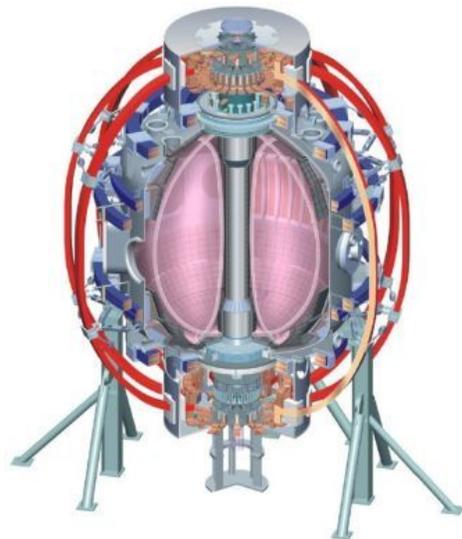


# Development of Improved Vertical Position Control

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**Location**  
**Date**

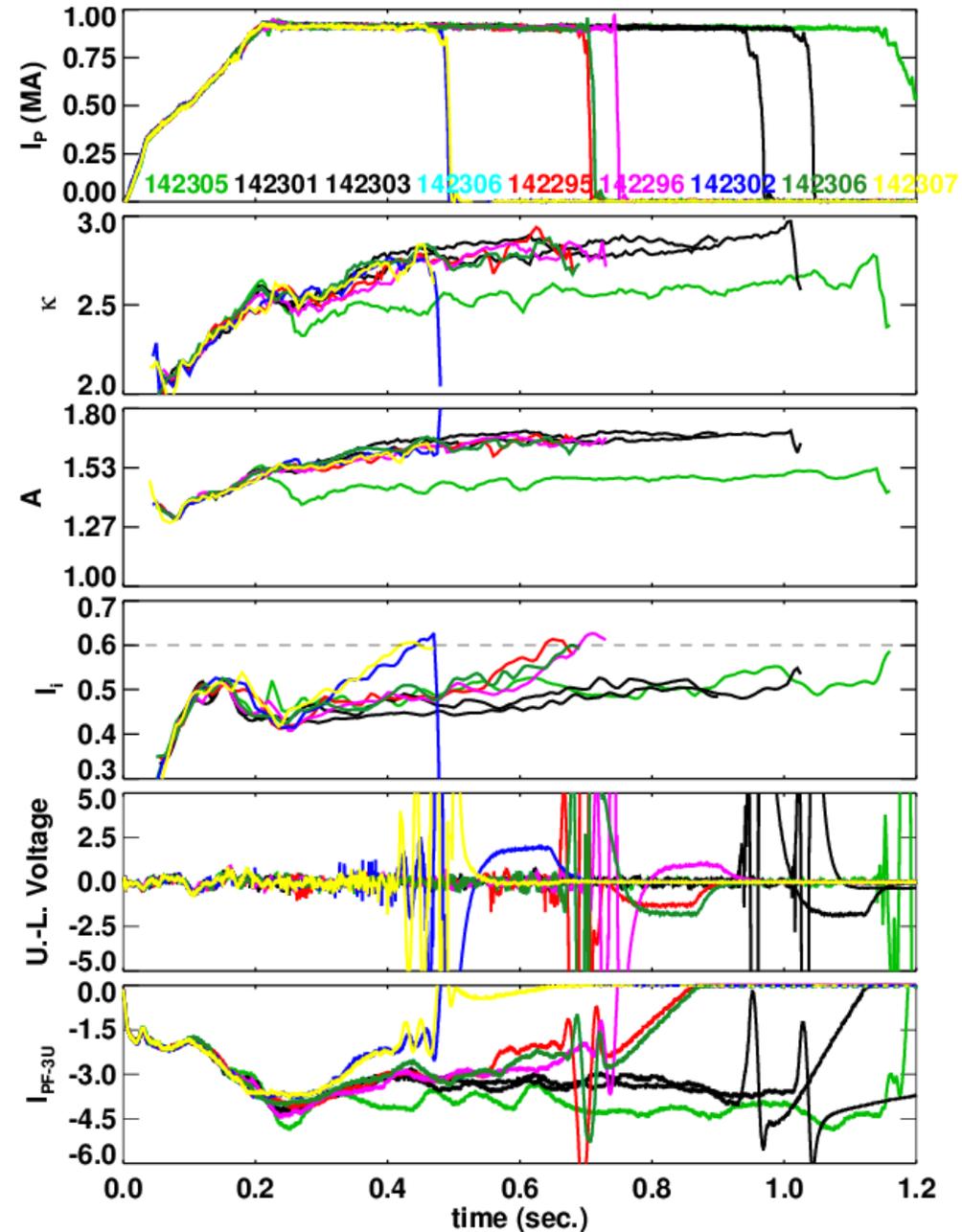


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# XP in 2010 Showed that Vertical Position Control can be Lost at Higher Aspect Ratio

- 1 Fiducial (green) and 8 shots at higher aspect ratio.
  - Black cases vertically stable, the colored ones have VDEs.
- *VDE is always triggered when  $I_i=0.6$ .*
  - This is not a particularly high value.
  - Would preclude use of the scenario for many XPs.
  - Many upgrade scenarios with central NBCD have  $I_i>0.6$
- *Motivates improvements to the  $n=0$  controller.*



