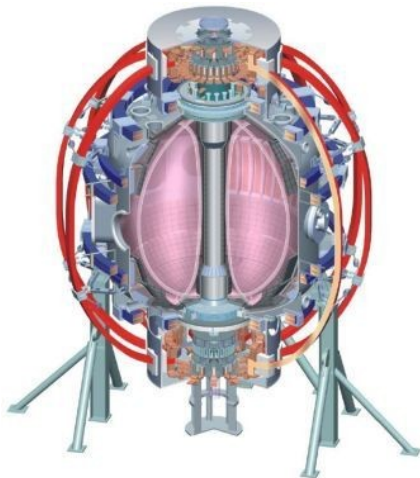


Separatrix Location as Determined by OEDGE Modeling

**M.A. Jaworski, J. Kallman, B. LeBlanc, D. Stotler
(PPPL), S. Sabbagh (Columbia), V. Surla (U-Illinois)**

NSTX 2010 Result Review, Dec. 1, 2010 – B318 PPPL

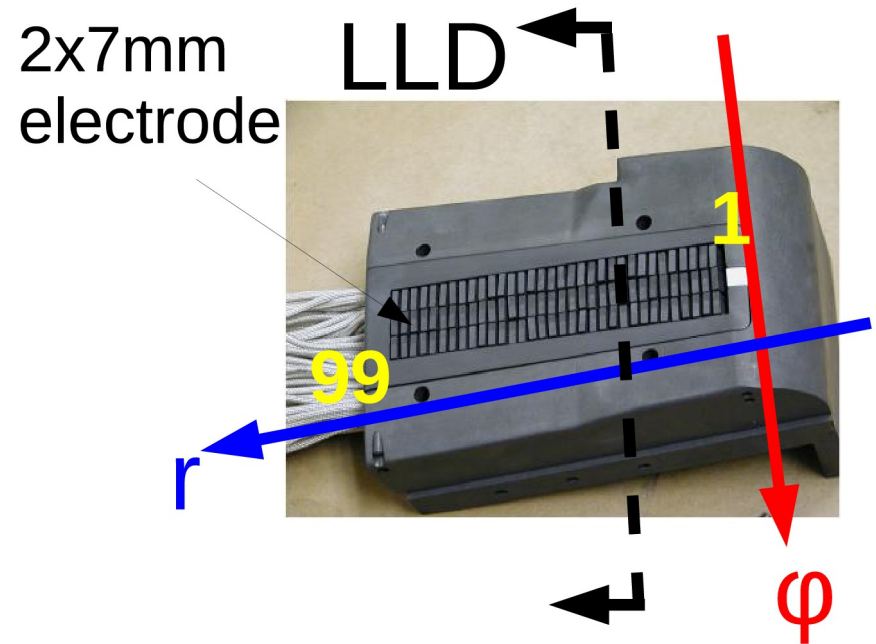


*College W&M
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 ASIPP
 ENEA, Frascati
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 IPP, Garching
 ASCR, Czech Rep
 U Quebec*

