

Understanding and controlling the plasma kink mode response on DIII-D

by

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E.J. Strait², and F. Turco¹**

1. Columbia University

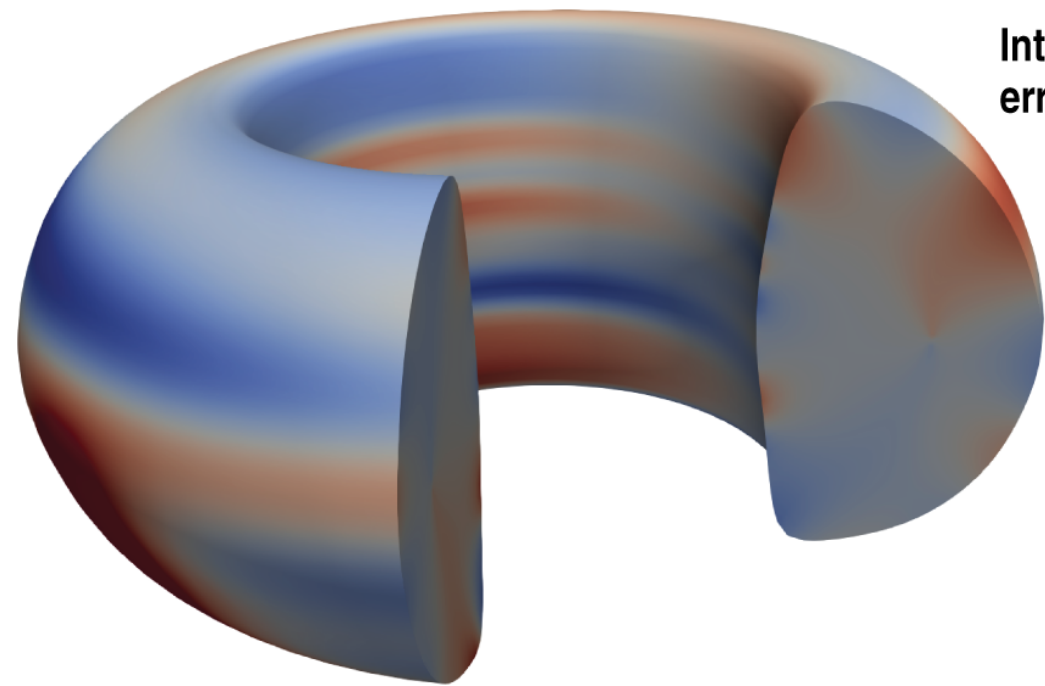
2. General Atomics

3. ITER Organization

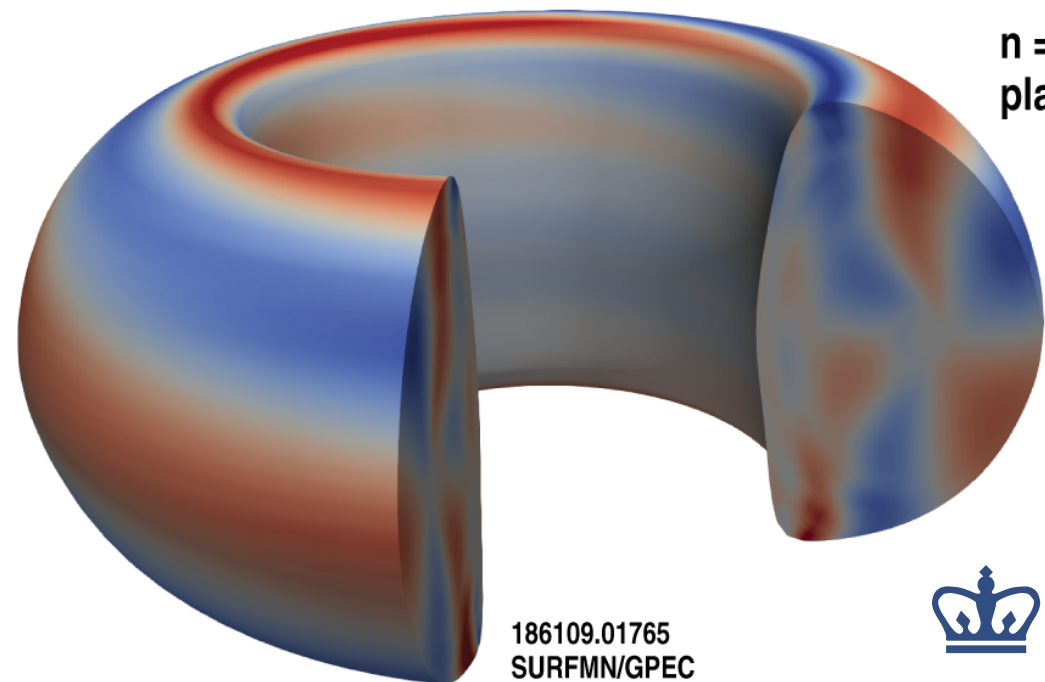
Presented at

**Princeton Plasma Physics
Laboratory**

February 10, 2025



**Intrinsic
error field**



**n = 1
plasma response**

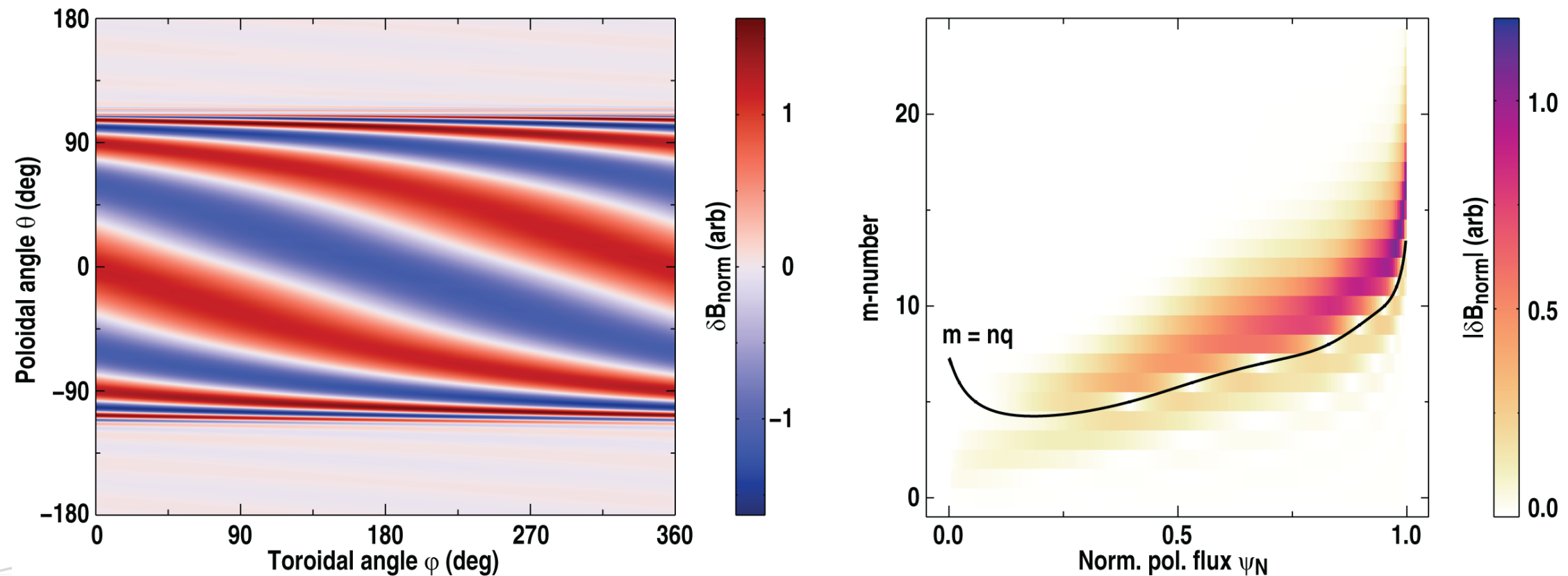
Stable tokamak kink response is useful for model validation and plasma control

The kink mode is a long-wavelength, helical distortion with $m > nq$

- Often stable but weakly damped → can be driven by applied 3D fields
- Stability boundary sets a key pressure limit

Ideal MHD least-stable $n = 1$ mode

DCON, 176078, $t = 2.45$ s



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Stable response is an observable for simulation comparisons

- Measure using applied perturbations
- Can be predicted by MHD codes

And a lever for plasma control

- Error field correction, ELM suppression

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The kink mode is a long-wavelength, helical distortion with $m > nq$

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– **Expand**
operating
space



Stable response is an observable for simulation comparisons

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And a lever for plasma control

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– **Identify**
stabilizable
regimes

– **Inform**
control
models

Outline

1. Background

- DIII-D, stable kink excitation, measurements, feedback

2. Resistive contribution to plasma response at low torque

- In the ITER baseline regime

3. Simulating feedback-controlled error field correction

- Integration of error field and MHD response codes

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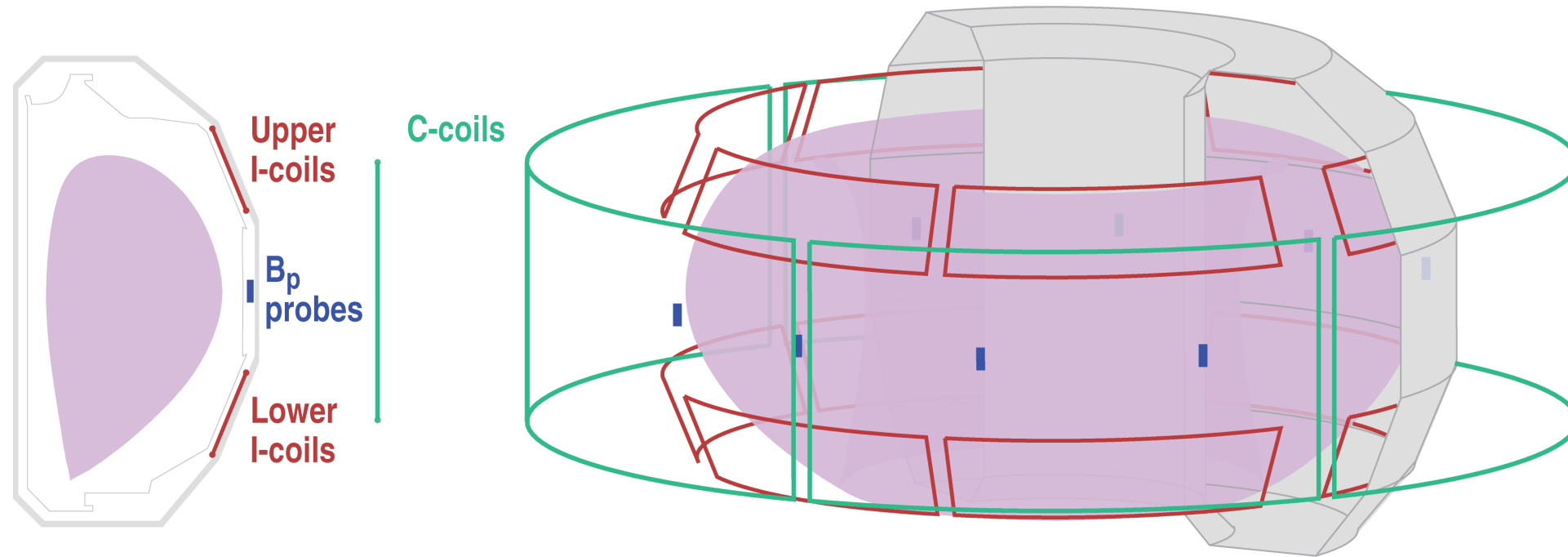
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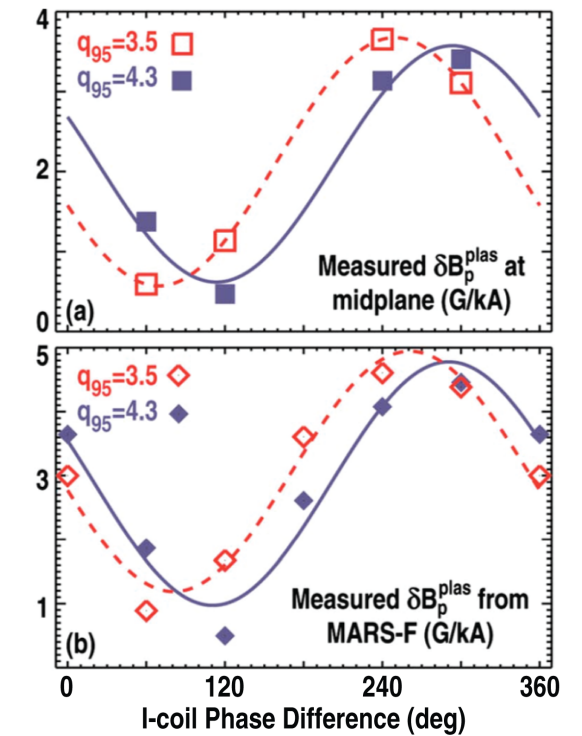
DIII-D is well equipped for 3D response studies



- **12 internal coils (I-coils)** with adjustable lower/upper phasing
- **6 external coils (C-coils)**
- **>100 pair-difference magnetic sensors**
- **Plasma rotation can be controlled** with balanced NBI
- **High disruption tolerance**

Applied 3D fields can be used to excite and control the plasma kink mode

- **Driven stable plasma response consistent with kink mode excitation predictions¹**
 - Varied poloidal structure of applied field
 - Compared two different q_{95} values



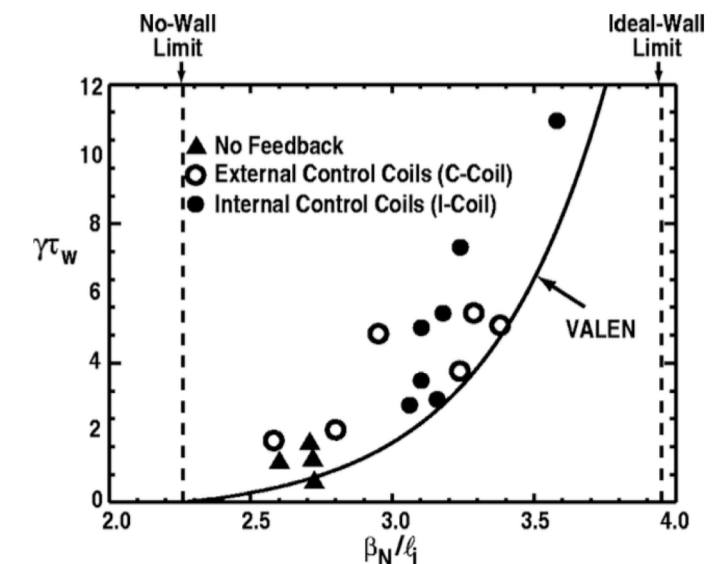
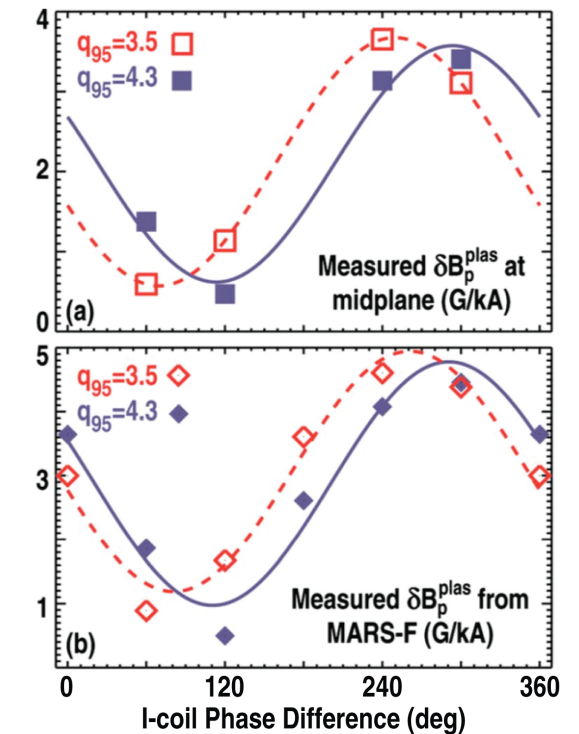
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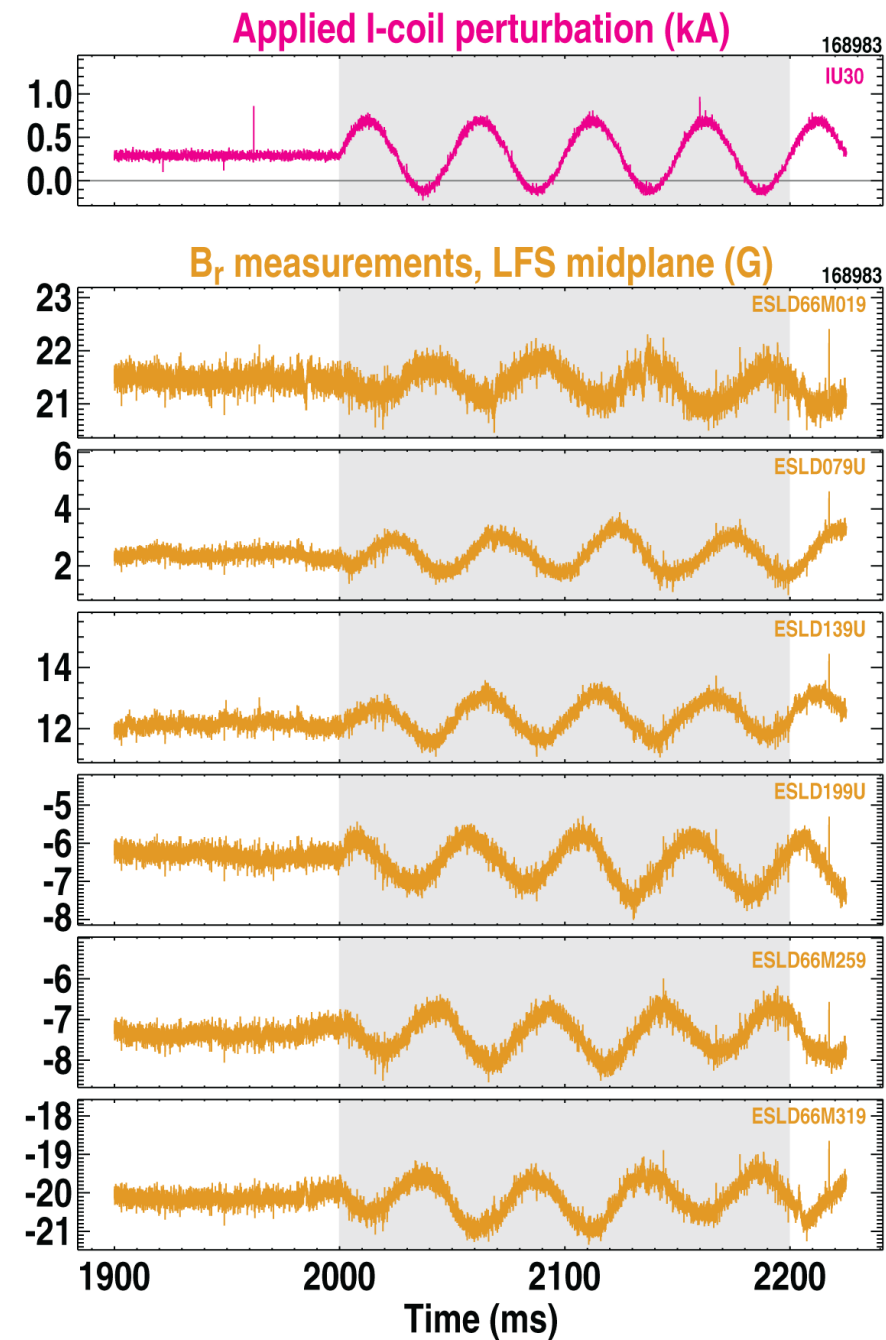
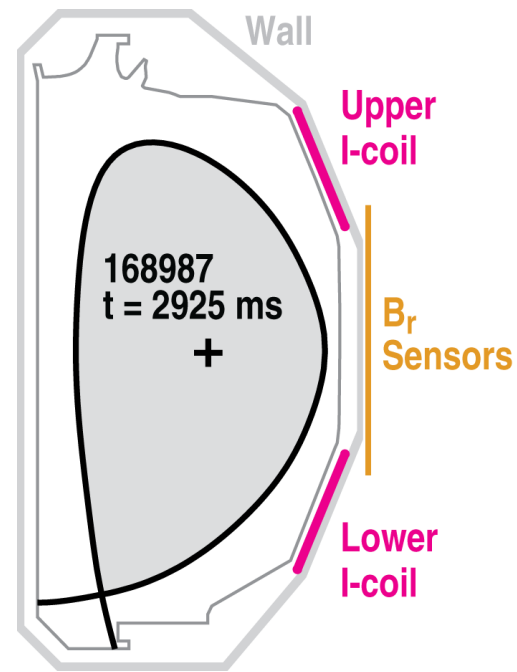
- Varied poloidal structure of applied field
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- **Unstable resistive wall mode (RWM) growth rates consistent with simulated dispersion relation²**

- Kink mode interaction with wall eddy currents = RWM
- Feedback control enables approach to ideal wall β -limit

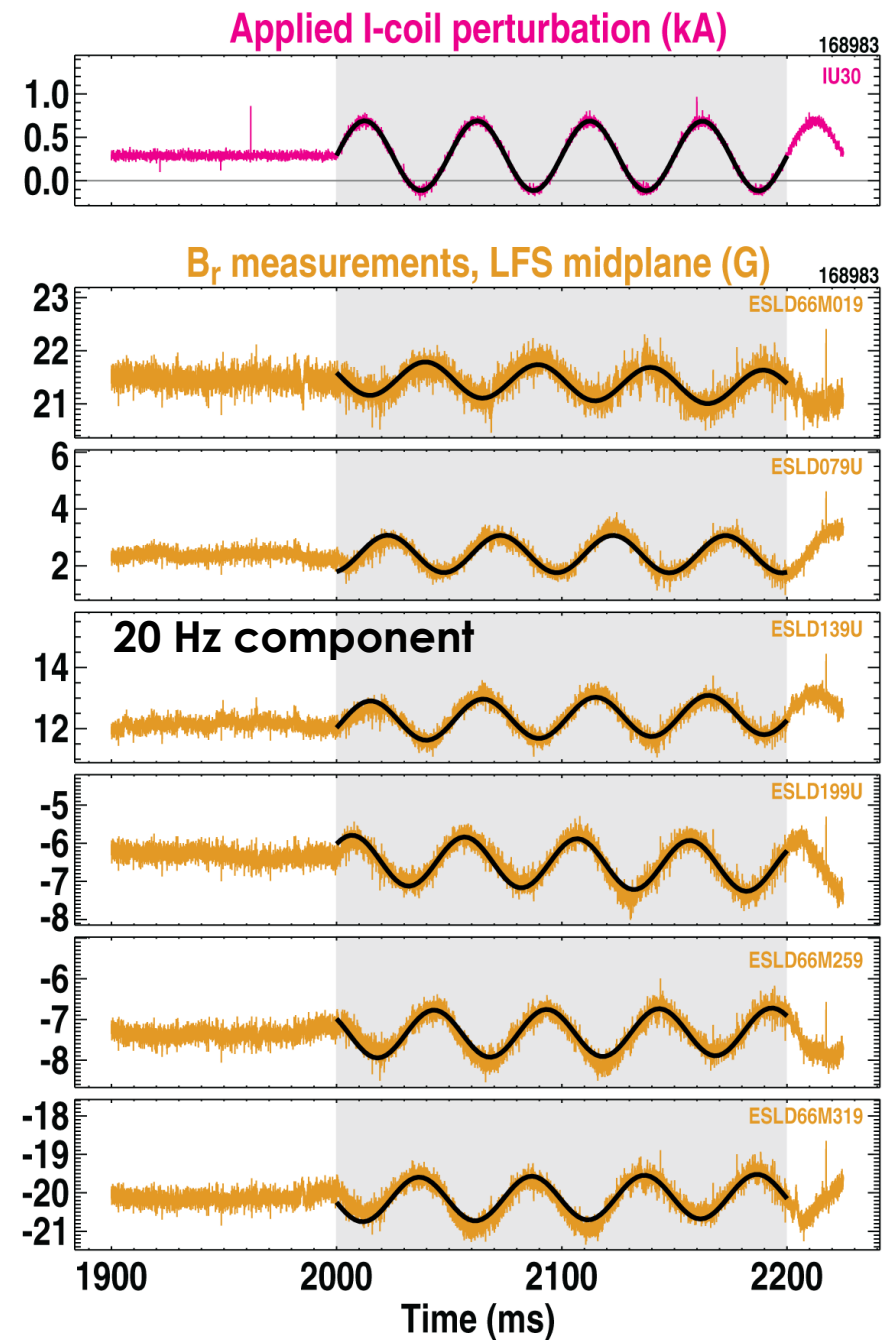
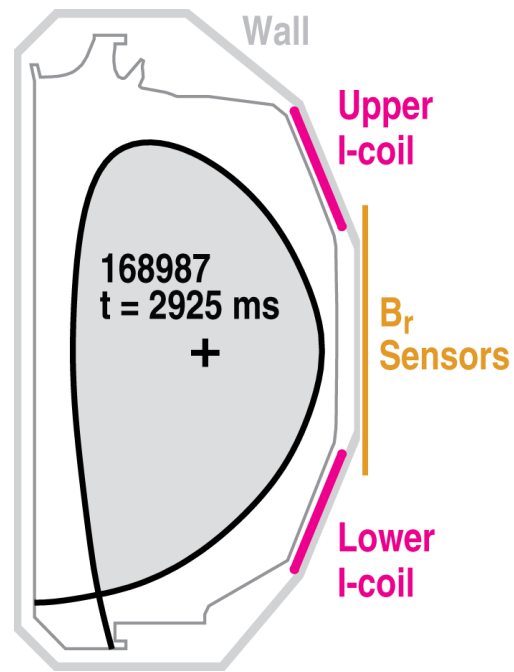