# Strategy To Fix Problem

- Improve the detection of small vertical motion.
  - “dZ/dt Observer”
- Re-optimize vertical control gains with improved observer.
- If necessary, use RWM coils for vertical control.

# Vertical Position Controller is a PD Controller Using Loop Voltages for $dZ/dt$ Measurement

- Proportional controller is simply the Isoflux shape control algorithm:

$$V_{PF-3,P} = M \times PID(\text{segment error})$$

- Fast derivative controller is based on the up-down loop voltage difference.

$$V_{PF-3,D} = D \times (\dot{\psi}_{Upper-Loop} - \dot{\psi}_{Lower-Loop})$$

- The underlying assumption is that the plasma vertical position can be measured by only 2 loops:

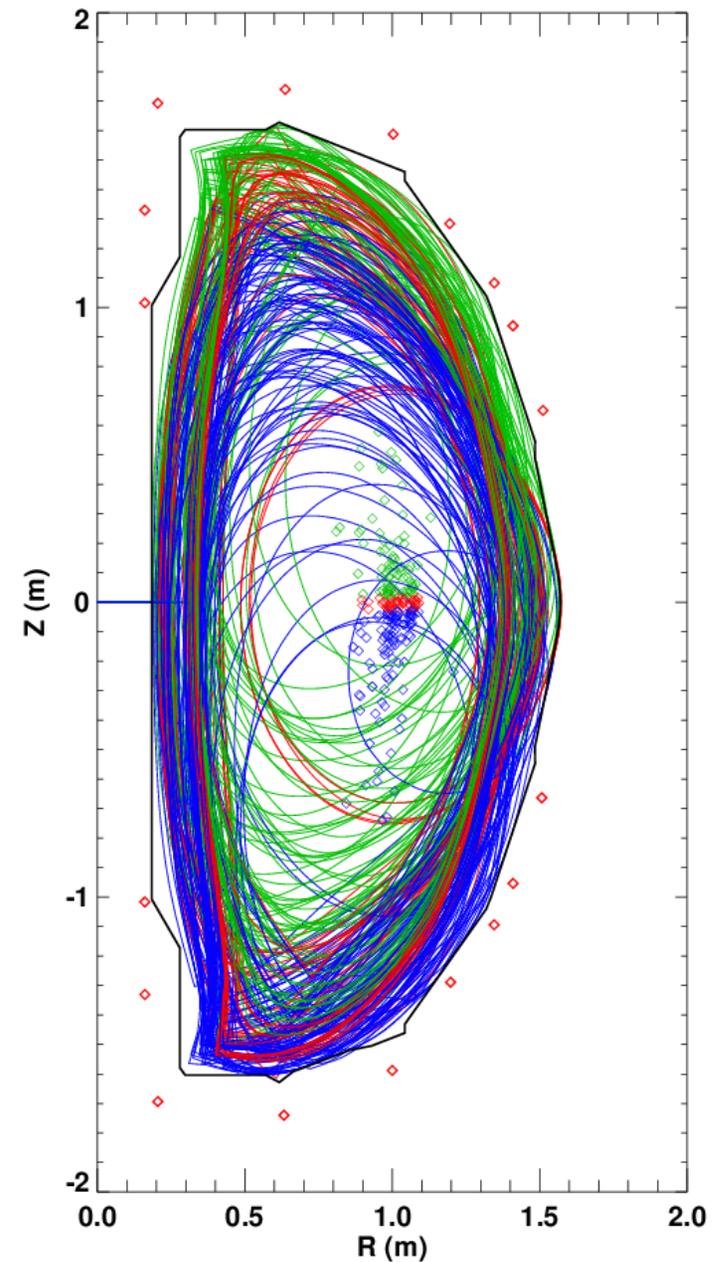
$$I_P Z_P = C \times (\psi_{Upper-Loop} - \psi_{Lower-Loop})$$

