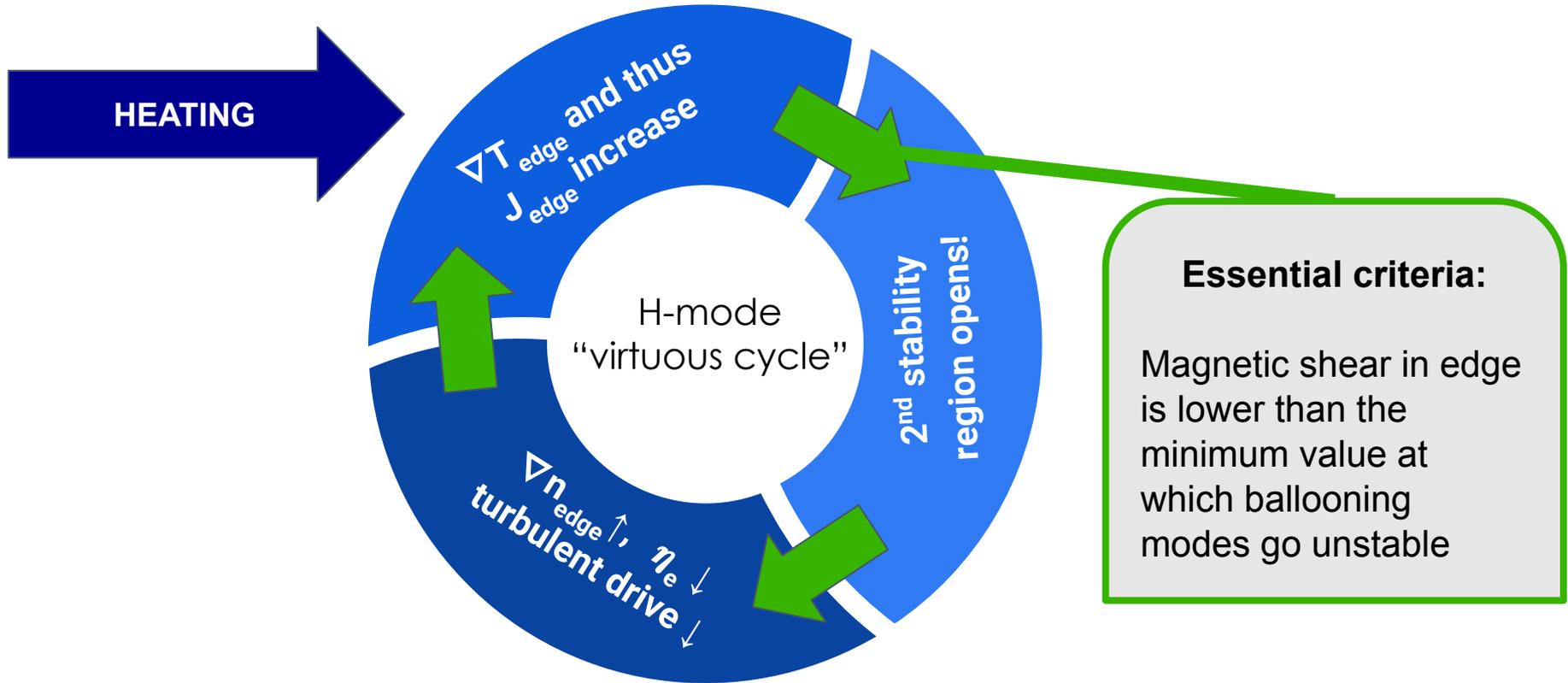
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- **Introduction to Negative Triangularity**

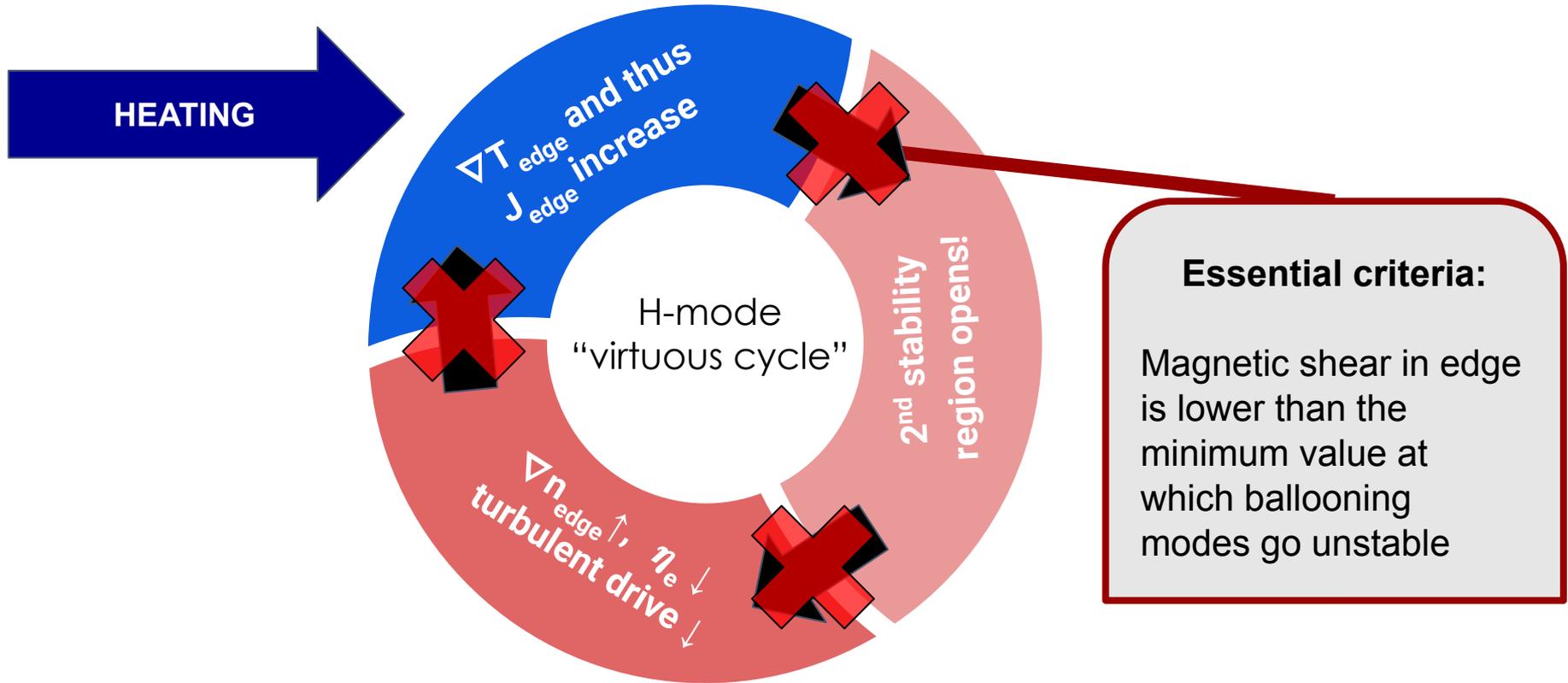


- **H-mode suppression in Neg-D: a case of ballooning instability?**
- **How does shape impact second stability access?**
- **Extrapolation of ballooning physics to reactors**

# H-mode access follows “virtuous cycle”



# Neg-D: ballooning modes clamp $\nabla n_{\text{edge}}$ - stuck in L-mode!



## Essential criteria:

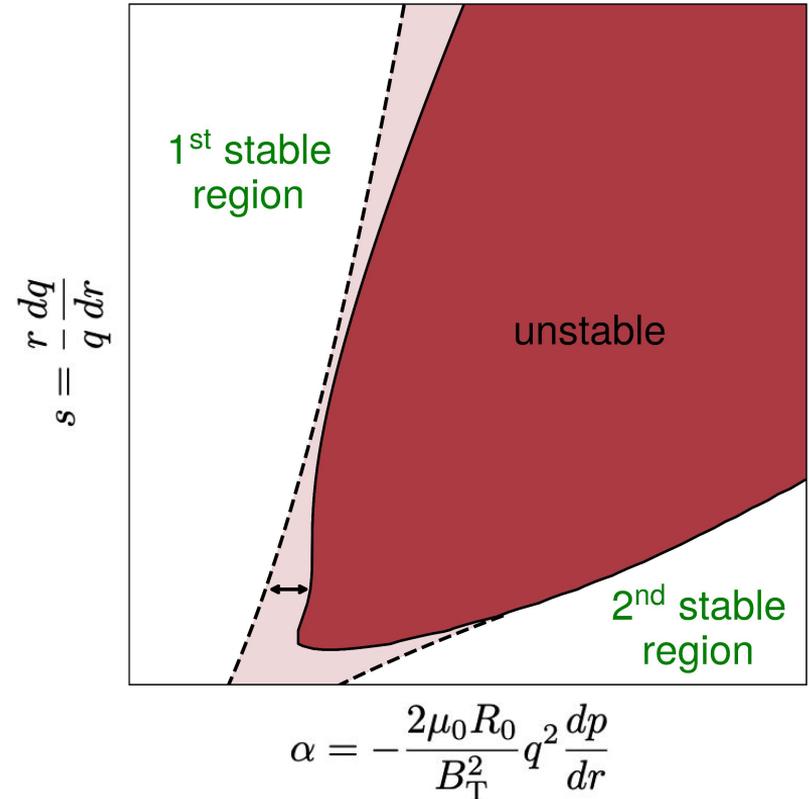
Magnetic shear in edge is lower than the minimum value at which ballooning modes go unstable

# Ballooning mode instability is a function of $s$ and $\alpha$

- Local shear:

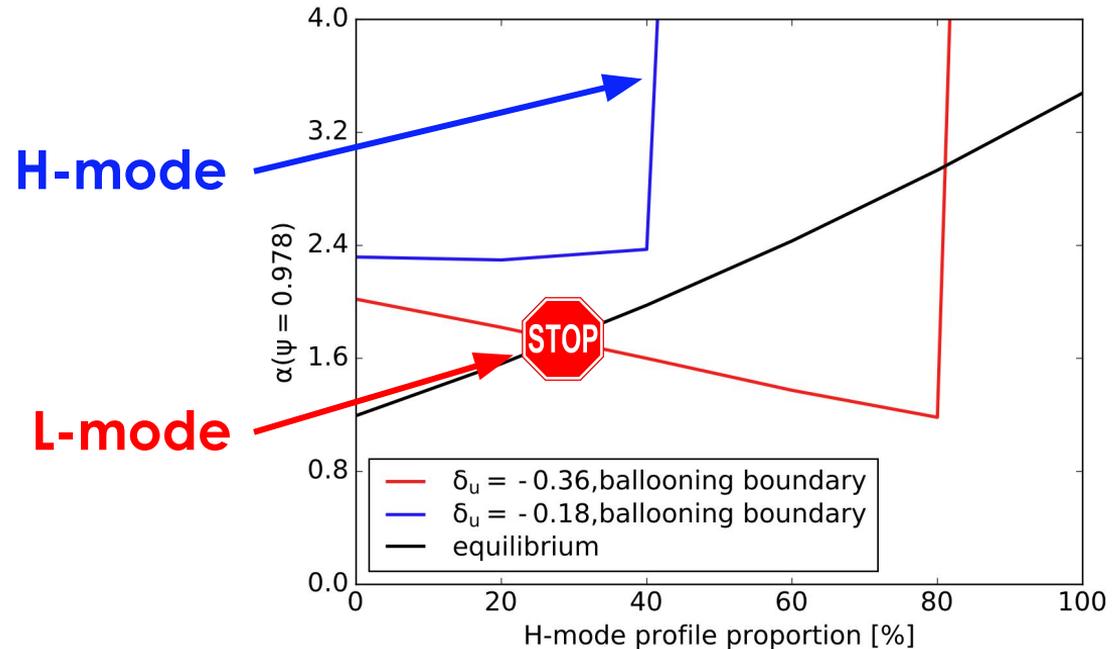
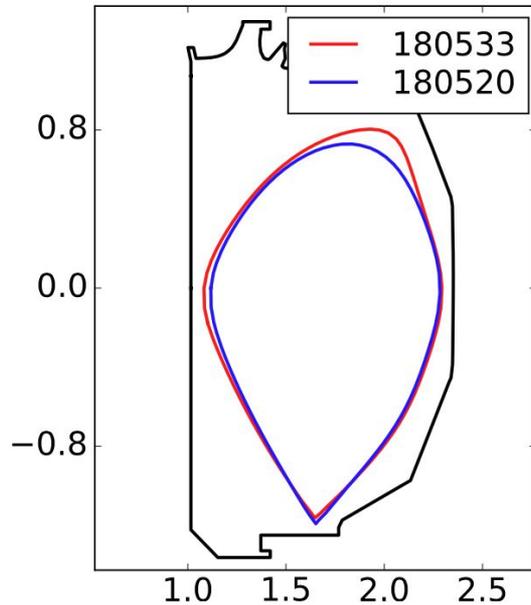
$$\hat{s}(r, \theta) \sim s(r) - \alpha(r) \cos \theta$$

