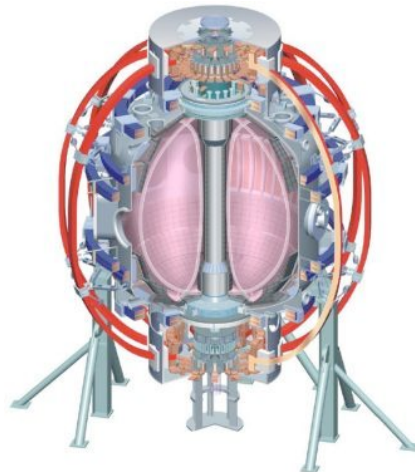


# Relay Feedback and X-point Height Control

College W&M  
Colorado Sch Mines  
Columbia U  
CompX  
General Atomics  
INL  
Johns Hopkins U  
LANL  
LLNL  
Lodestar  
MIT  
Nova Photonics  
New York U  
Old Dominion U  
ORNL  
PPPL  
PSI  
Princeton U  
Purdue U  
SNL  
Think Tank, Inc.  
UC Davis  
UC Irvine  
UCLA  
UCSD  
U Colorado  
U Illinois  
U Maryland  
U Rochester  
U Washington  
U Wisconsin

**Egemen Kolemen**  
*S. Gerhardt and D. A. Gates*

**2010 Results Review**  
**Nov/30/2010**



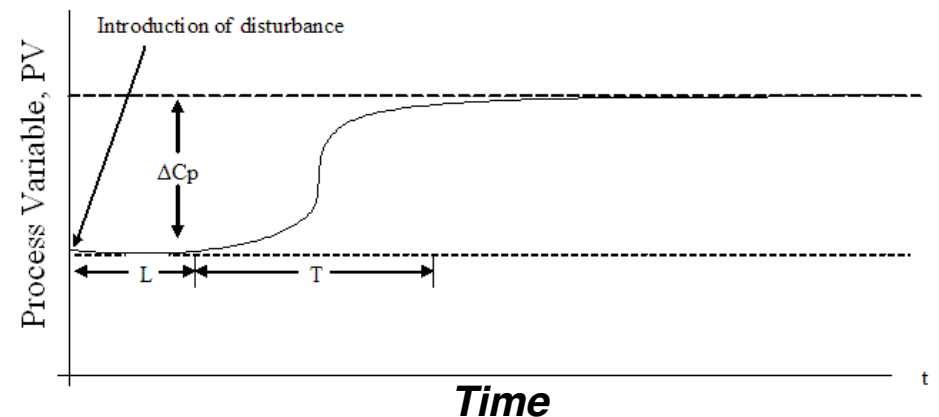
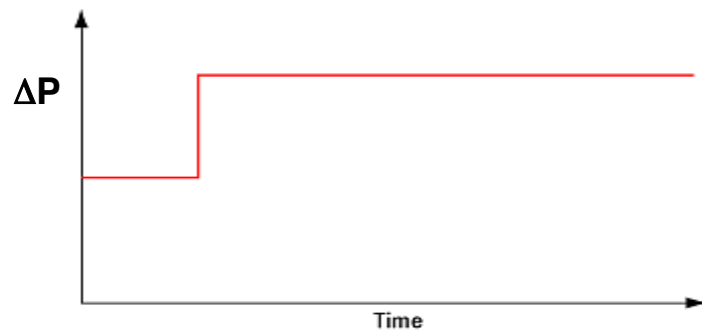
Culham Sci Ctr  
U St. Andrews  
York U  
Chubu U  
Fukui U  
Hiroshima U  
Hyogo U  
Kyoto U  
Kyushu U  
Kyushu Tokai U  
NIFS  
Niigata U  
U Tokyo  
JAEA  
Hebrew U  
Ioffe Inst  
RRC Kurchatov Inst  
TRINITI  
KBSI  
KAIST  
POSTECH  
ASIPP  
ENEA, Frascati  
CEA, Cadarache  
IPP, Jülich  
IPP, Garching  
ASCR, Czech Rep  
U Quebec

## 2009 Run: Experimental System ID (Open Loop)

- System Id: Identify the effect of the actuator on the boundary shape.

$$\dot{y}(t)T + y(t) = Ku(t - L)$$

- Reaction Curve Method



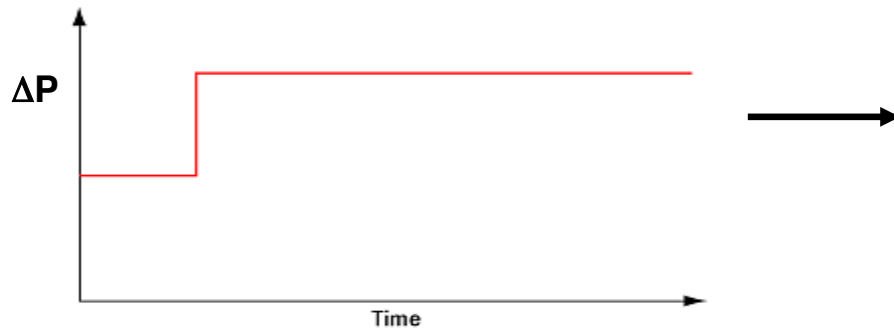
- From Step Response obtain:
  - Time delay, rise time and size of change gives the control tuning parameters.

## 2009 Run: Experimental System ID (Open Loop)

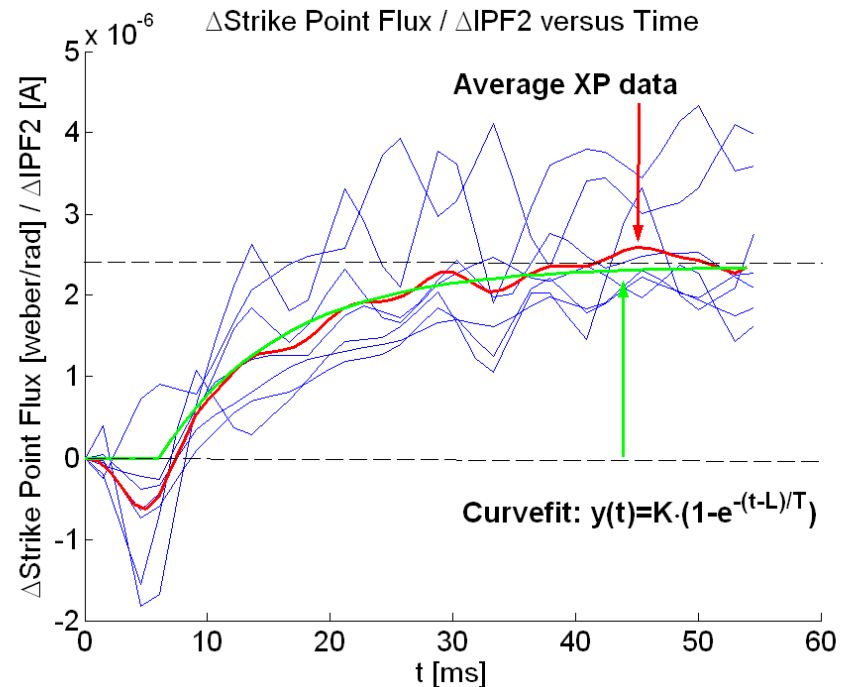
- System Id: Identify the effect of the actuator on the boundary shape.

$$\dot{y}(t)T + y(t) = Ku(t - L)$$

- Reaction Curve Method

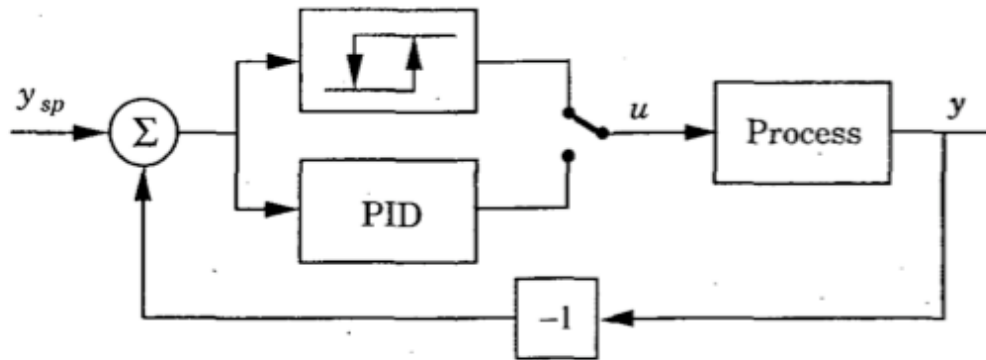


- Problem:
  - Many shots needed
  - Need the actuator in open loop.
  - Not precise

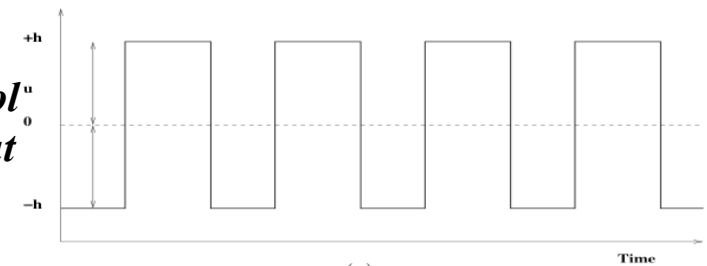


**System Id results from 2009 run**

# Experimental System ID: Closed Loop Auto-tune with Relay Feedback

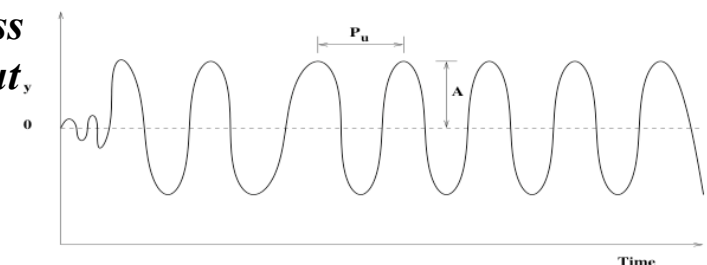


*Control  
Output*



(a)

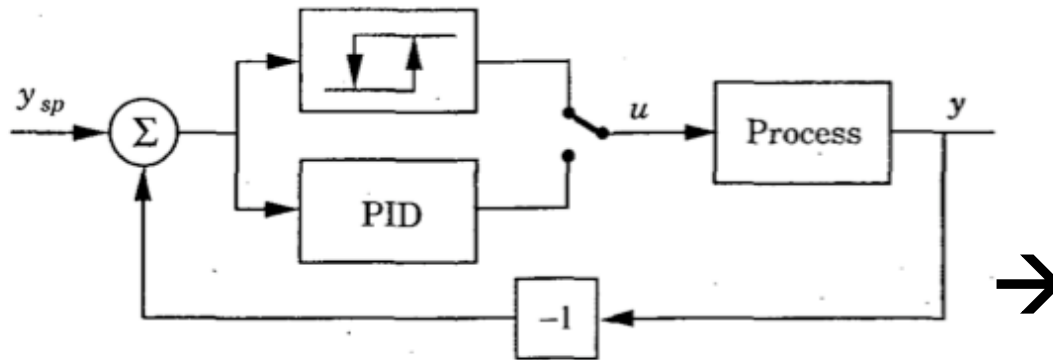
*Process  
Output*



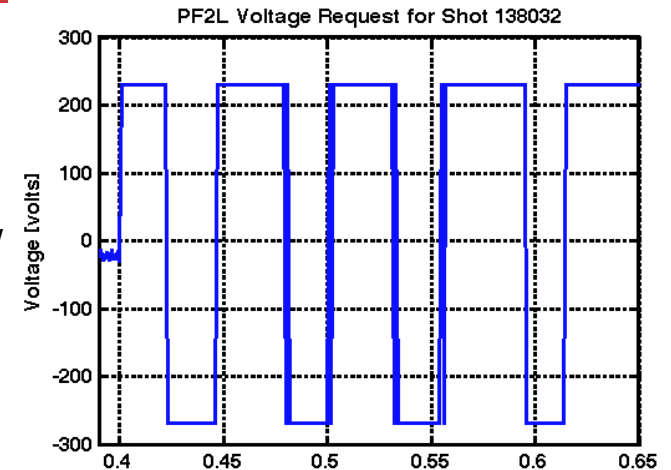
(b)

