



U.S. DEPARTMENT OF
ENERGY

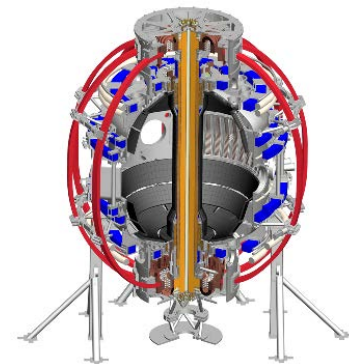
Office of
Science



Vertical stability calculations

J. Menard, E. Kolemen, S. Gerhardt

NSTX-U Results Review
PPPL B318
September 21, 2016



Background

- Recently published ST-FNSF / Pilot Plant paper required vertical stability projections
- Used rigid plasma model, LRDFIT / ISOLVER structure model and code infrastructure
- Benchmarked against NSTX natural VDE data with coil voltages frozen → plasma drift
- Assessed FNSF drift recovery vs. vertical offset
 - Determined marginal $\Delta Z/a$ vs I_i and wall position

Rigid plasma vertical growth rate model

For a vertically unstable plasma with velocity far below the Alfvén speed, plasma inertia can be ignored and the plasma motion away from the neutral point z_0 can be modeled as an equilibrium force balance with the $\vec{J} \times \vec{B}$ force balanced by the opposing force from image currents I_v in nearby vessel or other passive conducting structures:

$$\hat{z} \cdot \int dV \rho_m \frac{d\vec{v}}{dt} = \hat{z} \cdot \int dV \vec{J} \times \vec{B} + \Gamma_v I_v \approx 0 \quad (1)$$

The vessel or conducting wall current I_v is induced by the plasma motion or velocity $\dot{z} = dz/dt$. If the vessel / passive conductors have self-inductance L_v , mutual inductance to the plasma M_{vp} , and current decay rate $\lambda_v = R_v/L_v$, then:

$$\Gamma_v I_v = Y(t) \Delta F_z \quad Y(t) \equiv e^{-\lambda_v t} \int_0^t e^{\lambda_v t'} (\dot{z}/z_0) dt' \quad (2)$$

$$\Delta F_z \equiv z_0 \Gamma_v \frac{M_{vp}}{L_v} \frac{\partial I_P}{\partial z} \quad F_z \equiv \hat{z} \cdot \int dV \vec{J}_\phi \times \vec{B}_R \approx \left. \frac{\partial F_z}{\partial z} \right|_{z_0} (z - z_0) \quad (3)$$

$$\Rightarrow \left. \frac{\partial F_z}{\partial z} \right|_{z_0} (z - z_0) + Y(t) \Delta F_z = 0 \quad (4)$$

Growth rate dependence on stability index f

$$\Rightarrow \left. \frac{\partial F_z}{\partial z} \right|_{z_0} (z - z_0) + Y(t) \Delta F_z = 0 \quad (4)$$

$$\dot{Y} = -\lambda_v Y + \dot{z}/z_0 \quad \Rightarrow \quad \dot{z} + \gamma z = \gamma z_0 \quad (5)$$

$$f \equiv - \left(\frac{\partial F_z}{\partial z} \right) / \left(\frac{\Delta F_z}{z_0} \right) \quad (6)$$

$$\gamma \equiv \frac{\lambda_v f}{1 - f} \quad (7)$$

$$f \leq 0 \Rightarrow \text{stable} \quad f > 0 \Rightarrow \text{unstable} \quad f \geq 1 \Rightarrow \text{ideally - unstable} \quad (8)$$

Two eigenmode growth rate model

In general, the force on the plasma from plasma-motion induced image currents can be expressed as:

$$\Gamma_v I_v = \sum_{k=1} Y_k(t) \Delta F_k \quad Y_k(t) \equiv e^{-\lambda_k t} \int e^{\lambda_k t'} (\dot{z}/z_0) dt' \quad (8)$$