New Langmuir Probe Array for this Run

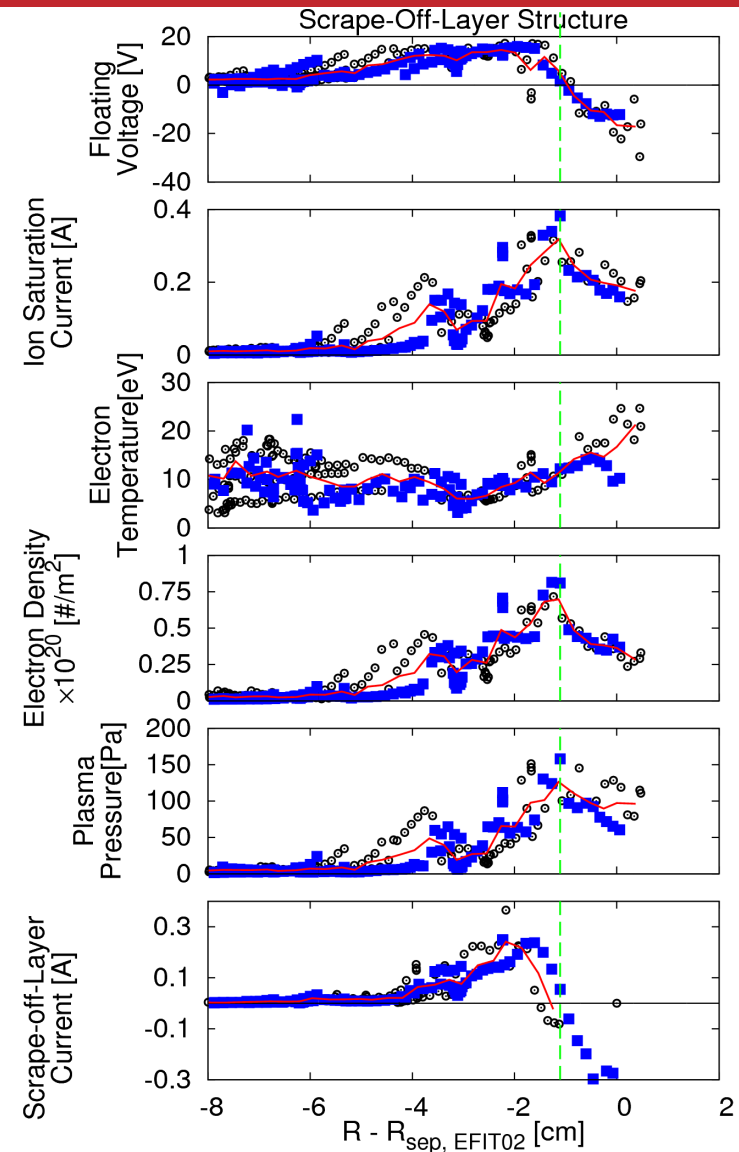
- Dense array of electrodes provides high spatial resolution
- Radially covers the LLD inboard leading edge
- Collaborative effort with U-Illinois (myself, V. Surla)
- Partially filled with standard swept probes, triple Langmuir probes and scrape-off-layer current monitors
- More recent work with the data is in APS posters by J. Kallman and V. Surla



Publications already out on HDLP:
J. Kallman, RSI, 2010
M.A. Jaworski, RSI, 2010

SOL Structure Obtained During Strike Point Sweeps

- Probe positions referenced to magnetic reconstruction
 - **Blue** points = single probe
 - **Black** points = triple probe or SOLC probe
 - **Red** line = Binned average
- Allows SOL structure to be obtained during a strike-point sweep over the array
- Provides additional means of locating the **separatrix**
 - Make use of plasma pressure peak to define separatrix location
 - Zero crossing of V_f and SOLC coincide – need more statistics



Probe Interpretation Sanity Check #1

- Local floating potential and Scrape-Off-Layer Currents intimately tied
 - Floating potential must adjust to be consistent with currents flowing to surface
 - Equivalent to biasing (w.r.t. plasma potential) the PFC to drive a current
- Langmuir probe I-V interpretation compared to independent current measurement
 - I-V characteristic gives plasma N_e , T_e , V_f
 - Dedicated probes measure SOLC in addition to swept
 - Probe data shown consistent over four orders of magnitude
- Scrape-off-layer currents play role in other PMI processes via V_f
 - Sheath heat-transmission coefficient
 - Ion impact energy through sheath

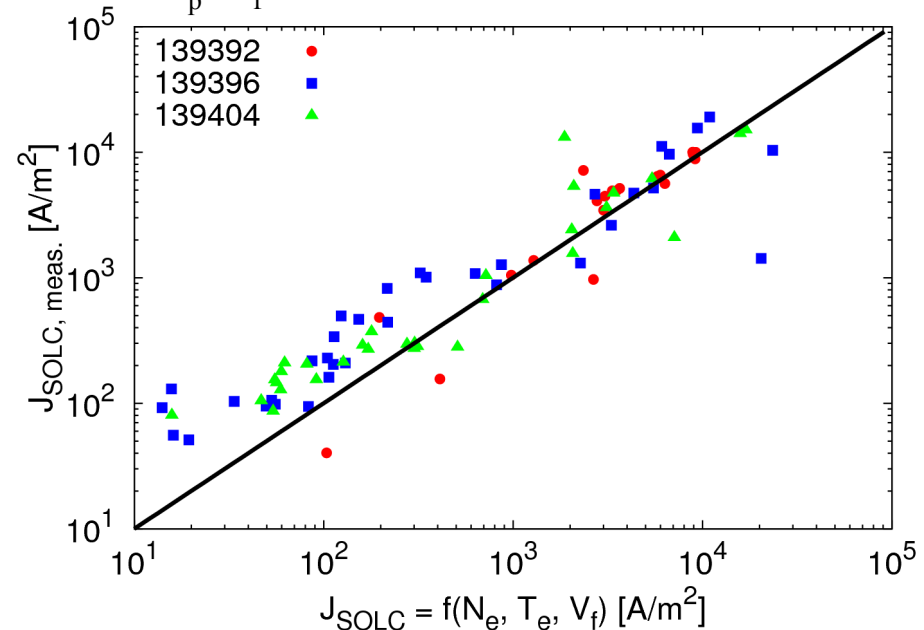
Assumptions:

S.E.E. = 0 (oblique angle of inc.)