- The closed-loop plant response period ( $P_u$ ) & amplitude ( $A$ ) are used for PID controller tuning.
- Advantages:
  - Only a single experiment is needed.
  - Closed loop:
    1. More stable
    2. Enable system ID for actuators that can't be open loop (for example: vertical control)

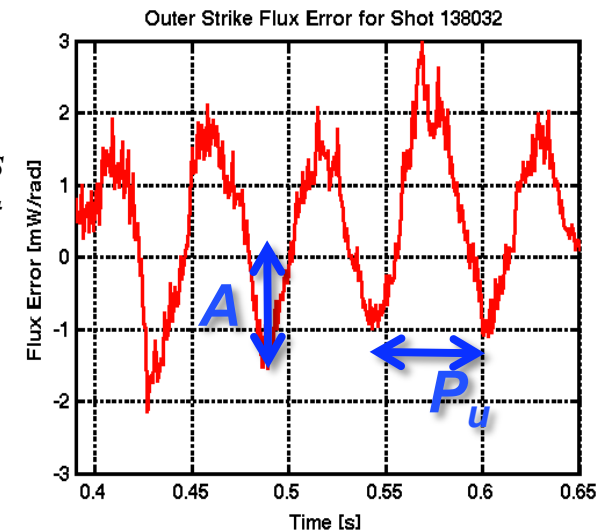
# Experimental System ID: Closed Loop Auto-tune with Relay Feedback



*Control  
Output*

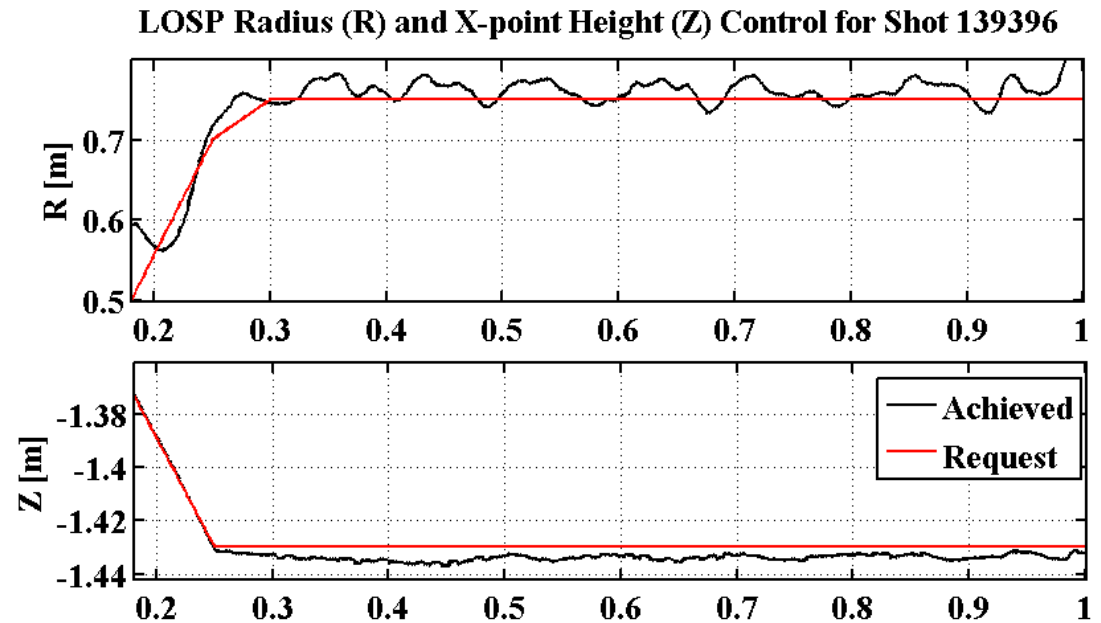
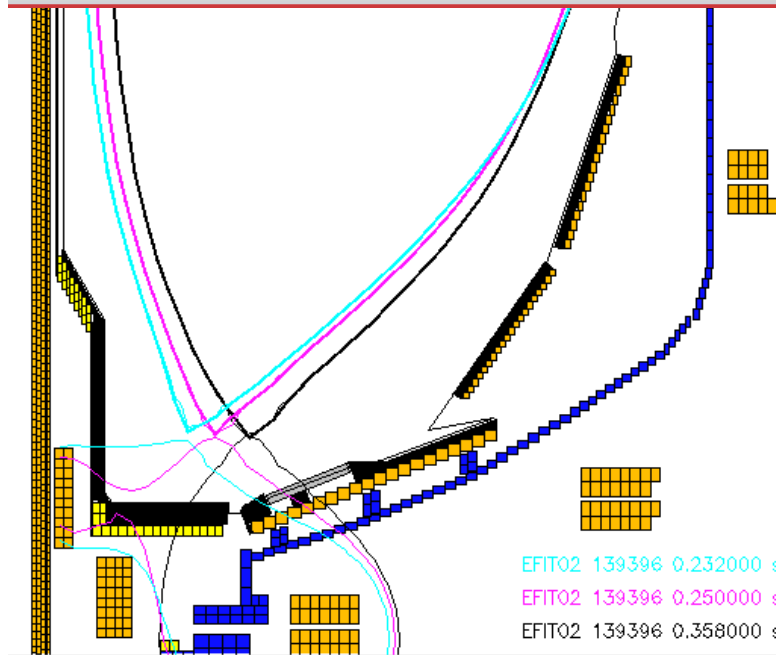


*Process  
Output*



- The closed-loop plant response period ( $P_u$ ) & amplitude ( $A$ ) are used for PID controller tuning.
- Advantages:
  - Only a single experiment is needed.
  - Closed loop:
    1. More stable
    2. Enable system ID for actuators that can't be open loop (for example: vertical control)

# Successful Developed Combined X-point Height / SP Control



Evolution of Plasma Boundary: X-point height roughly constant as OSP ramps

- Tuned via Relay-Feedback.
- Achieved RMS <1 cm X-point height error and <2 cm SP.
- Scenario used for LLD experiments.

## For 2011: Solution to “Hand-off” Problem

- Problem when changing between control phases.
- Normal Control has two parts:
  1. Trajectory control: Scenario Development (Feed forward)
  2. Feedback control: Controlling parameters close to the defined scenario.
- Need: Ability to add these two waveforms.
  - Simply be able to add PID output to the Voltage from the last phase. (We have this capability only for Relay Feedback but not for regular PID).
- Then, we will avoid “hand-off” problem



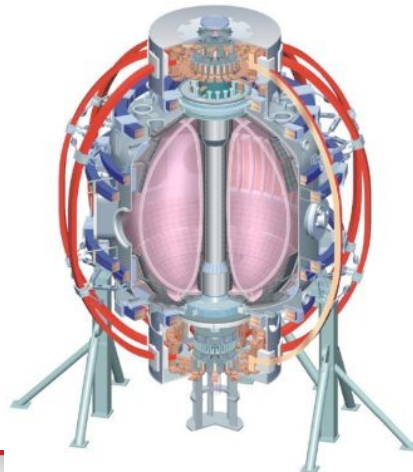
# Squareness XP

College W&M  
 Colorado Sch Mines  
 Columbia U  
 CompX  
 General Atomics  
 INL  
 Johns Hopkins U  
 LANL  
 LLNL  
 Lodestar  
 MIT  
 Nova Photonics  
 New York U  
 Old Dominion U  
 ORNL  
 PPPL  
 PSI  
 Princeton U  
 Purdue U  
 SNL  
 Think Tank, Inc.  
 UC Davis  
 UC Irvine  
 UCLA  
 UCSD  
 U Colorado  
 U Illinois  
 U Maryland  
 U Rochester  
 U Washington  
 U Wisconsin