Synchronous analysis yields plasma response to rotating 3D perturbation



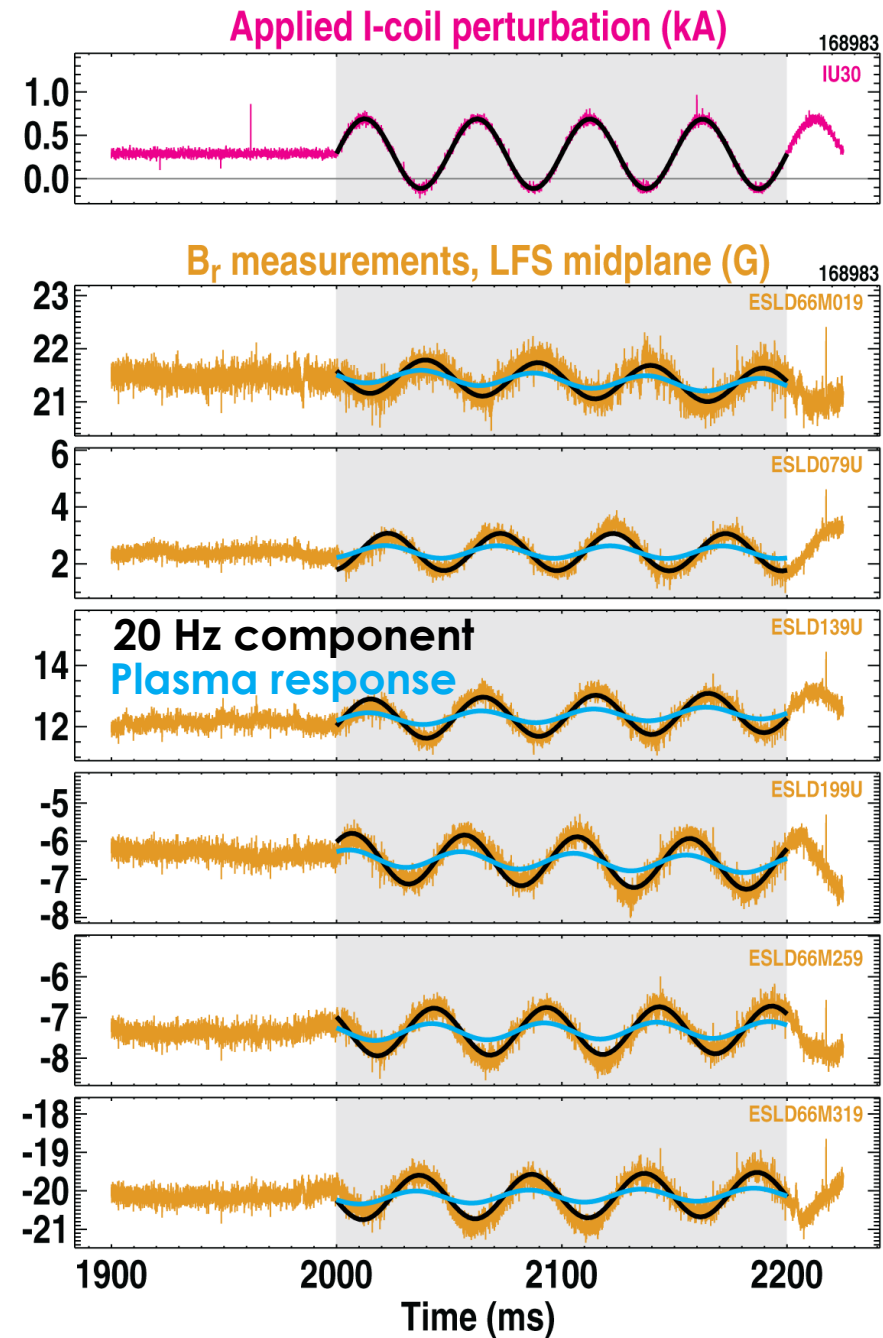
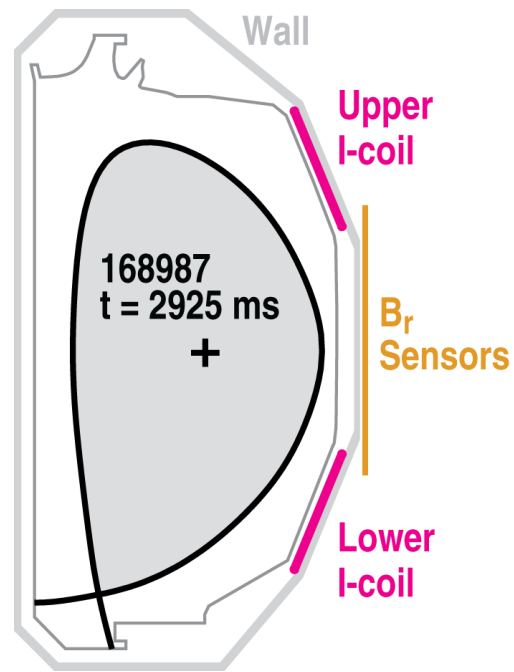
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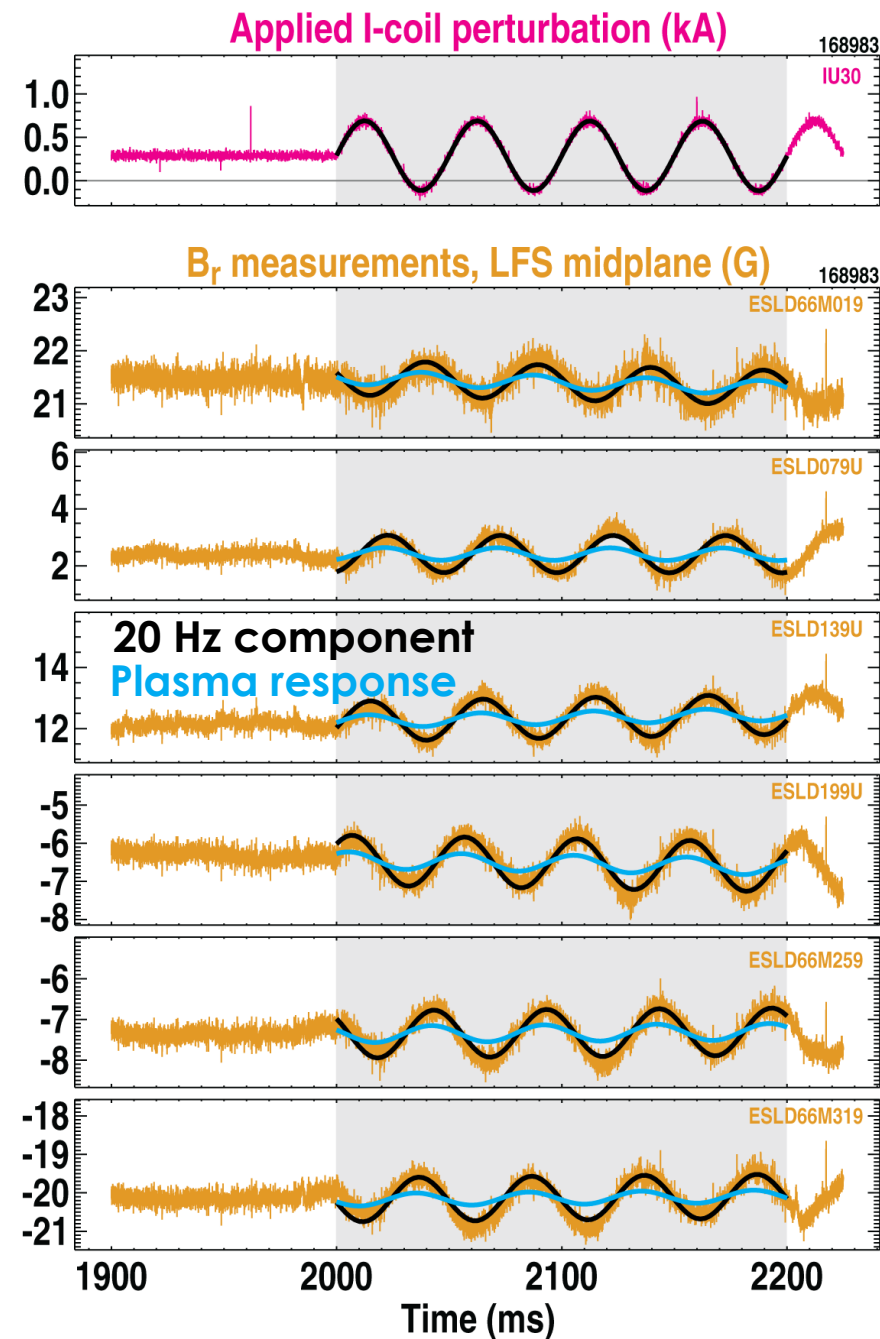
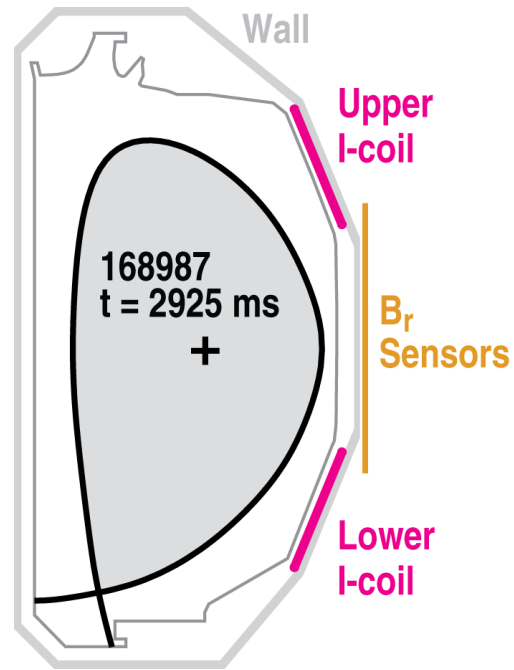
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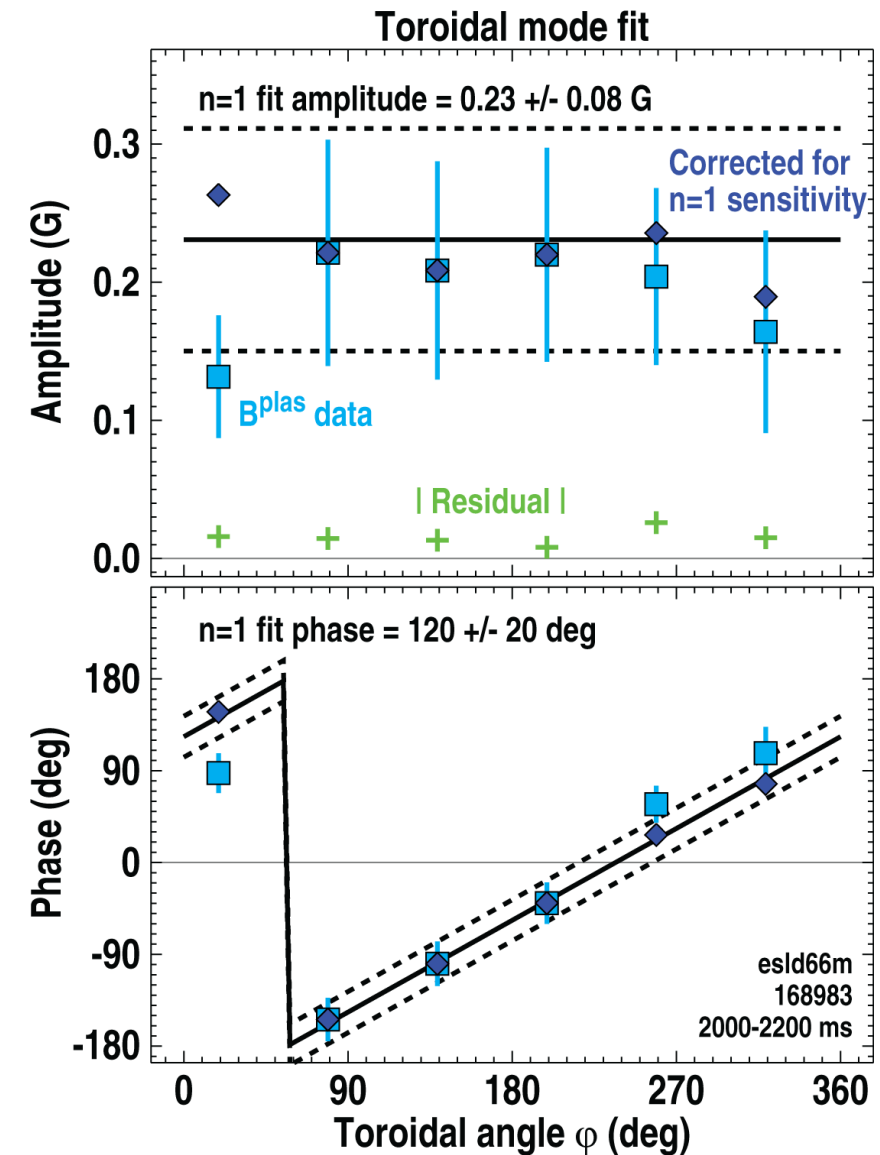


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Synchronous analysis yields plasma response to rotating 3D perturbation



Fit resonances with perturbation frequency and n -number



Single-mode model describes tokamak n=1 plasma response and kink stability

- Simple response model has a single mode^{1,2}

$$\tau_w \frac{dB_s}{dt} = \gamma \tau_w B_s + M_{sc}^* I_c$$

1. H. Reimerdes, *et al.*, *Phys. Rev. Lett.* **93** (2004) 135002.
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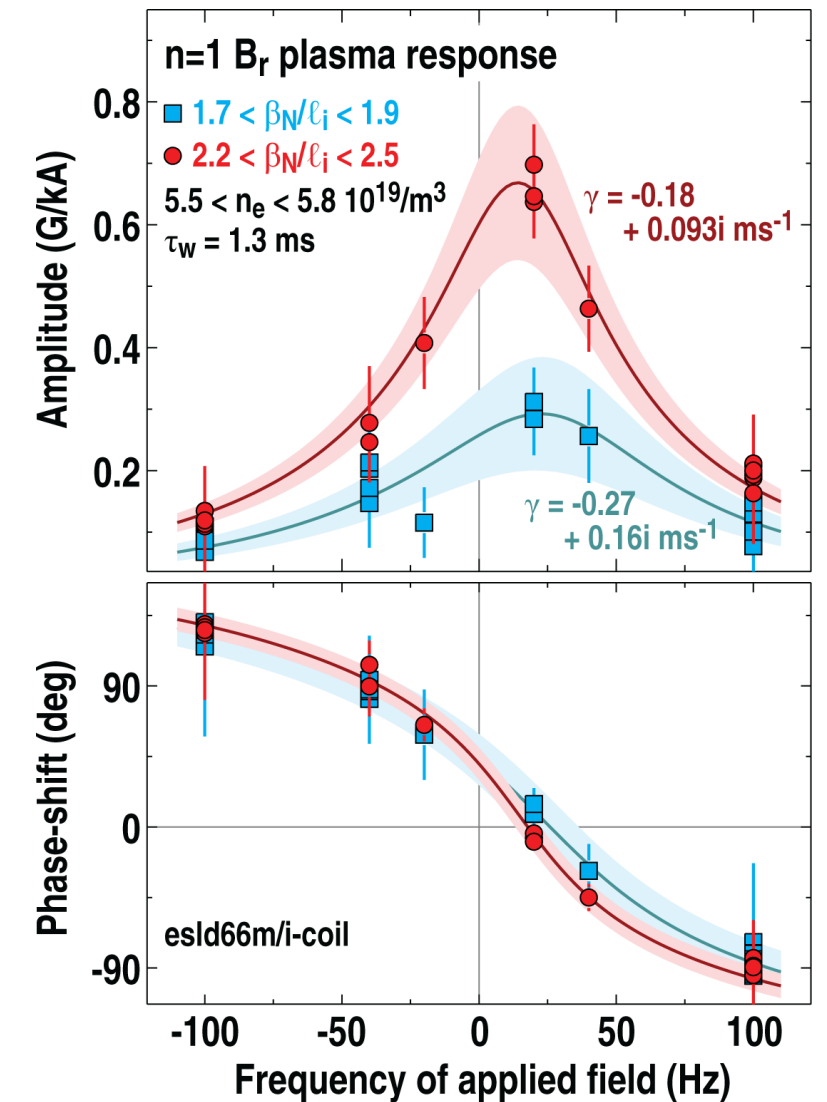
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- In the Fourier domain

$$\frac{B_{s,plas}}{I_c} = \frac{B_s - B_{s,vac}}{I_c} \approx M_{sc}^* \frac{1 + \gamma \tau_w}{(i\omega \tau_w - \gamma \tau_w)(i\omega \tau_w + 1)}$$

- Model consistent with measured n=1 response
 - Peak at **resonance** with mode frequency



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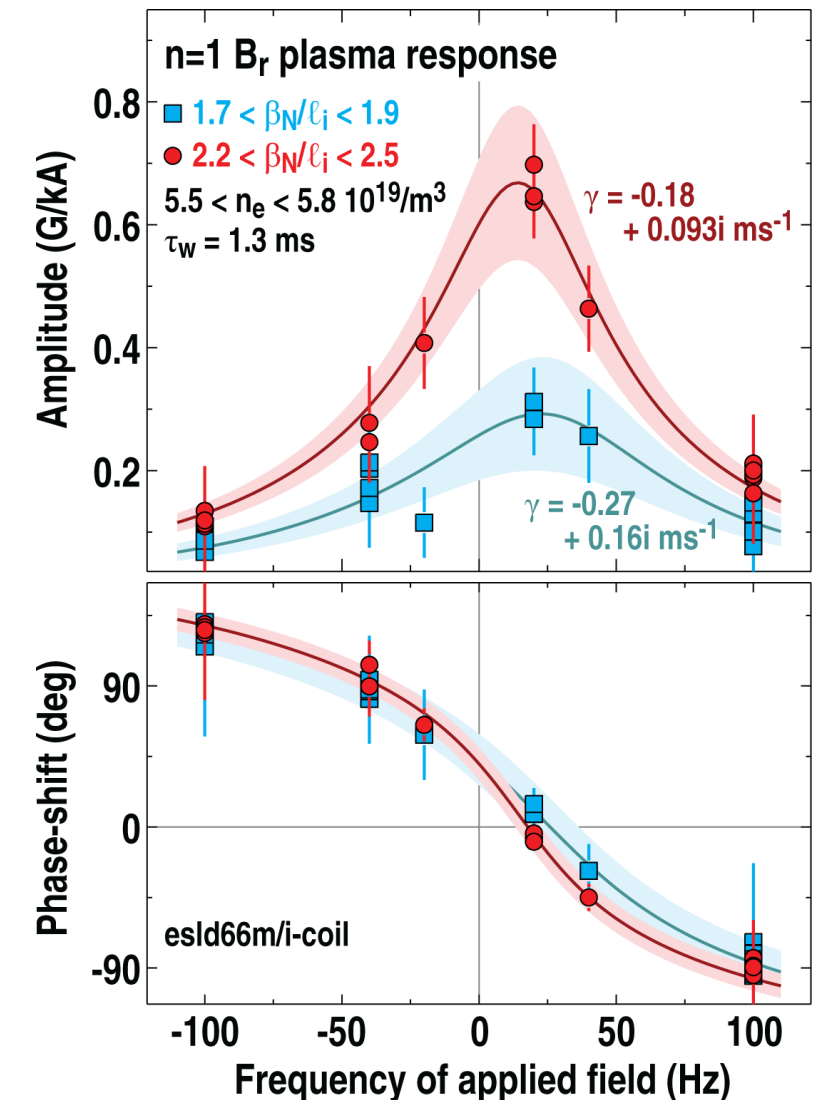
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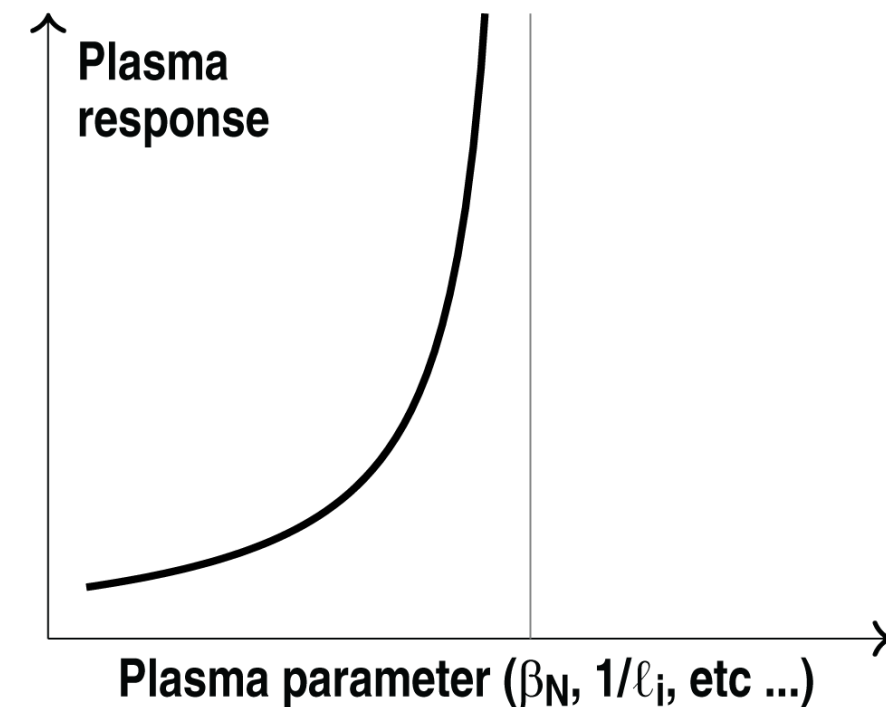
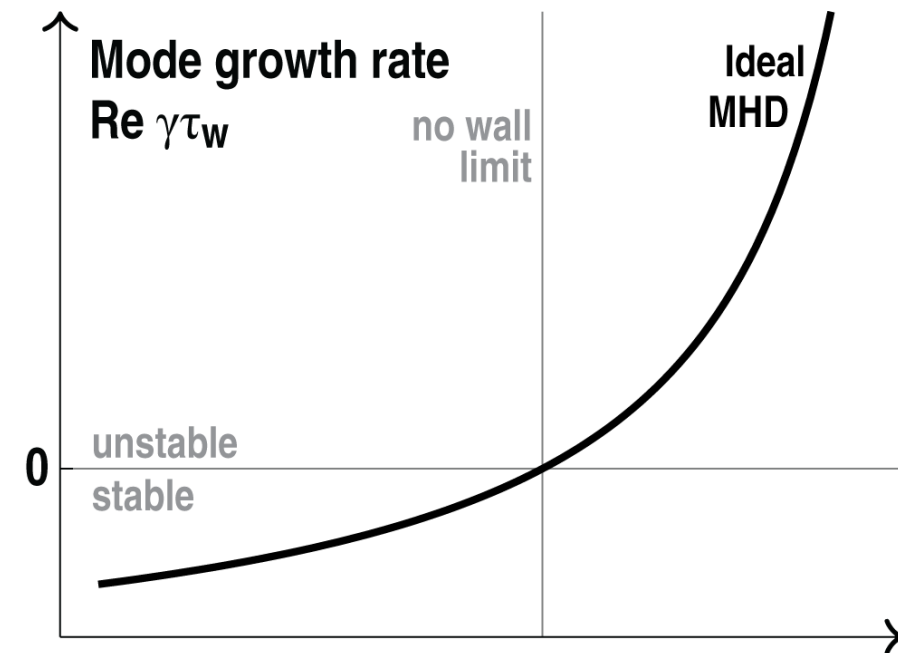
- Also compatible with RWM feedback and error field control experiments^{3,4}