- Shear stabilization prop. to  $\hat{s}^2$
- 1<sup>st</sup> stability region:
  - As  $s$  increases,  $\max(\alpha)$  increases
- 2<sup>nd</sup> stability region:
  - Requires  $\alpha > s$  to achieve  $\hat{s} \ll 0$



# DIII-D H-modes limited by $n = \infty$ ballooning modes (1/2)

- A slight change in  $\delta_u$  responsible for loss of H-mode on DIII-D
  - correlated with loss of access to the second stability region!

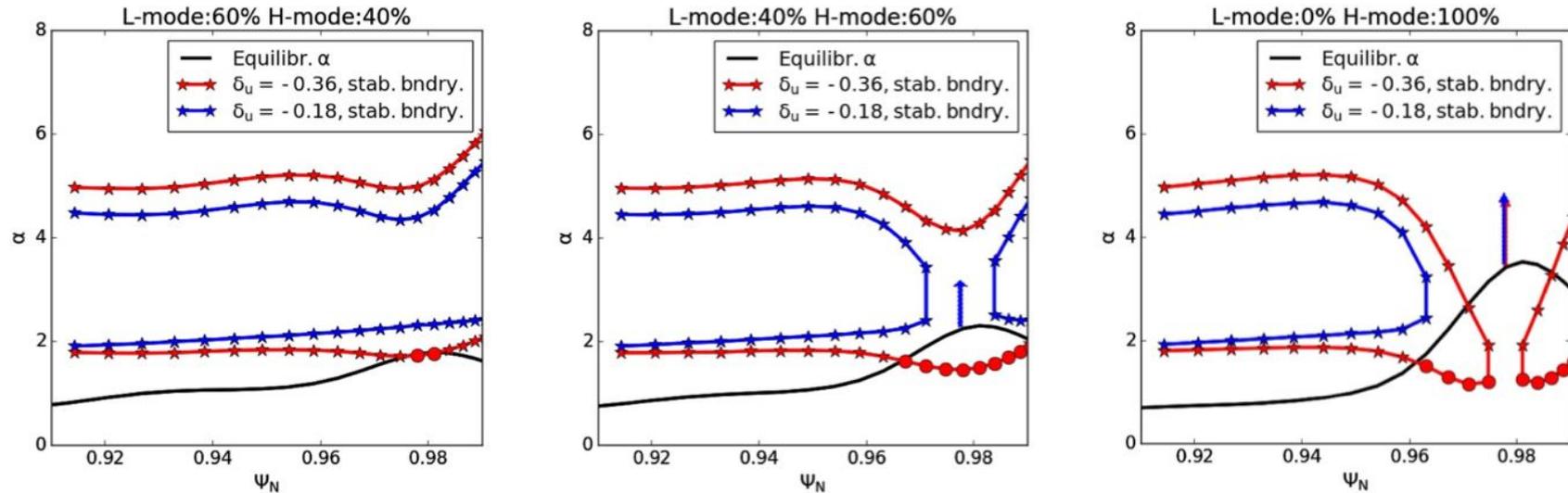


Saarelma, et. al. PPCF (2021)



# DIII-D H-modes limited by $n = \infty$ ballooning modes (2/2)

- Ballooning stability boundaries can be calculated in 1D
  - a function of both the **plasma profiles** and the **equilibrium shape**

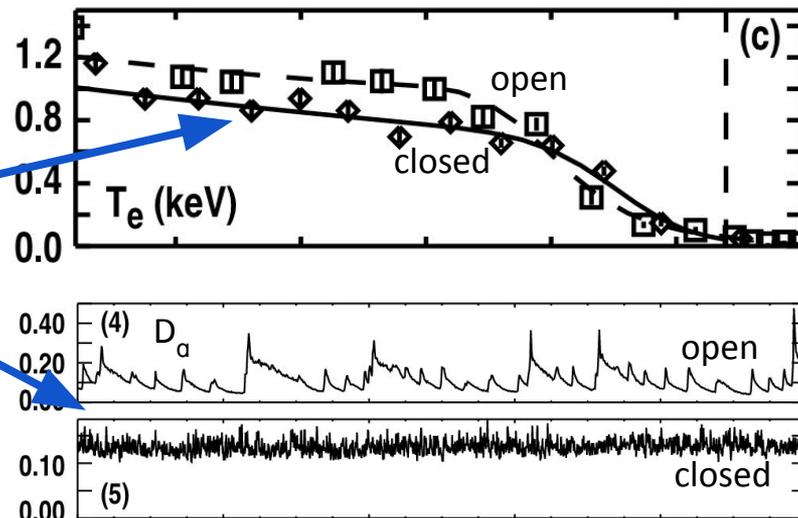


- At strong shaping, ballooning modes clamp pedestal gradients

Saarelma, et. al. PPCF (2021)

# Caveats: 1<sup>st</sup>-stable operation not strictly L-mode

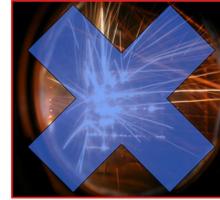
- On DIII-D, C-Mod, ASDEX, JT-60U (and others?), H-mode operation in the 1<sup>st</sup> stability regime has been reported
- Generally associated with:
  - High shear / collisionality
  - Reduced pedestal pressures
  - Increased ELM frequency
  - Decreased ELM amplitude
- Neg-D on DIII-D: ELMs suppressed with increased NBI heating (Guanying Yu)



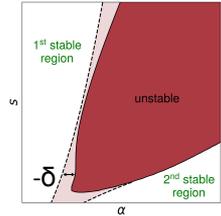
Ferron, et. al. NF (2000)

# Outline

- Introduction to Negative Triangularity



- H-mode suppression in Neg-D: a case of ballooning instability?



- How does shape impact second stability access?
- Extrapolation of ballooning physics to reactors

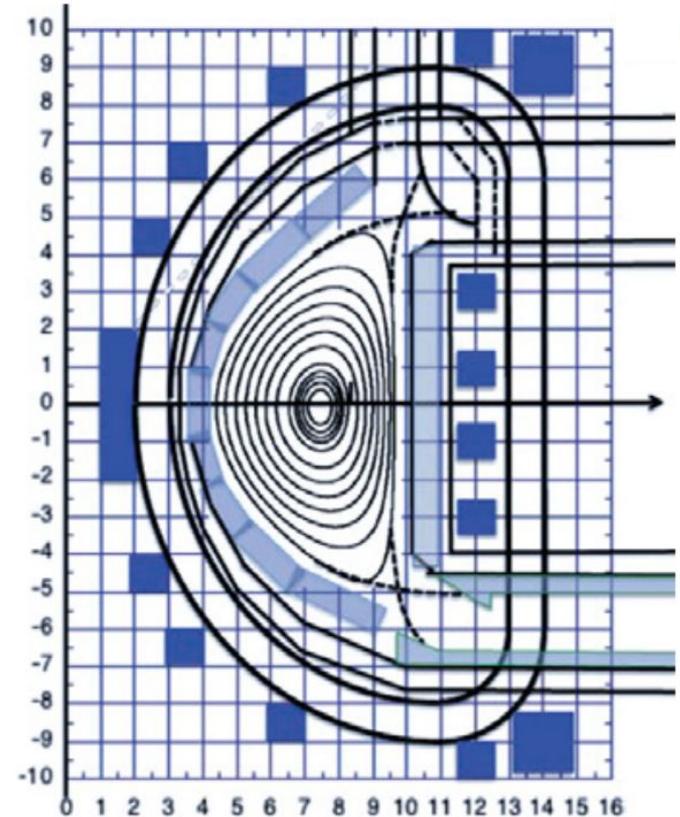
# Goals and methods

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- Understand broadly how shape impacts second stability access
  - Will Neg-D reactors still be in L-mode?
  - Are there other alternatives for shape-based H-mode suppression?
- CHEASE used for equilibria generation
- BALOO used for infinite- $n$  ballooning calculation
- Profiles from EPED parameterization
- Bootstrap current self-consistently calculated from Sauter definitions

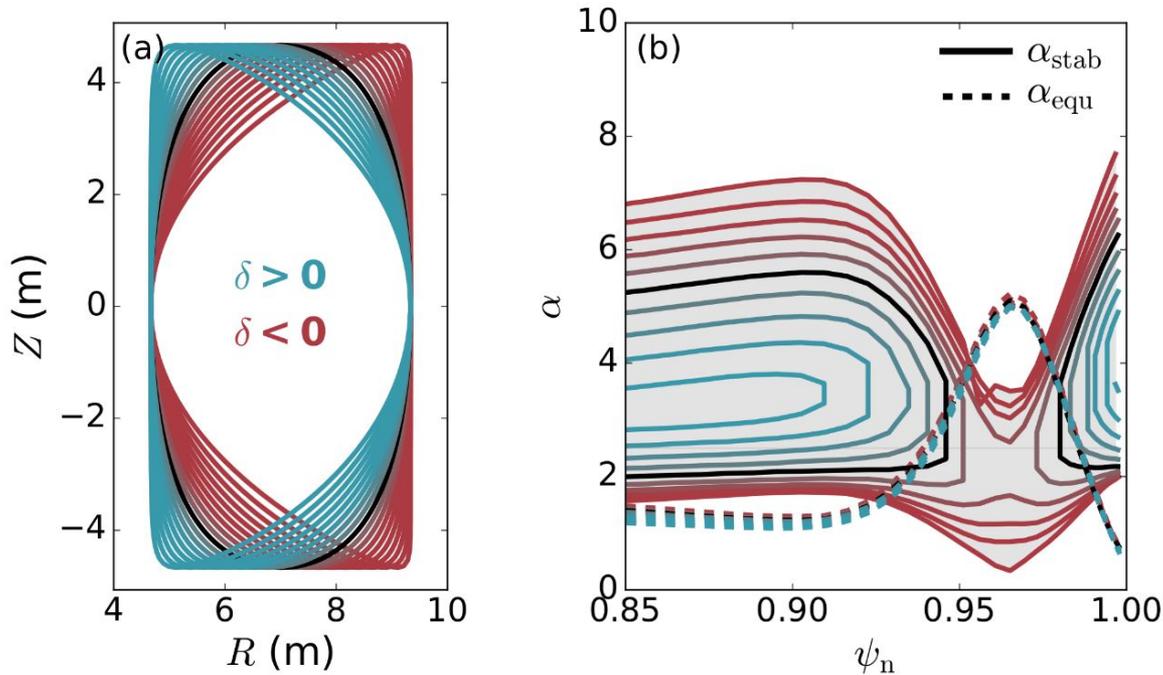
# Base equilibria from neg-D reactor study

