ASC XP-823

Error Field Correction and Long Pulse J.E. Menard, S.P. Gerhardt

$$
\begin{aligned}
& \text { Part } 1 \\
& \text { Determine the source of, and optimal correction for, } \\
& \text { the observed } n=3 \text { error field. } \\
& \qquad \text { Part } 2 \\
& \text { Optimize the } n=1 \text { feedback time constant and gain } \\
& \text { for optimal pulse length at high- } \beta \text {. }
\end{aligned}
$$

## n=3 Applied Fields Can Improve Discharge Performance

- Impact on rotation appears as soon as $\mathrm{n}=3$ field is turned on.
- Some polarities of $n=3$ cause acceleration, others braking $\rightarrow$ there is an intrinsic $n=3$ error field.
- Pulse length improves with the $\mathrm{n}=3$ polarity yielding maximum rotation.

What determines the required $n=3$ correction level? The plasma current? The PF 5 coil?

## Try to Find The Optimal Correction at 750kA, 900kA, and 1100kA



## Method Utilized to Determine the $\mathrm{n}=3$ Correction

- Average the rotation over three CHERS time points before the $\beta$ collapse.
- Plot rotation at various radii as a function of RWM coil current.
- Fit the data as (see to right):
- A simple parabola. (blue)
- Two lines on either side of the maxima (green)
- Estimate the optimal current from:
- Maxima of parabola
- Intersection of the lines.

| $X P$ | $I_{p}(k A)$ | Average three time <br> points surrounding: |
| :---: | :---: | :---: |
| XP 823 | 750 | 0.43 |
| XP 701 | 900 | 0.6 |
| XP823 | 1100 | 0.42 |

## Shots Used in Analysis For Optimal n=3 Correction

| Shot | Plasma Current | XP | EFC Coil 1 Current |
| :---: | :---: | :---: | :---: |
| 124411 | 900 | 701 | 0 |
| 124428 | 900 | 701 | -250 |
| 124430 | 900 | 701 | -300 |
| 124432 | 900 | 701 | 306 |
| 124433 | 900 | 701 | 306 |
| 124434 | 900 | 701 | 434 |
| 124437 | 900 | 701 | -413 |
| 124438 | 900 | 701 | -650 |
| 124439 | 900 | 701 | 650 |
| 124440 | 900 | 701 | -300 |
| 128039 | 750 | 823 | 0 |
| 128043 | 750 | 823 | -200 |
| 128046 | 750 | 823 | 250 |
| 128047 | 750 | 823 | -230 |
| 128048 | 750 | 823 | -350 |
| 128049 | 750 | 823 | -576 |
| 128895 | 1000 | 823 | 0 |
| 128896 | 1000 | 823 | -275 |
| 128897 | 1000 | 823 | 316 |
| 128898 | 1000 | 823 | 650 |
| 128899 | 1000 | 823 | -650 |
| 128900 | 1000 | 823 | -1000 |
| 128901 | 1000 | 823 | 970 |
| 128902 | 1000 | 823 | -400 |

- Shots span two years.
- No n=1 DEFC or RWM feedback in any of these.
- XP701 data used gapcontrol algorithm, XP823 used Isoflux.


## Example Results for the Three Currents



Parab. Opt.: -155.603 A, Linear. Opt.: -344.075 A

Rotation at $\mathrm{R}=130$ shown, but similar results at larger radii.

Two methods don't always agree, parabola is typically better.


Parab. Opt.: -297.058 A, Linear. Opt.: -341.228 A


## Pull it all Together...No Clear Trends

| $\mathrm{I}_{\mathrm{P}}(\mathrm{kA})$ | PF 5 Current <br> $(\mathrm{kA})$ | Typical Correction <br> From Parabolic Fits (A) | Typical Correction From Linear <br> Intersections (A) | SPG's Recommended <br> Correction (A) |
| :---: | :---: | :---: | :---: | :---: |
| 750 | 8255 | 175 | 300 | 250 |
| 900 | 9065 | 250 | 340 | 300 |
| 1100 | 9834 | 115 | 200 | 200 |

- Recommended correction based on both rotation optimizations and pulse length.
- 1100 kA optimizes to smaller correction than 750kA \& 900kA $\rightarrow$ inconsistent with $I_{P}$ scaling and difficult to reconcile with PF5.
- Maybe the TF?
- Probably OK to always use 250 A n=3.
- Toroidal phase and poloidal spectrum of correction not optimized...need NCC for that.


## Feedback Algorithms Upgraded at the Beginning of 2008 Run

## Change 1: EF/Mode Identification

Before: A single $\mathrm{n}=1$ amplitude and phase (2 numbers), based on some preset combination of $B_{P}$ and $B_{R}$ Sensors

After: Separate $\mathrm{n}=1$ amplitude and phase from $\mathrm{B}_{\mathrm{R}}$ and $\mathrm{B}_{\mathrm{P}}$ sensors (4 numbers)

## Change 2: Correction Current Request

Before: Single feedback gain and toroidal phase
After: i) Separate gain and feedback phase for $B_{P}$ and $B_{R}$ mode amplitudes.
ii) Single pole filter on the SPA requests ( $\tau_{\text {LPF }}$ ), to remove transients, or to simulate the effect of conducting structures.