A more accurate yet analytically tractable approximation is to fit the full response force to a reduced model with two image current decay times λ_1 and λ_2 and corresponding force coefficients ΔF_1 and ΔF_2 . The corresponding equation for the vertical growth-rate γ then becomes:

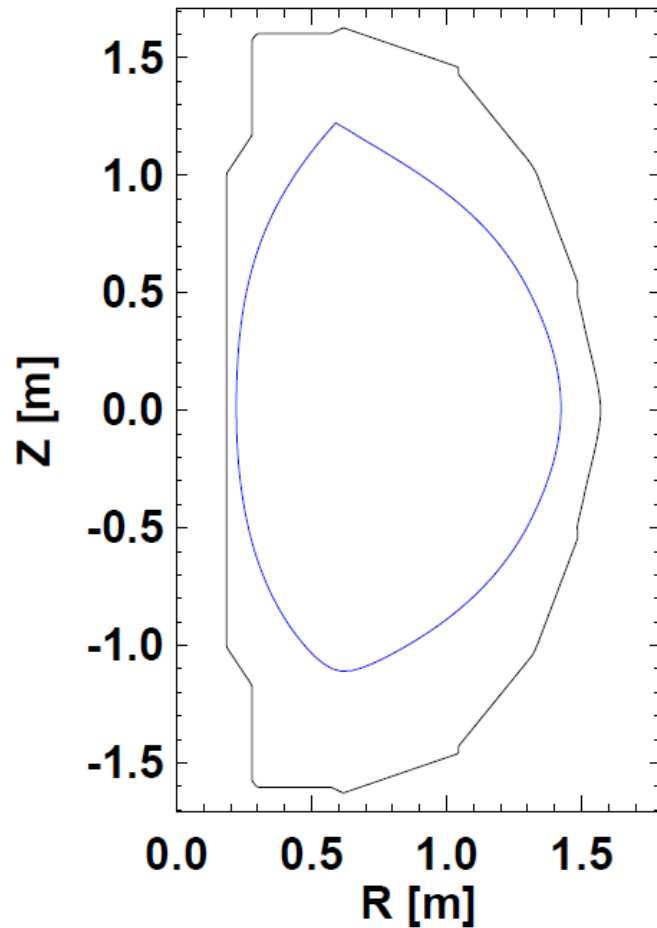
$$d + s_1 \frac{\gamma}{\gamma + \lambda_1} + s_2 \frac{\gamma}{\gamma + \lambda_2} = 0 \quad d \equiv \left. \frac{\partial F_z}{\partial z} \right|_{z_0} \quad s_1 \equiv \frac{\Delta F_1}{z_0} \quad s_2 \equiv \frac{\Delta F_2}{z_0} \quad (9)$$

$$a \equiv s_1 + s_2 + d \quad b \equiv d(\lambda_1 + \lambda_2) + s_1 \lambda_2 + s_2 \lambda_1 \quad c \equiv d \lambda_1 \lambda_2 \quad (10)$$