- Base target:
  - $R_0 = 7$  m
  - $\kappa = 2$
  - $B_0 = 6$  T
  - $\beta_N = 2.5$
  - $a_{\text{minor}} = 2.6$  m
  - $\zeta = 0.1$
  - $I_p = 15$  MA
- Everything will be scanned....
- Configuration with  $\delta = -0.8$  already analyzed with KINX
  - Pedestals in the 1<sup>st</sup> stable region

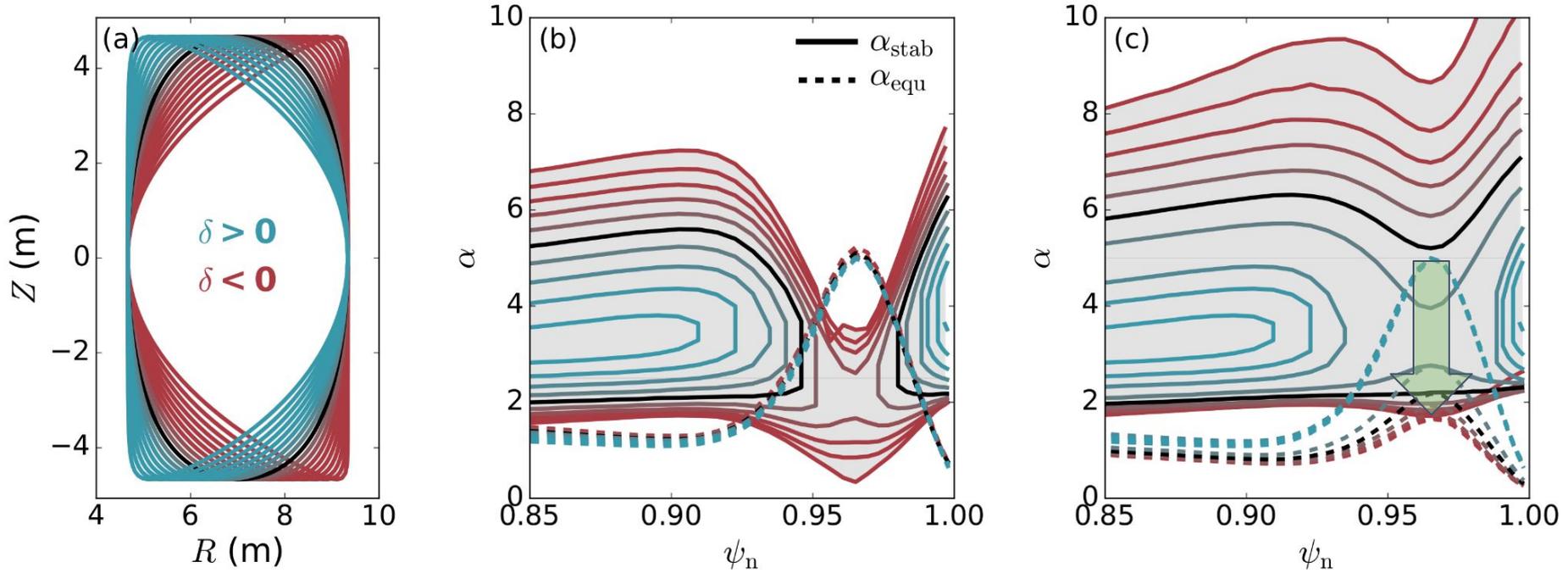


Medvedev, et. al. NF (2015)

# Reduced triangularity closes second stability region

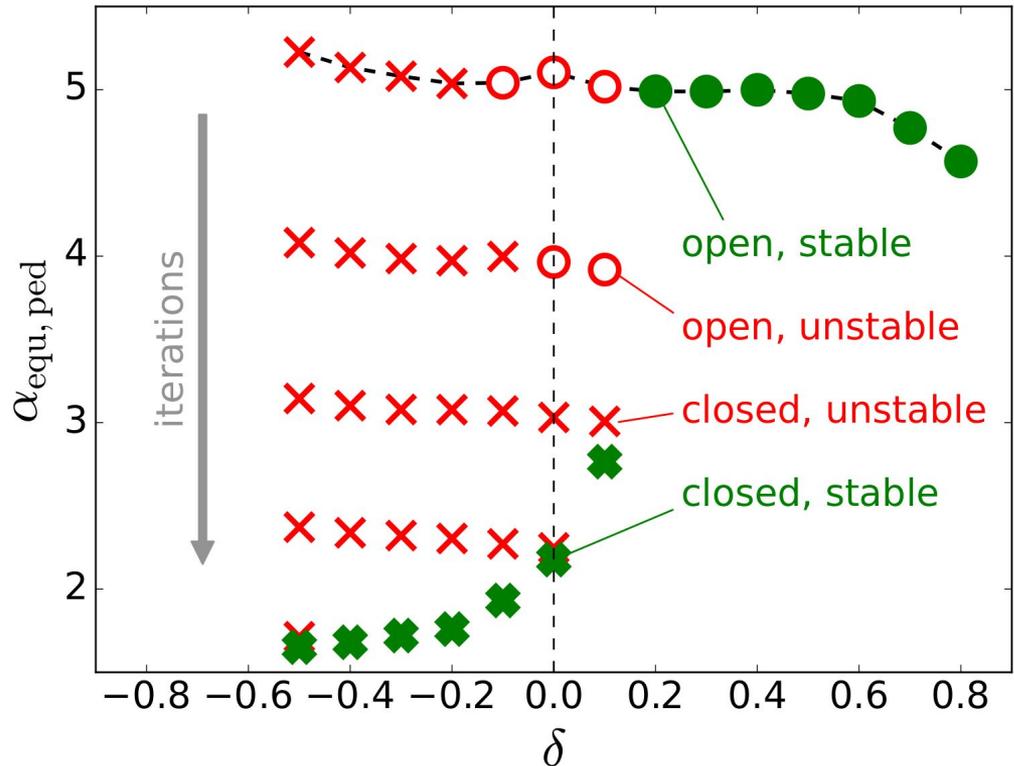


# Pedestal height reduced to maintain MHD stability



# Reduced $\delta < 0$ leads to reduced edge pressure

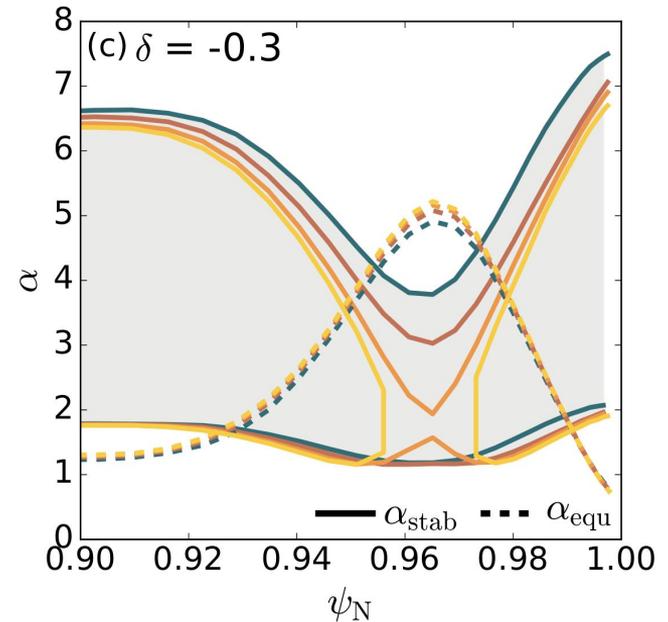
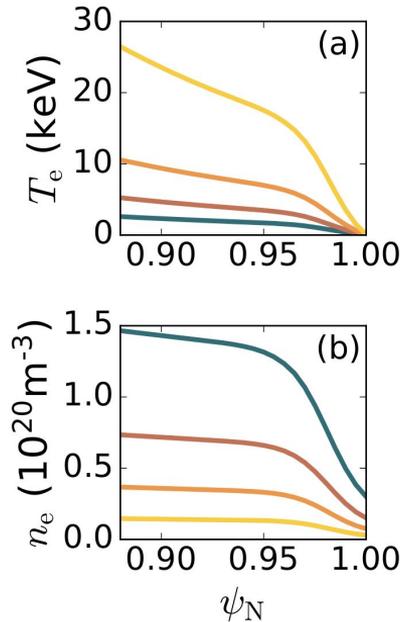
- Pedestal height is iteratively decreased until maximum stable profile is found
- Critical  $\delta$  exists for which 2<sup>nd</sup> stability can be accessed
- Ballooning-limited pedestal height decreases with  $\delta < 0$



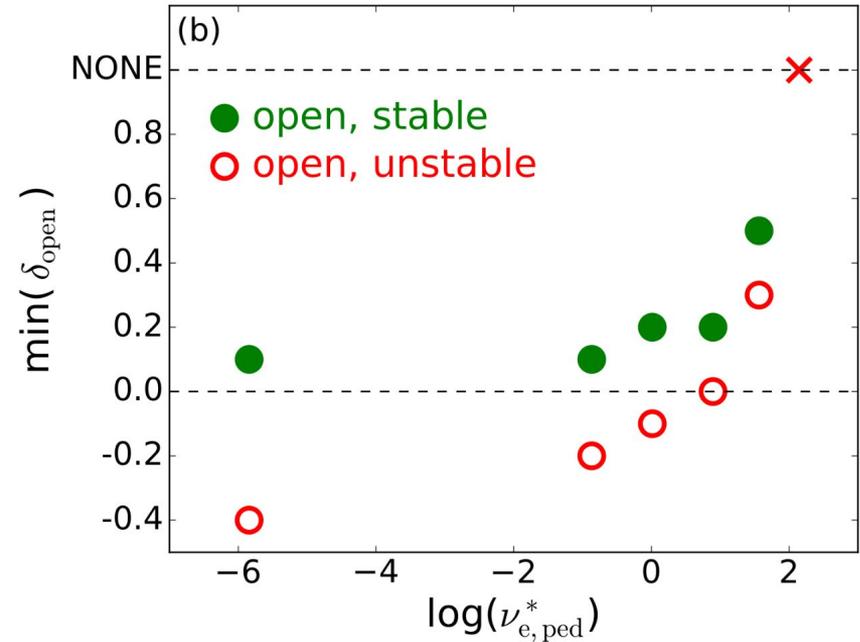
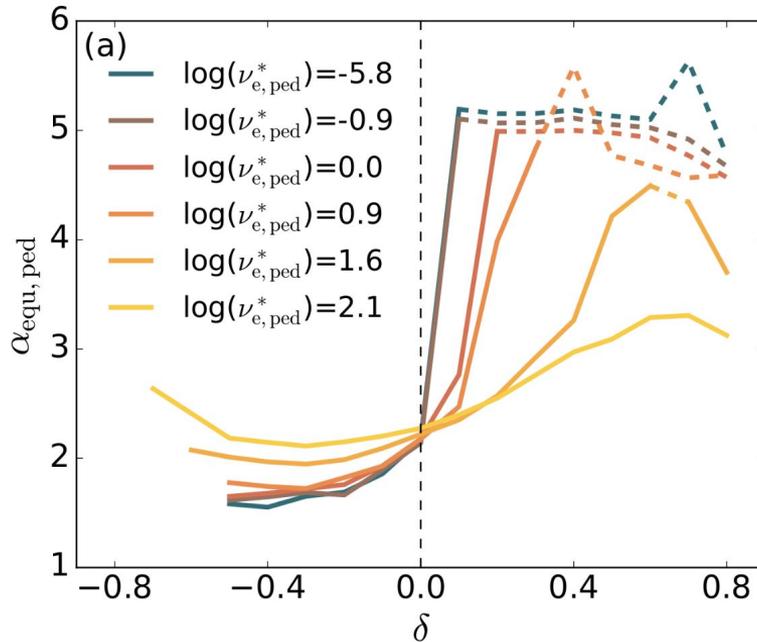


# Details of the kinetic profiles also impact stability

- We can play with:  $\mathbf{T/n} \uparrow \rightarrow \mathbf{v} \downarrow \rightarrow \mathbf{Jboot} \uparrow \rightarrow \mathbf{s} \downarrow$
- With enough bootstrap current, access to the second stability region can be achieved even at  $\delta \ll 0$ !