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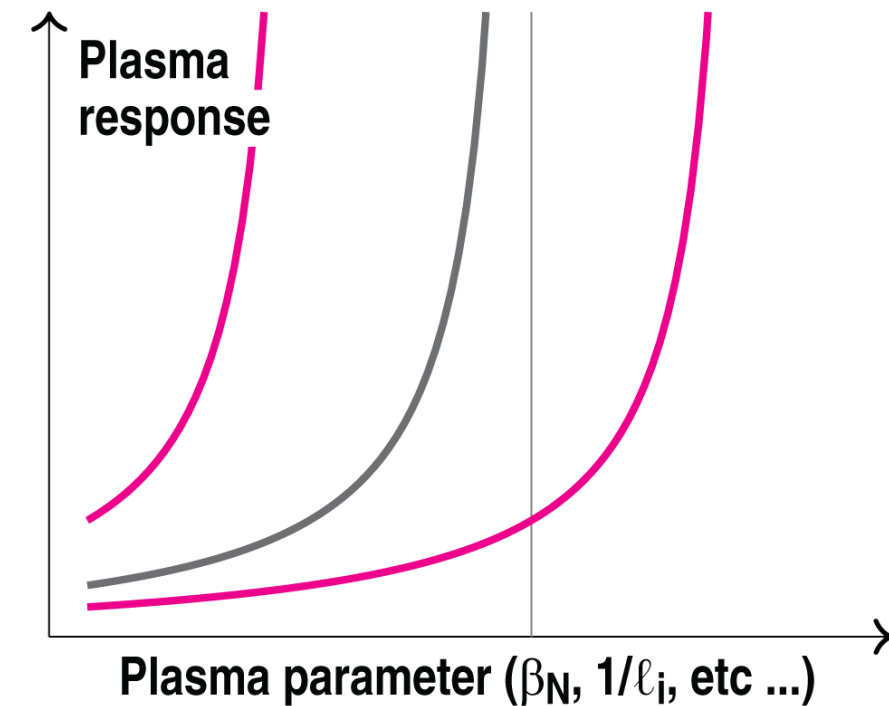
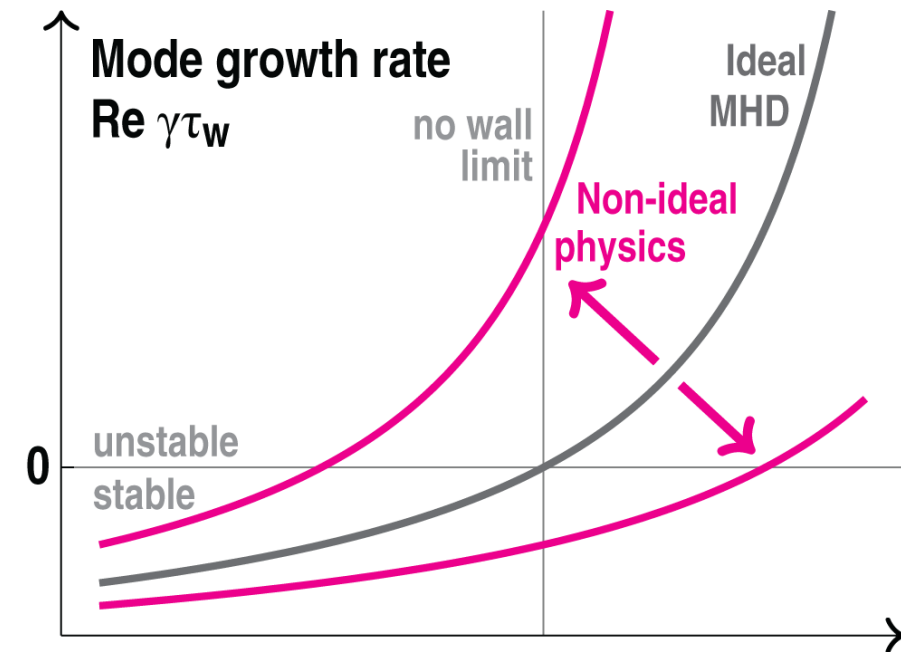
Plasma response depends on mode stability

- **Increasing response indicates approaching stability limit**
 - In ideal MHD this is the no-wall limit



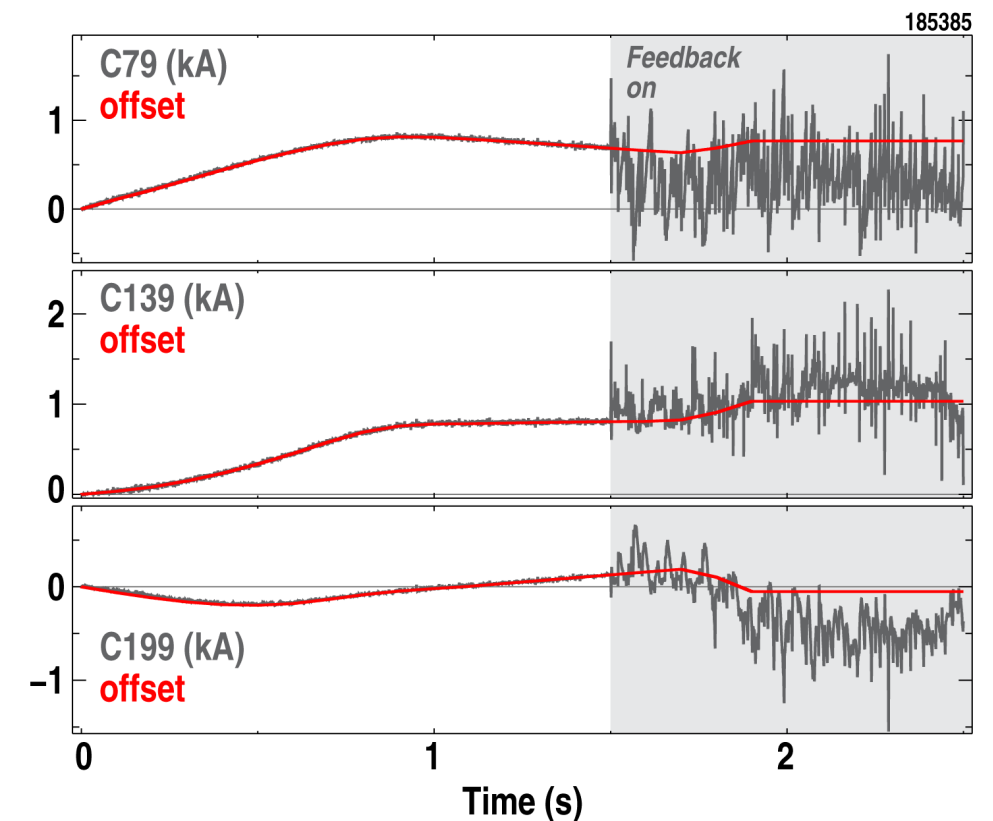
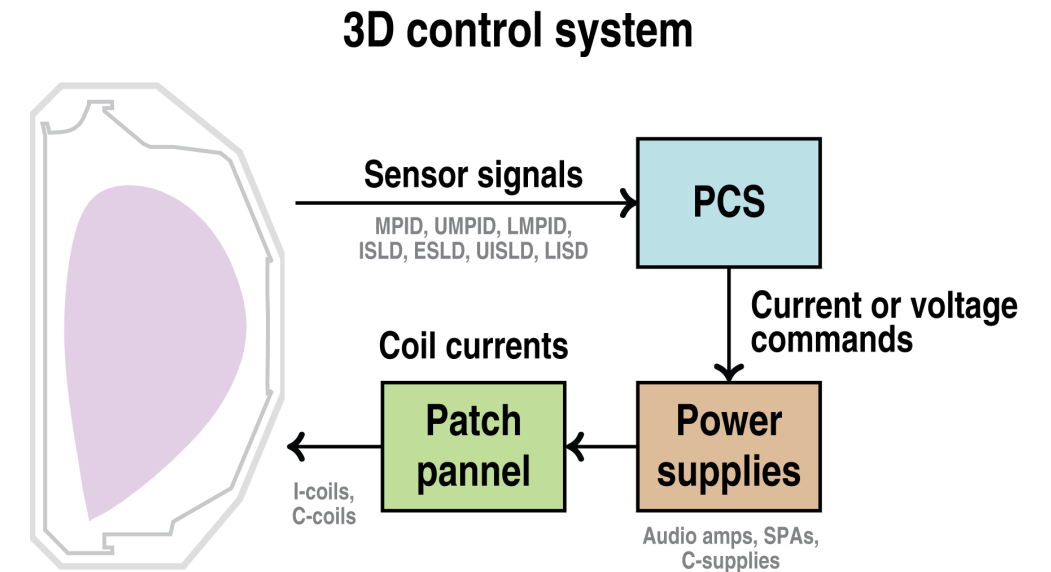
Plasma response depends on mode stability

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- **Non-ideal physics modifies limits and response**
- **Response is a useful tool for stability control and model validation**



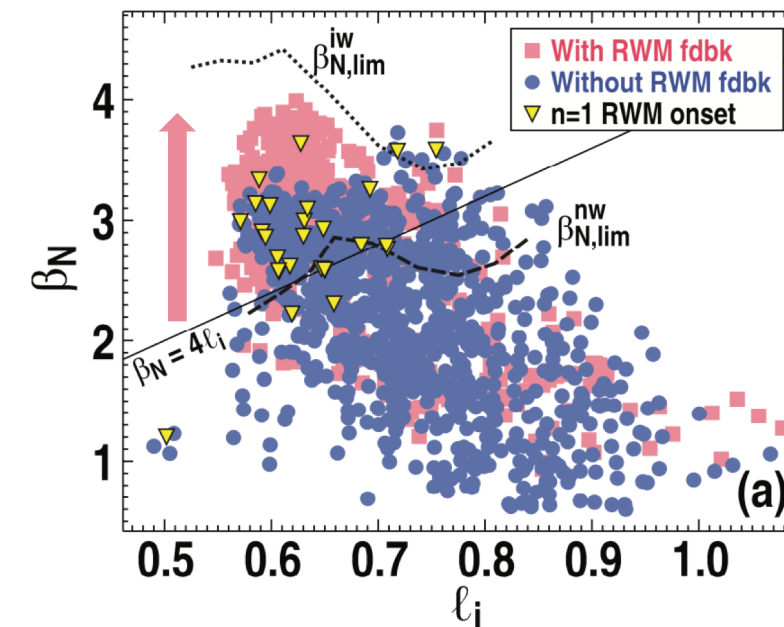
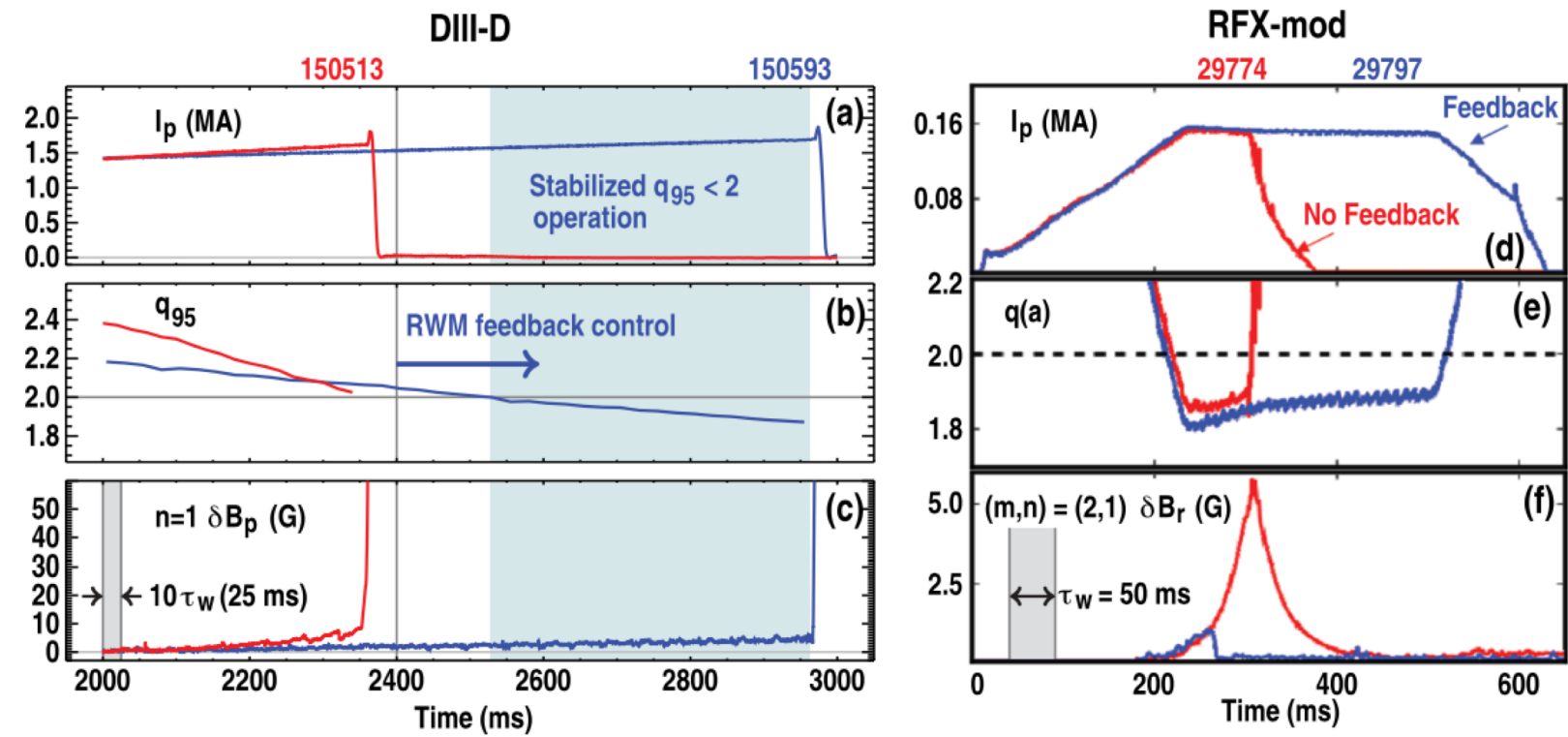
Magnetic feedback enables error field optimization

- **Measure perturbed field with magnetic sensors, feed back with 3D coils**
- **Feedback optimizes error field correction**
 - Sum with feedforward correction derived from Ohmic COMPASS scans
- **Important for sensitive plasmas**
 - **High β_N** → strong plasma response, possible unstable RWMs
 - **Low input torque** → locking likely



Magnetic feedback helps expand the tokamak operating space

- **To below $q_{\text{edge}} = 2$**
 - In DIII-D and RFX-MOD¹
- **To higher β_N**
 - In DIII-D high- q_{min} scenario²



1. JM Hanson, et al., *Phys. Plasmas* **21** (2014) 072107.

2. JM Hanson, et al., *Nucl. Fusion* **57** (2017) 056009.

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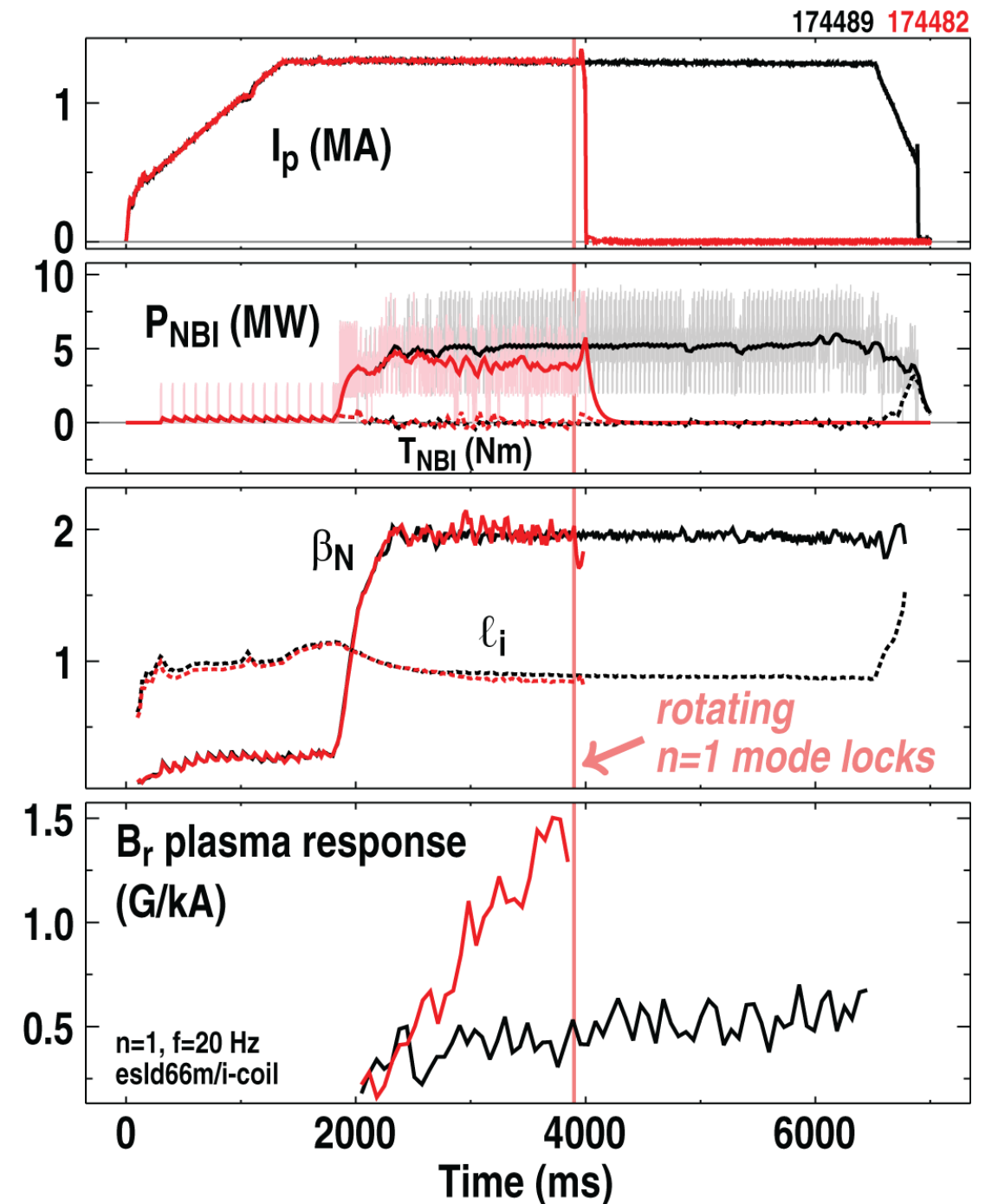
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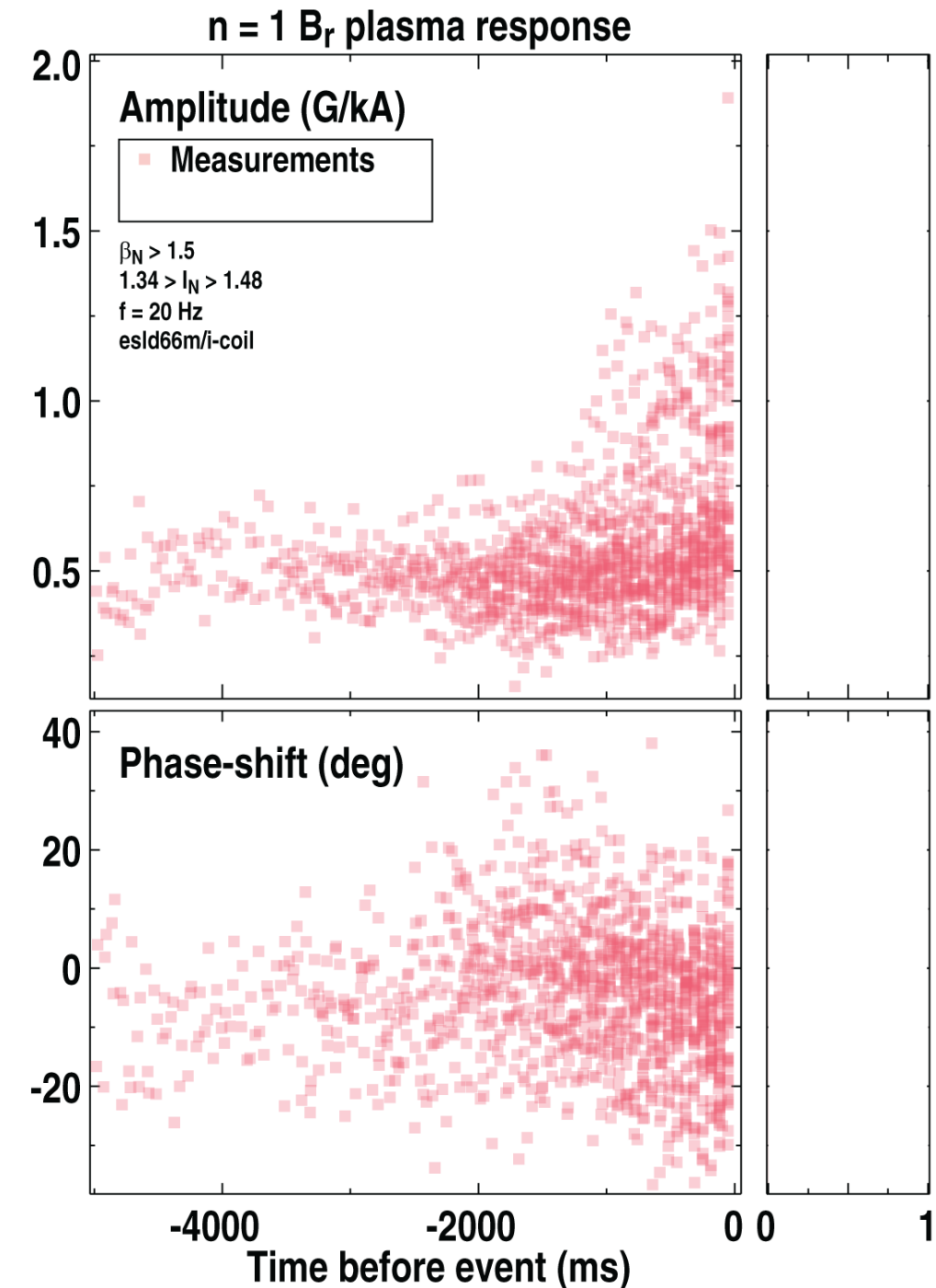
DIII-D ITER baseline demonstration discharges present stability challenge

- **Combination of low torque, low $q_{95} \approx 3$ and H-mode edge leads to stability challenges¹**
 - Below ideal MHD limits, *but* ...
 - ... current profile shape near $q=2$ and $3 \rightarrow$ tearing
- **Low frequency plasma response increase prior to tearing mode locking**



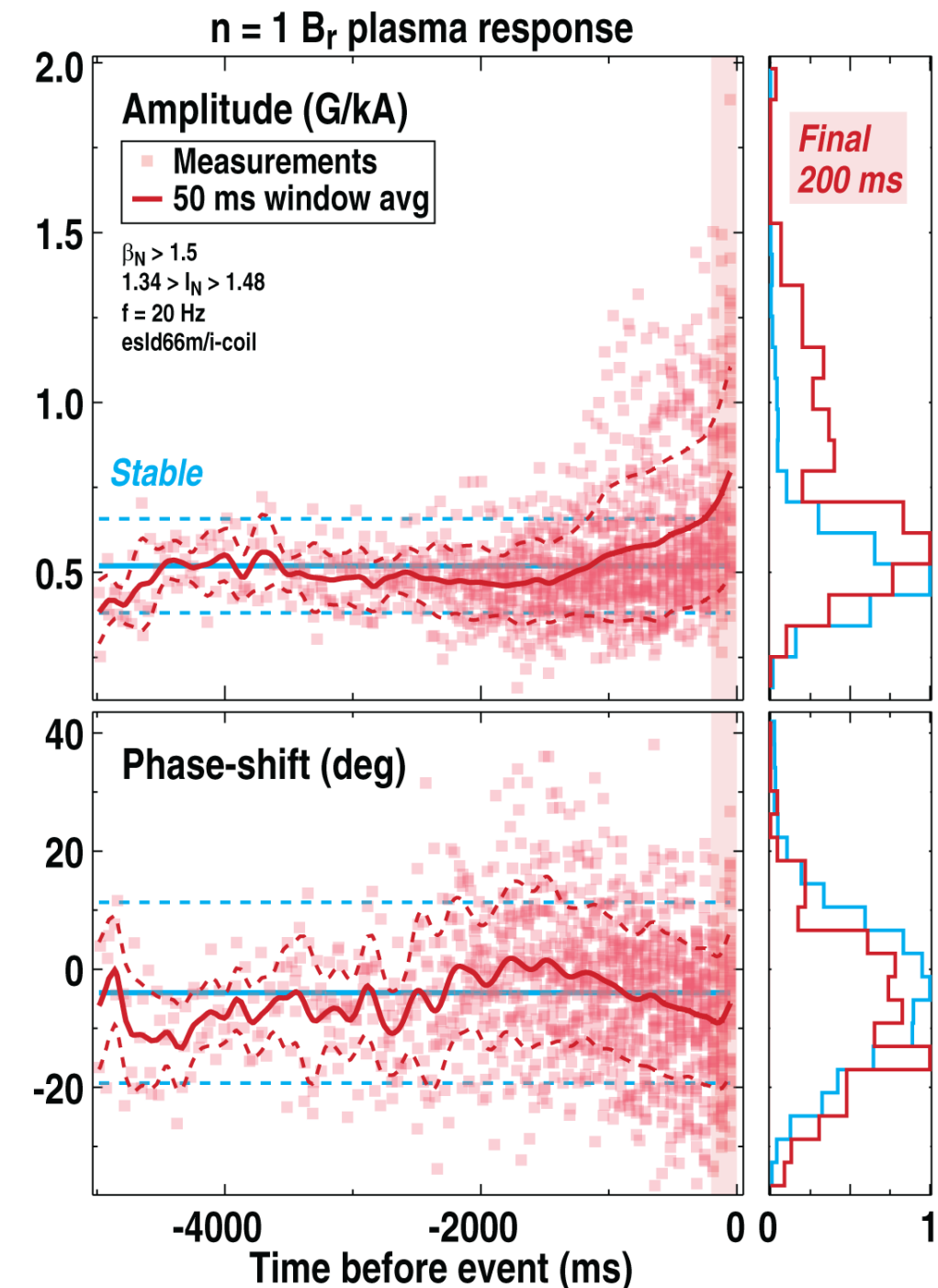
Many shots exhibit response increase before locking