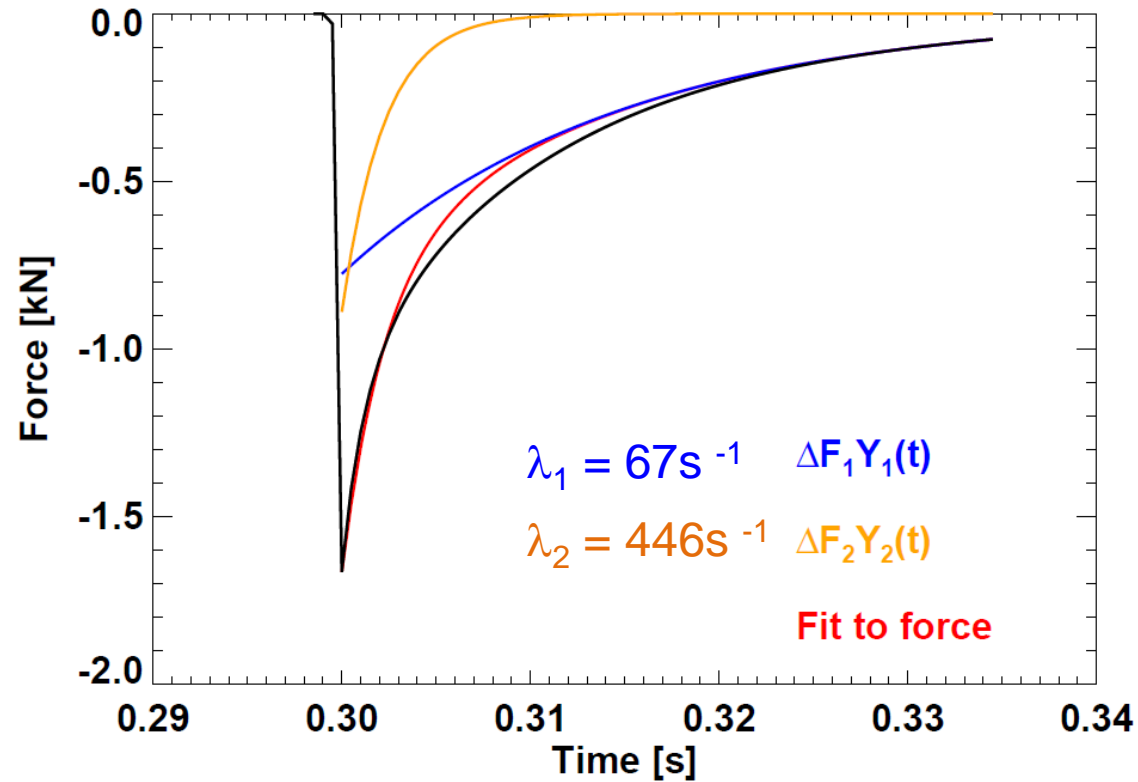
$$\Rightarrow \gamma = \frac{-b - \sqrt{b^2 - 4ac}}{2a}$$