Deuterium dominant species

$$T_i/T_e = 1$$

$V_p - V_f$ given by “classical” formula



$$\gamma(V_s) = -\frac{eV_s}{kT_e} + 2.5\frac{T_i}{T_e} + 2 \left[\left(1 + \frac{T_i}{T_e}\right) \left(\frac{2\pi m_e}{m_i}\right) \right]^{-1/2} \exp\left(\frac{eV_s}{kT_e}\right)$$

OEDGE Code Suite for 2D Description of SOL

- **O** – Onion-skin method (OSM)
 - Generalization of the 2-point model – integrates fluid equations along a flux-tube
 - Assumes parallel transport \gg perpendicular transport
 - Integration **from** target less sensitive than solution from midplane
- **E** – Eirene (neutral transport code)
 - Determines background neutral pressure in machine and interaction with plasma solution – yields chord-integrated line emission
 - Takes a wall model as part of the input for calculating the recycling from each surface – will provide more rigorous recycling analysis
- **D** – DIVIMP (impurity transport code)
 - Monte Carlo impurity model – utilizes sputtering tables to determine launch probabilities – tracks impurities, chord-integrated line emission
- OEDGE used to address several divertor/SOL issues
 - C^{13} transport during impurity injection on DIII-D (Elder, McLean)
 - Fueling and detached plasma description in Alcator C-MOD/DIII-D (Lisgo)
 - X_{perp} extraction from JRT plasmas on DIII-D (Elder, APS2010)

General Onion-Skin Method Compared with 2-Point Model

- Comparison with 2-point model
 - Straightened out plasma (no B variation) vs. equilibrium recon.
 - All ionizations at PFC vs. distributed source definition
 - No radiation (simple 2-PM) vs. distributed radiation
- Reduced complexity model (SOL13) until neutral solution operating (EIRENE)
 - 2/7 power makes end-point integration robust (boon of OSM methodology) $2^{(2/7)} \rightarrow 20\%$
 - Solves for density and velocity after integration of temperature and flux
 - SOL22 simultaneously solves all three conservation equations (particles, momentum, power)
- Provides sanity check #2

2 point model

$$2n_t T_t = n_u T_u$$

$$T_u = \left[T_t^{7/2} + \frac{7}{2} \frac{q_{\parallel} L}{2\kappa_{0e}} \right]^{2/7}$$

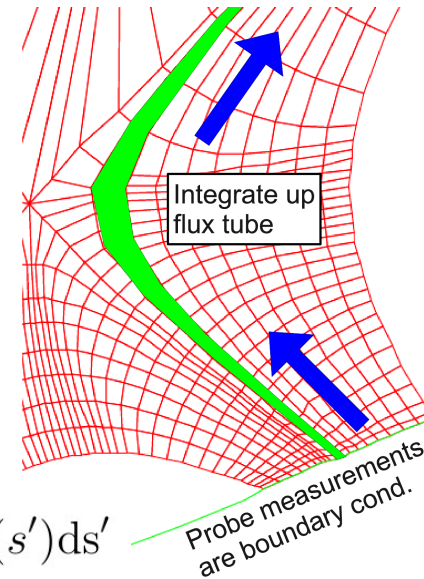
$$q_{\parallel} = \gamma(V_s) n_t k T_t c_{st}$$

upstream



target

VS.



$$\Gamma(s) = n_0 c_{s0} + \int_0^s S_p(s') ds'$$

$$p_0 = n(s) [kT_e(s) + kT_i(s) + mv(s)^2]$$

$$T_e(s) = \left[T_{e0}^{7/2} + \frac{7}{2\kappa_{0e}} \left(q_{\parallel,0} s + \int_0^s P_{rad}(s') ds' \right) \right]^{2/7}$$

Probe Data Integration Yields Upstream Quantities → Separatrix Properties at Midplane

- Separatrix location defined from crossing of upstream quantity with MPTS profile
 - Mid-plane density crossing consistent with T_e and P_e in SOL13 model vs. 2-PM
 - Calculation quantities consistent with discontinuity (T_e , P_e) in MPTS profiles
- Variance from equilibrium reconstruction observed at both target and upstream
 - Pressure peak consistently inboard of magnetics answer
 - Only one shot analyzed this way so far – more on the way