- Thesis: Using more loops will lead to a better estimation of the plasma position.
  - Eliminate  $n=1$  pickup from random loop orientation problems.
  - More information for shapes that are distorted.

# Numerical Tests Have Found That More Loops Are Better (I)

- Constructed ~220 NSTX equilibria.
  - Shift them off the axis, change the divertor coils, change  $I_p$ .
- Computed the flux at the various flux loop locations.
- Fit the magnetic axis location to a function:

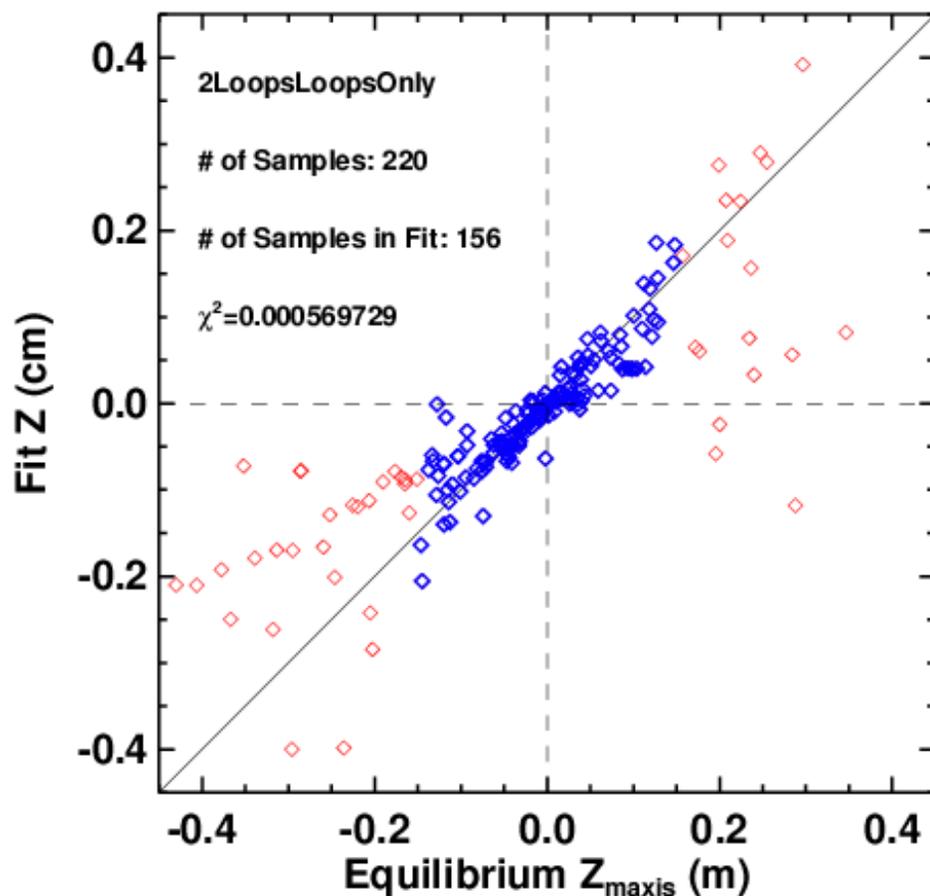
$$I_p Z_P = \sum_{i=1}^{NumLoopPairs} C_i \times (\psi_{Upper-Loop,i} - \psi_{Lower-Loop,i})$$