**Egemen Kolemen**

*S. Gerhardt and D. A. Gates*

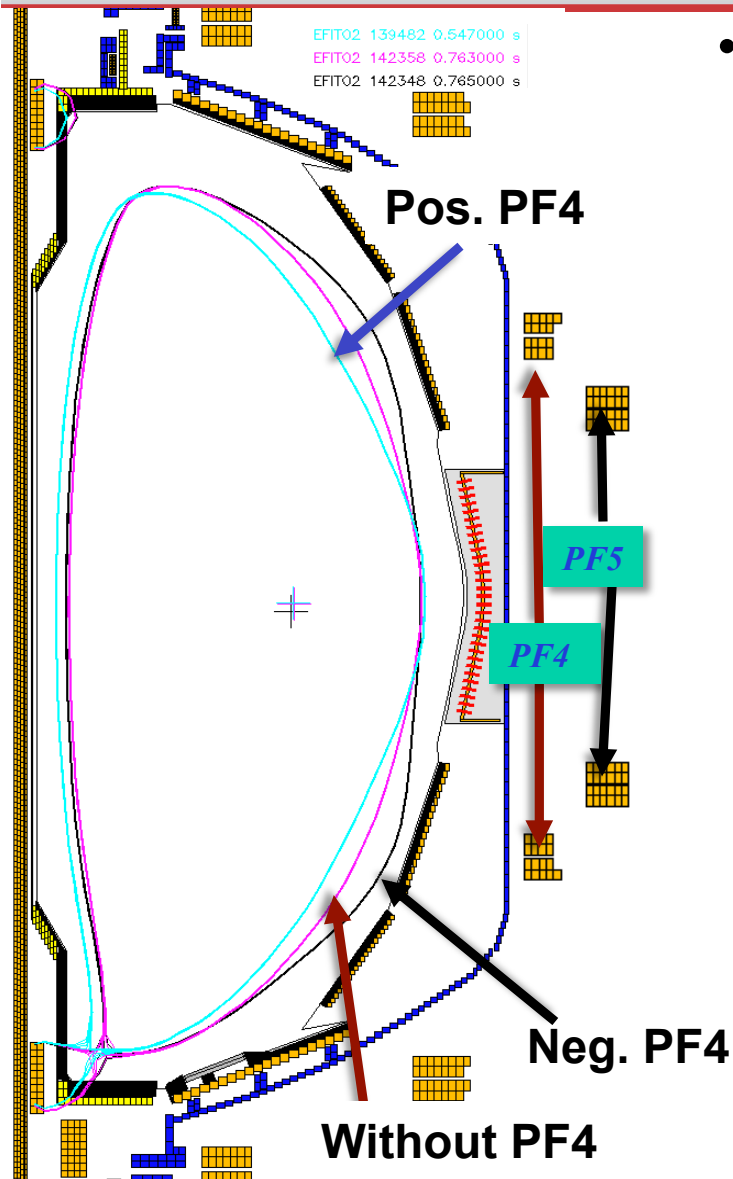
**2010 Results Review  
Nov/30/2010**



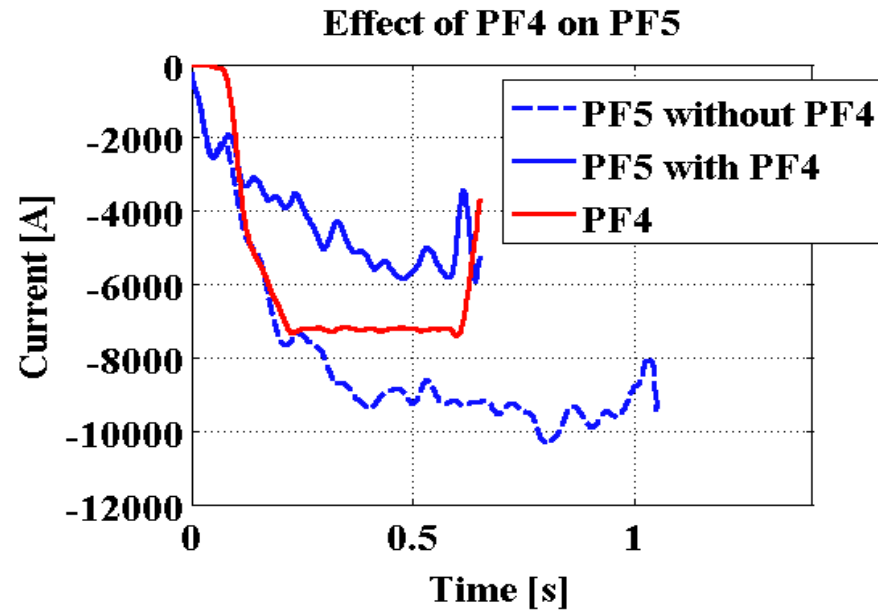
Culham Sci Ctr  
 U St. Andrews  
 York U  
 Chubu U  
 Fukui U  
 Hiroshima U  
 Hyogo U  
 Kyoto U  
 Kyushu U  
 Kyushu Tokai U  
 NIFS  
 Niigata U  
 U Tokyo  
 JAEA  
 Hebrew U  
 Ioffe Inst  
 RRC Kurchatov Inst  
 TRINITI  
 KBSI  
 KAIST  
 POSTECH  
 ASIPP  
 ENEA, Frascati  
 CEA, Cadarache  
 IPP, Jülich  
 IPP, Garching  
 ASCR, Czech Rep  
 U Quebec



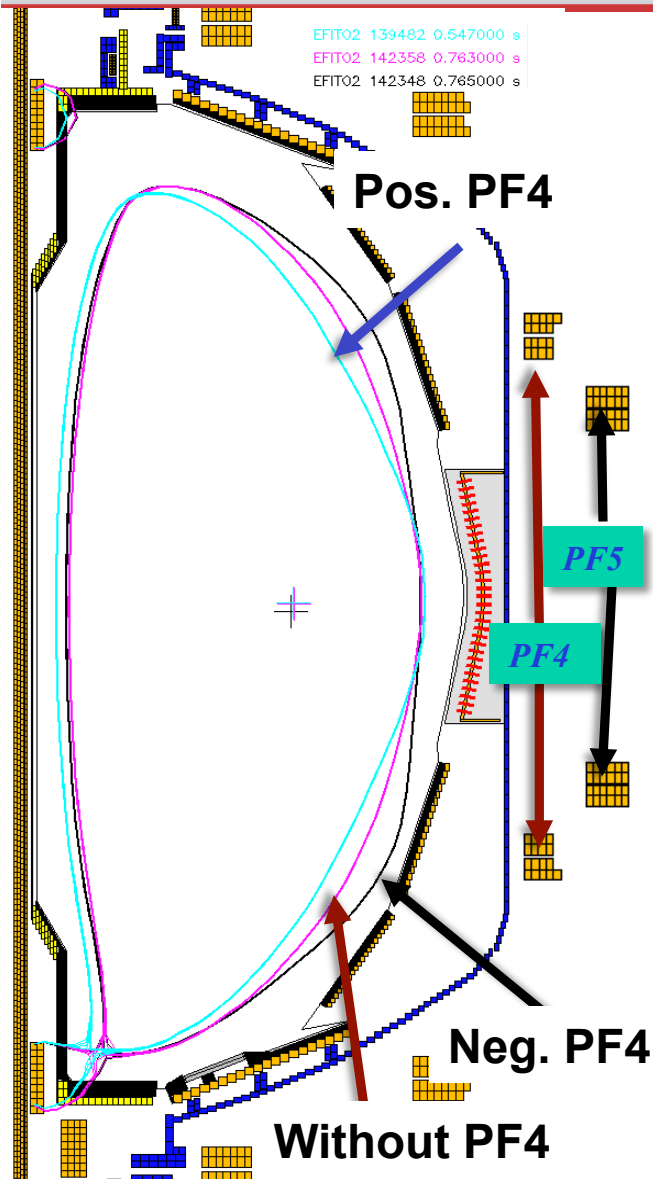
# First Ever Use of PF4 for Shape Optimization



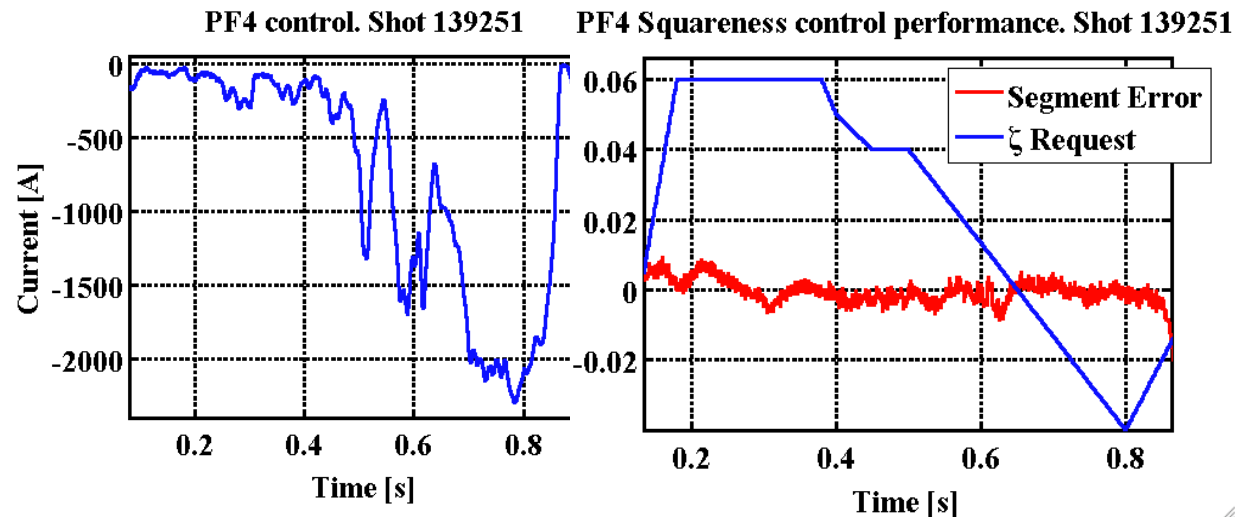
- Motivation 1: Increased current capability of NSTX Upgrade may require vertical field from the PF4 in addition to PF5.
- Preprogram PF4 with PF5 for outer gap control



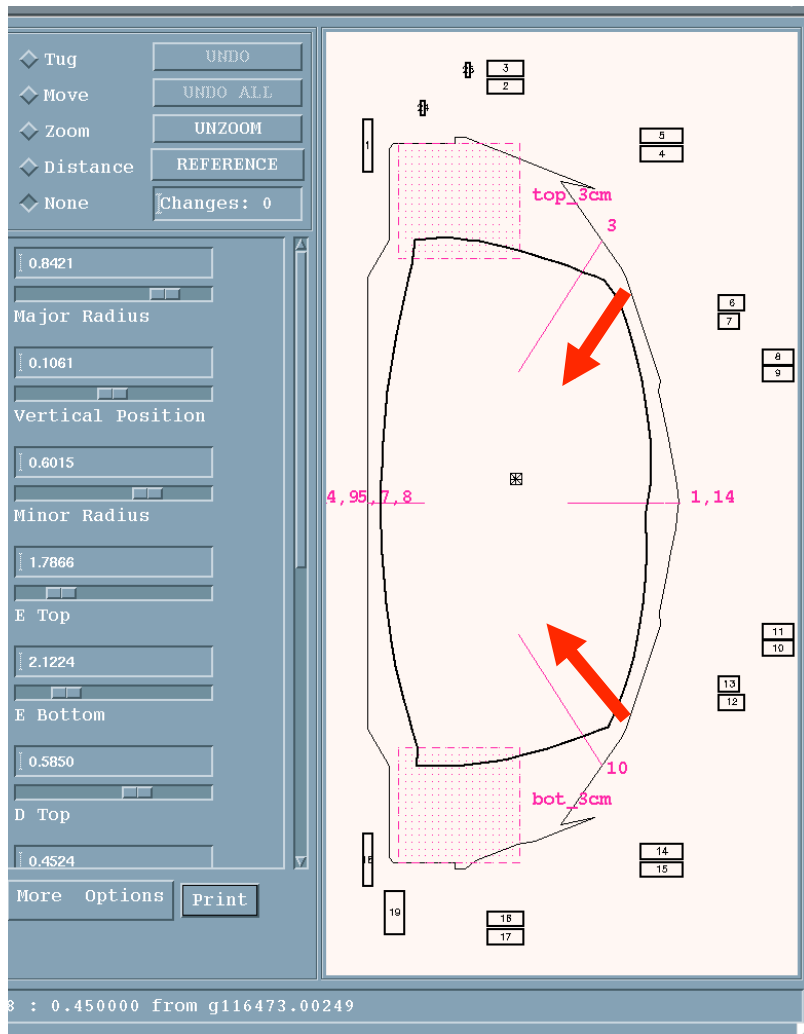
# Squareness, $\zeta$ , Control with PF4



- Motivation: Assess the physics impact of squareness variation while other shape parameters are fixed.
- PF4 best  $\zeta$  control candidate. PF3/PF4 effect  $\zeta$  but PF3 used for vertical stability.
- Achieved stable  $\zeta$  tracking via PF4.
- Effect of  $\zeta$  on plasma is being studied.