Passive current force in reduced model

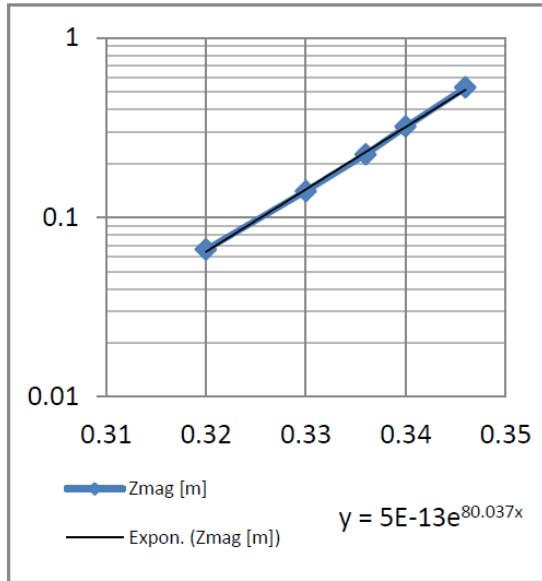
Shot = 127083, t = 0.300s



Vertical force on plasma from passive conductors for z-step = 1.9623665cm

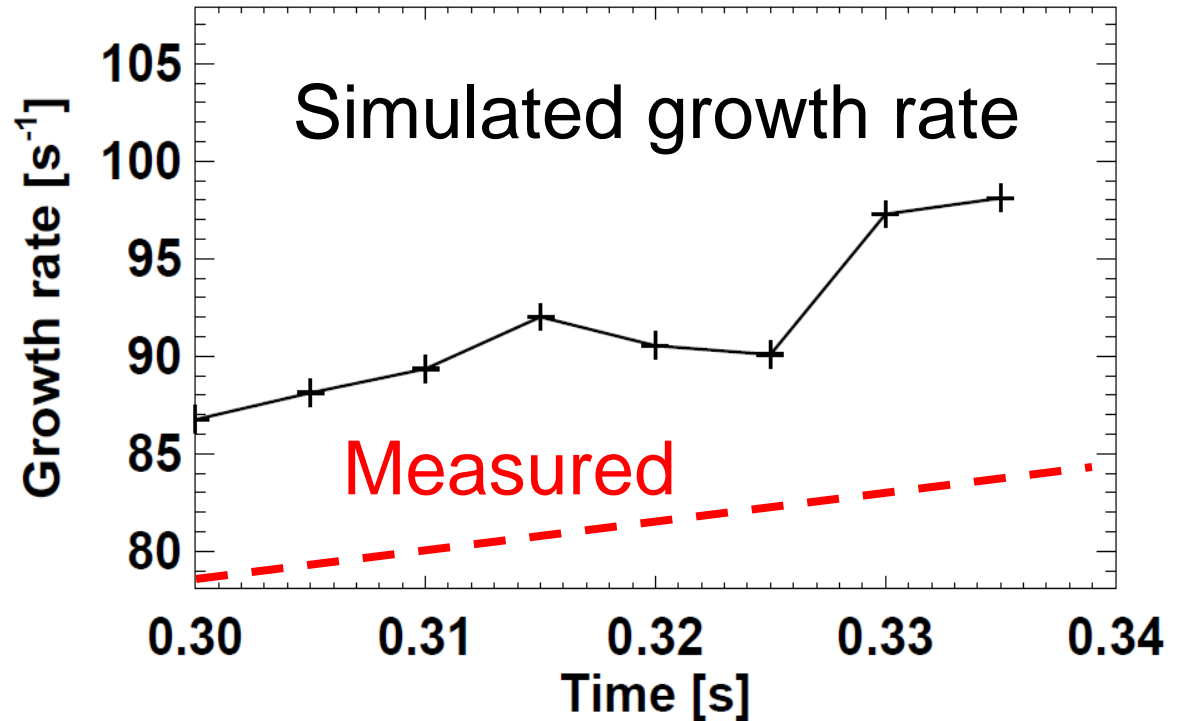


Simulated γ 10-15% higher than expt



127083
LRDFIT01

time [s]	Zmag [m]
0.306	0.022
0.31	0.03
0.32	0.066
0.33	0.14
0.336	0.224
0.34	0.32
0.346	0.529



Future: Need to assess variation in predicted growth rate vs. # of conducting wall eigenvalues retained

Model for vertical position dynamics

$$z_j = z(t = t_j) \quad F_z(z_j) + \left. \frac{\partial F_z}{\partial z} \right|_{z_j} \Delta z_{j+1} + \sum_{k=1} Y_k(t_{j+1}) \Delta F_k + \chi_{j+1} = 0$$