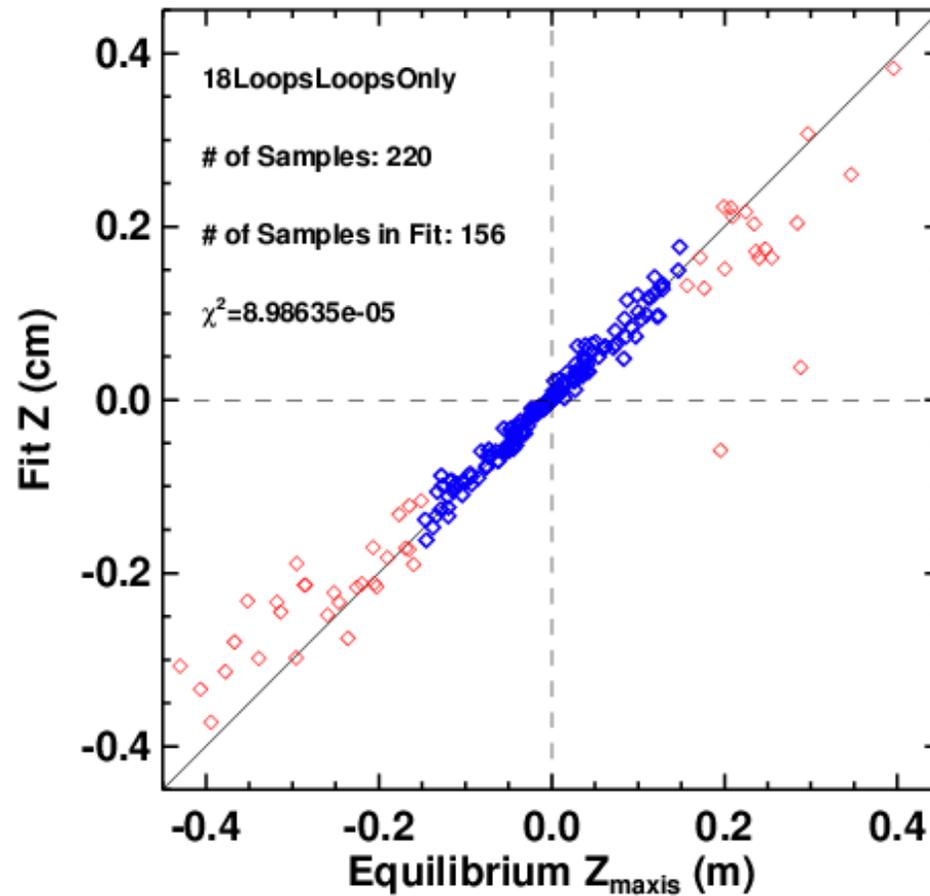
# Numerical Tests Have Found That More Loops Are Better (II)

- Use only blue points in the fits ( $|Z_{\text{maxis}}| < 15 \text{ cm}$ )

*1 Pair of Loops  
(On Primary Passive Plates)*



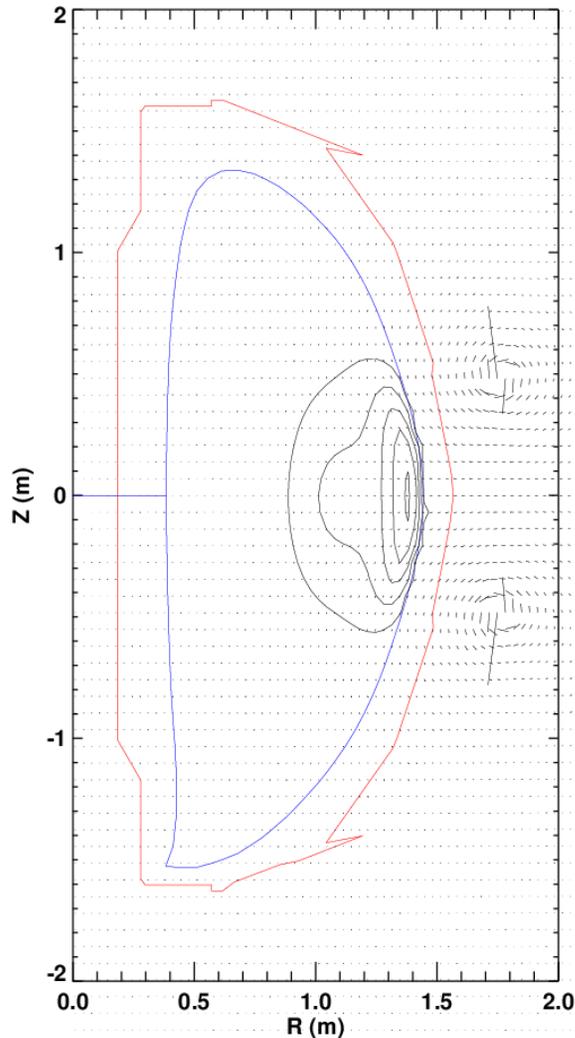
*9 Pair of Loops  
(6 Cat. 4, 3 Cat. 3)*