- Compare time-evolutions of 52 discharges with $n=1$ locking events



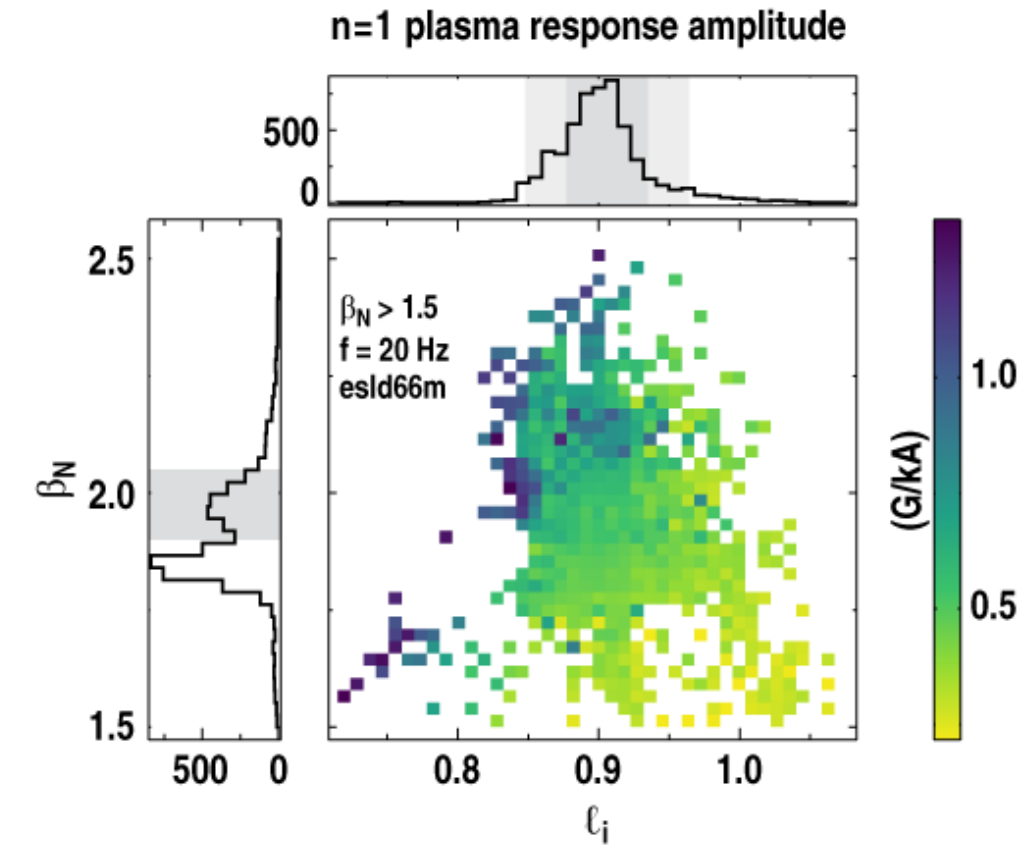
Many shots exhibit response increase before locking

- Compare time-evolutions of 52 discharges with $n=1$ locking events
- Average evolution shots increasing response amplitude
 - Exceeds baseline of 60 stable shot
- Not all cases show increased response
 - β_N influences response but not TM stability in this regime¹
 - Modes sometimes lock more quickly than 100 ms response timescale



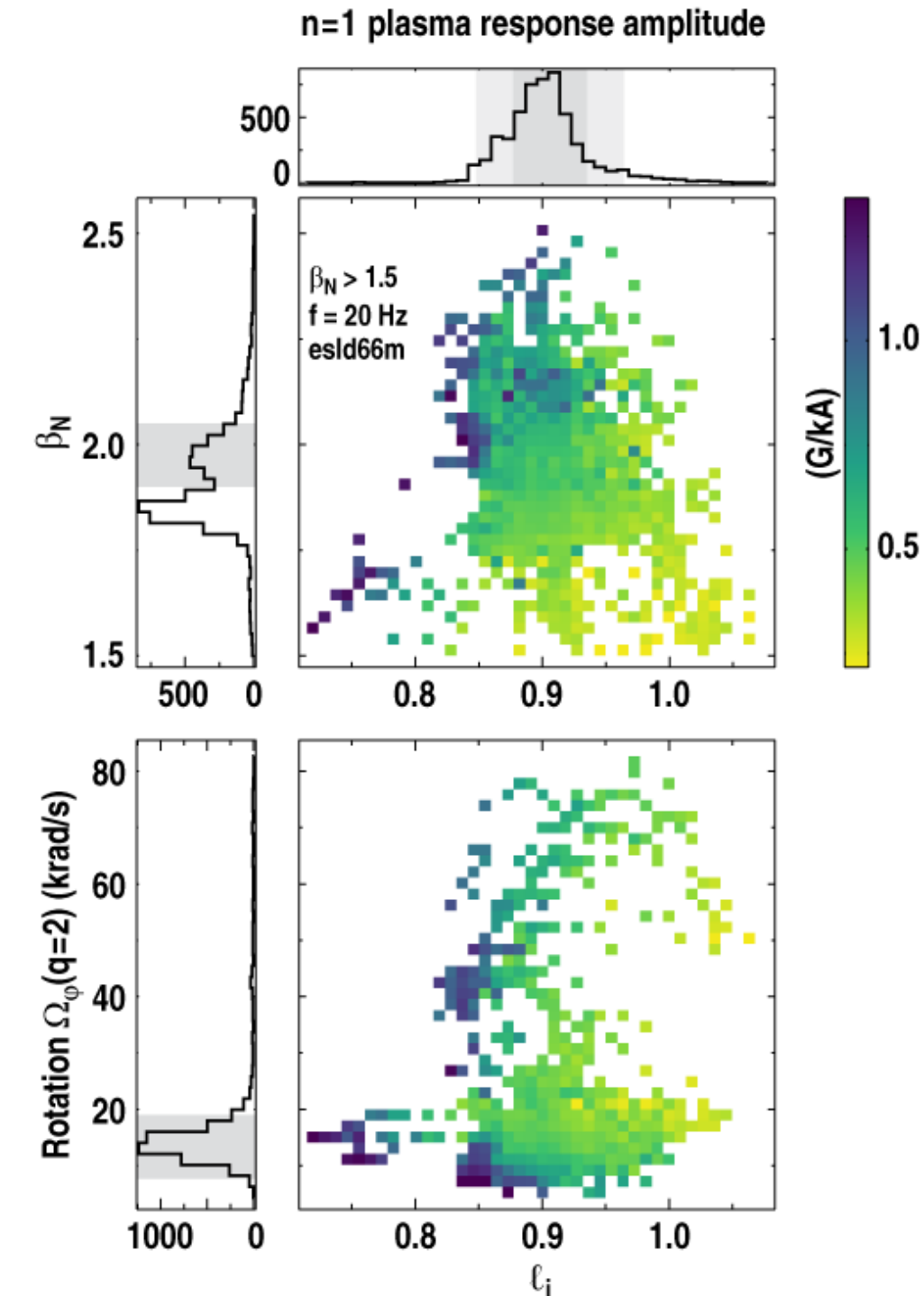
Plasma response is sensitive to MHD equilibrium

- **Examine large ITER demo shot dataset**
 - 148 shots with $\beta_N > 1.5$, $I_N \approx 1.4$
 - 5525 100 ms time-intervals
- **Sensitivity to β_N and ℓ_i suggests ideal MHD link**



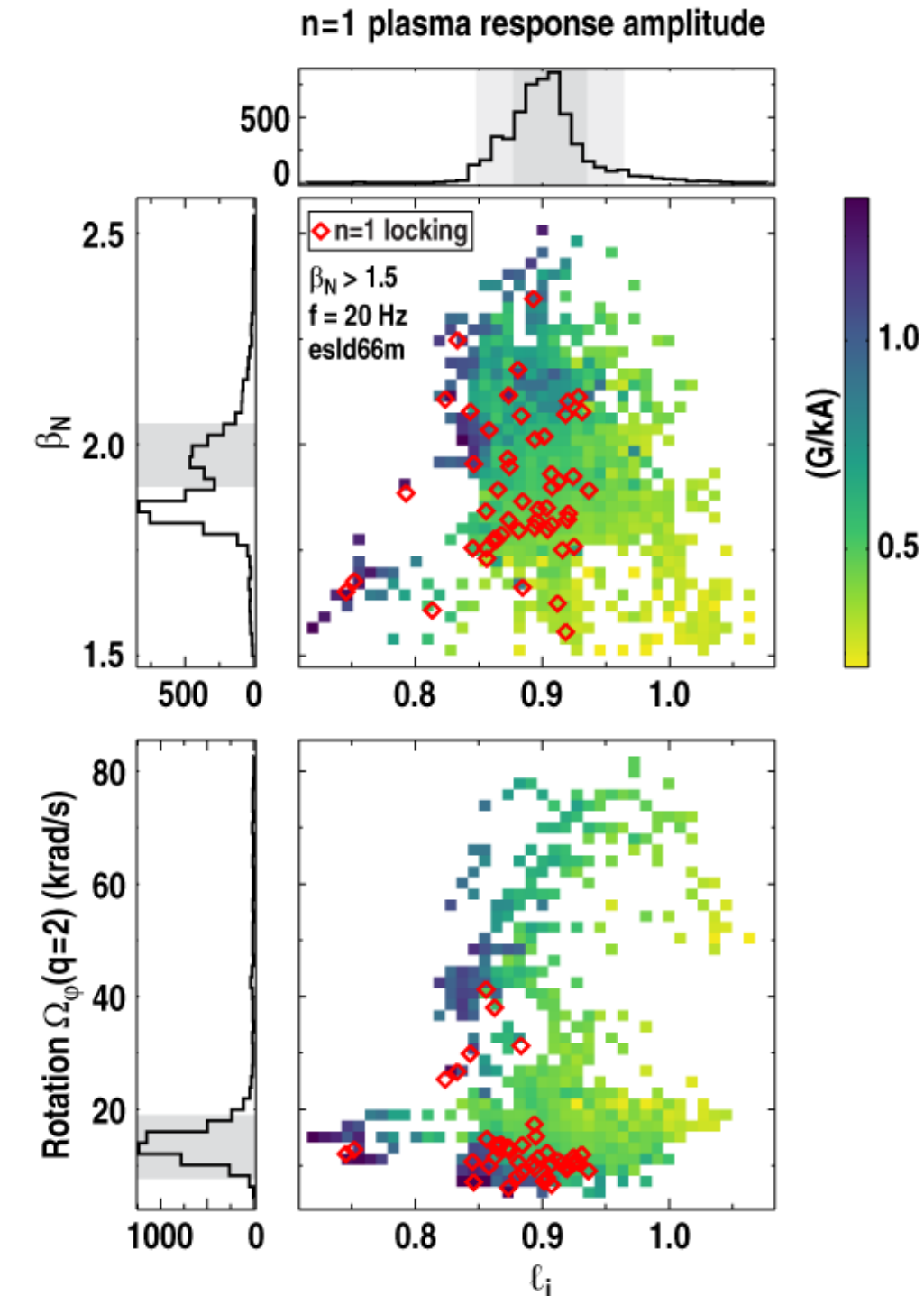
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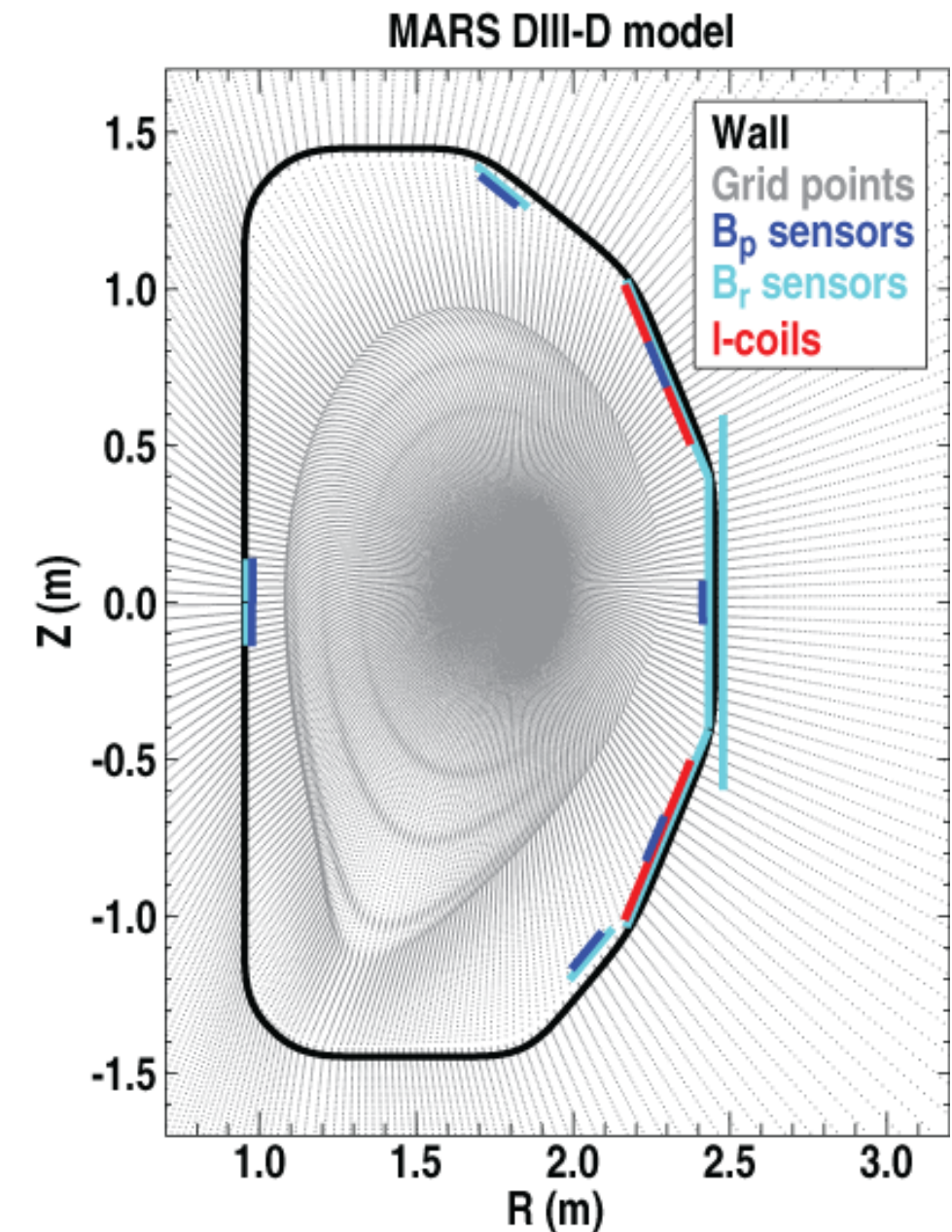
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- **Strongest response at low ℓ_i and low rotation**
- **Higher incidence of locking in this regime**
 - 52 n = 1 mode locking events
 - All followed by disruption, sometimes at reduced I_p



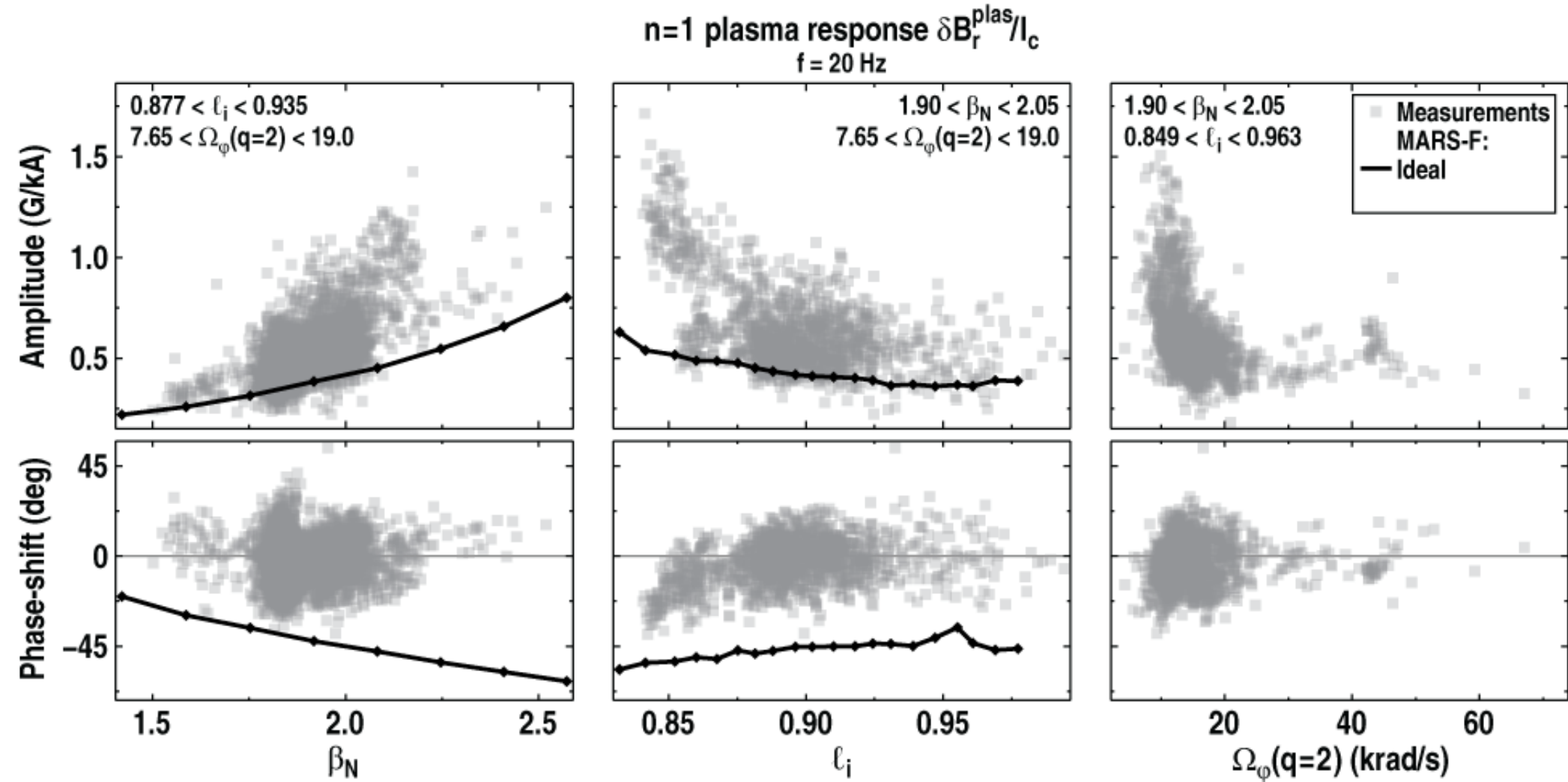
MARS-F code simulates toroidal mode plasma response

- **MARS-F solves linearized, perturbed MHD model with resistive wall and coils¹**
 - Solves for perturbed field over a large domain
 - Can apply rotating perturbations with coils
 - Compare with magnetic sensor measurements by averaging predictions over sensor locations
- **A variety of plasma physics contributions can be included**
 - Plasma rotation
 - Single-fluid resistivity
 - Kinetic contributions



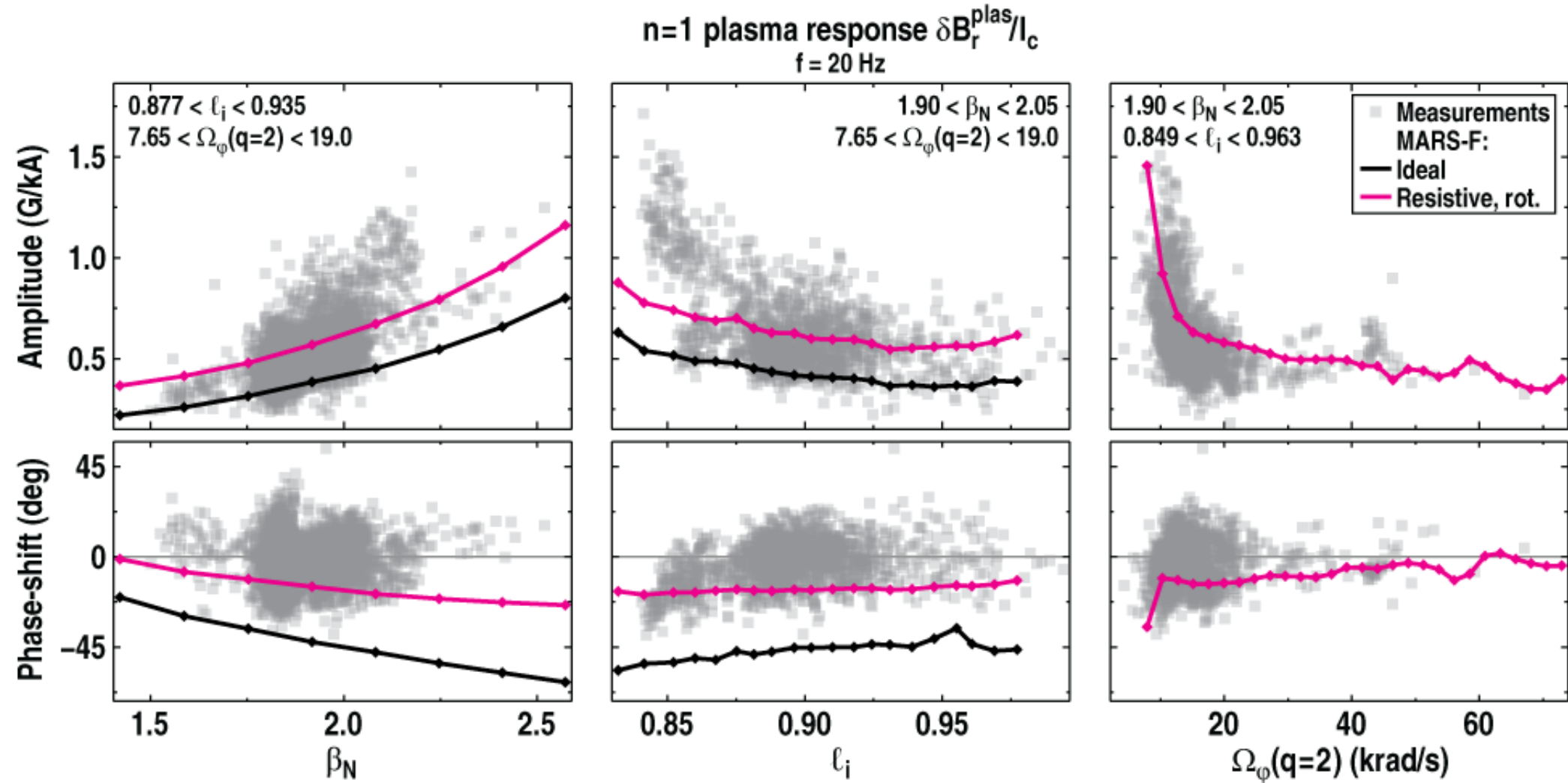
Resistive response simulations compatible with experimental dependencies

- Ideal MHD qualitatively consistent with β_N and ℓ_i dependencies



Resistive response simulations compatible with experimental dependencies

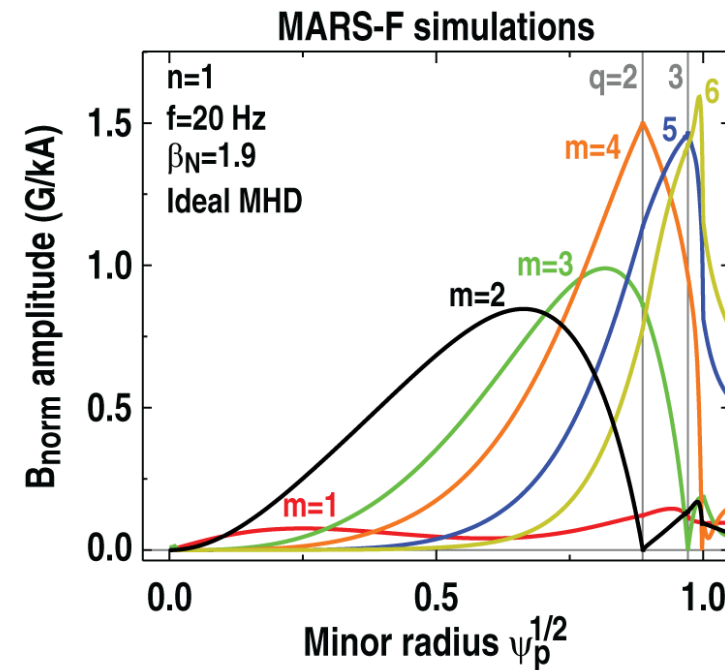
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- **Including resistivity and rotation improves agreement**
 - Modeling consistent with large change at low rotation