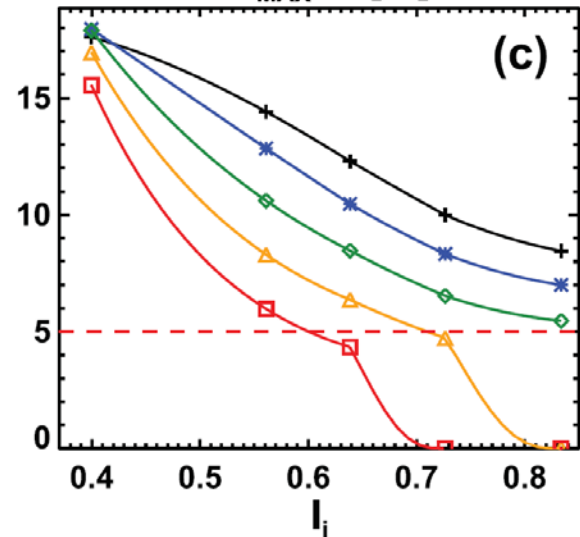
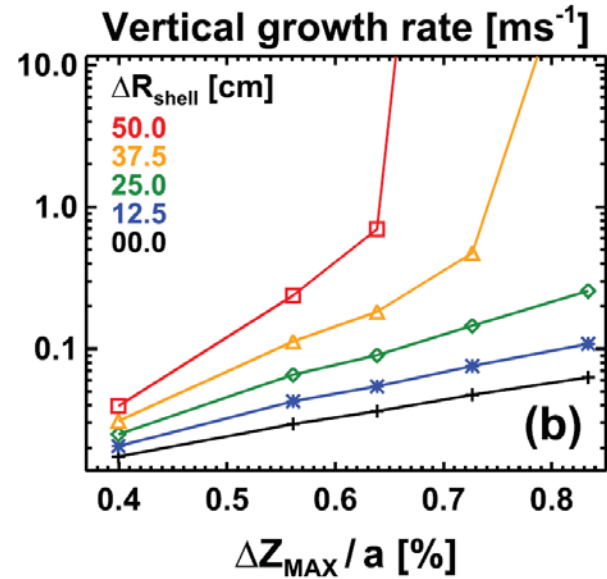
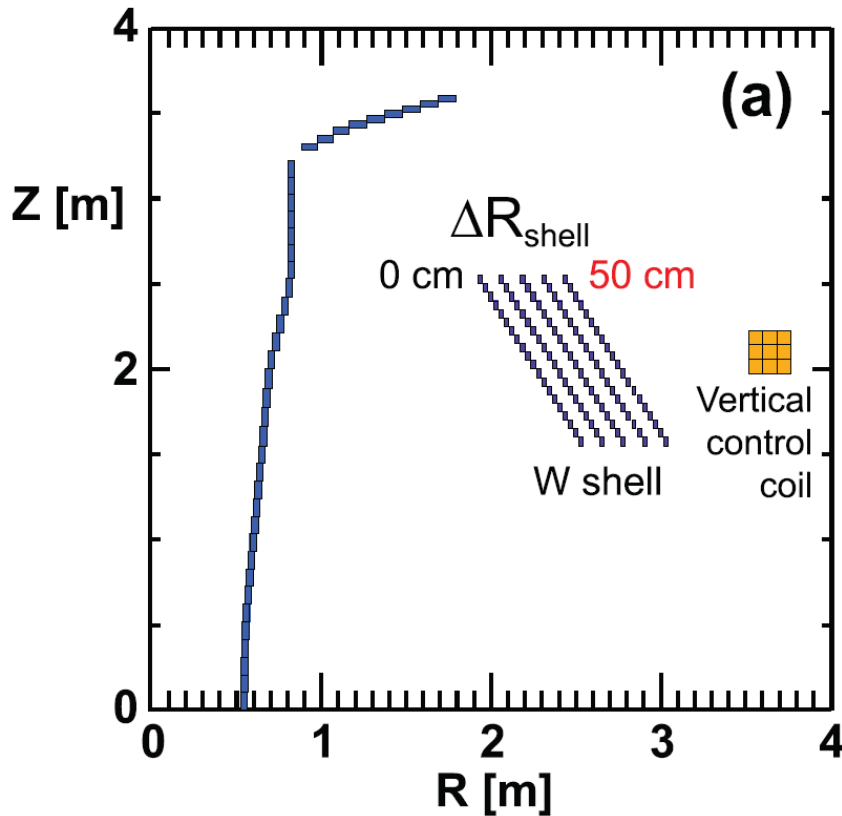
Depends linearly on Δz_{j+1}

→ Solve for $\Delta z_{j+1} (\Delta z_j, \dots)$

Force from control coils

- Assess ability to recover plasma from vertical offset:
 - Let plasma drift exponentially to vertical offset ΔZ
 - Apply step voltage to control coils
 - Determine if coil force can return plasma to mid-plane
 - Assess power vs. max offset ΔZ_{\max} as metric for controllability

Example controllability calculation for FNSF



Acceptable control



Possible future work / ideas

- Benchmark against NSTX-U (when we get some uncontrolled drift rate data)
- Correlate NSTX / NSTX-U controllability vs. open loop growth rate and/or stability index
- Complete / extend dynamical model for modular closed-loop control simulations
 - Optimize sensor positions, assess EFC/RWM coils for $n=0$
 - Implement $n=0$ stability calculator in PCS and/or TRANSP
 - Adjust elongation based on calculated marginal point?