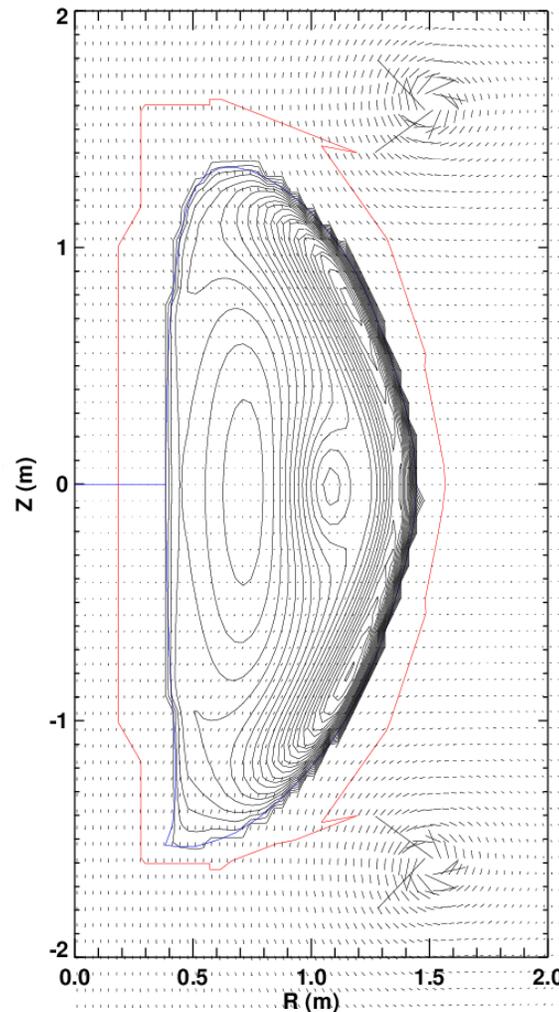
# Vertical Position Control May Be Possible With the RWM Coils

Calculate force assuming 1 amp of power supply currents  $F_Z = \sum J_\phi B_R$

**RWM Coils:  $F_Z=78$**



**PF-3 Coil:  $F_Z=1500$**



**RWM Coils make far less force for the same power supply current.**

*(ratio is not as bad for lower-elongation plasmas)*

**However....**

**1) SPA are very fast (to 3 kA in 1-2 msec)**

**2) RWM coil field may not couple as strongly to the passive plates.**

**Use this as a last resort if we have insufficient vertical control margin after other things are tried.**

# Run Plan

- Debugging: Compare PCS calculations to identical off-line versions.
- XMP (?): Test that system is correctly coupled to the PF-3 coils.
- Day 1: Optimize gains with PF-3 as actuator, new  $dZ/dt$  observer.
  - Reload vertically unstable target,  $A \sim 1.75$ ,  $\kappa = 2.9$
  - Use divertor gas injection to drive  $I_i$  up ?
- Day 2 (if necessary):
  - Repeat unstable scenario, using RWM coils for  $n=0$  control. Do a derivative gain scan.

## What if this does not work?

- Could replace the PD controller with something more sophisticated.
- More voltage capability on PF-3.
- Make PF-2 bi-polar for vertical control.
  - Or always run with a PF-2 positive bias (not-desirable!)

# Backup

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# PCS Status

- dZ/dt Observer
  - Complete specification has been written.
  - Electronics for voltage difference amplifiers have been ordered.
  - Requested they be ready for the ISTP.
  - Have not started coding it in PCS.
  
- RWM coils for  $Z_{\text{axis}}$  control.
  - Specification has been written.
    - Will be part of the RWM proportional control algorithm.
  - Relies on the improved dZ/dt observer for the measurement.
  - Have not started on the PCS code yet.