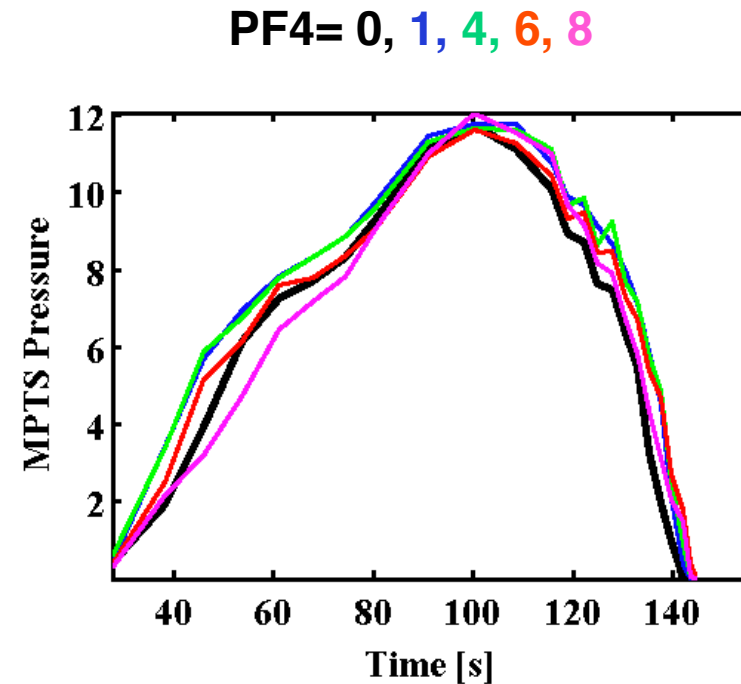
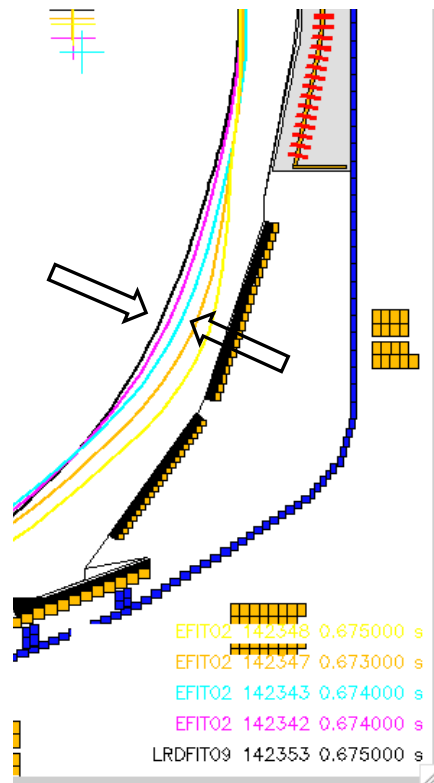


## XMP Control Results: PF3-PF4 interaction



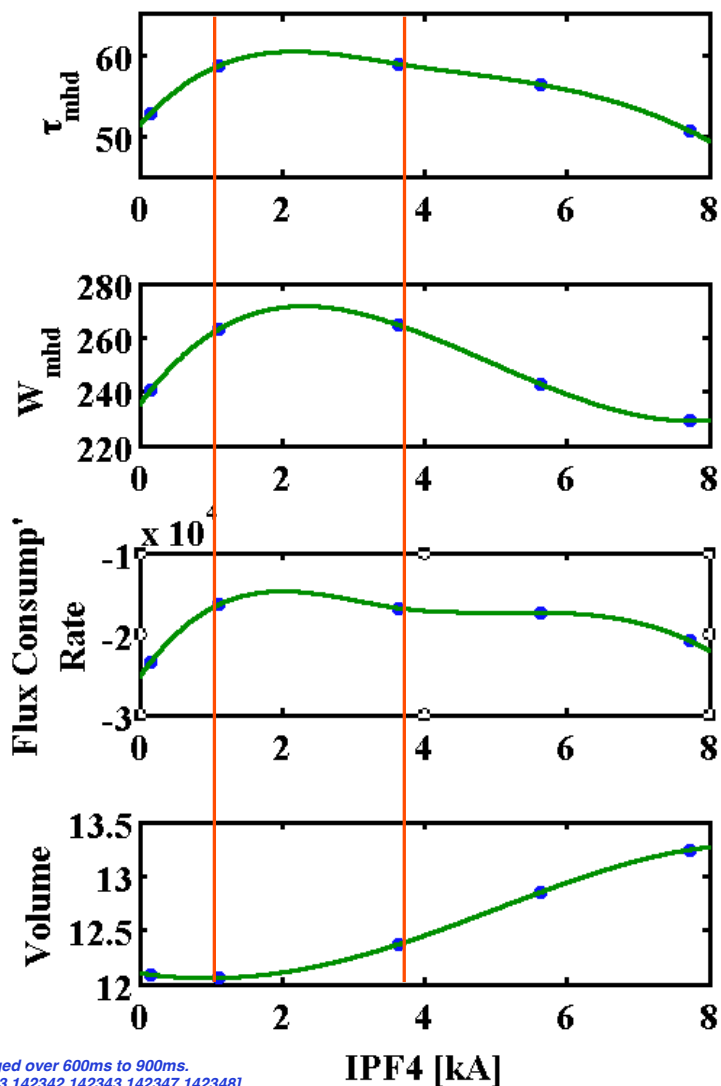
- To solve this problem, move the PF3 and PF4 control segment.
- Could not do this:
  - Problem with PCS Segment Editor.
  - Hopefully will be fixed for 2011.
- To overcome the problem without changing the segments:
- Hand adjust a non-realistic looking shape request.
- Squareness Request of +0.4 from the normal request.
- Works but don't use the squareness in these shots.

## Pressure Profile Change as PF4 Increases



- PF4 (opposing PF5) up to 5 kA (~2 inches in figure) increases pressure
- Too high PF4 interacts with the wall and plasma is not as good.

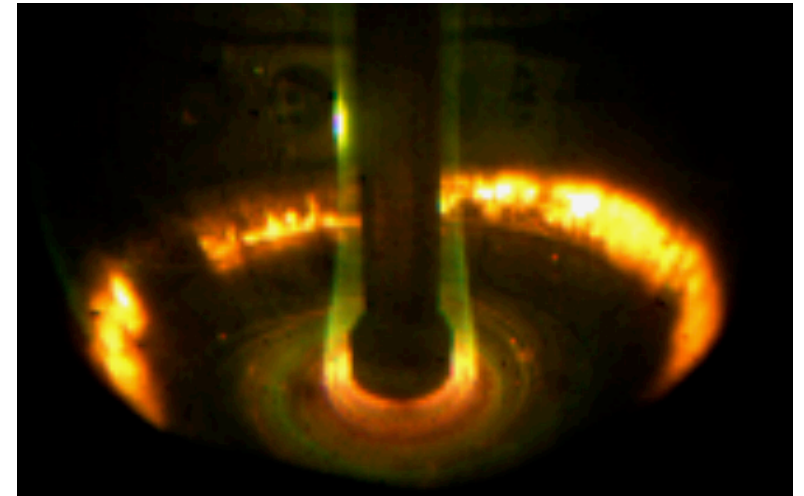
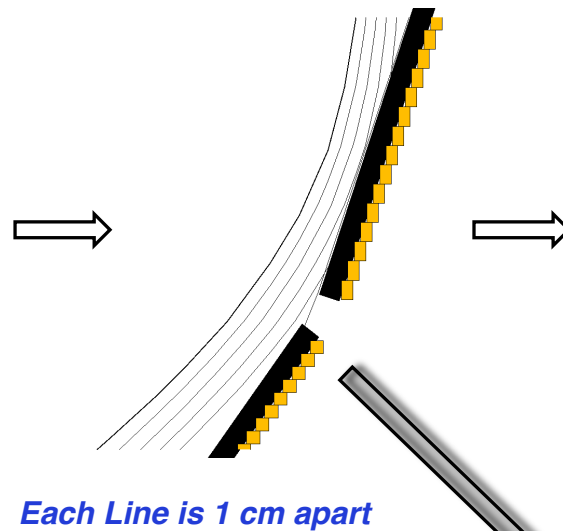
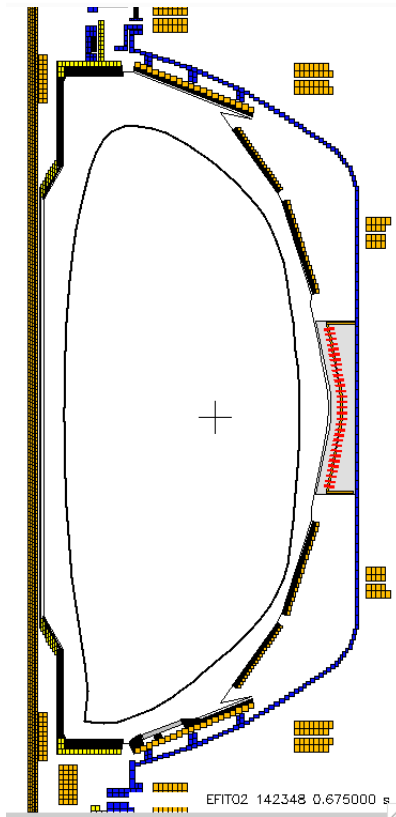
## Higher Performance: PF4 of 1-4 kA



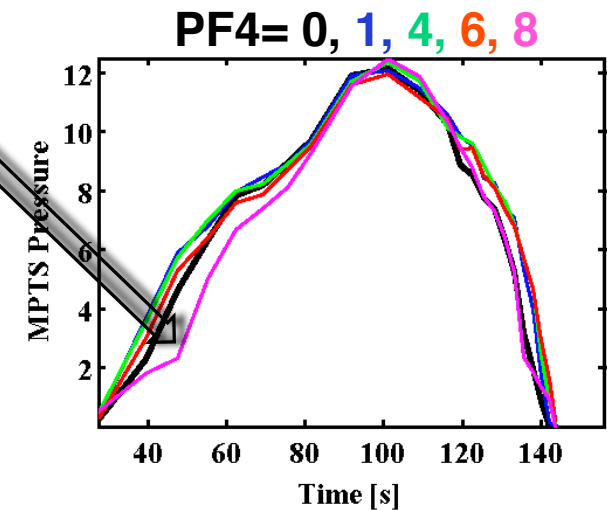
- Optimal PF4  $\sim$ 1-4 kA for performance.
- Confinement time increases
- Energy confinement increases
- Flux consumption reduces.
- Too high PF4 interacts with the wall and plasma is not as good.
- **Note for comparison:**
- Negative squareness results were **all** worse than PF4=0 fiducial case.

Averaged over 600ms to 900ms.  
[142353,142342,142343,142347,142348]

## PF4 at 8 kA, High Squareness



- As PF4 gets close to 8 kA:
- Last closed flux surface gets 3-4 cm close to the wall.
- Pressure profile degrades