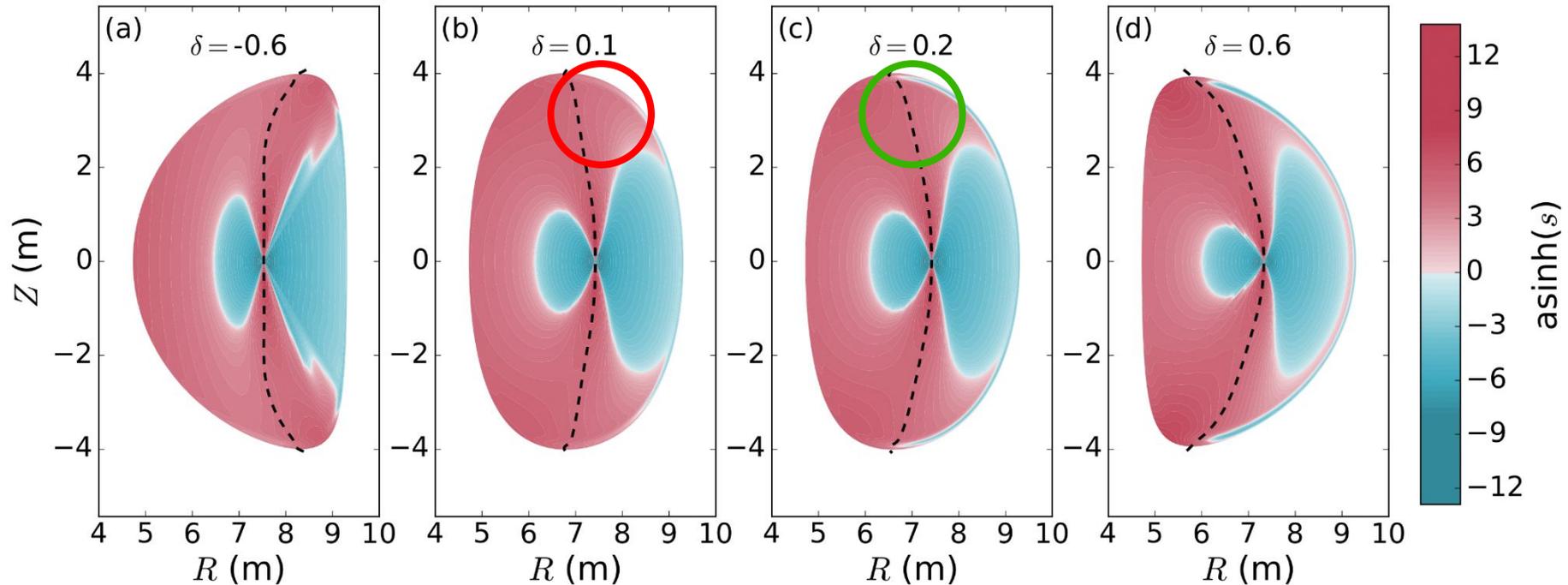


# Large changes in $\nu^*$ needed to change access



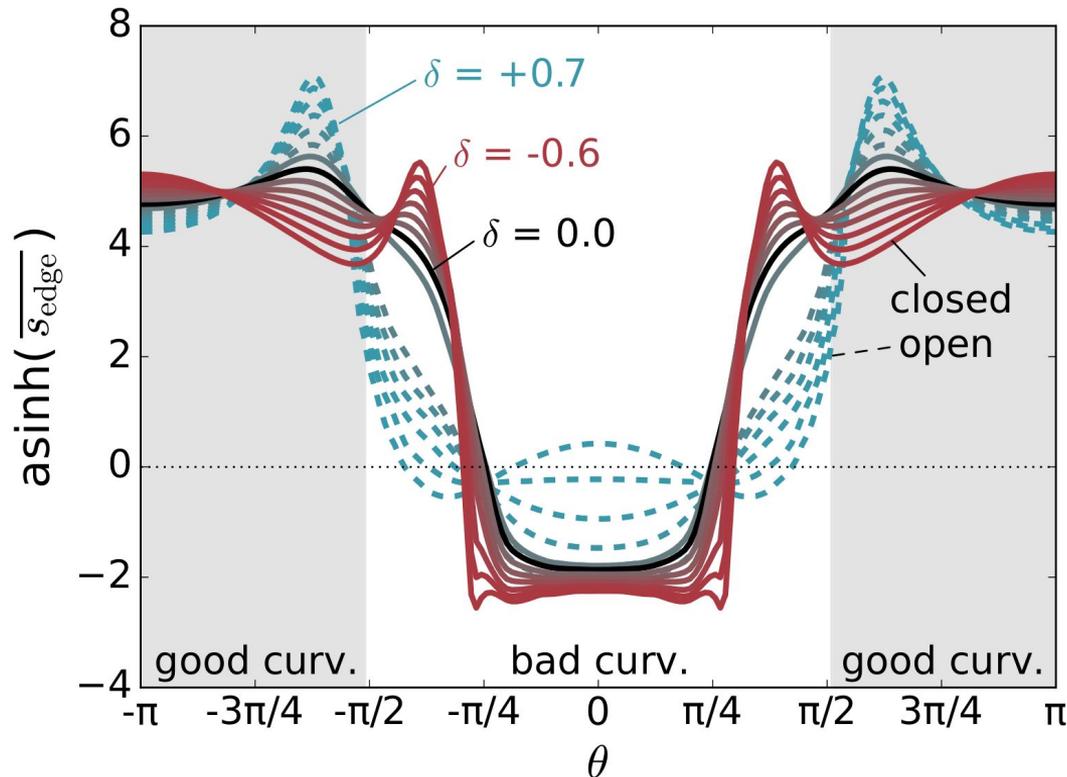
# Why this effect? Triangularity modifies local shear!

- Local shear defined as: 
$$s \equiv -\frac{\vec{B} \times \nabla\psi}{|\nabla\psi|^2} \cdot \nabla \times \left( \frac{\vec{B} \times \nabla\psi}{|\nabla\psi|^2} \right)$$

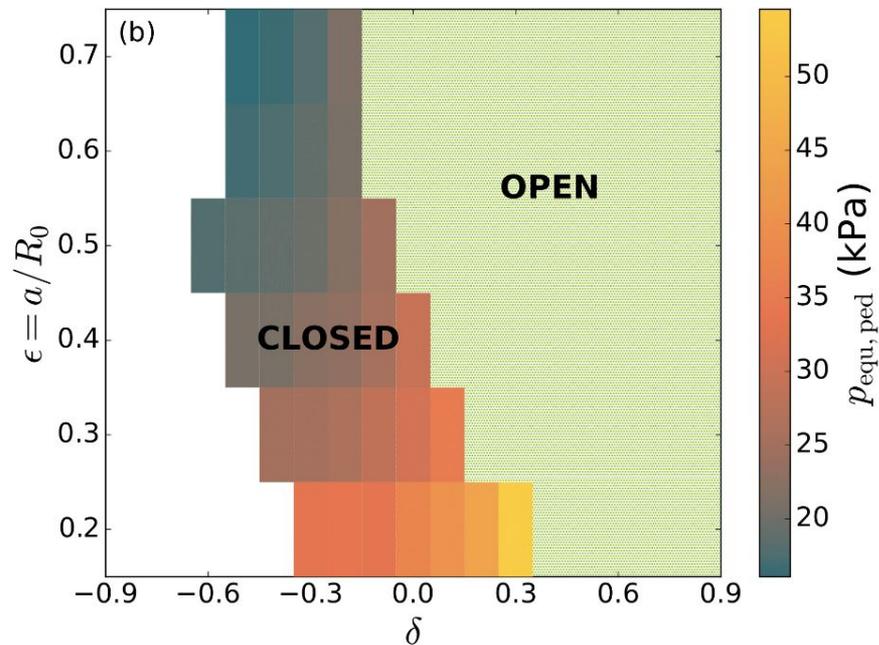
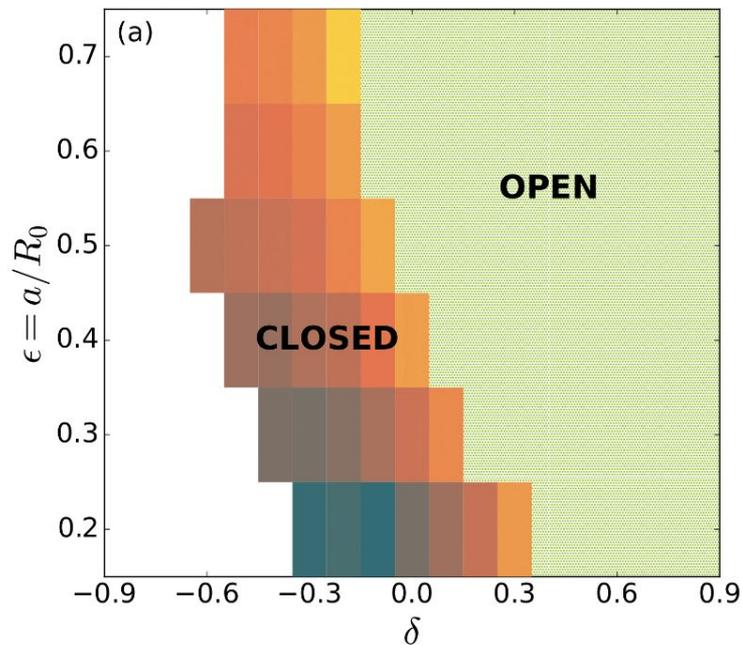


# Increased local shear in bad curv. prevents 2<sup>nd</sup> stability

- Local shear strong function of geometry
- When peak of shear profile ventures into the bad curv. region, access to 2nd stability is lost!
- This forces a LFS zero-crossing  
-> destabilizing