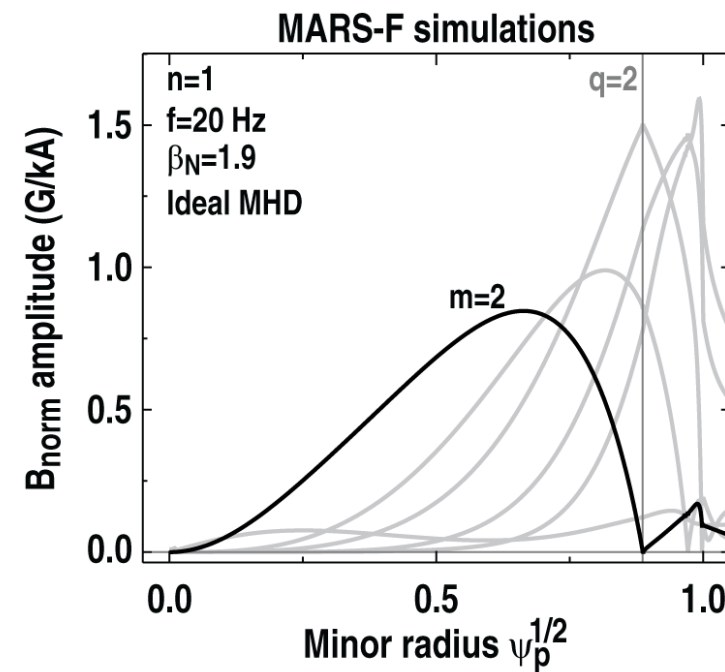
Resistive simulations show enhanced resonant response

- **Ideal MHD: pitch-resonant fields screened at rational surfaces**



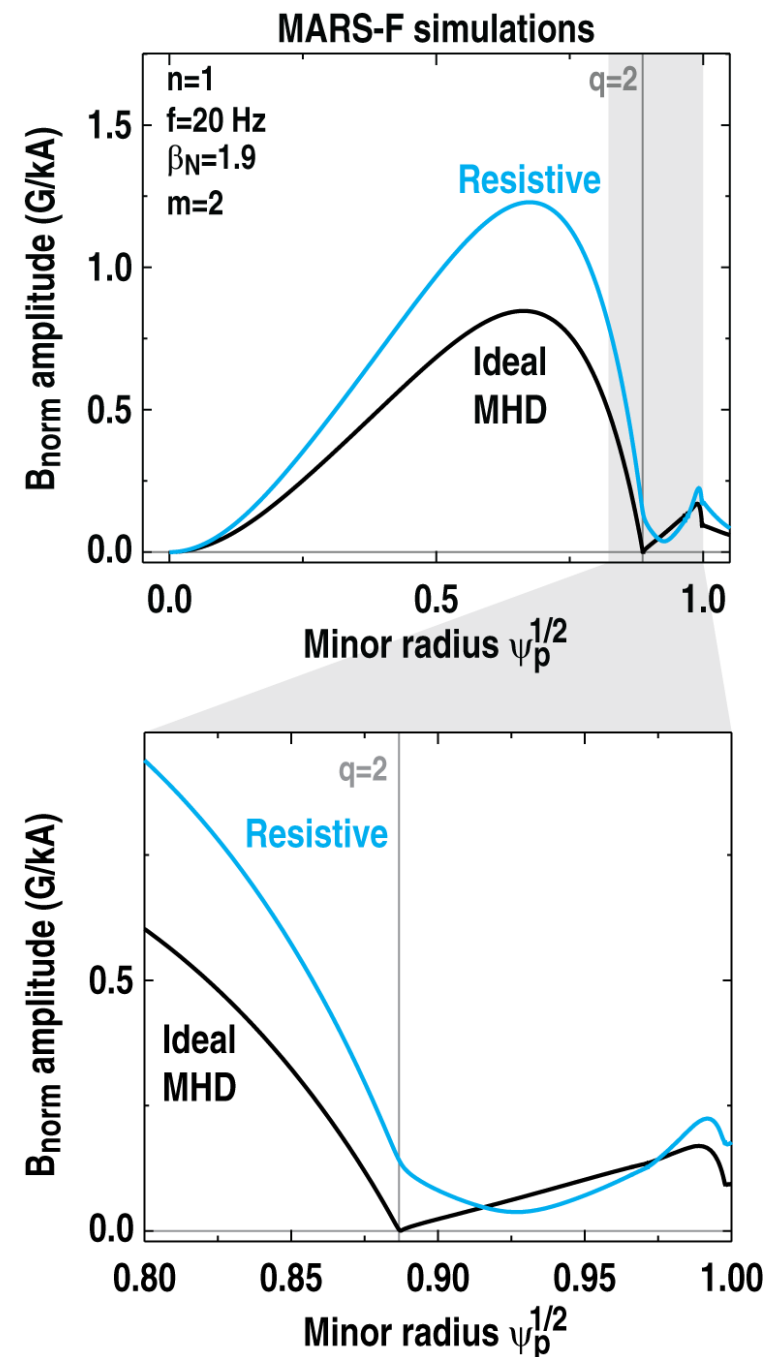
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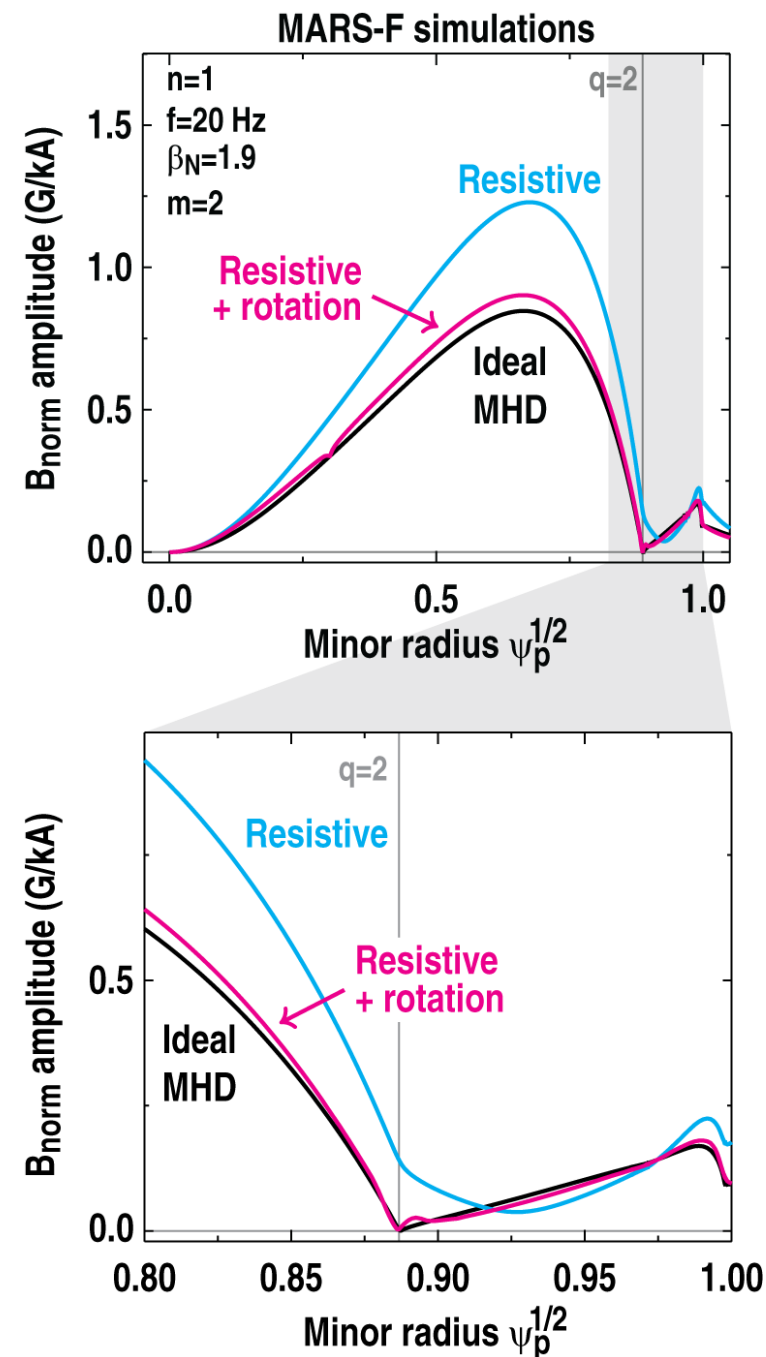
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 - Permitting non-zero resonant components



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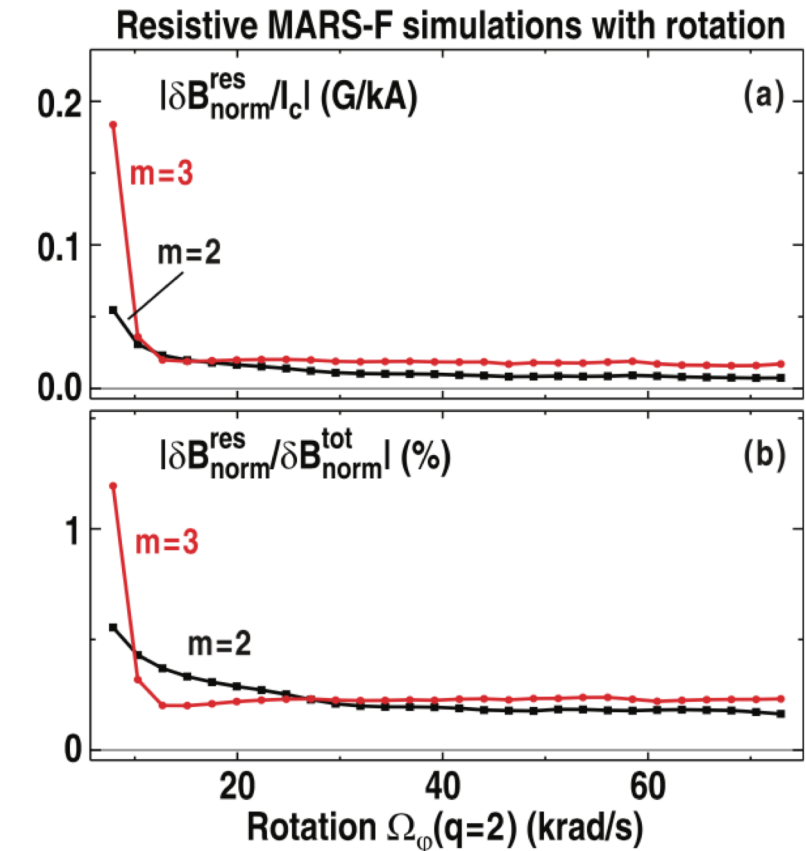
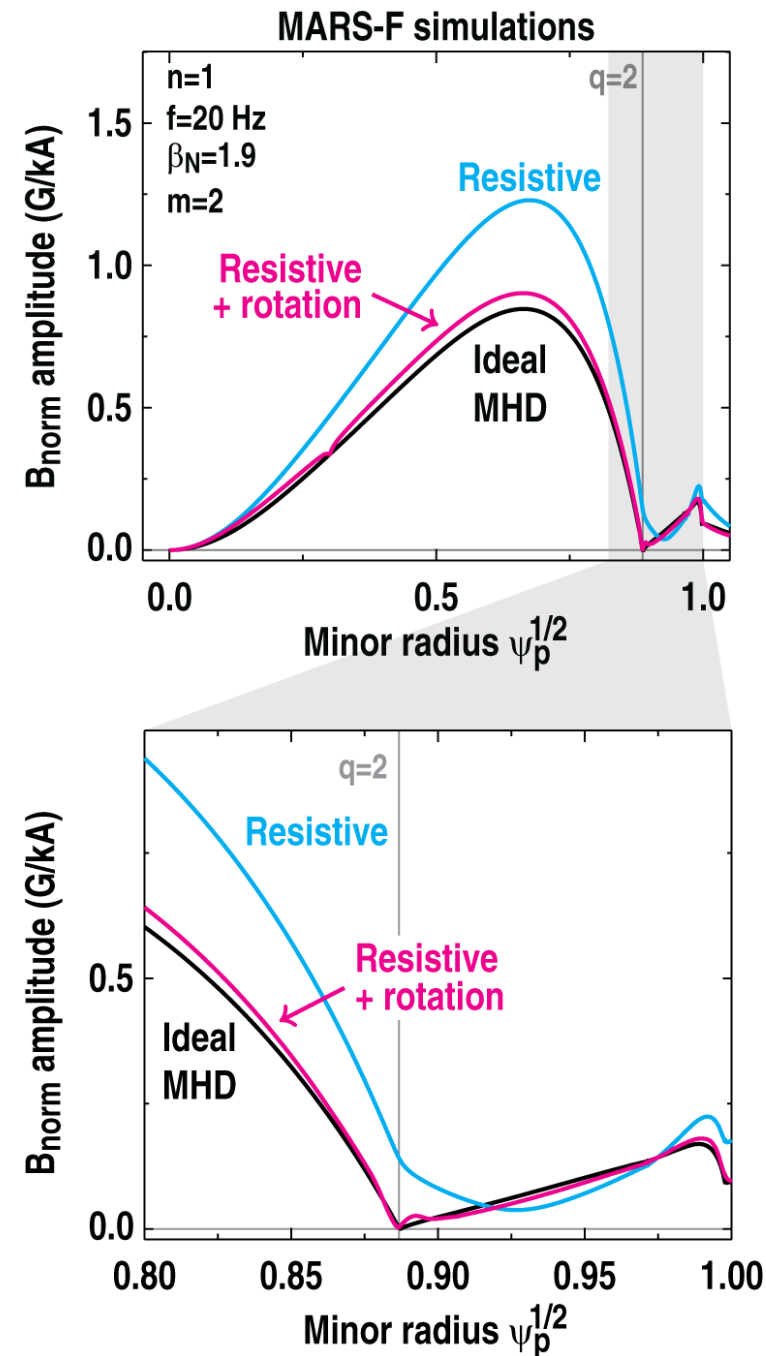
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- **Plasma rotation helps restore screening**



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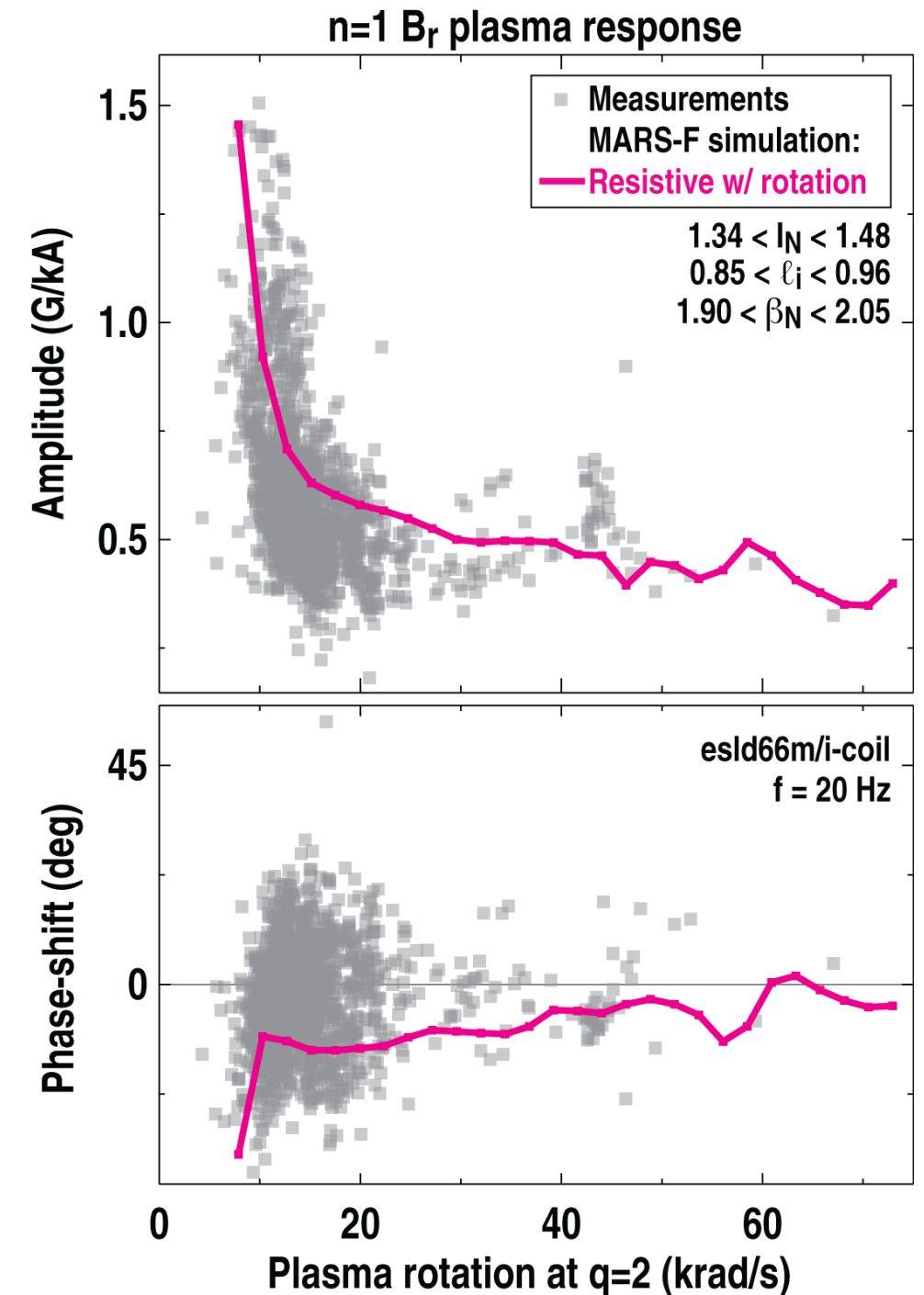
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- **Resonant fields increase strongly at low rotation¹**

What have we learned about the transition to locking?

- **Is the applied perturbation driving tearing?**
 - Simulations show resonant field increase ...
 - ... but $q = 2$ surface rotates faster than perturbation: ≈ 1 kHz vs 20 Hz
 - This regime has (2,1) stability and locking issues even without perturbations¹

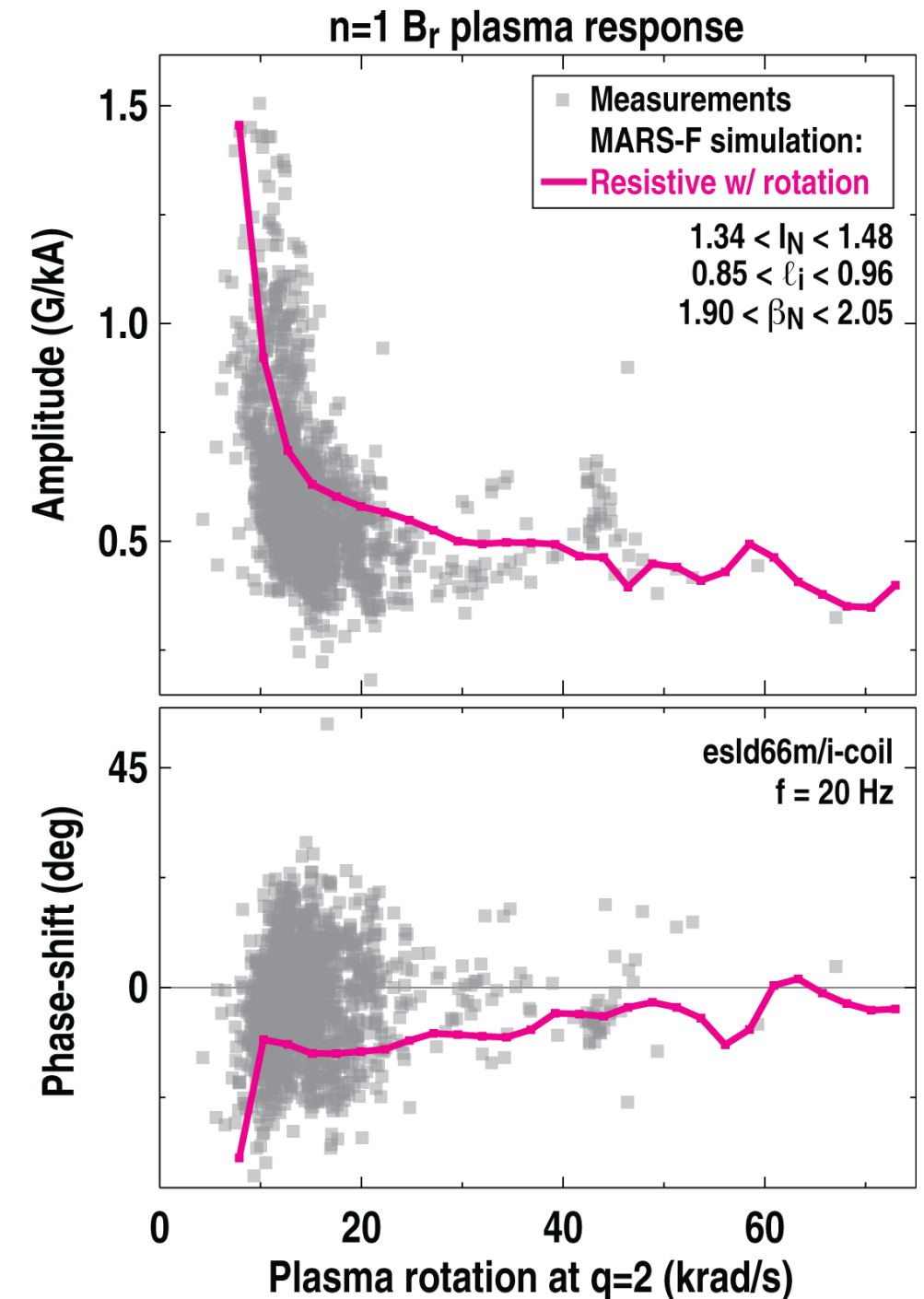


1. F. Turco, et al., *Nucl. Fusion* **58** (2018) 106043.

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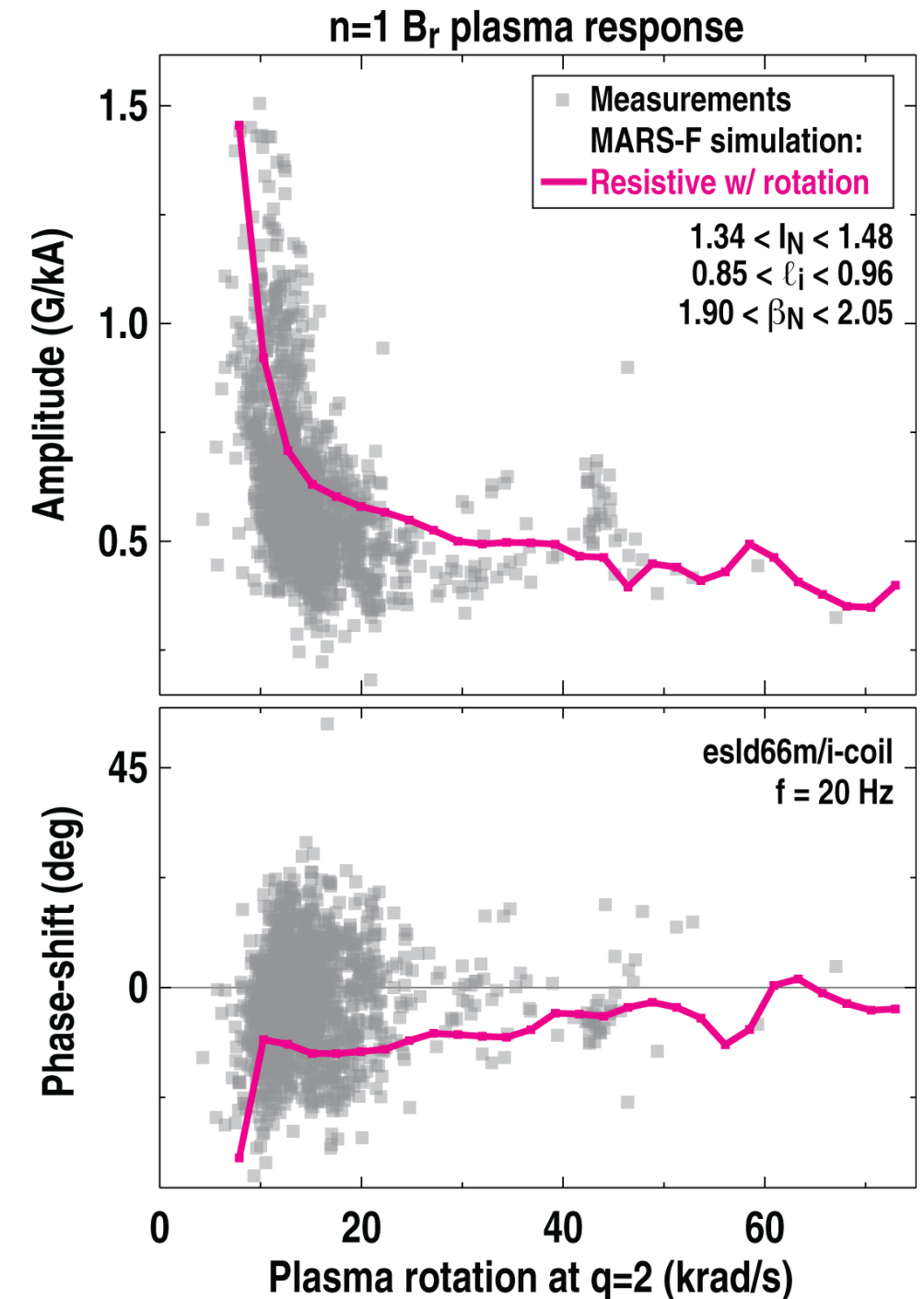