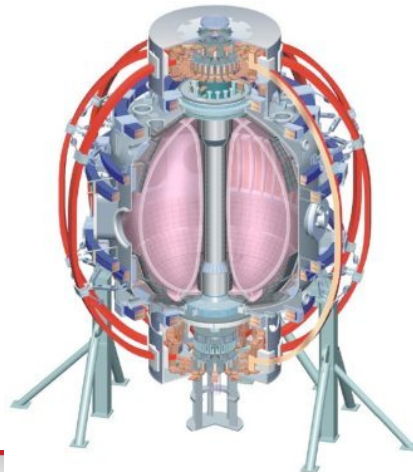


# Vertical Stability for NSTX and NSTX-U

**Egemen Kolemen**  
*D. A. Gates, S. Gerhardt*

**Monday Physics Meeting**  
**PPPL, NJ**  
**Nov/15/2010**

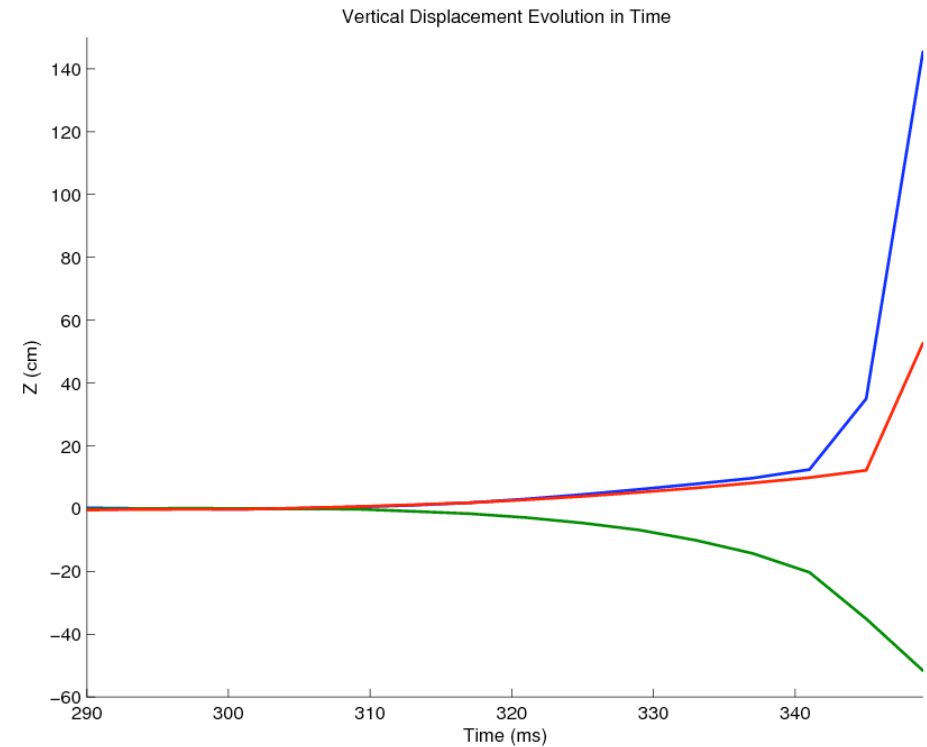
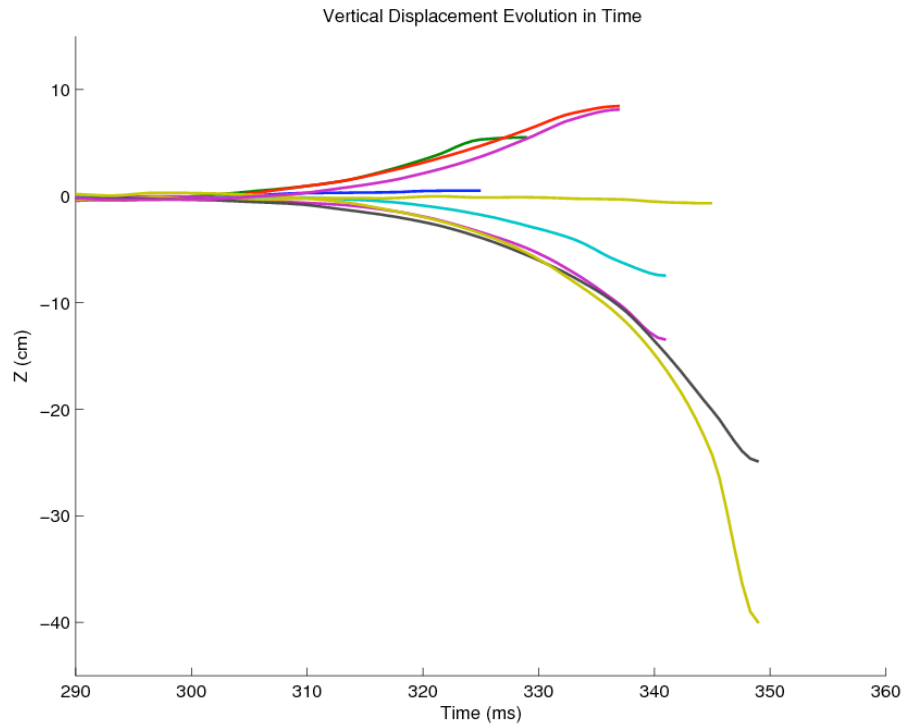
College W&M  
Colorado Sch Mines  
Columbia U  
CompX  
General Atomics  
INL  
Johns Hopkins U  
LANL  
LLNL  
Lodestar  
MIT  
Nova Photonics  
New York U  
Old Dominion U  
ORNL  
PPPL  
PSI  
Princeton U  
Purdue U  
SNL  
Think Tank, Inc.  
UC Davis  
UC Irvine  
UCLA  
UCSD  
U Colorado  
U Illinois  
U Maryland  
U Rochester  
U Washington  
U Wisconsin



Culham Sci Ctr  
U St. Andrews  
York U  
Chubu U  
Fukui U  
Hiroshima U  
Hyogo U  
Kyoto U  
Kyushu U  
Kyushu Tokai U  
NIFS  
Niigata U  
U Tokyo  
JAEA  
Hebrew U  
Ioffe Inst  
RRC Kurchatov Inst  
TRINITI  
KBSI  
KAIST  
POSTECH  
ASIPP  
ENEA, Frascati  
CEA, Cadarache  
IPP, Jülich  
IPP, Garching  
ASCR, Czech Rep  
U Quebec



# 2008 Run: Vertical Displacement Measurements

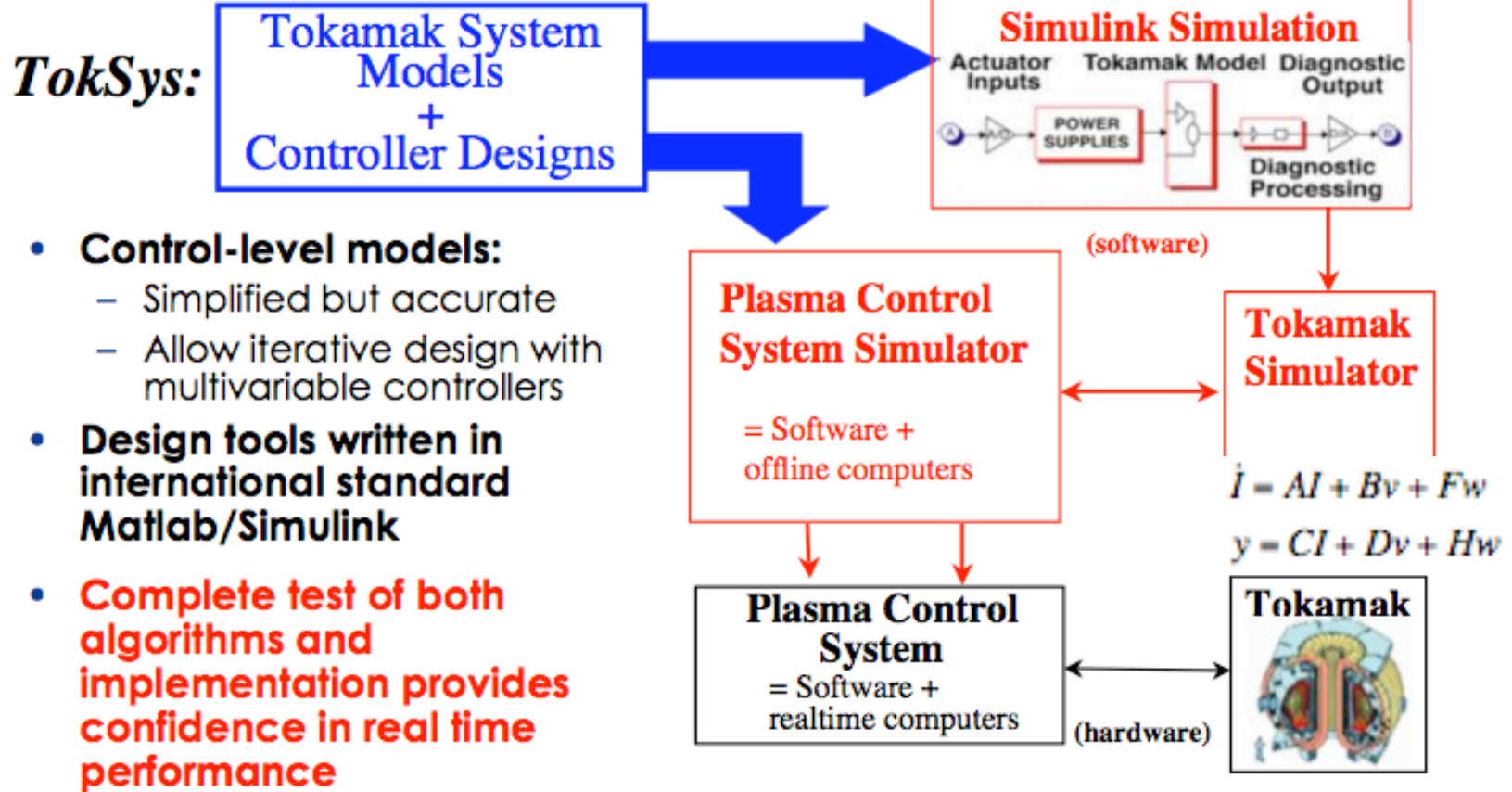


*Vertical displacement for controllable shots  
(Cut off at the point of return)*

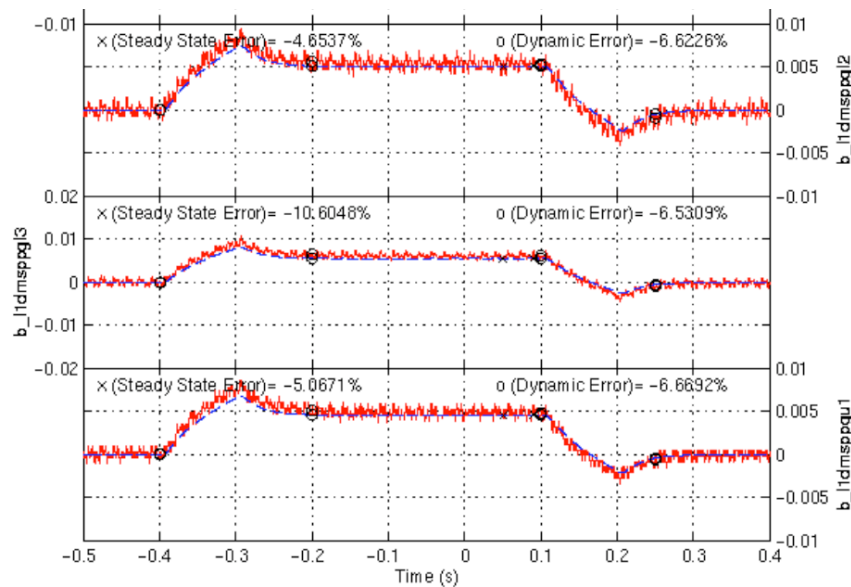
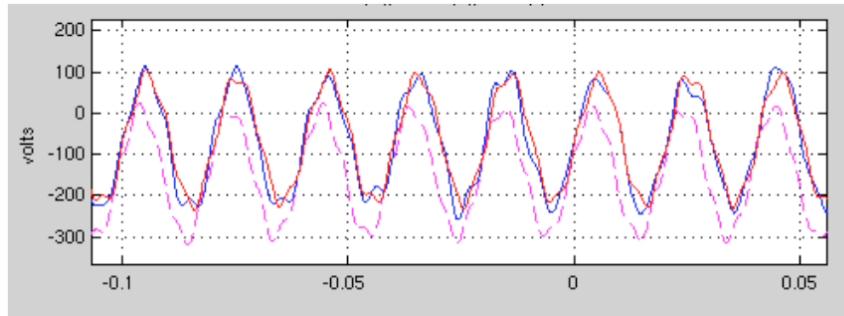
*Vertical displacement for uncontrollable shots*

- At 300 ms, we turned the controller off and let the plasma drift.
- When we turned the control back on some of the shots recovered while others hit the wall.