# Decreased aspect ratio enables H-mode at lower $\delta$

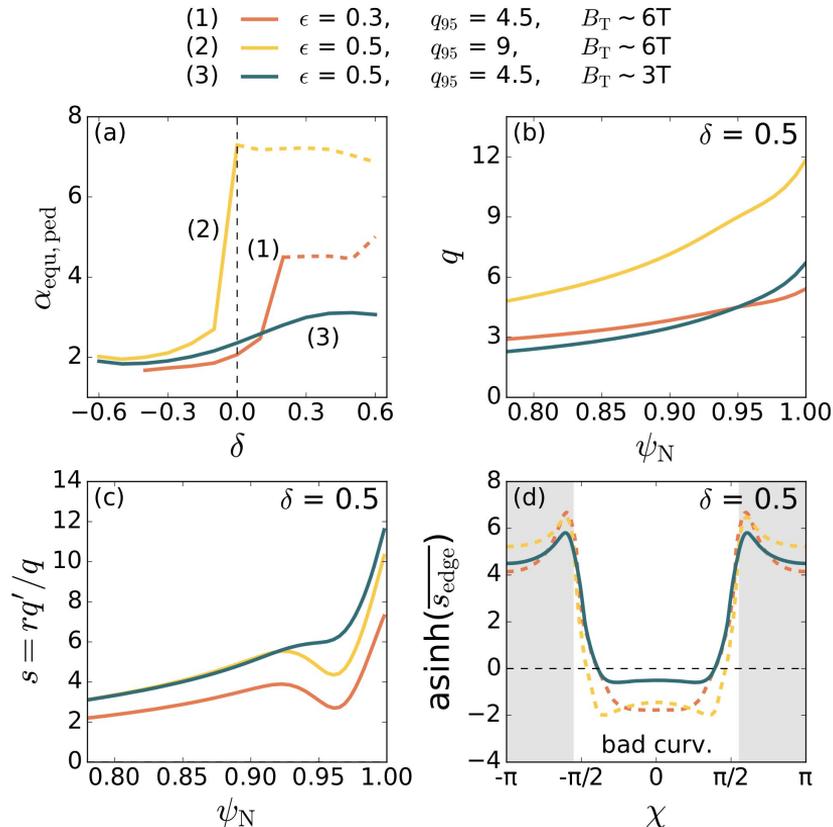


# Three effects important for stability in $\delta - \epsilon$ space

1. Strengthening of  $B_p$  on bad curv. side
  - High- $\beta$  gives rise to large Shafranov shift
  - Shortens “bad curv. connection length”
2. At low aspect ratio, local shear in bad curv. region is diminished
  - As  $\beta$  increases, LFS local shear decreases
  - Facilitates shear reversal at high enough  $\beta$
3. At low aspect ratio and high  $q$ , favorable curvature is enhanced
  - Suppresses unfavorable contribution of  $B_p$  to  $\kappa_n$

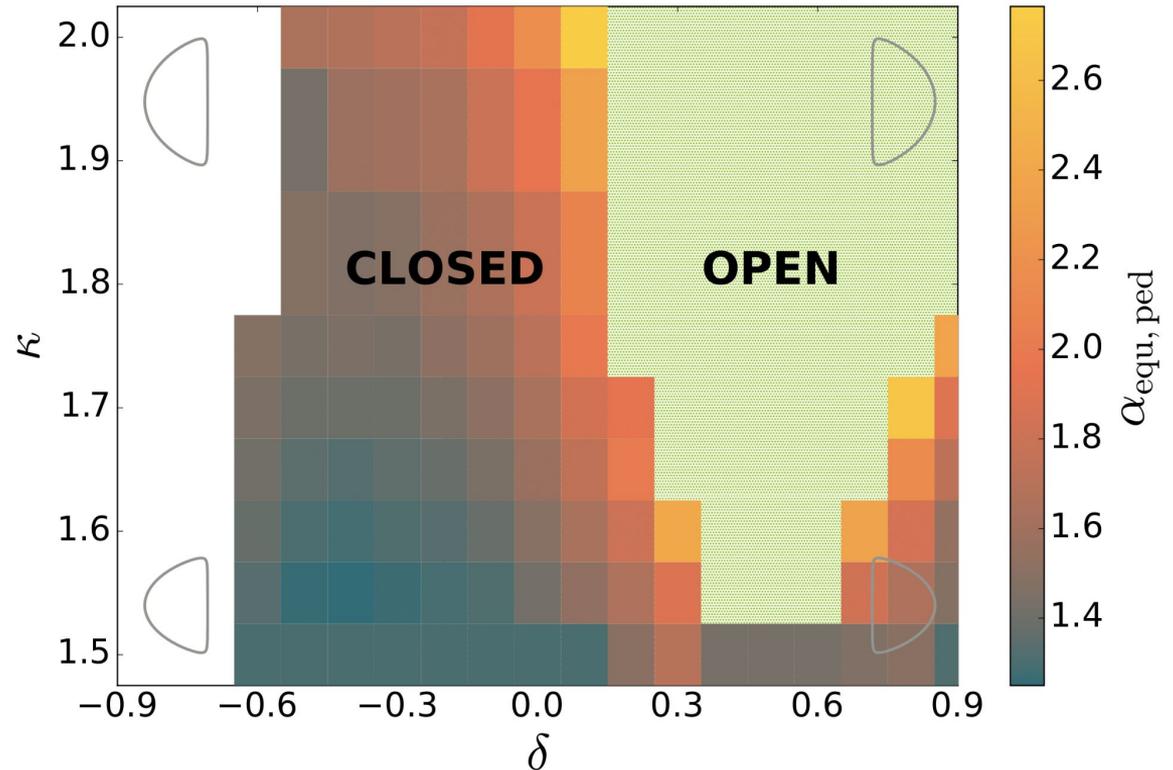
# Local shear must be sufficiently negative for stability

- Increase  $\epsilon$  at constant  $B_p, I_p$ :
  - $q_{95}$  increases
  - $\delta_{crit}$  decreases
  - $\max(\alpha)$  increases
- Increase  $\epsilon$  at constant  $q_{95}, I_p$ :
  - $B_T$  drops
  - $\delta_{crit}$  increases
  - $\max(\alpha)$  increases
- At low  $q_{95}$ , high  $\epsilon$ , local shear is not low enough!



# At low elongation, 2<sup>nd</sup> stability access fully closes

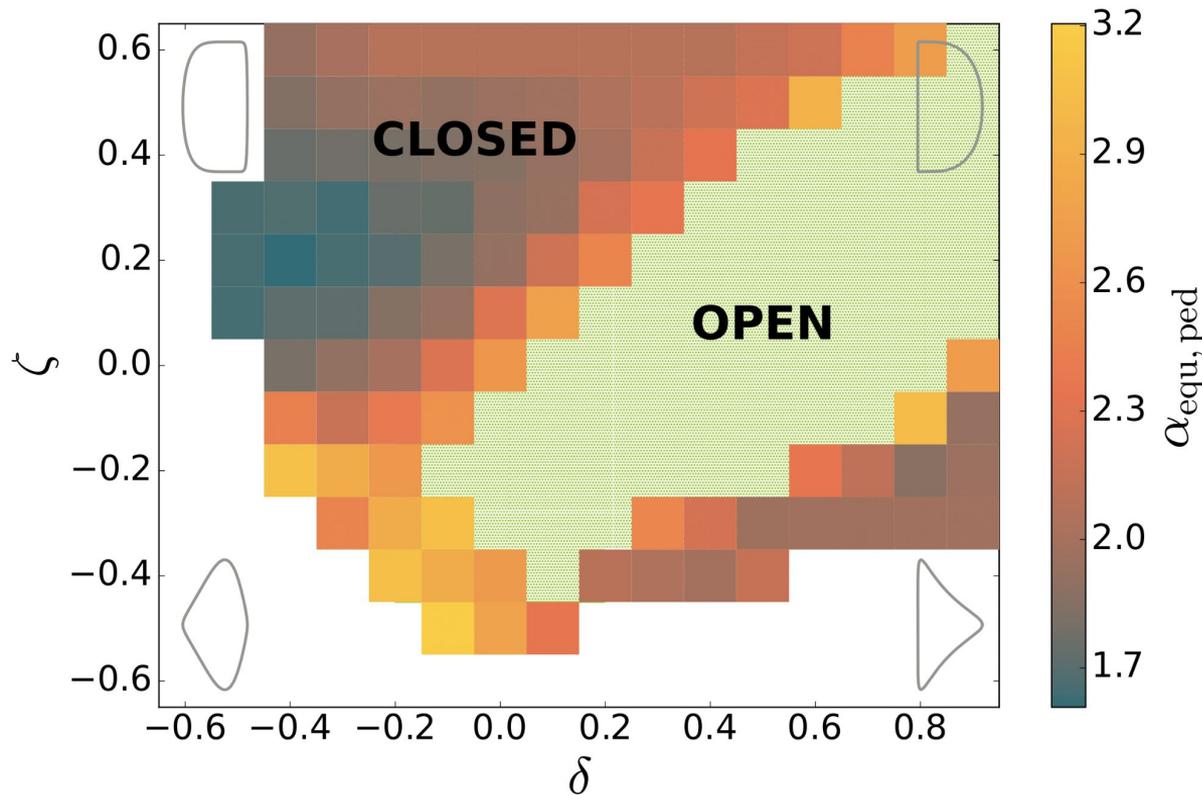
- At large  $\kappa$ , stability is relatively unaffected
- At small  $\kappa$ , 2<sup>nd</sup> stability is closed for all  $\delta$
- Lower ballooning-limited pedestals at high  $\kappa$