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 - But increasing error field amplification likely contributes to locking and disruption
- **Ultimate solution:** current profile optimization for (2,1) tearing stability²



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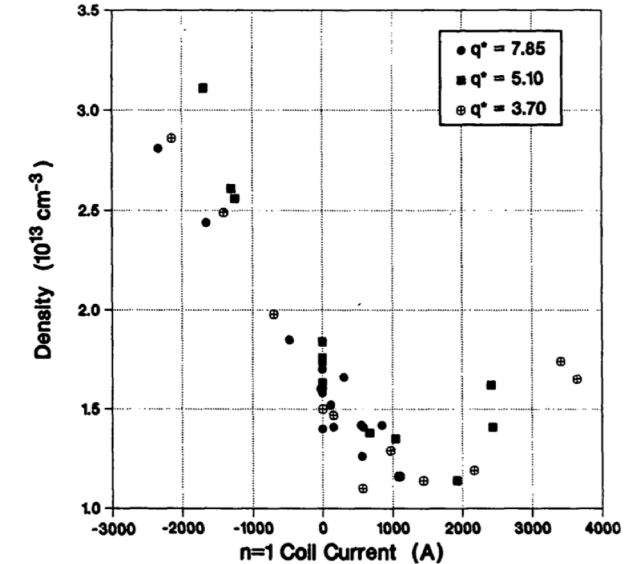
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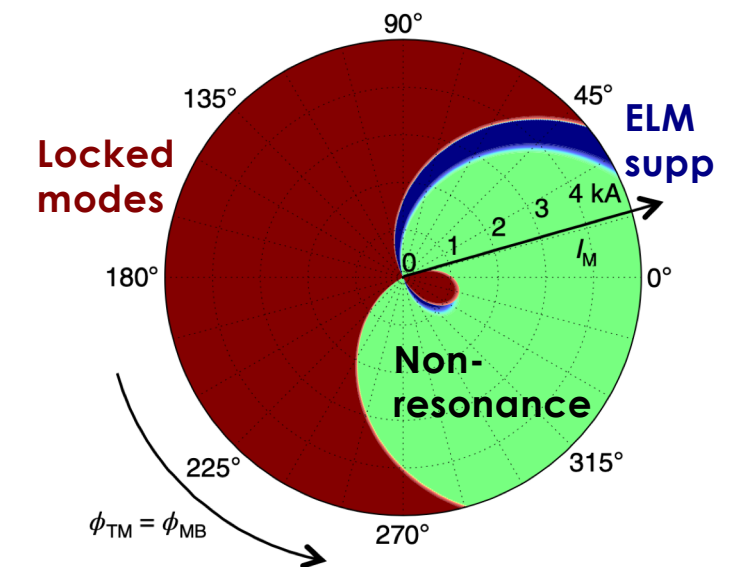
Correcting plasma error field response improves tokamak performance

- **Small equilibrium coil deviations from axisymmetry lead to field errors**
 - Implicated in MHD instability onsets and locking
 - Observed in many tokamaks
 - Critical threshold $\delta B/B_0 \sim 10^{-4}$
- **Low density locked mode threshold improved with applied n=1 field¹**
 - Attributed to error field correction
- **Now understand that managing 3D field can have many benefits**
 - Rotation optimization², ELM suppression³ ...

DIII-D Low density locked mode threshold¹



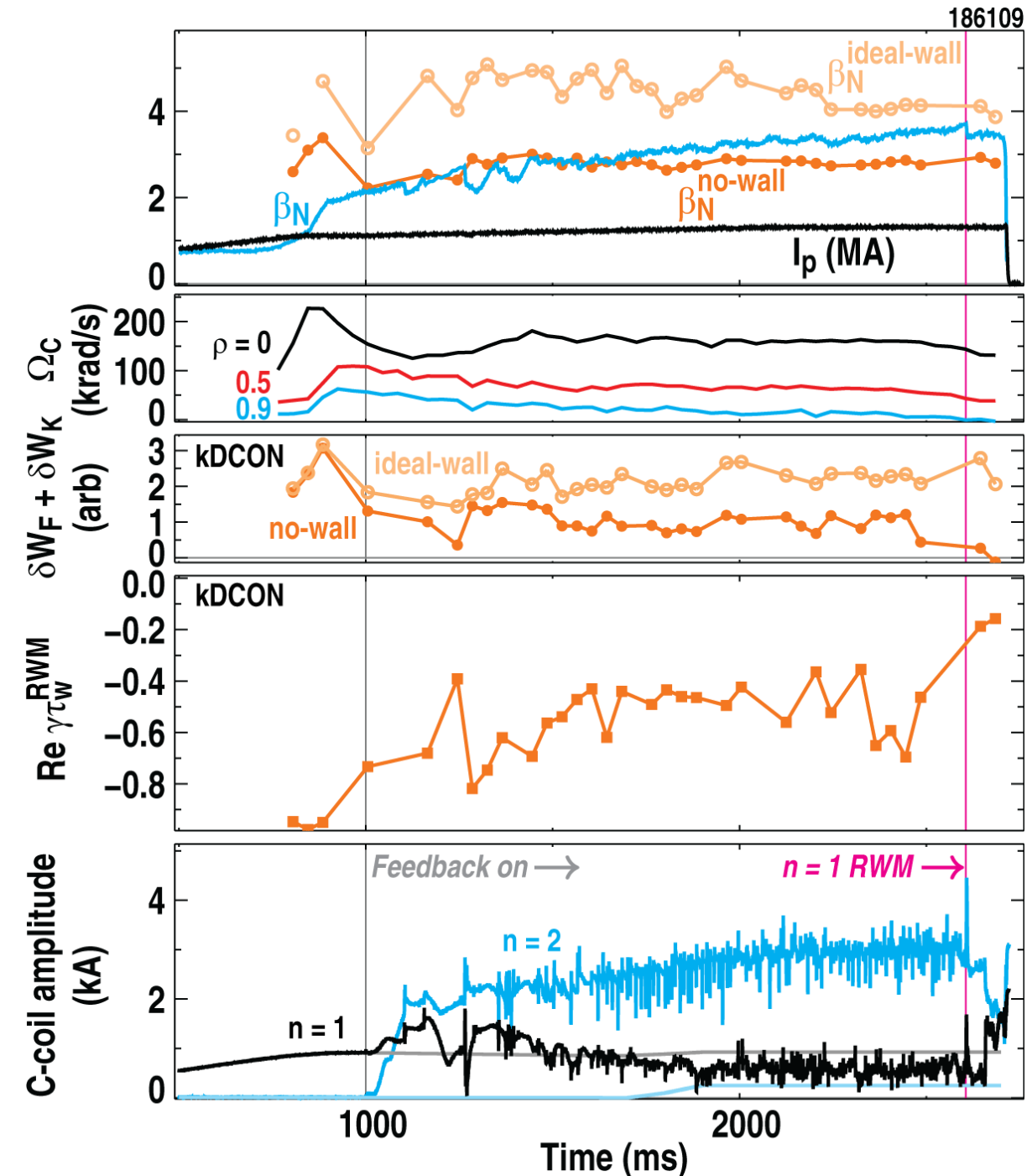
KSTAR simulated 3D operating window³



1. JT Scoville, et al., *Nucl. Fusion* **31** (1991) 875.
2. AM Garofalo, et al., *Nucl. Fusion* **42** (2002) 1335.
3. J-K Park, et al., *Nature Phys.* **14** (2018) 1223.

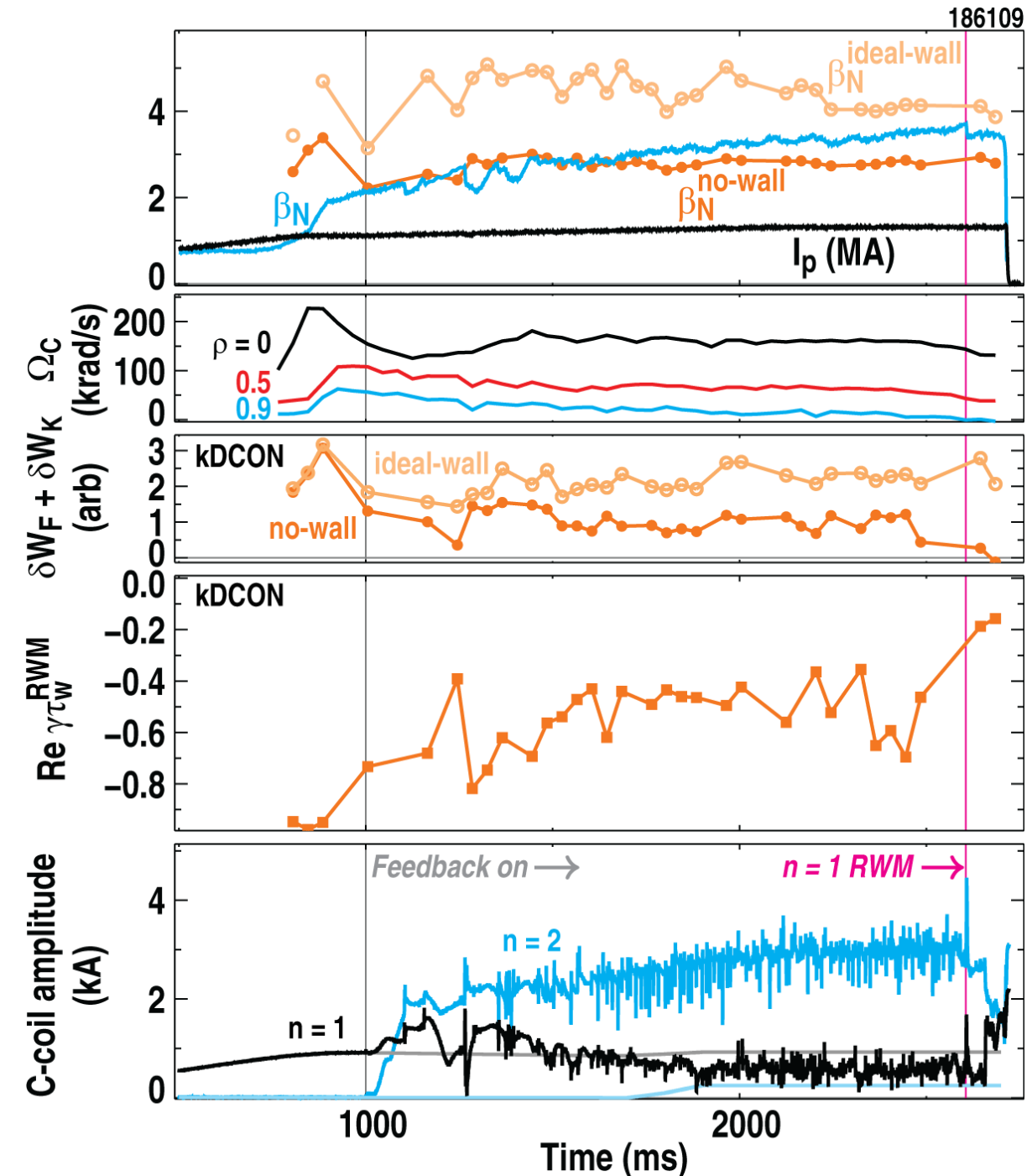
Advanced tokamak discharge reaches stability limit with $n=1 + n=2$ feedback control

- β_N ramped to 3.8, above ideal $n=1$ no-wall limit¹
- Born-locked $n=1$ mode before disruption
 - Growth time: $1 \text{ ms} \approx \tau_w$
 - Coincides with approach to kinetic MHD marginal point



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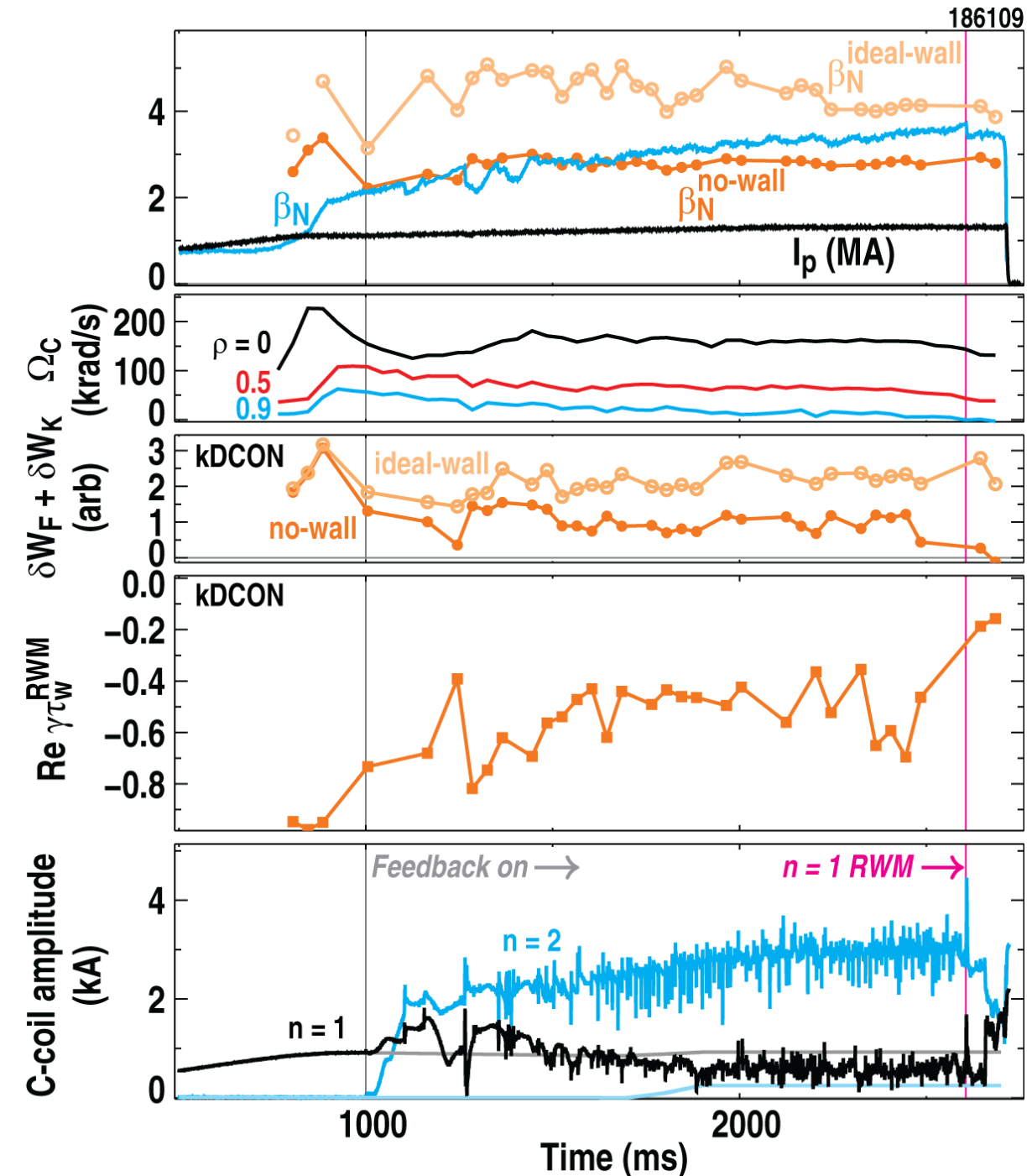
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 - Fast RWM control and EF correction
 - Baseline evolution indicates EF response



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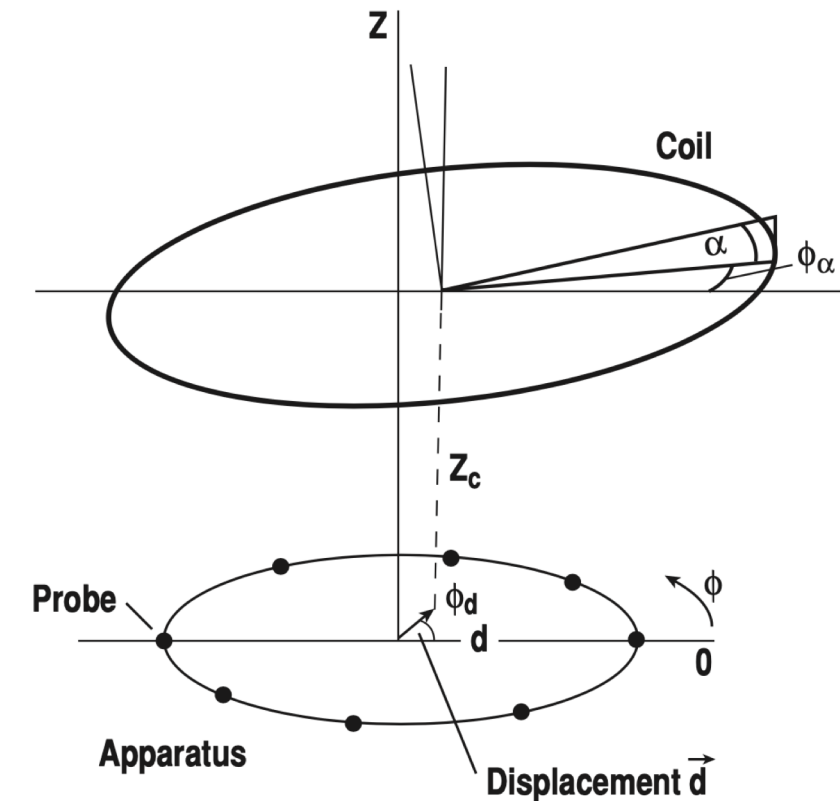
• *Can we understand what the feedback did?*



Recent developments enable error field correction simulations

- **DIII-D n=1 and n=2 EF source model is well established¹**
 - Based on in-vessel coil asymmetry measurements
- **Can simulate plasma response with DCON²/GPEC³**
 - Critical to include: *plasma selects EF harmonics*
 - *Ideal MHD + kinetic model* allows stable response prediction above no-wall limit
- **Idea: apply codes to simulate DIII-D high β feedback**
 - Multi-harmonic plasma response “collapsed” into single-mode model

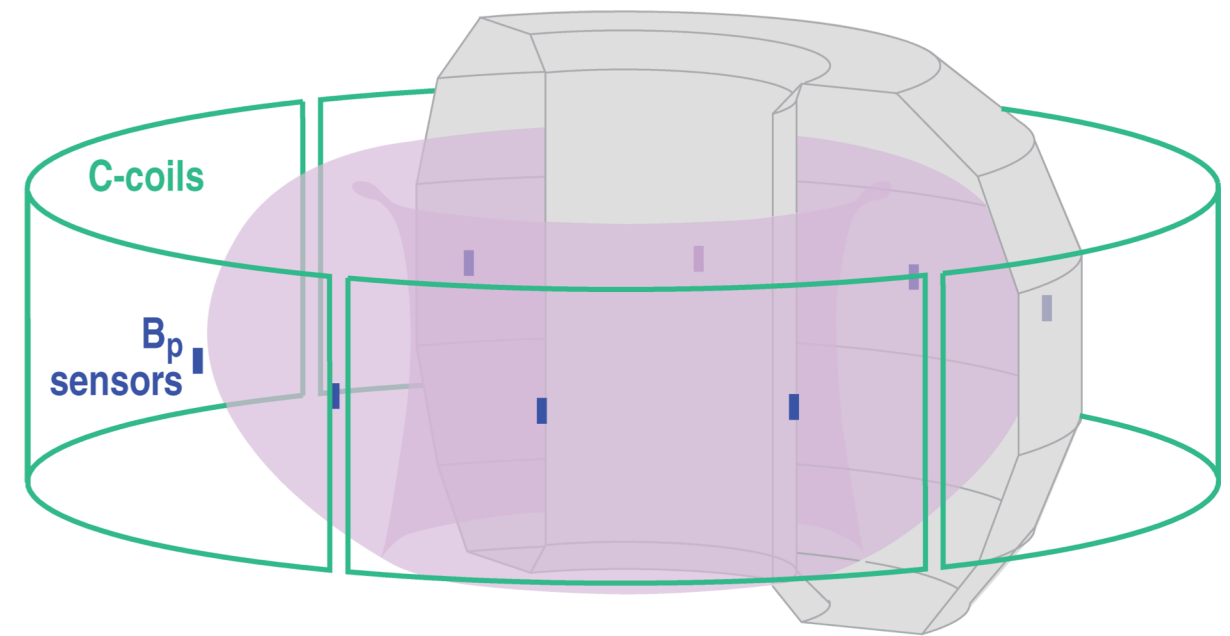
Perturbed coil and measurement apparatus¹



Simplifying assumptions lead to tractable model for feedback error field correction

1. Single toroidal arrays of coils and sensors, single-n

- Represent toroidal modes with complex scalars B_s or I_c
- Consistent with toroidal mode fitting in feedback algorithm



2. Fields are small enough that plasma response is linear

- Perturbed fields proportional to applied coil currents $B_s = A_{sc} I_c$
- Not always true: EF can change plasma rotation, changing A_{sc}

3. Plasma response is fast relative to equilibrium time scale

- Response time $\tau_w \approx 2.5 \text{ ms} \ll \tau_E \approx 100 \text{ ms}$
- Leads to time-independent model

Model equations are straightforward¹

- Sensor mode has vacuum and plasma response contributions, from intrinsic EF and coils

$$B_s = B_s^{\text{EF},v} + B_s^{\text{EF},p} + (A_{sc}^v + A_{sc}^p)I_c$$

The diagram illustrates the contribution of different software components to the sensor mode equation. SURFMN (green text) is associated with the vacuum field term $B_s^{\text{EF},v}$. GPEC (orange text) is associated with the plasma response terms $B_s^{\text{EF},p}$, A_{sc}^v , and A_{sc}^p . Arrows indicate the flow of information from the software components to the corresponding terms in the equation.