# TokSys is an Integrated Plasma Control Environment That Allows Systematic Design and Testing of Controllers



# How the Model was Obtained?

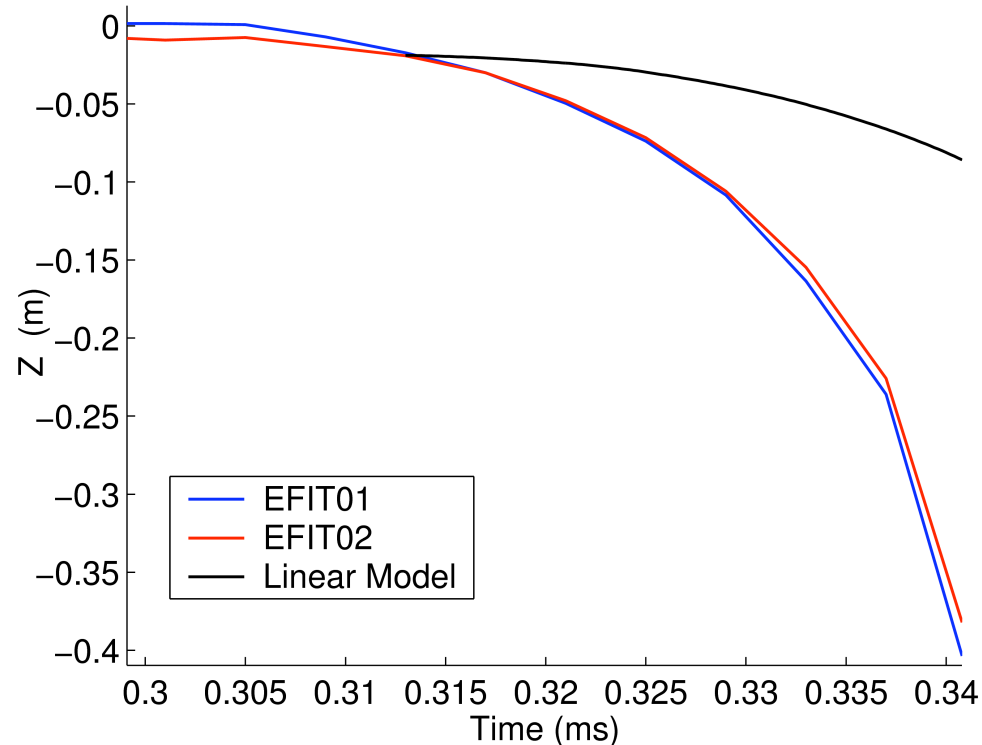


**Comparison of model/experimental B-Probe traces for OH coil. Red trace is experiment, blue trace is model. Steady state and dynamic error values are % differences between model & exp and are defined between X's for steady state and O's for dynamic.**

- It is a linear set of circuit equations.
- All we need is A, B, C matrices.
- Set of System ID experiments on NSTX 2003-4.
- Model obtained to fit the sensor/probe measurements as good as possible.
- Rigid plasma model

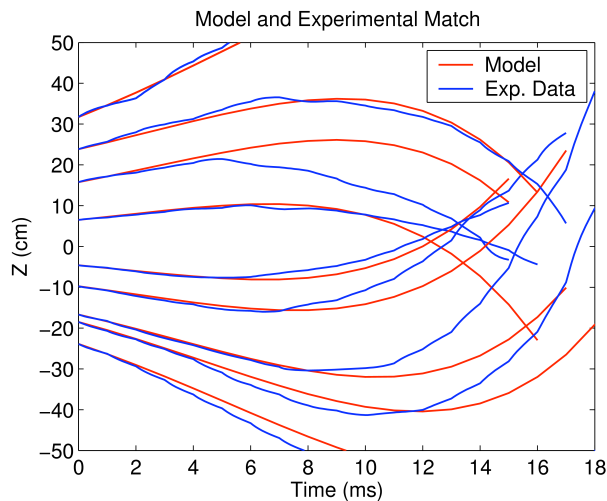
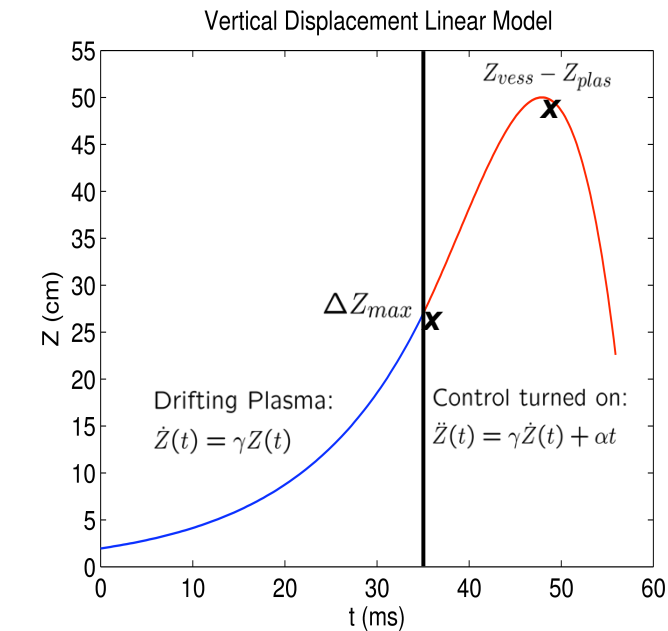
## Mismatch Between XP and Toksys

- XP data 3-4 times more unstable (20-25 Hz versus 54-95 ) than the model.



***Example of a mismatch between TokSys numerical plasma model and the experimental data. Depending on how the model is used plasma or te coil model.***

# All XPs Can Be Modeled with a Linear Equation With the Same Two Parameters



- Where  $\gamma = 75s^{-1}$ . The first order effect of the coils on the vertical motion is assumed to be:

$$\dot{Z}(t) = \gamma Z(t)$$

i.e. the current changes the velocity of the rigidly moving plasma. Also during the ramp up  $I$  is proportional to  $t$ . Combining these two effects, we can find an approximation for the dynamics of the vertical motion after the control is turned on as:

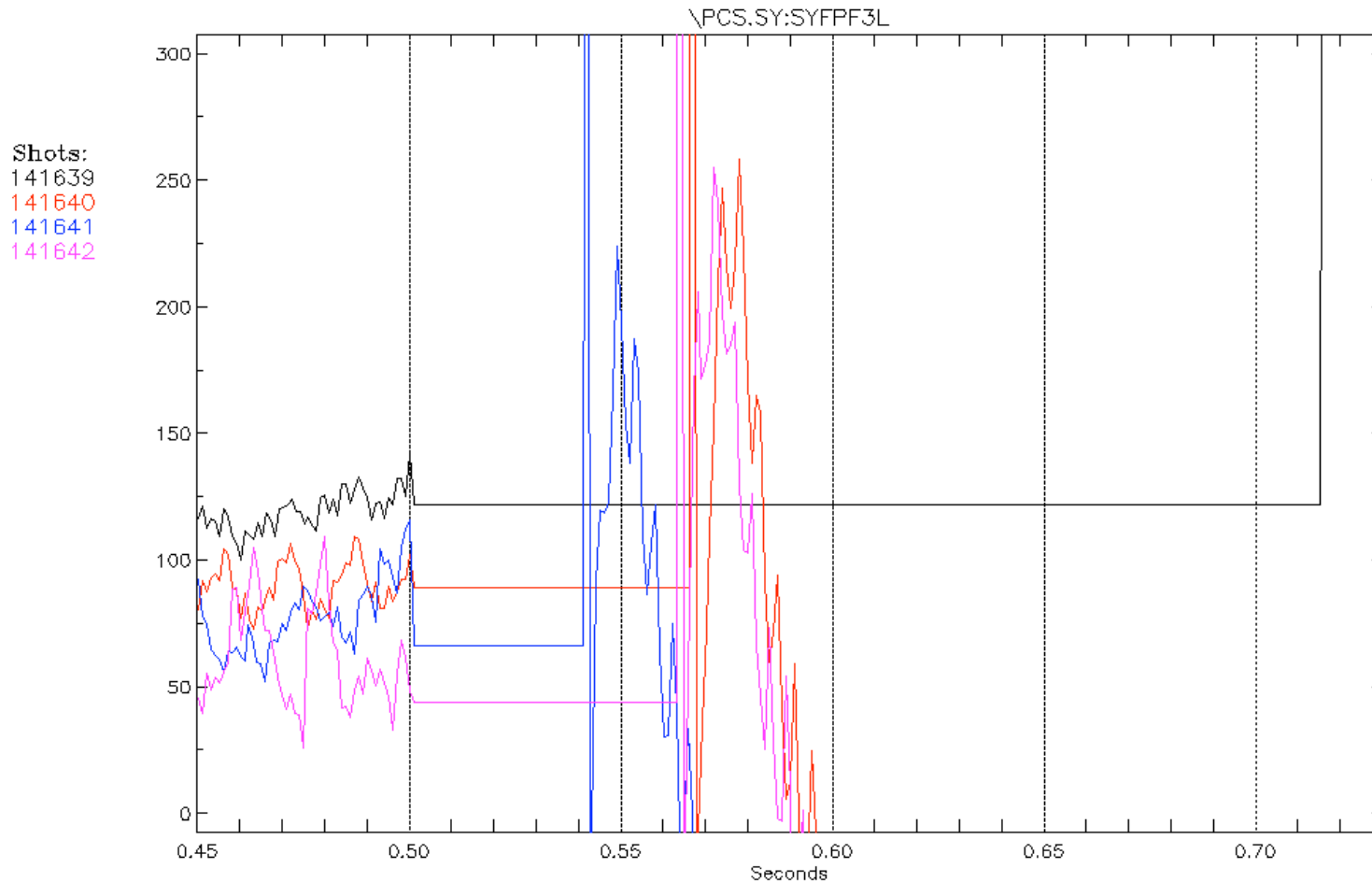
$$\ddot{Z}(t) = \gamma \dot{Z}(t) + \alpha t$$

$\alpha$  is found by data fitting as  $4.5e5$

## How Can it be Improved?

1. Solving perturbed Grad-Shafranov Equation  
This option was discussed. Probably can increase accuracy
2. 3D field effects. Better model the axisymmetric model that corresponds to the 3D pieces that make the plasma wall
3. Run updated new shots to improve the System ID.