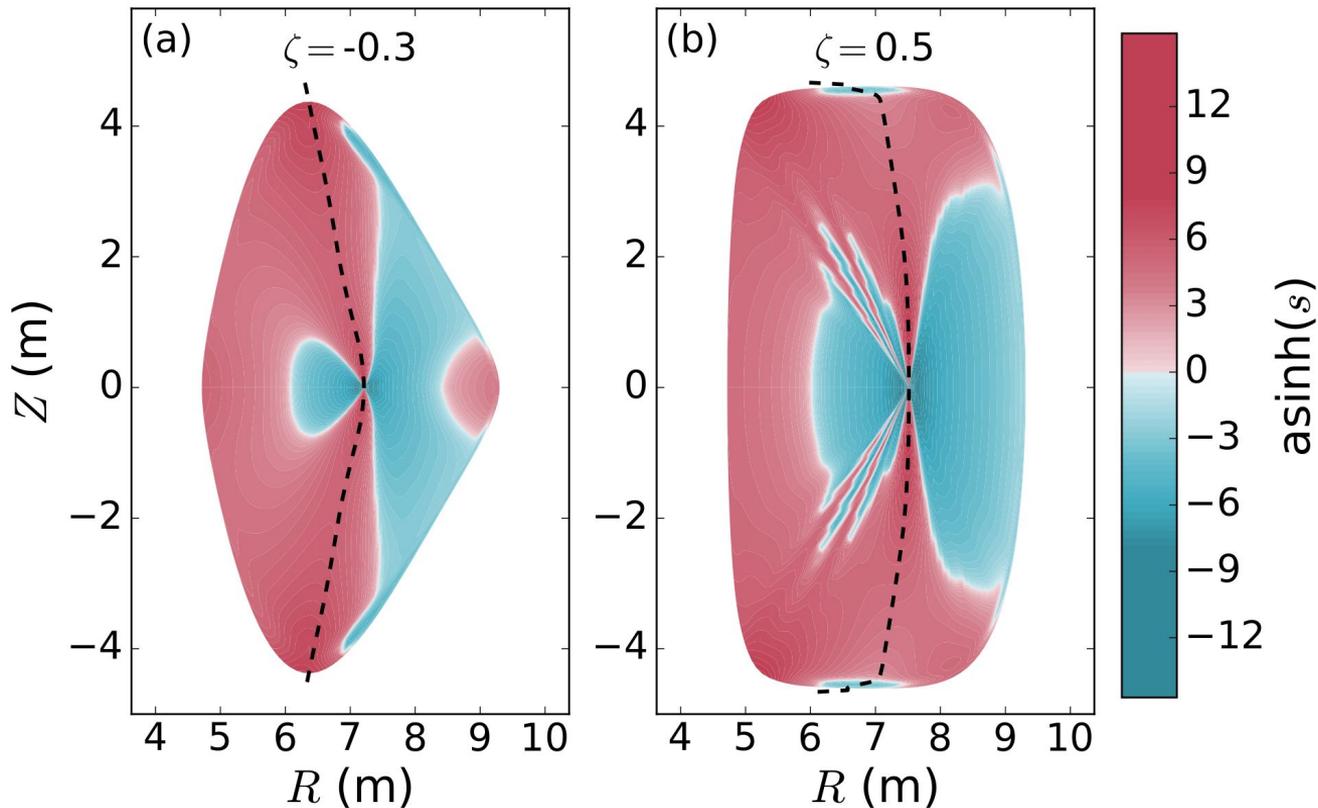


# For stability, squareness cannot be too high or too low

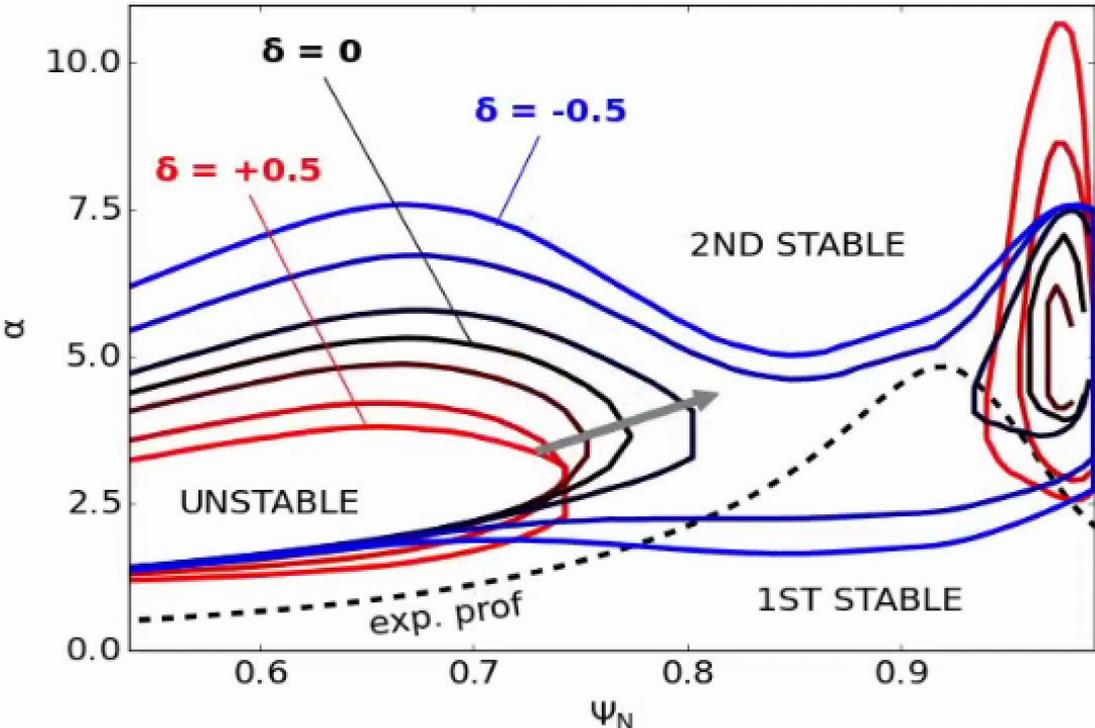
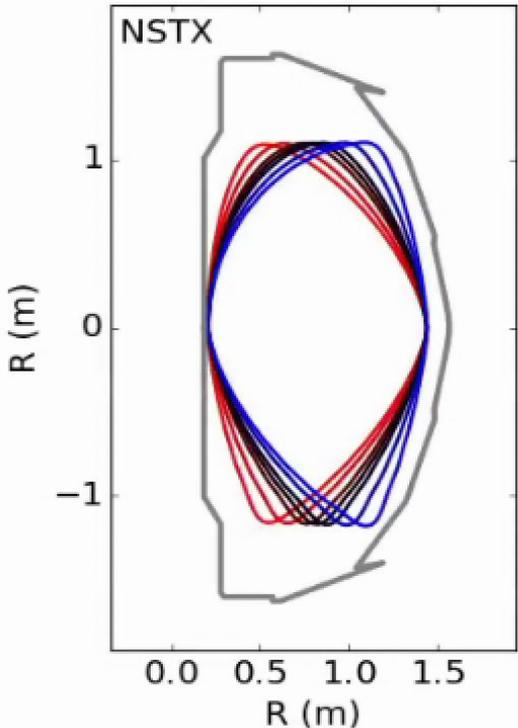
- Medium squareness needed for 2<sup>nd</sup> stability access
- Still a strong function of  $\delta$ !
- Similar to old DIII-D experiments



# Extreme squareness also modifies bad curv. local shear!

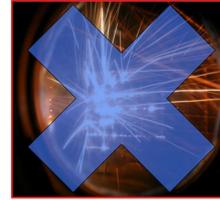


# Bonus: NSTX H-mode suppression through Neg-D



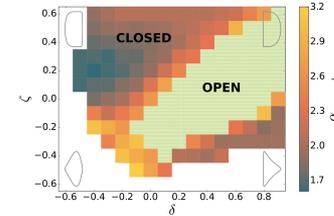
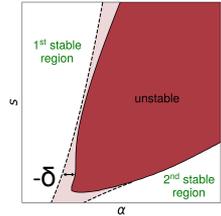
# Outline

- Introduction to Negative Triangularity



- H-mode suppression in Neg-D: a case of ballooning instability?

- How does shape impact second stability access?

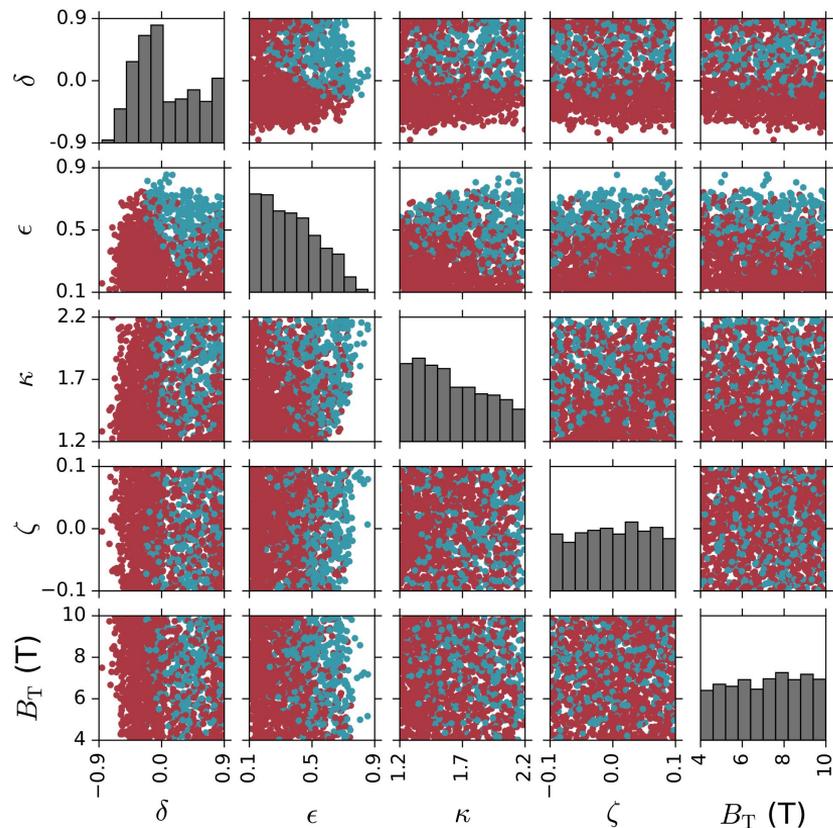


- Extrapolation of ballooning physics to reactors

# Database of >1500 random equilibria generated

- Parameters selected from:

-0.9	>	$\delta$	>	0.9
0.1	>	$\epsilon$	>	0.9
1.2	>	$\kappa$	>	2.2
-0.1	>	$\zeta$	>	0.1
2 m	>	$a_{\text{minor}}$	>	4.5 m
4 T	>	$B_T$	>	10 T
8 MA	>	$I_p$	>	20 MA
$0.5e20 \text{ m}^{-3}$	>	$n_{e,\text{ped}}$	>	$2e20 \text{ m}^{-3}$
$1e20 \text{ m}^{-3}$	>	$n_{e,\text{core}}$	>	$3e20 \text{ m}^{-3}$
1 keV	>	$T_{e,\text{ped}}$	>	2.5 keV
15 keV	>	$T_{e,\text{ped}}$	>	3 keV
0.03	>	$\Delta_{\text{ped}}$	>	0.07



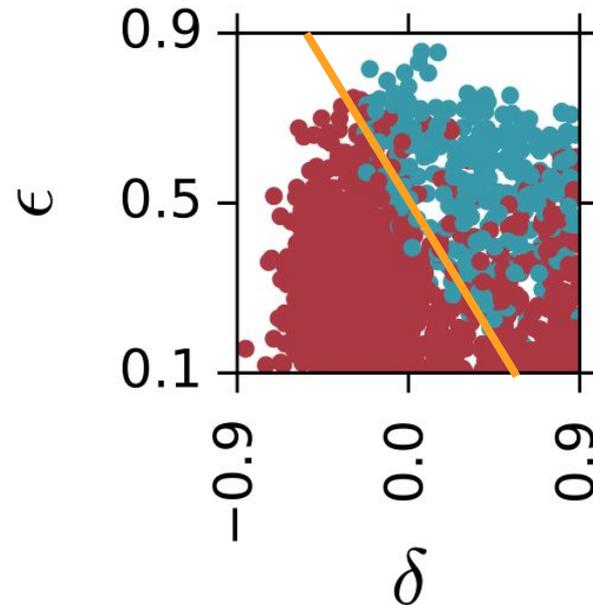
# Simple linear classification can ~predict stability access

- Best LDA predictor (89% accuracy score):

$$x = 15.629 - 0.419B_T - 13.140\epsilon - 3.096\kappa - 3.361\delta + 3.450\zeta$$

- Predicted stable if:  $\frac{1}{1 + \exp(x)} > 0.5$

- Using only  $\delta$  and  $\epsilon$ , already accuracy of 84%
- Adding collisionally has no strong effect
  - Shape is most important!