- Proportional gain feedback law as in real-time algorithm

$$I_c = G_{cs}B_s$$

- Feedforward commands, sensor baselining, and sensor vacuum compensation also included
 - But omitted here for simplicity

Solving yields predicted coil currents and sensor fields

- **Closed loop solution**

$$I_c = \frac{G_{cs}}{1 - A_{sc}G_{cs}} B_s^{\text{EF}}, \quad \text{with } B_s^{\text{EF}} = B_s^{\text{EF},v} + B_s^{\text{EF},p} \text{ and } A_{sc} = A_{sc}^v + A_{sc}^p$$
$$B_s = \frac{1}{1 - A_{sc}G_{cs}} B_s^{\text{EF}}$$

- **Infinite gain limit yields “optimal” current for nulling EF sensor field**

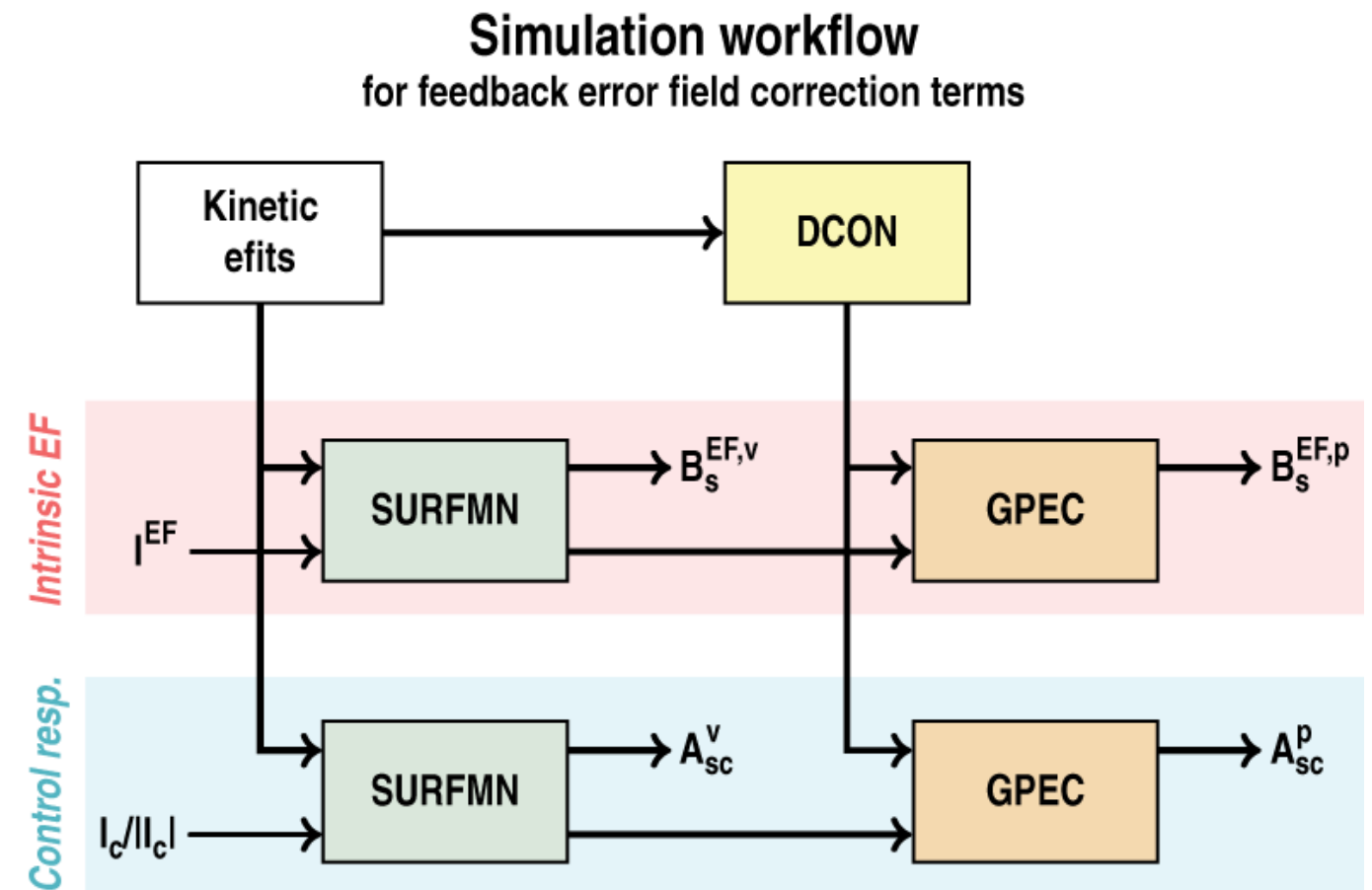
$$I_c^{\text{opt}} = -\frac{1}{A_{sc}} B_s^{\text{EF}}$$

Modular simulation codes enable flexible workflow

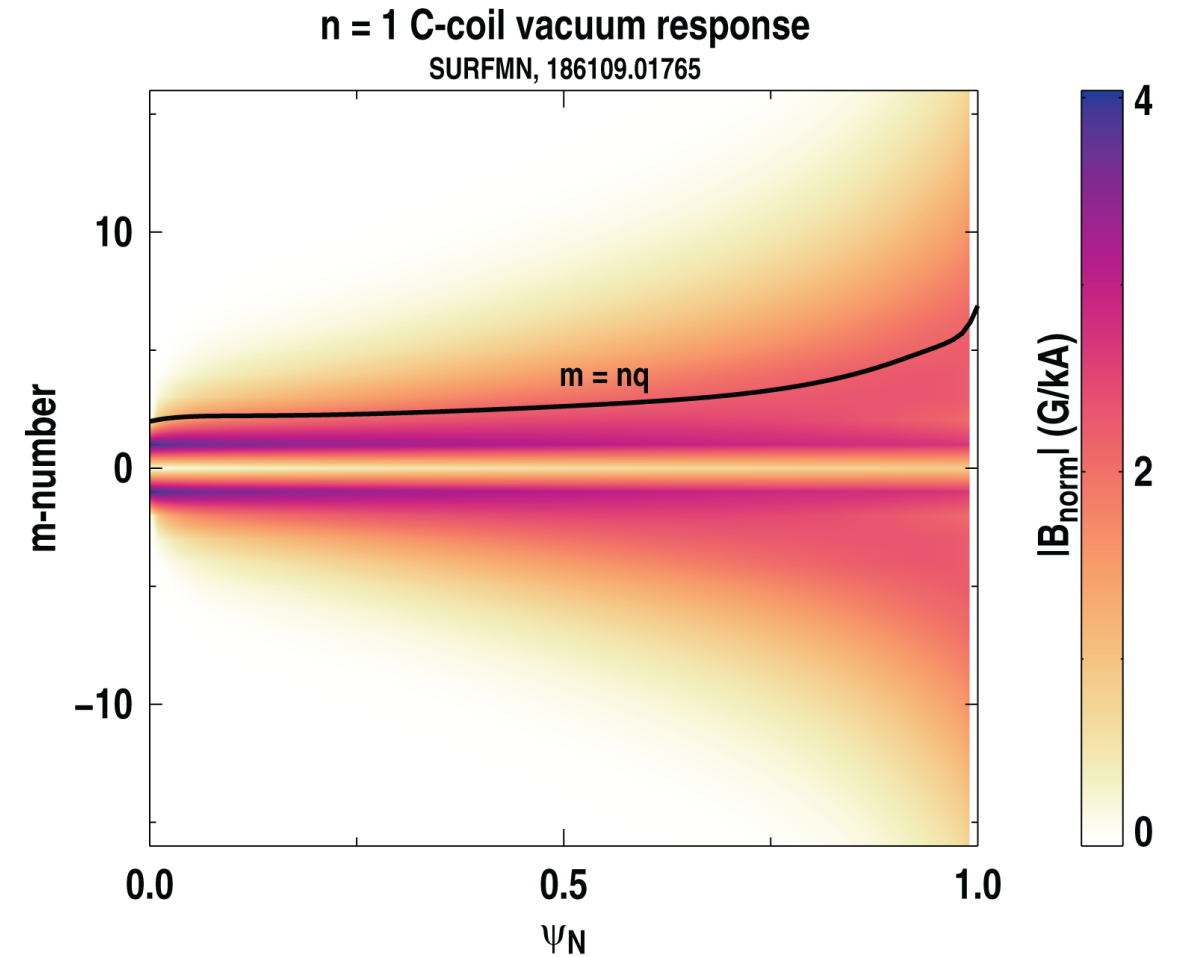
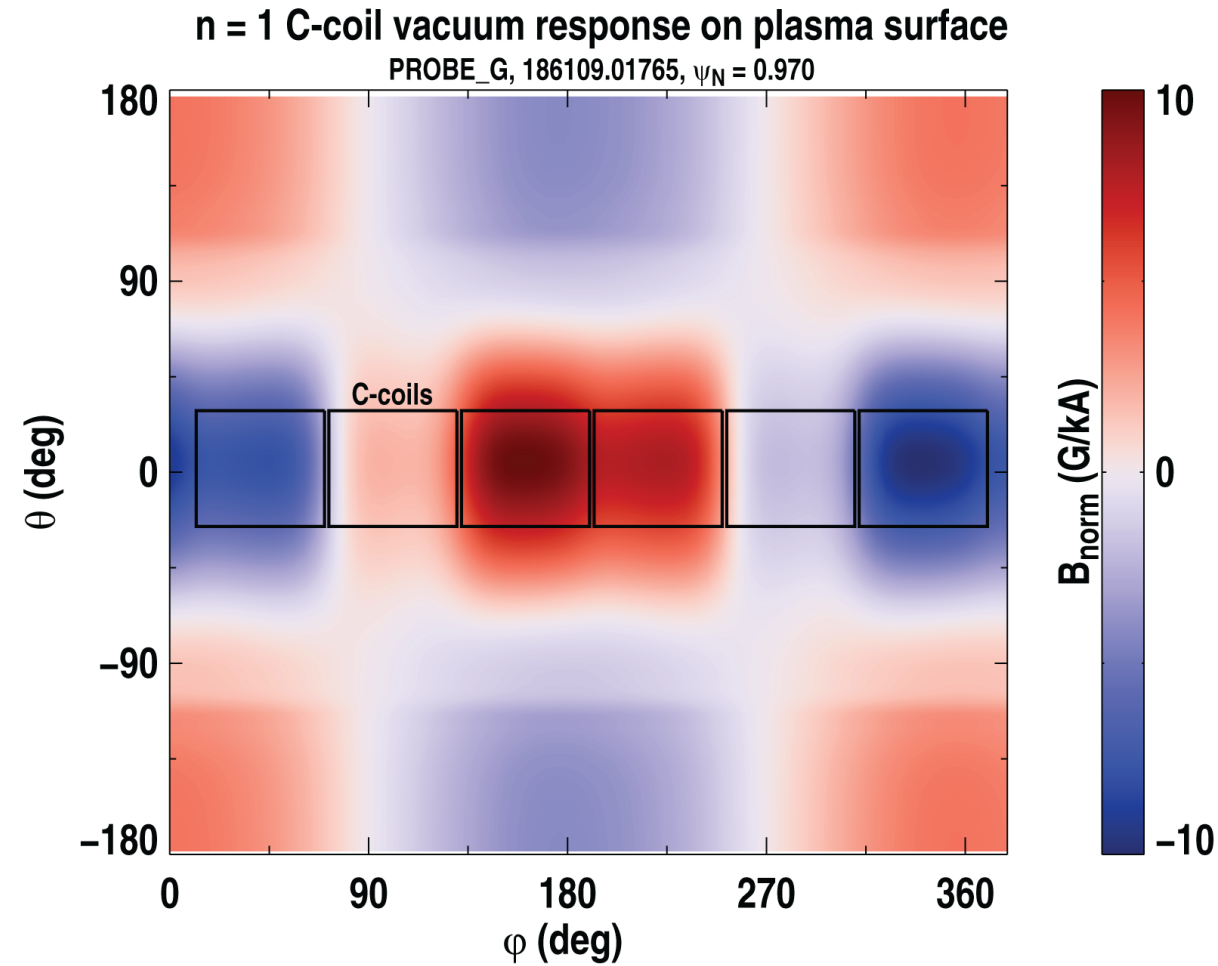
- **SURFMN:** 3D vacuum fields, given coil currents¹
- **DCON:** MHD mode spectrum and stability²
- **GPEC:** MHD spectrum response to 3D fields³

- **Exploit model linearity**

- Fields from different code runs can be summed
- Extract amplification terms A_{sc} with unit amplitude coil currents
- Sensor fields from integrals over sensor areas

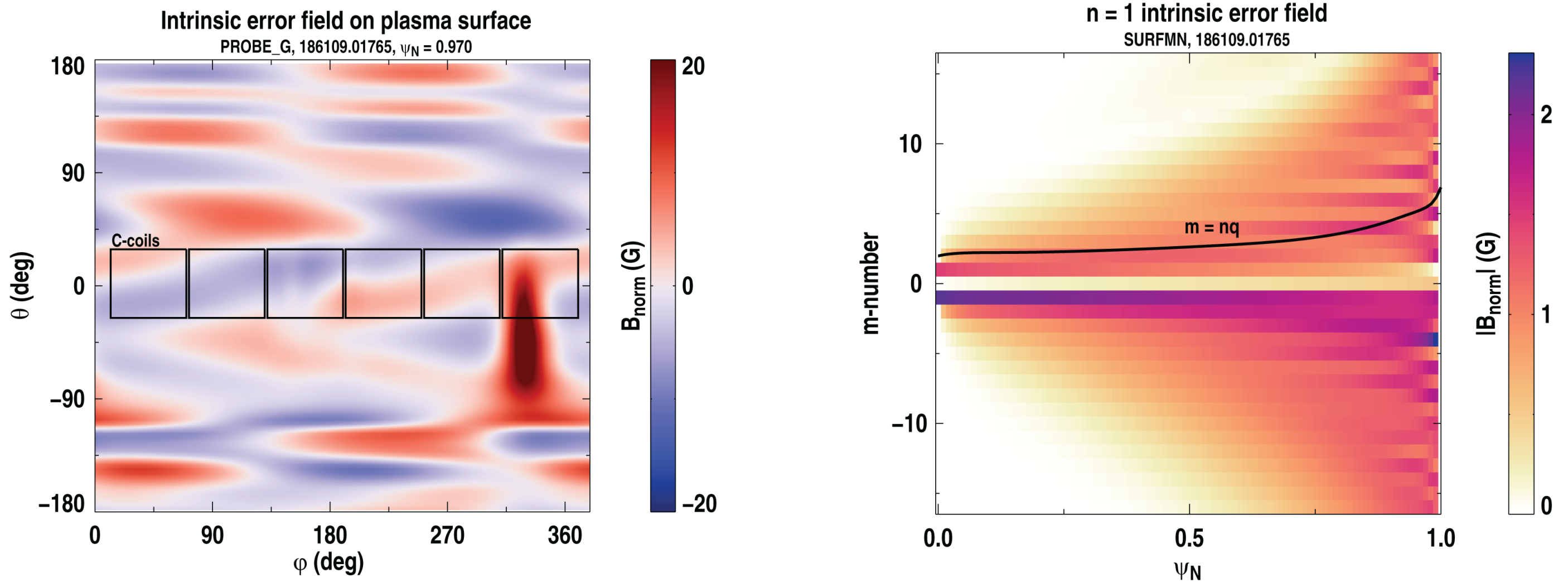


C-coil $n=1$ vacuum field has a broad m -spectrum



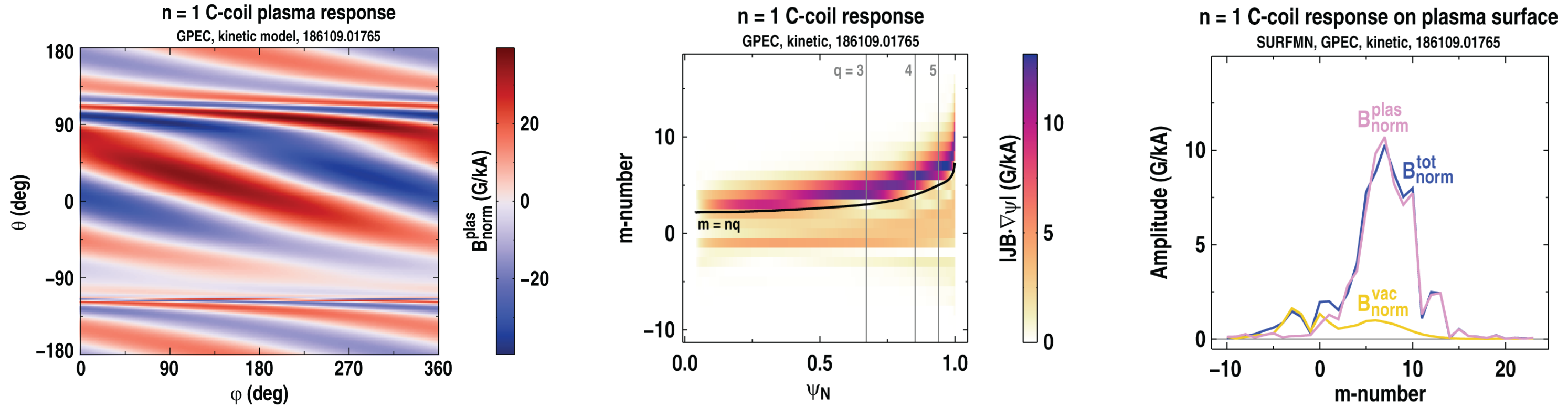
- SURFMN predicts $n=1$ C-coil perturbation can couple to pitch-resonant and nonresonant harmonics

Intrinsic error field spectrum is also broad



- **SURFMN predicts broad intrinsic error field spectrum**
 - Anti-resonant peak in right-handed plasma

Kink-like plasma response to C-coil field predicted

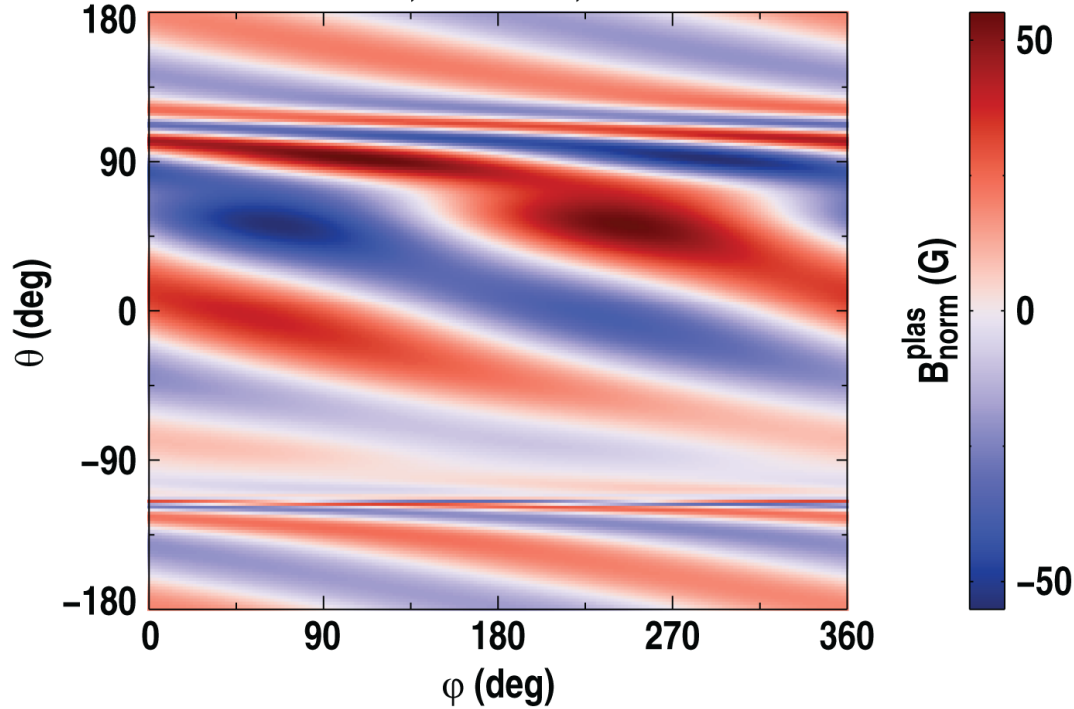


- **Plasma response dominates** over vacuum field

Intrinsic error field response prediction is also kink-like

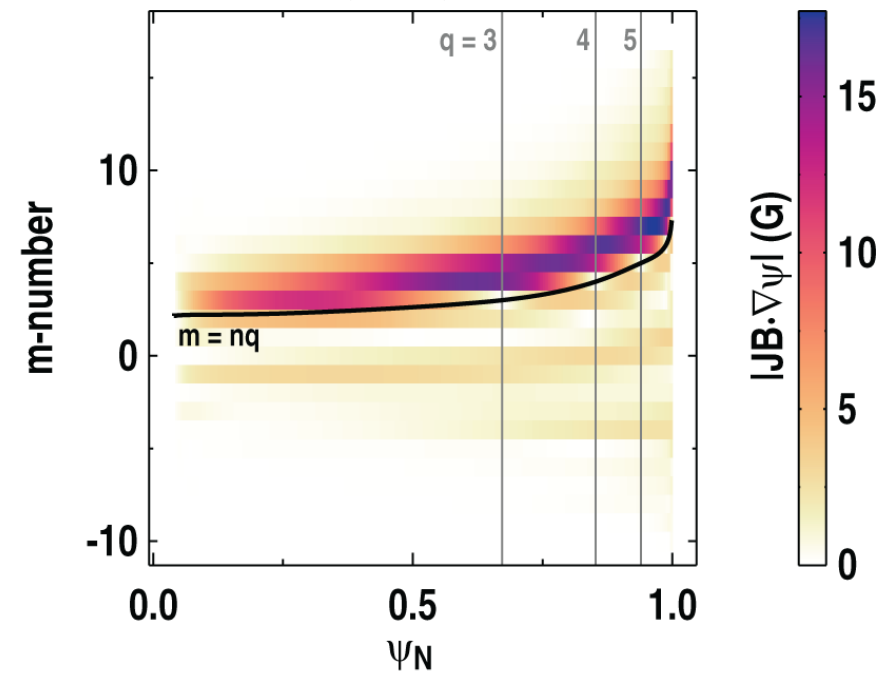
n = 1 intrinsic error field response

GPEC, kinetic model, 186109.01765



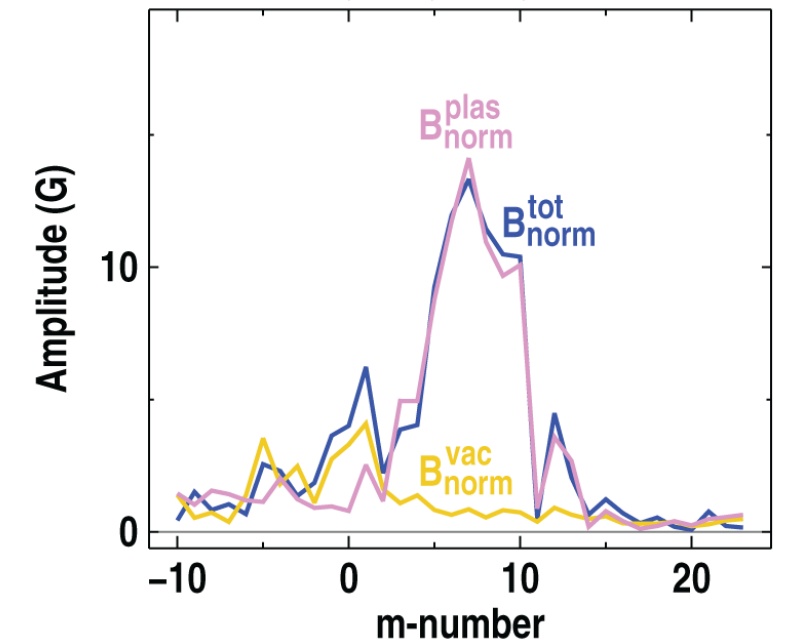
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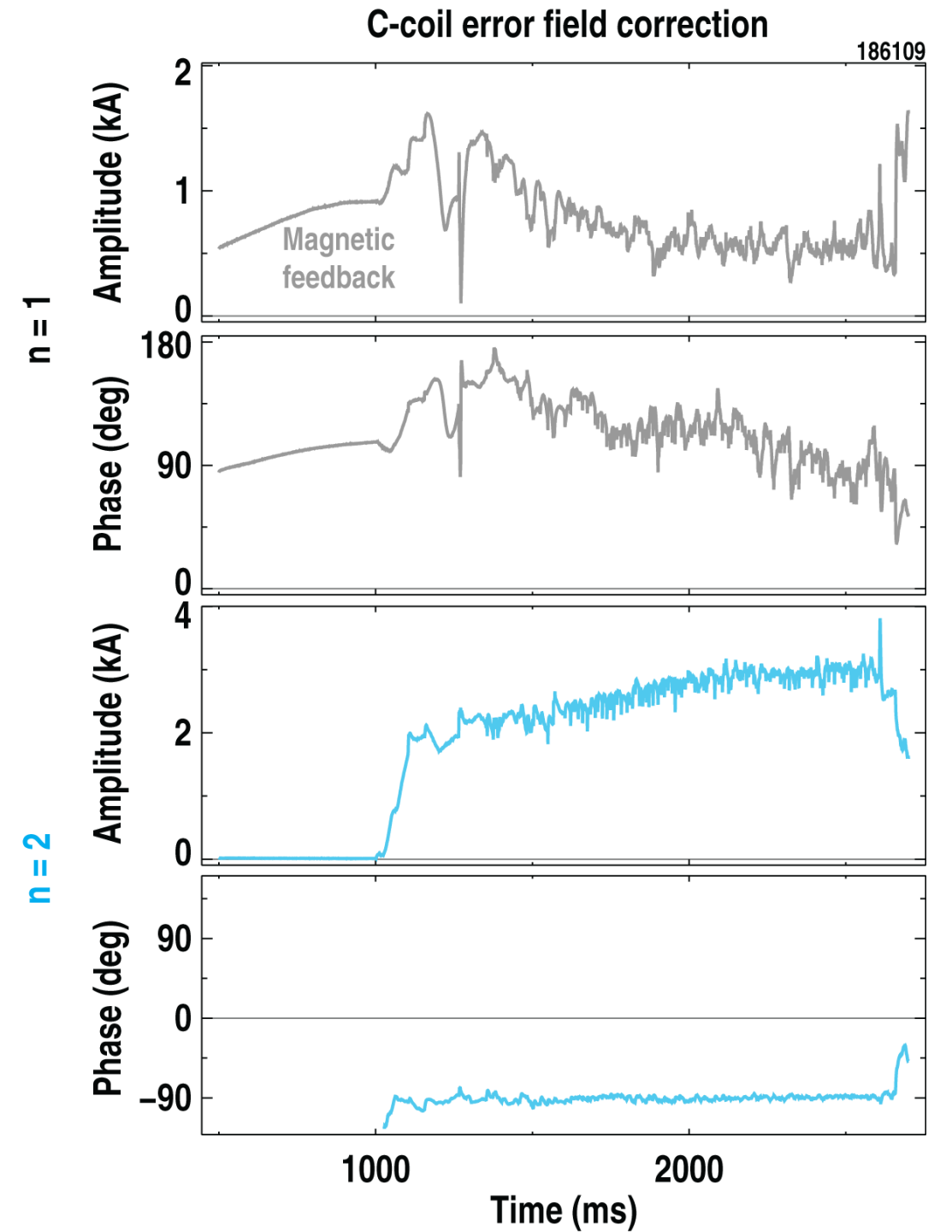
n = 1 intrinsic EF response on plasma surface