## $\mathrm{n}=1$ feedback gain, LP filter optimized for $\mathrm{I}_{\mathrm{P}}=1.1 \mathrm{MA}$

 Expands 2007 data set at 900 kA- Instead of applying known n=1 EF, used OHxTF EF (1.1MA uses full OH swing)
- Used $B_{p} U / L$ averaging from 2007, included $n=3$ EFC (new for 2008)
- Increased gain scan by factor of 3: 0.7 in $2007 \rightarrow$ up to 2 in 2008
- Response to $n=1$ RFA from OHxTF error field changes little for $G_{p}>1$
- System marginally stable at $G_{P}=2$ for $\tau_{\text {LPF }}$ as low as $1-2 \mathrm{~ms}$
$\rightarrow$ Optimal control parameters: $G_{P}=1-1.5, \tau_{\text {LPF }}=2-5 \mathrm{~ms}$


RWM coil 1 current per turn


## $\mathrm{n}=3$ EFC + n=1 feedback important at lower current (<900kA) for extending pulse lengths

-Pulses commonly disrupt near $\sim 0.6$ s w/o mode control

- 128925: Gain of $2, \tau_{\text {LPF }}=5 \mathrm{msec}$
- At high beam power (high $\beta_{N}=5.5 \rightarrow 6$ ), mode control insufficient to avoid disruption (not shown)



## $\mathrm{n}=3$ EFC + n=1 feedback was successfully applied

 to wide range of plasma current $=0.75-1.1 \mathrm{MA}$- Pulses run reliably until nearly all OH flux is consumed


$$
\begin{aligned}
& \mathrm{G}=2, \tau_{\mathrm{LPF}}=50 \mathrm{msec} \\
& \mathrm{G}=2, \tau_{\mathrm{LPP}}=5 \mathrm{msec} \\
& \mathrm{G}=2, \tau_{\mathrm{LPP}}=5 \mathrm{msec} \\
& \mathrm{G}=2, \tau_{\mathrm{LPF}}=1 \mathrm{msec} \\
& \mathrm{G}=2, \tau_{\mathrm{LPF}}=5 \mathrm{msec}
\end{aligned}
$$

## Be Careful...Don't Use Too Much Gain!

Experience From LITER Day 2 Experiments

129070: No EFC, discharge collapses in mid-flattop,

129071: Use settings from XP 823, $\mathrm{G}=2, \tau_{\text {SPA-req }}=.002$, big feedback oscillation.

129072: $G=0.7, \tau_{\text {SPA-req }}=.002$, success!


The parameters of 129072 were "locked-in" as the standard pre-programmed $n=3+n=1$ DEFC.

## Optimized mode control + Lithium $\rightarrow$ record NSTX pulse-lengths

-Flux consumption reduced following LITER experiments

-Lower $\mathrm{V}_{\text {LOOP }}$ at lower $\mathrm{P}_{\mathrm{NBI}}$


$\cdot \mathrm{Li}+$ optimized EFC with
( $\mathrm{G}=1, \tau_{\text {LPF }}=2 \mathrm{msec}$ ) $\rightarrow$

- Avoid late $\mathrm{n}=1$ rotating mode
- rotation sustained
$-\beta_{N} \geq 5$ sustained 3-4 $\tau_{C R}$
- record pulse-length $=1.8 \mathrm{~s}$


Neutral Beam Power


## Begnond is Backup

## RFA suppression algorithm was "Trained" in 2007

- Use Time With Minimal Intrinsic EF.
- Apply $\mathrm{n}=1 \mathrm{EF}$ to reduce rotation, destabilize RWM.
- Find corrective feedback phase that reduces applied EF currents.
- Increase gain until applied EF currents are nearly completely nulled and stability restored.
Turn off applied field, and utilize optimized setting for RFA and RWM feedback.


Final "Optimal" Configuration
Use identification of the mode form $B_{P}$ sensors
Use a feedback phase of ??? ${ }^{\circ}$
Use a feedback gain of 0.7

## Case 1: 750 kA in XP 823 (I).



Consider Radii Denoted By Orange Line


## Case 1: 750 kA in XP 823 (II).




## Parabolic Optimization:150-200 <br> Linear Optimization: 250-350 <br> Parabolic Function Seems Like a Reasonable Choice

## Case 2: 900 kA in XP 701 (I).



Consider Radii Denoted By Orange Line

(11) NSTX

## Case 2: 900 kA in XP 701 (II).



Parabolic Optimization: 200-300
Linear Optimization: ~340
Linear Intersections Seems to Capture the Trend Better

## Case 3: 1100 kA in XP 823 (I).

Consider Time Denoted By Blue Line


Consider Radii Denoted By Orange Lines


## Case 3: 1100 kA in XP 823 (II)