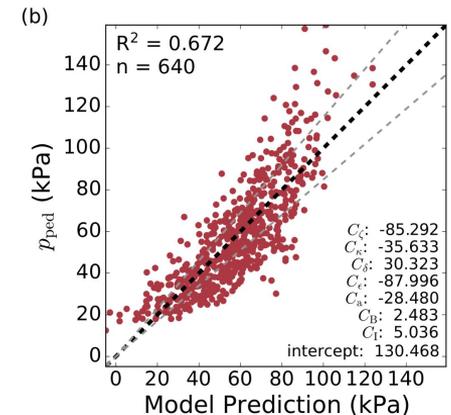
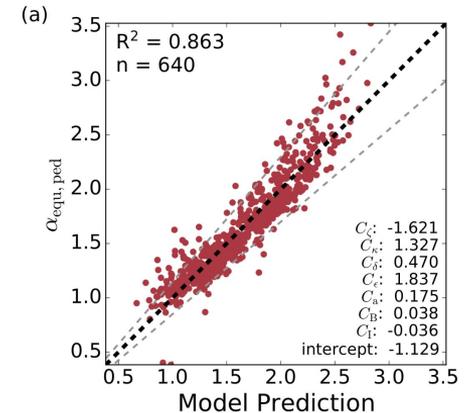


# Scalings to maximum pedestal height available

- For cases where the maximum edge pressure is limited by ballooning modes, pedestal limit fit by:

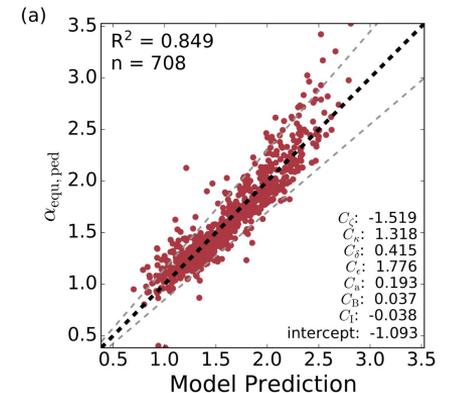
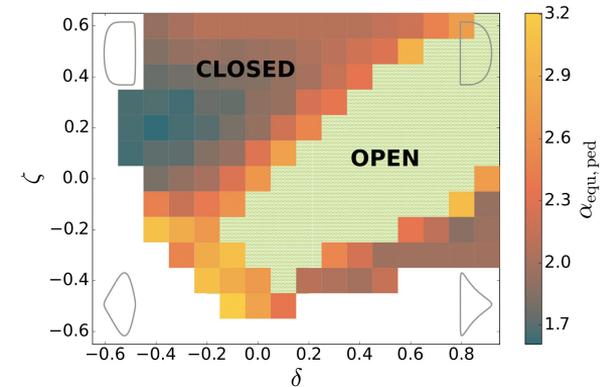
$$\alpha_{\text{equ,ped}} = C_0 + C_\kappa \kappa + C_\epsilon \epsilon + C_\delta \delta + C_\zeta \zeta \\ + C_a a_{\text{minor}}[\text{m}] + C_B B_T[\text{T}] + C_I I_p[\text{MA}]$$

- Critical stabilizing factors associated with the pressure gradient, rather than pressure itself
- Scaling available for incorporation in to systems codes, but recommend to run BALOO directly
  - BALOO module added to STEP code



# Conclusions: Neg-D reactors robustly suppress H-mode

- Neg-D presents an interesting ELM-free scenario
- H-mode suppression in Neg-D likely set by  $n = \infty$  ballooning modes, which are destabilized by increased bad curvature local shear
- Stability is a complicated function of shape!
  - Easier access at low aspect ratio
  - Restricted at low elongation
  - Restricted at large and small squareness
- Preliminary scaling laws developed for systems codes

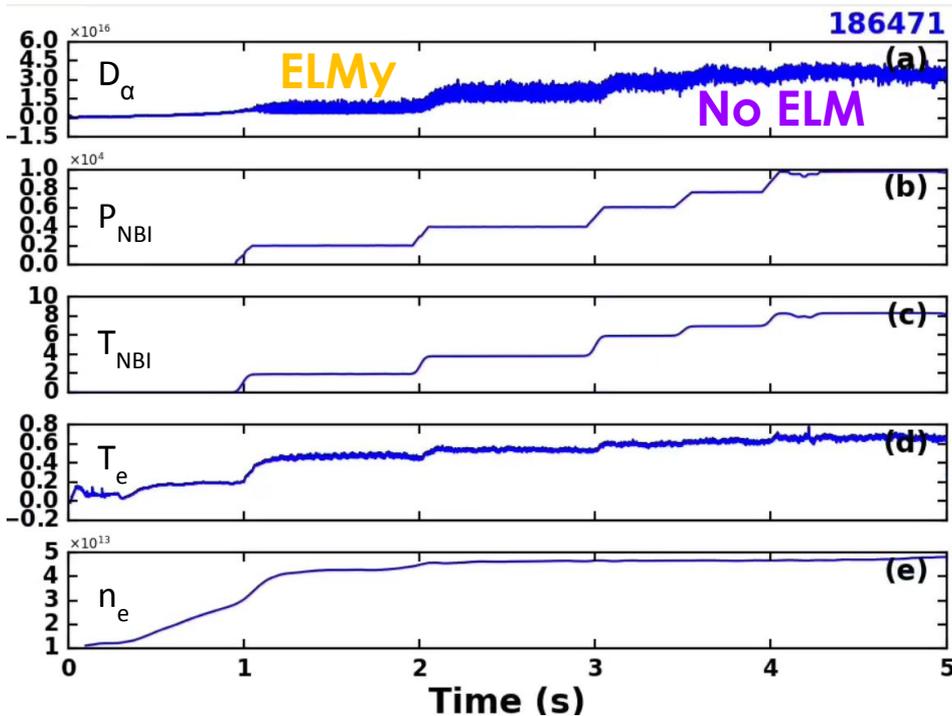




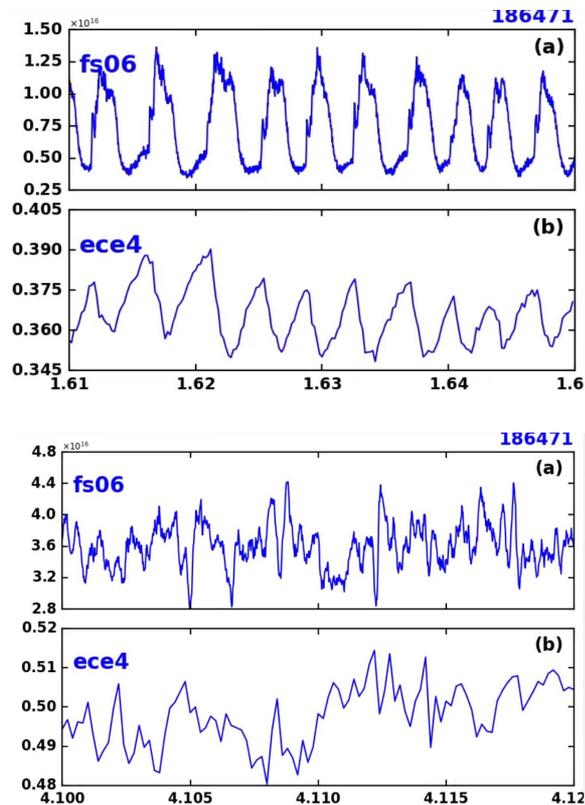
# Backup Slides

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# ELMs suppressed at high power in DIII-D neg-D ( $\delta = -0.4$ )



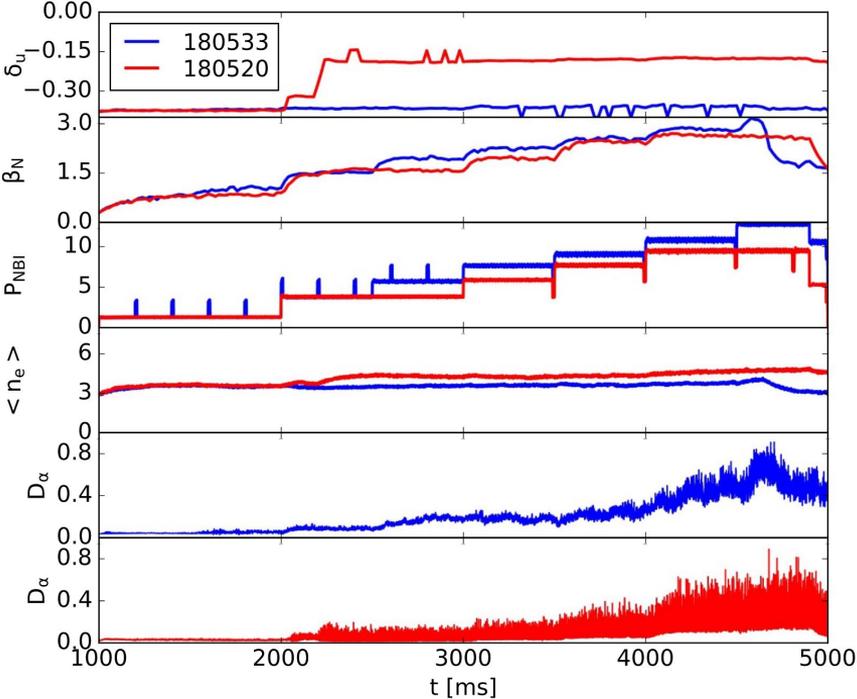
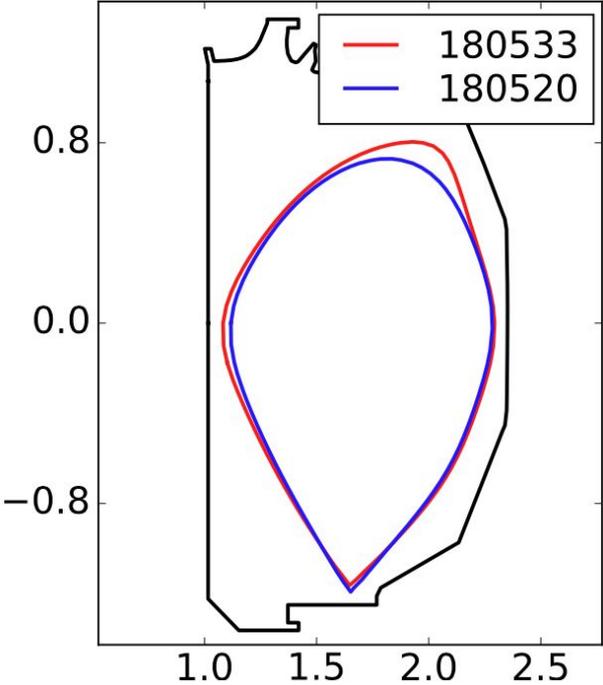
Courtesy of Guanying Yu



ELMy

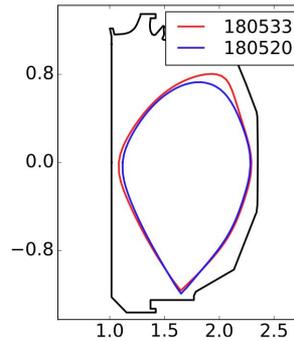
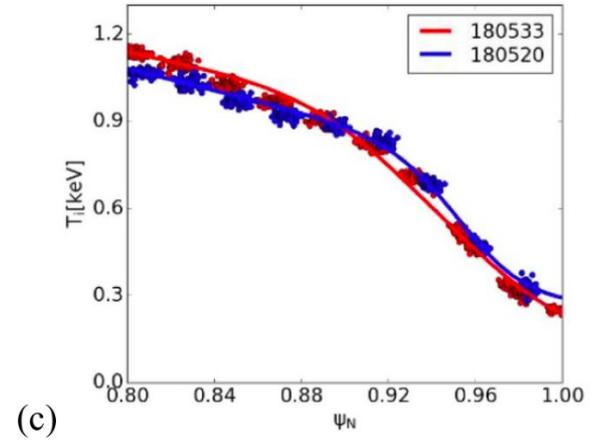
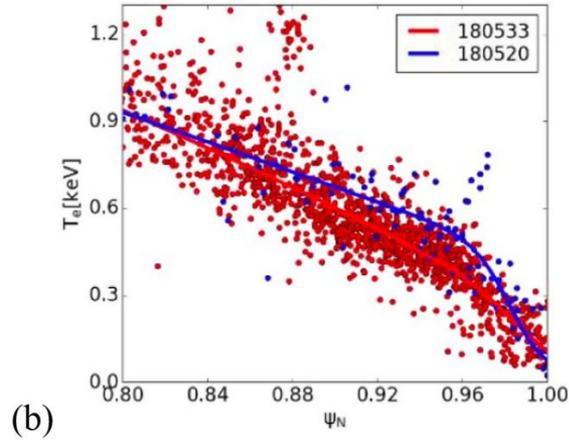
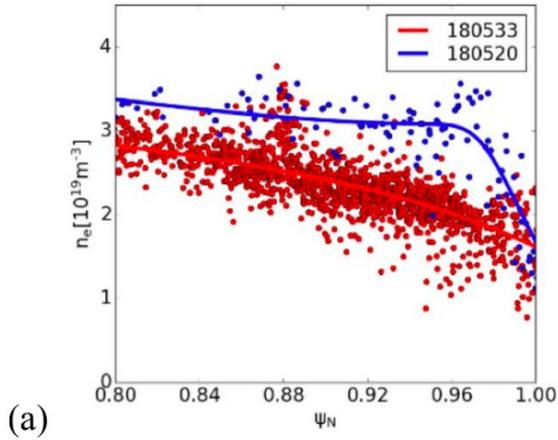
No ELM