SURFMN, GPEC, kinetic, 186109.01765



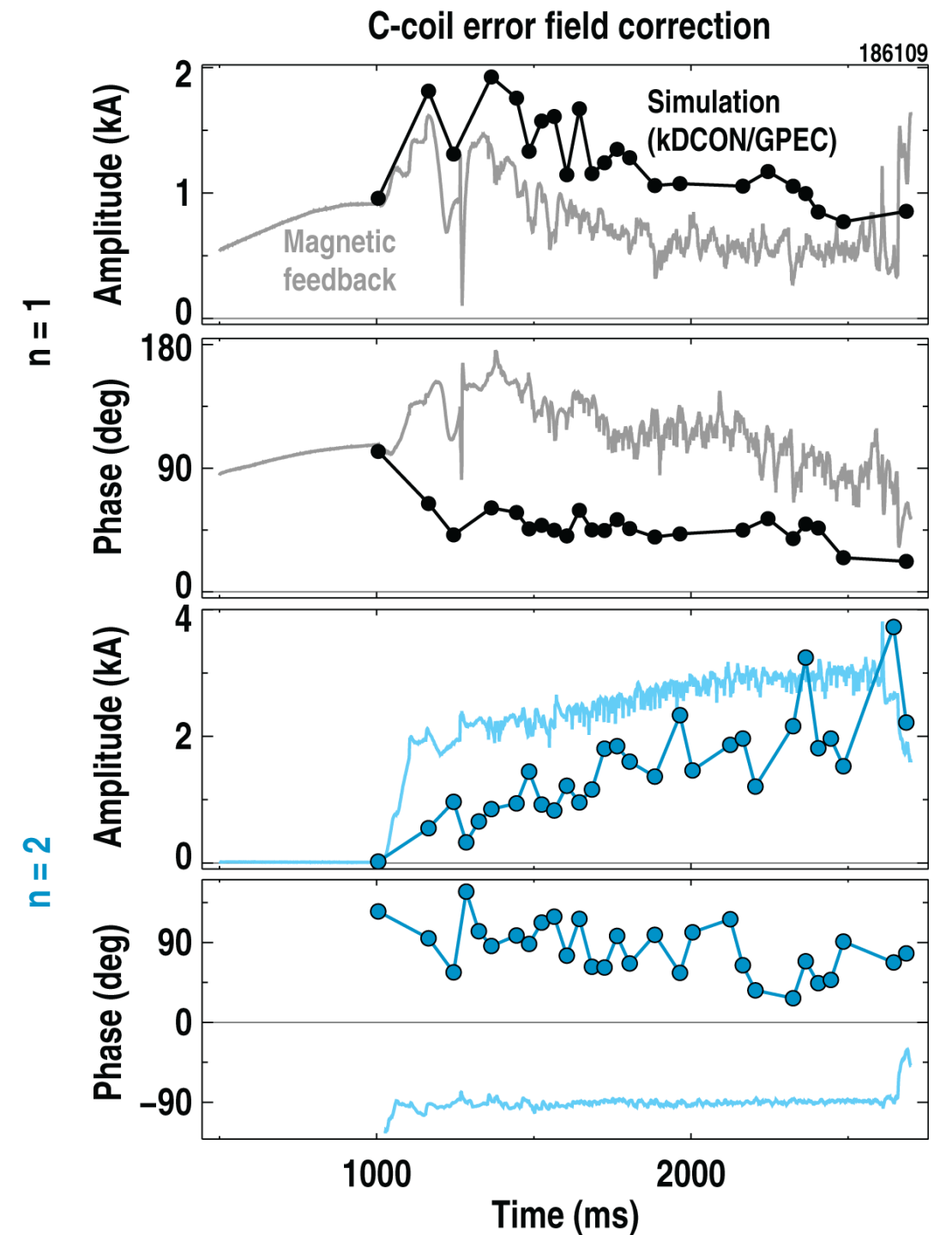
- Coils that couple to the plasma kink mode should be excellent for error field control

Can simulations predict feedback baseline evolution?



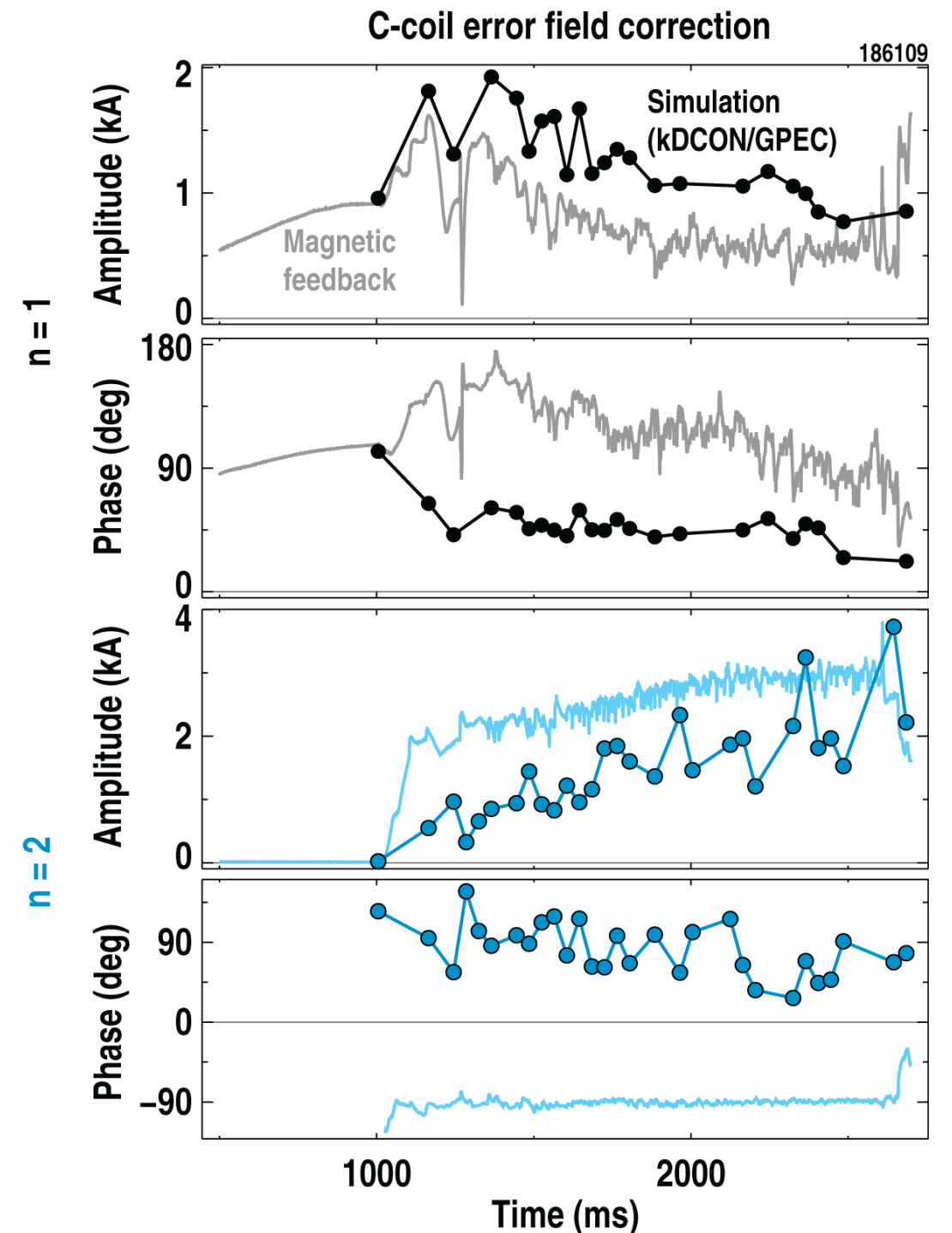
Can simulations predict feedback baseline evolution?

- Predict $n=1$ amplitude to within 50%, phase to within 90°
- $n=2$ predictions are more scattered
 - Large phase disagreement



Can simulations predict feedback baseline evolution?

- Predict $n=1$ amplitude to within 50%, phase to within 90°
- $n=2$ predictions are more scattered
 - Large phase disagreement
- Several possible explanations for discrepancies
 - Sub-optimal feedback? *shot did exhibit rotation braking and instability*
 - EF source model inaccuracies?
 - Plasma response calculation? *180 phase shift would be surprising*



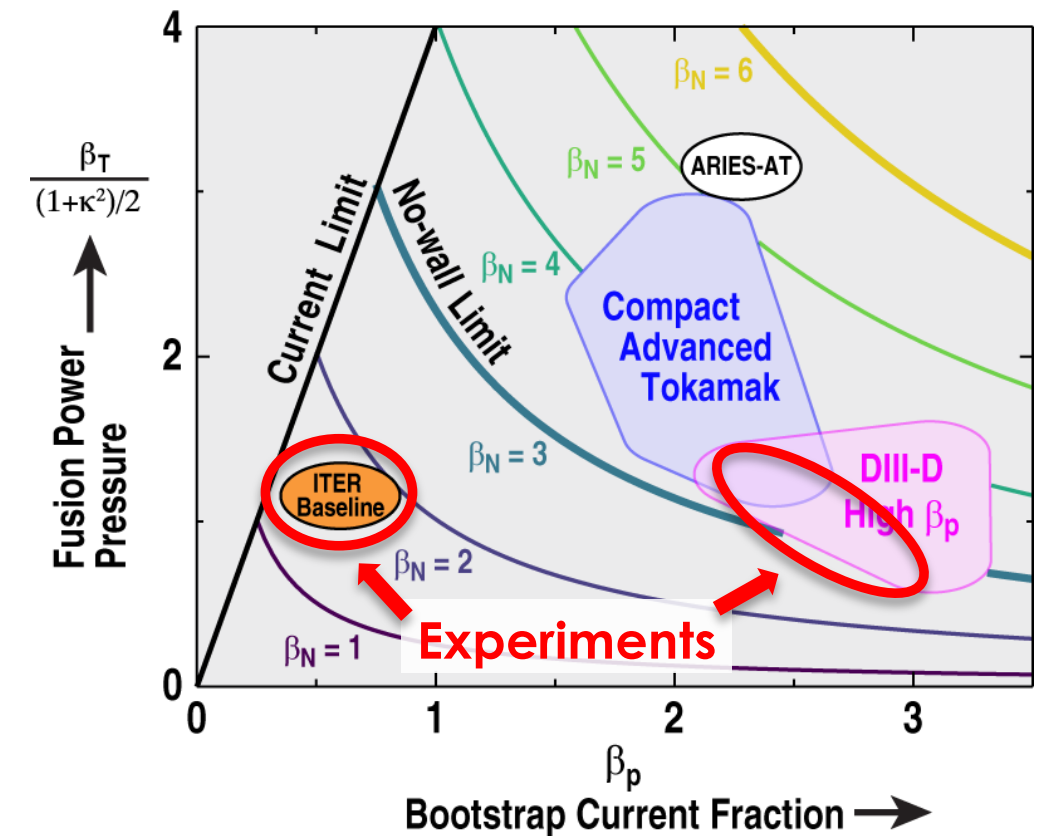
Conclusions

- **Kink mode response is a key observable for validating simulations and lever for plasma control**
 - Easily driven with applied 3D fields
- **Resistive response linked to mode locking in low-torque regime**
 - Measurements consistent with resistive MHD simulations
 - Simulations show weakening shielding at rational surfaces as rotation slows
- **New simulations facilitate error field correction predictions**
 - Link error field source model with plasma response simulation
 - Validation effort ongoing

Extra slides

DIII-D can explore different operating regimes of interest for fusion

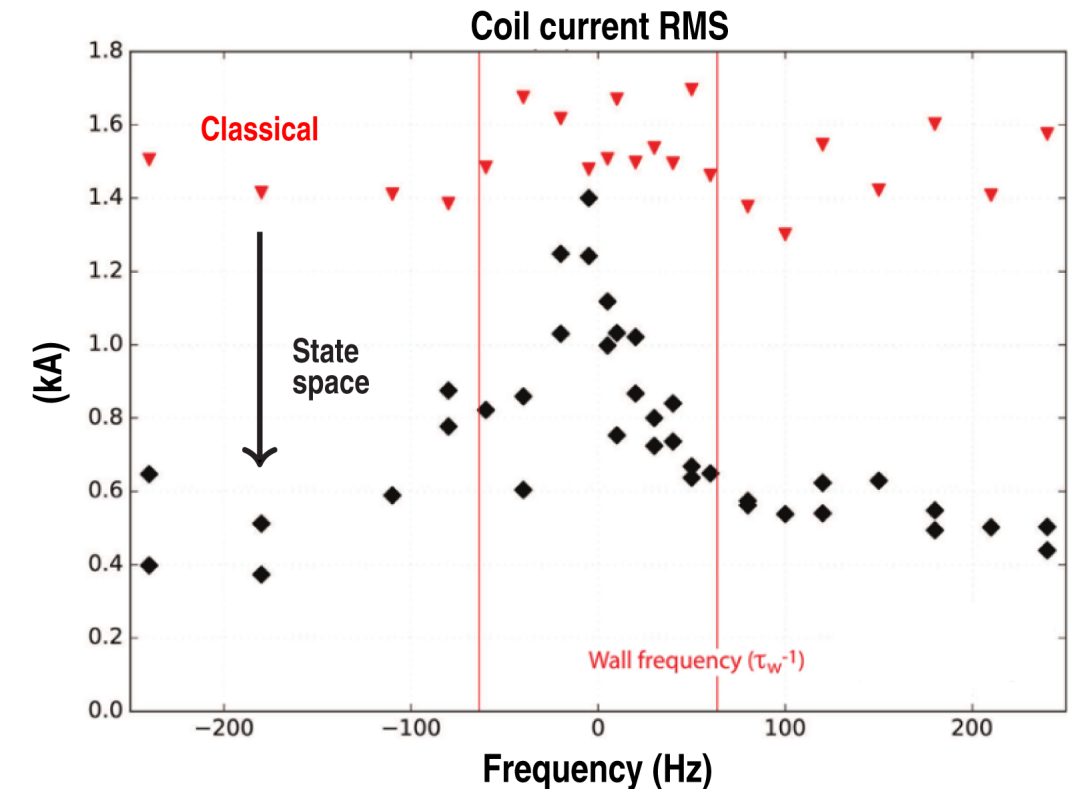
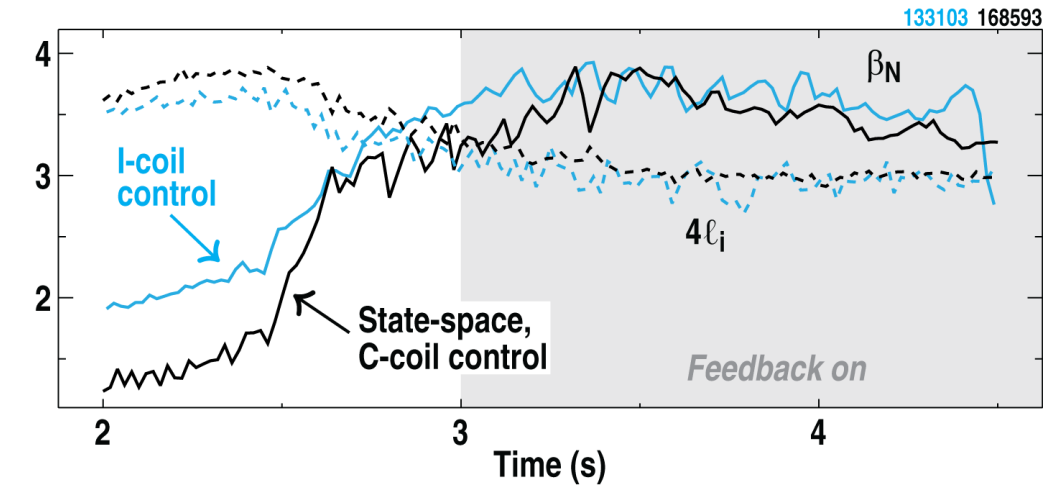
- **High current scenarios have good confinement, but high current drive need**
 - Example: ITER baseline scenario (IBS)¹
 - Peaked current profile → high no-wall limit
- **Increasing β_p is associated with higher bootstrap and non-inductive fractions**
 - Higher degree of profile self-organization²
 - Broad current profile → high with-wall limit³
 - Advanced tokamak candidate for compact fusion pilot⁴
- **Stability challenges differ, will show results from different regimes**



Simulations inform control strategies

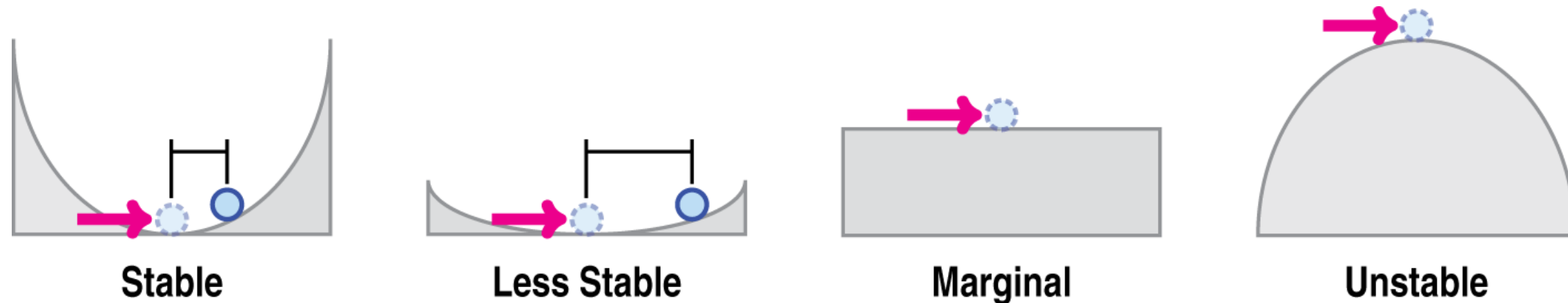
- **Evaluated state-space control approach¹**
 - Incorporating reduced-order VALEN model
- **Accessed $\beta > \beta^{\text{no-wall}}$ using external coils**
- **Led to reduced power requirement**
 - Compared with proportional gain

1. M. Clement, et al., *Nucl. Fusion* **58** (2018) 046017.



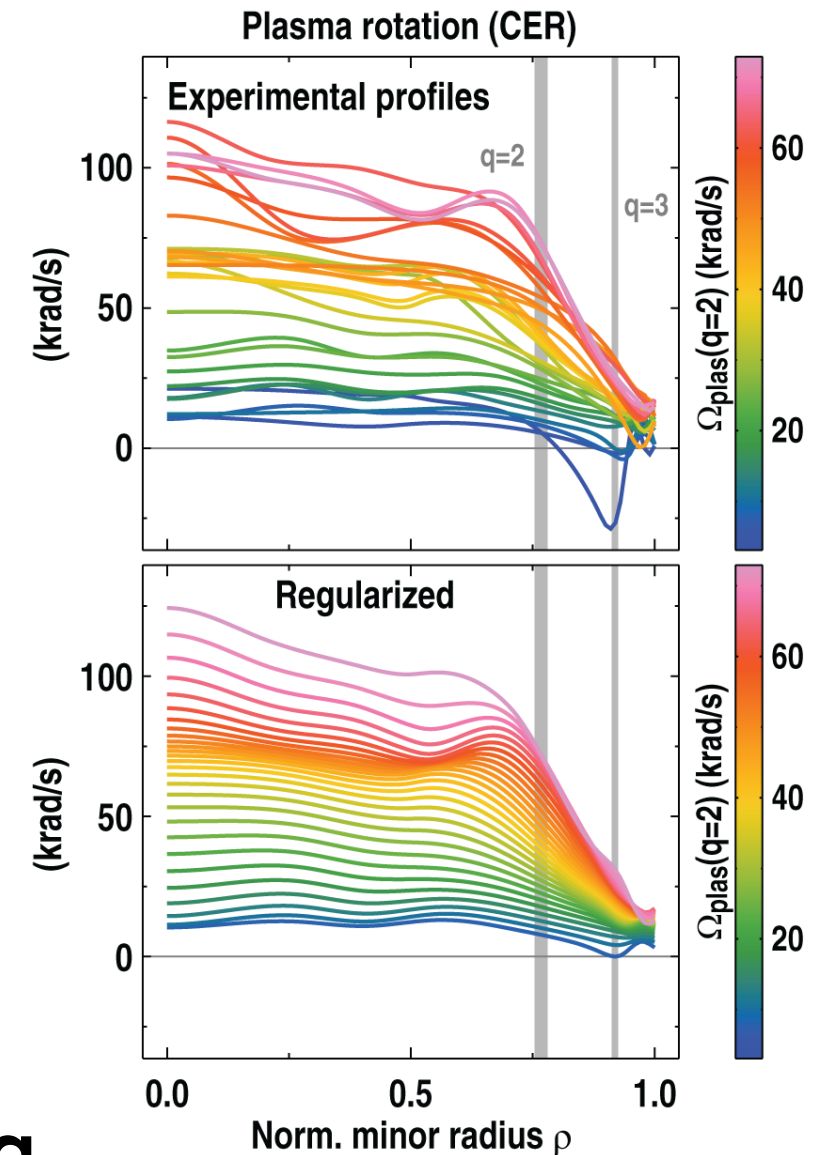
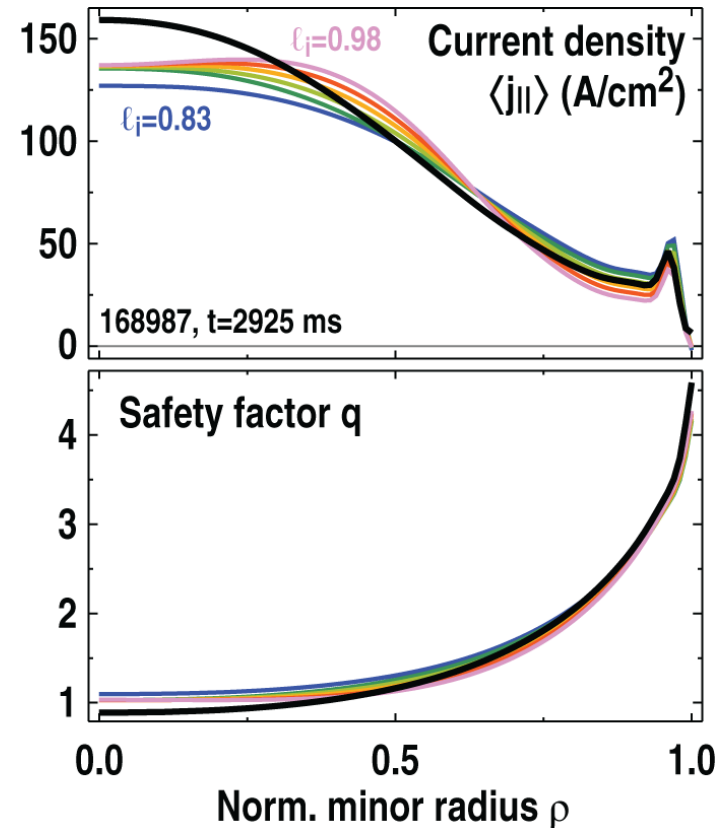
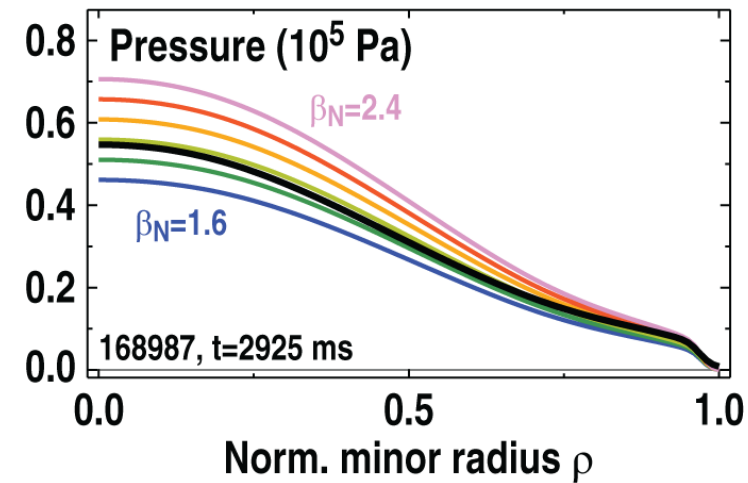
Perturbative experiments can help assess stability

- Consider a family of mechanical systems



- Apply a ***small perturbation***
- If the system is stable, we can ***measure a finite response***
- ***Response contains information*** about the proximity to marginal

Profile variations allow investigations of β_N , ℓ_i , and rotation dependencies



- Pressure and current profile variations created by scaling a single equilibrium
- Rotation profile variations created by interpolating experimental profiles