# 2010 Experiment: High Aspect Ratio Vertical Growth Rate

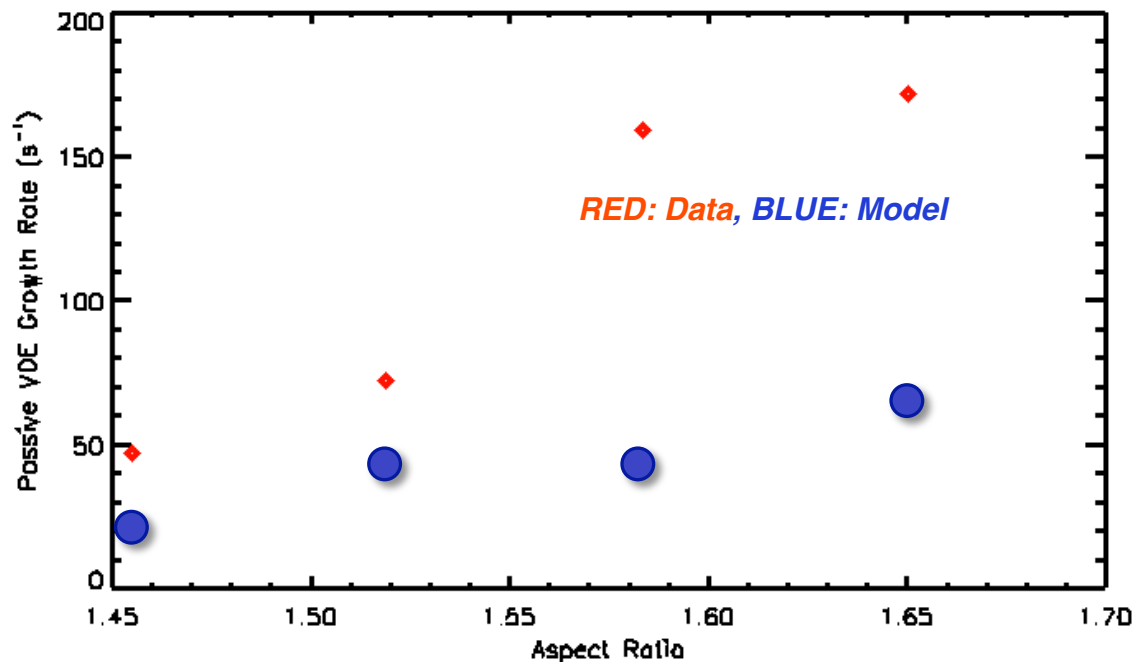


- Thanks to Relay Feedback, we were able to freeze voltage request in Isoflux for the first time.
- This enabled vertical growth rate measurements



## New Experimental Growth Rate (Gamma) 45-170 s<sup>-1</sup> versus 10-42 s<sup>-1</sup> for Model

- High Aspect Ratio More Unstable
- Need better vertical control for Upgrade



- Trying to fix the TokSys model
- Also, trying to update the Power Supply model (with R. Hatcher)
- Probably need better models (3D?).

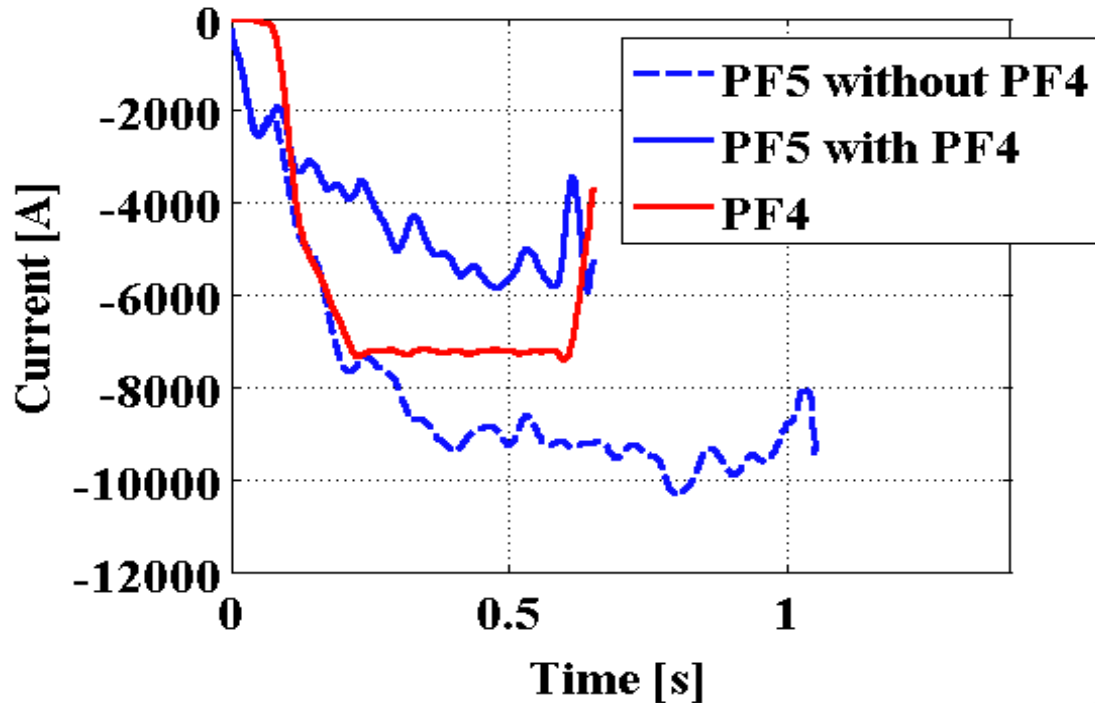
**END**

## What are the Alternatives?

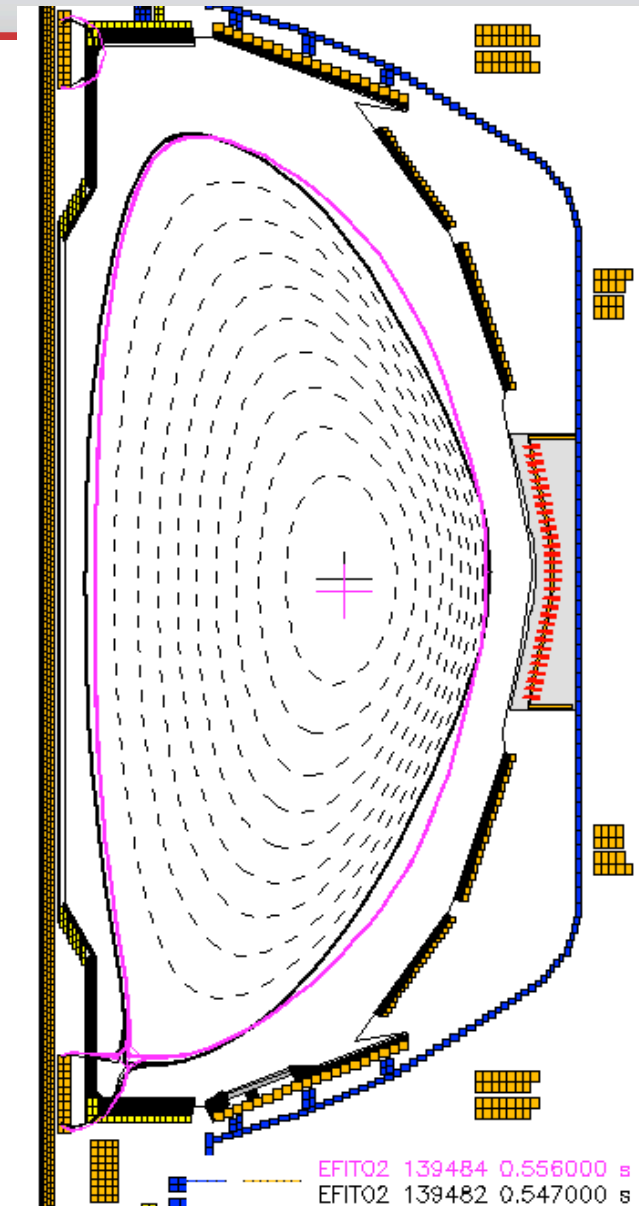
1. Solving perturbed Grad-Shafranov Equation  
This option was discussed. Probably can increase accuracy
2. 3D field effects. Better model the axisymmetric model that corresponds to the 3D pieces that make the plasma wall
3. Run updated new shots to improve the System ID.

# First Ever Use of PF4 for Shape Optimization

Effect of PF4 on PF5

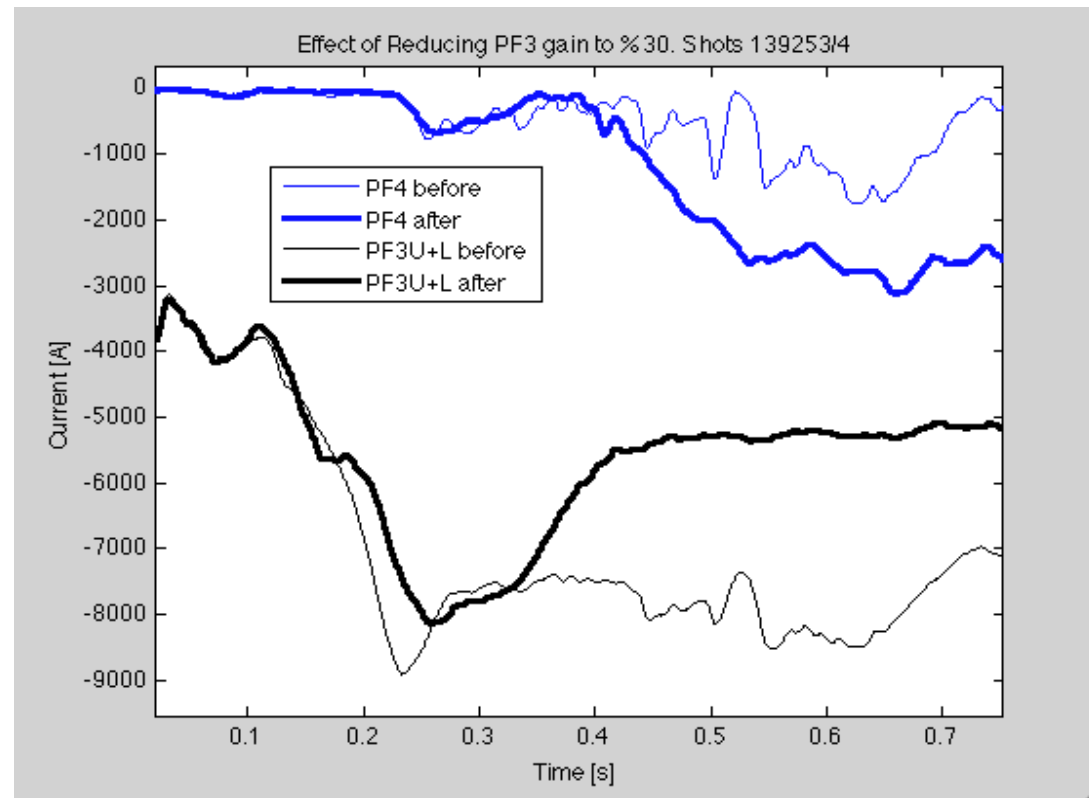


- Ramp PF4 to 7 kA
  - PF1A decreased to give the same kappa.
- PF5 decreases as PF4 increases.
- Squareness decreases.
- Keep other things the same.

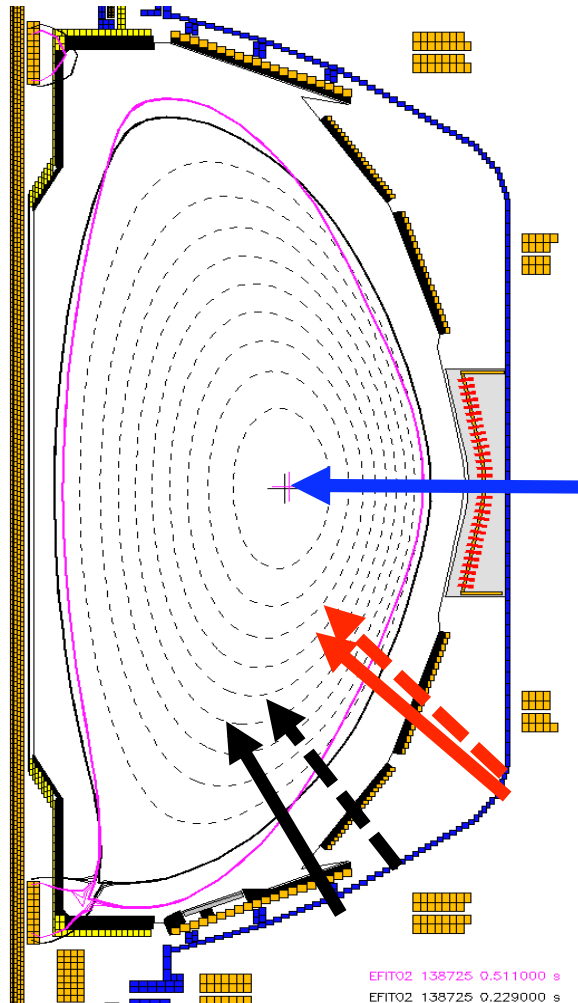


## XMP Control Results: PF3-PF4 interaction

- With PF4 control on, we reduced the gain for PF3 %30 at 360 ms.
- PF4 compensated for the loss of inward pushing effect of PF3.
  - PF4 can offset both PF3 and PF5.