# DIII-D NT discharges in L- and H-mode



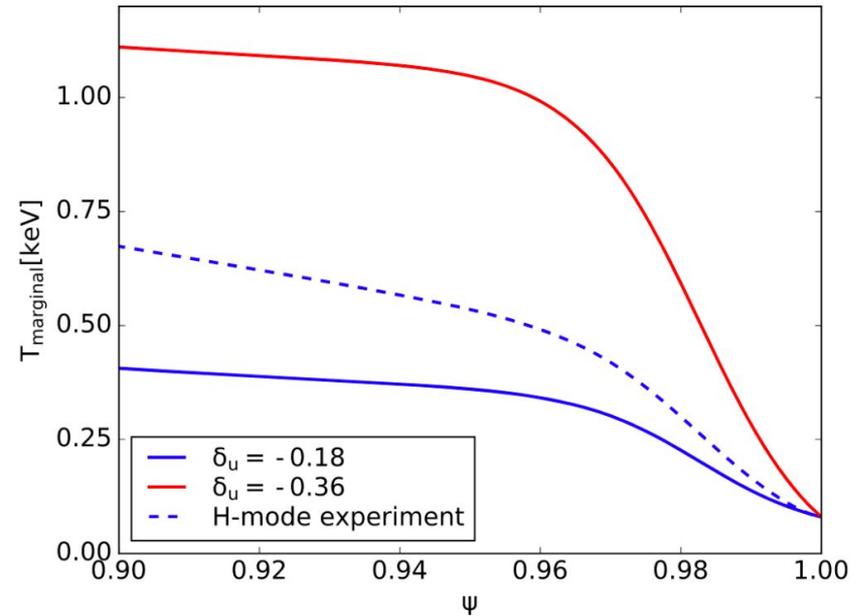
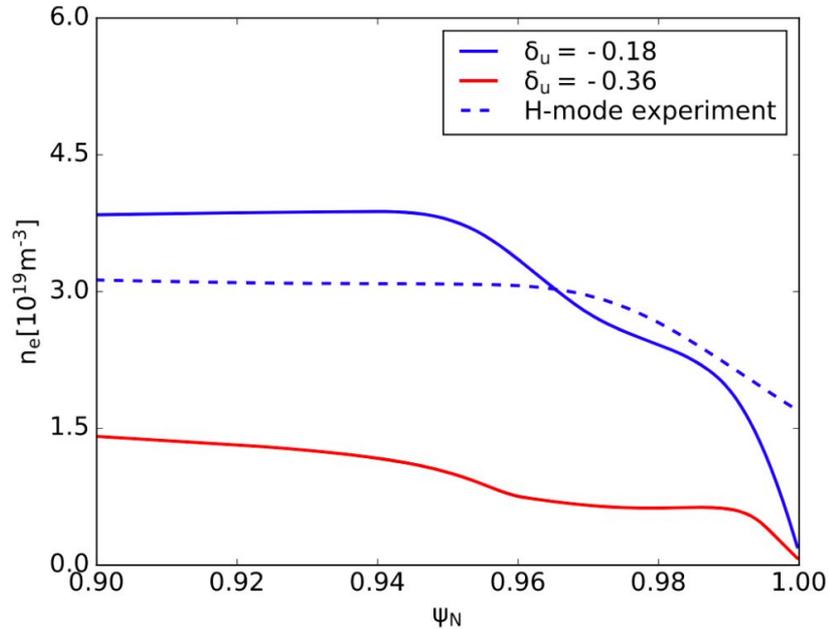
Saarelma, et. al. PPCF (2021)

# DIII-D NT profiles in L- and H-mode



Saarelma, et. al. PPCF (2021)

# Arbitrary adjustment of density profile



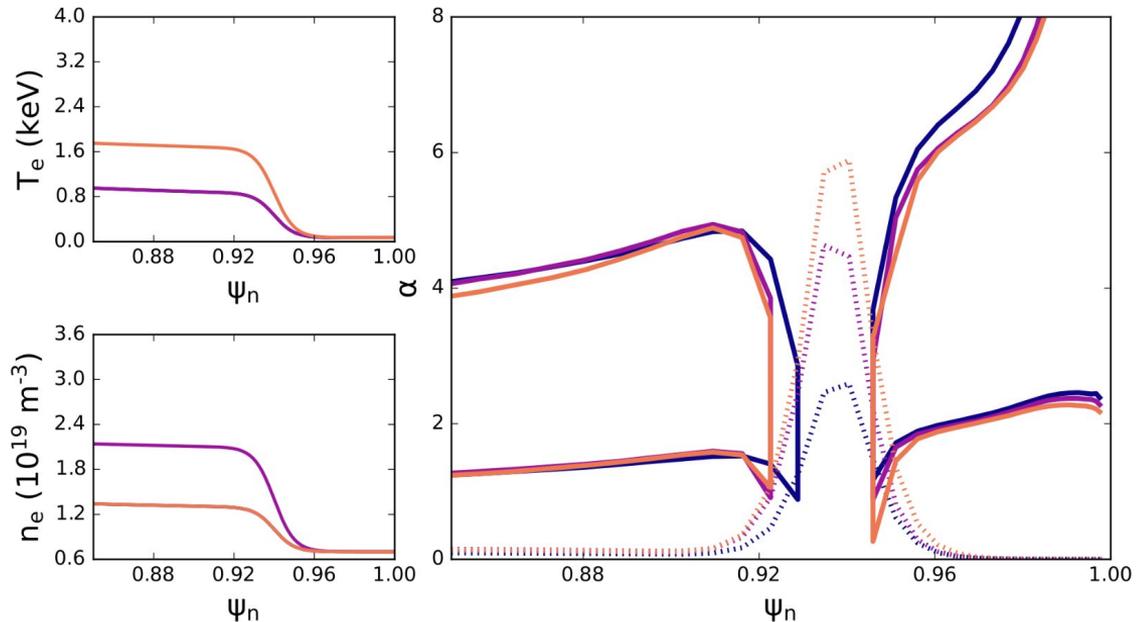
Saarelma, et. al. PPCF (2021)

# Armor H-mode access possible with arbitrary profiles

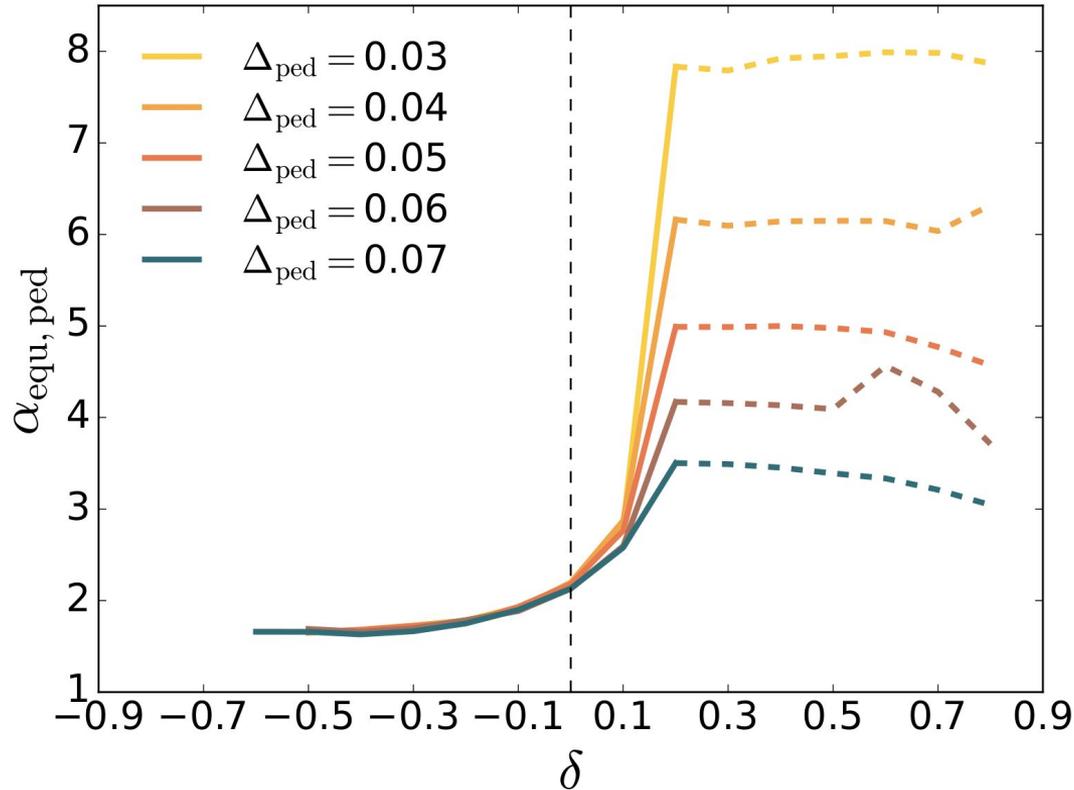
- At strong  $-\delta$ , H-mode access blocked by ballooning instability
- With arbitrary profile control, we can reopen 2<sup>nd</sup> stability access

- Profile adjustments:
  - **Steep gradient region limited to  $\psi_n = 0.93-0.95$**
  - Pedestal flattened outside of  $\psi_n = 0.96$  to avoid instability

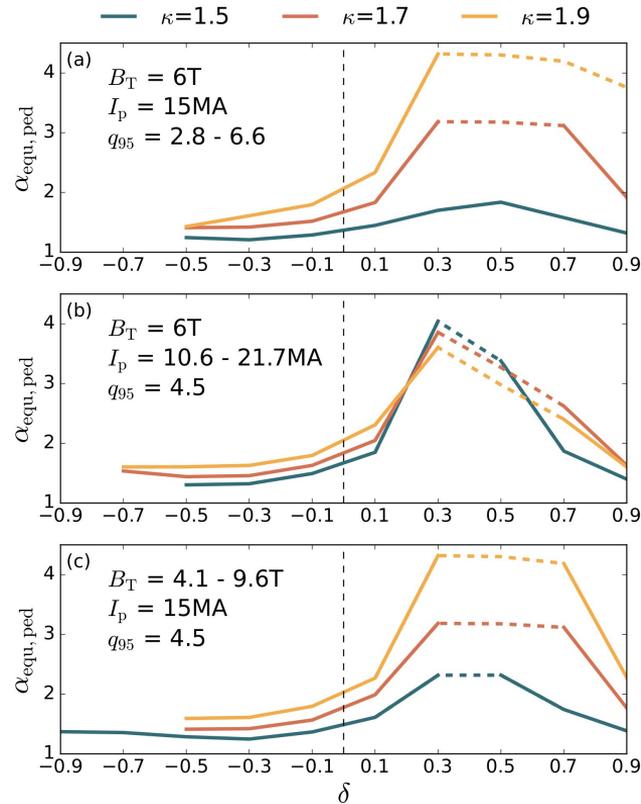
- Is this possible?



# Profile gradient dependence on pedestal width



# Elongation scans at fixed $q_{95}$





# Tests of breaking axisymmetry