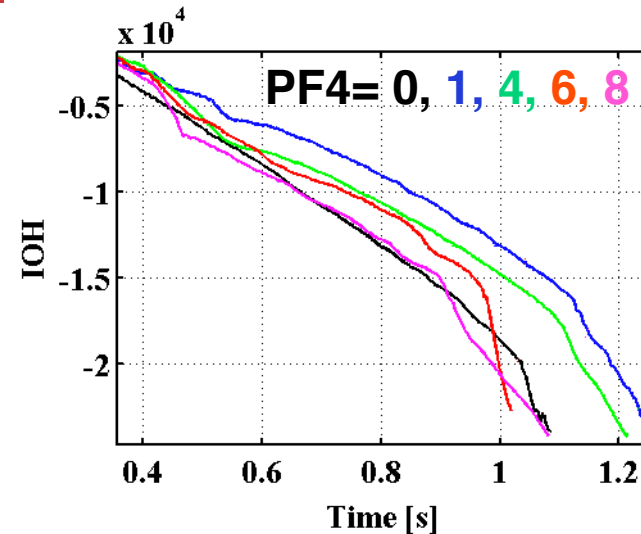
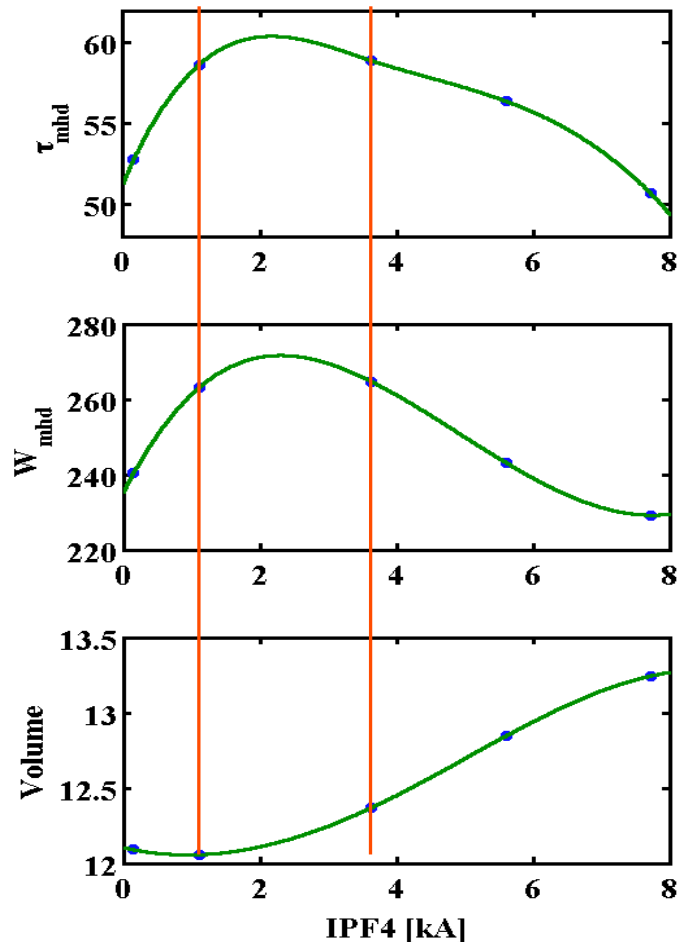


## XMP Control Results: PF3-PF4 interaction



- Figure show the result of a ramp on PF4 from 0 to 2.6 kA.
- As PF4 increases, squareness change.
- In order to align, PF3/4/5 control points (shown in dashed black, dashed red and blue) X-point moves down.
- To solve this problem, move the PF3 and PF4 control segment. Shown in solid red, black.
- Could not do this:
  - Problem with PCS Segment Editor.
  - Hopefully will be fixed for 2011.

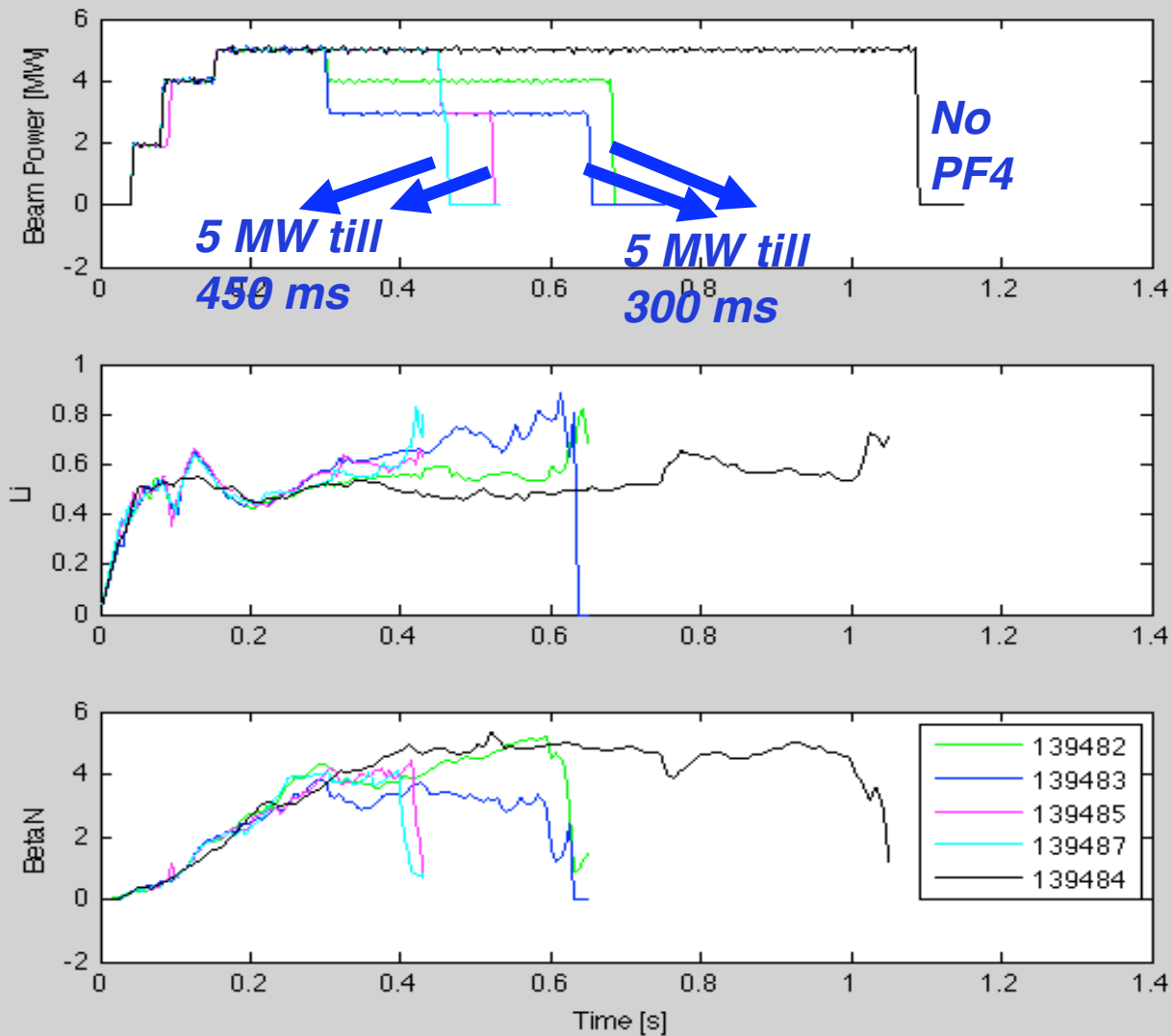
## Higher Performance: PF4 of 1-4 kA



- Optimal PF4  $\sim$ 1-4 kA for performance.
- Confinement time increases
- Energy confinement increases
- Flux consumption reduces.
- Too high PF4 interacts with the wall and plasma is not as good.



# Lower BetaN Limit for PF4 in the positive direction



## Toksys Results Growth Rate (Gamma) 20-25 s<sup>-1</sup>

<u>Shot #</u>	<u>Gamma s<sup>-1</sup></u>
127077	23
127078	25
127079	24
127080	22
127081	24
127082	22
127083	20
127084	20
127085	21
127086	23
127087	21

# Experimental LRDFIT Growth Rate (Gamma) 54-95 s<sup>-1</sup>

Egemen #	Shot	ms	Control Turned Off			Control Turned On			Peak Plasma Displacement			Gamma s <sup>-1</sup>	Voltage ave Pf3U&2L	
			t_0	z_0	li_0	t_turn	z_turn	li_turn	t_f	z_f	li_f			
VDE +Z	1	127074	20	0.301	-0.0018	1.3436	0.32	0.0046	1.3865	0.325	0.005	1.393	no vde at all	600
	2	127075	20	0.301	0.0005	1.3774	0.32	0.0344	1.4927	0.329	0.0552	1.61		
<b>max controlled</b>	<b>3</b>	<b>127076</b>	<b>30</b>	<b>0.301</b>	<b>-0.0025</b>	<b>1.4768</b>	<b>0.33</b>	<b>0.0663</b>	<b>2.1936</b>	<b>0.337</b>	<b>0.0845</b>	<b>3.500</b>	<b>70</b>	<b>1400</b>
	14	127087	30	0.301	-0.003	1.3482	0.33	0.0587	1.6485	0.337	0.0814	2.079	<b>74</b>	1200
un-controlled	10	127083	40	0.301	-0.002	1.378	0.34	0.1176	3.5021	0.341	0.1244	3.742	<b>78</b>	1600
un-controlled	13	127086	40	0.301	-0.0025	1.3885	0.34	0.0943	3.3401	0.349	0.5268	6.372	<b>64</b>	1600
VDE -Z	5	127078	35	0.301	-0.0013	1.3602	0.335	-0.0509	1.1928	0.341	-0.0746	1.158	<b>61</b>	800
	6	127079	35	0.301	-0.0009	1.3592	0.335	-0.0865	1.1954	0.341	-0.1347	1.168	<b>73</b>	1300
	7	127080	40	0.301	-0.0037	1.4283	0.34	-0.005	1.46	0.345	-0.0066	1.440	no vde - control made unstable	1500
	8	127081	40	0.301	-0.0034	1.4129	0.34	-0.1369	1.1969	0.349	-0.2491	1.087		
<b>max controlled</b>	<b>12</b>	<b>127085</b>	<b>40</b>	<b>0.301</b>	<b>0.0027</b>	<b>1.3899</b>	<b>0.34</b>	<b>-0.1504</b>	<b>1.1748</b>	<b>0.349</b>	<b>-0.4006</b>	<b>0.938</b>	<b>54</b>	<b>1600</b>
un-controlled	11	127084	40	0.301	0.0001	1.3759	0.34	-0.1879	1.1783	0.353	-0.6069	0.732	<b>67</b>	1600

straight VDE 4 127077 none

**74**