



Overview of the Disruption Prediction, Avoidance, and Mitigation Working Group and Initial Results

S.A. Sabbagh¹, R. Raman²

For the NSTX-U DPAM Working Group

¹Columbia University, New York, NY ²University of Washington, Seattle, WA

> NSTX-U PAC 37 Meeting PPPL, Princeton, NJ January 27th, 2016









V1.6

Overview of the NSTX-U Disruption Prediction, Avoidance, and Mitigation (DPAM) Working Group - OUTLINE

- Motivation and connection to DOE FES priorities
- Mission statement and Scope
- Disruption Prediction: Characterization and forecasting approach, implementation, and development
- Disruption Avoidance: Mode stabilization and control
- Disruption Mitigation: Preparation of NSTX-U MGI system
- Connection to JRT-16 Joint Research Target Milestones

Disruption avoidance is a critical need for future tokamaks; NSTX-U is focusing stability research on this

- □ The new "grand challenge" in tokamak stability research
 - □ <u>Can be done</u>! (JET: < 4% disruptions w/C wall, < 10% w/ITER-like wall)
 - ITER disruption rate: < 1 2% (energy load, halo current); << 1% (runaways)</p>
- □ <u>Strategic plan</u>: utilize/expand stability/control research success
 - Synergize and build upon disruption prediction and avoidance successes attained in present tokamaks (don't just repeat them!)
- FESAC 2014 Strategic Planning report defined "Control of Deleterious Transient Events" highest priority (Tier 1) initiative
 - Working group members had significant leadership roles in the 2015 DOE Workshops on solving issues of "Transient Events in Tokamaks"

NSTX-U will produce focused research on disruption avoidance with quantitative measures of progress

Long-term goal: many sequential shots (~3 shot-mins) without disruption

DPAM Working Group - Mission Statement and Scope

Mission statement

Satisfy gaps in understanding prediction, avoidance, and mitigation of disruptions in tokamaks, applying this knowledge to move toward acceptable levels of disruption frequency/severity using quantified metrics

Scope

- Location: Initiate and base the study at NSTX-U, expand to a national program and international collaboration (multi-tokamak data)
- Timescale: Multi-year effort, planning/executing experiments of various approaches (leveraging the 5 NSTX-U Year Plan) to reduce plasma disruptivity/severity at high performance
- Breadth: High-level focus on quantified mission goal, with detailed physics areas expected to expand/evolve within the group, soliciting research input/efforts from new collaborations as needed

More than 50 members presently on email list; 3 meetings held to date

Disruption Prediction

Disruption event chain characterization capability started for NSTX-U as next step in disruption avoidance plan





Approach to disruption prevention

- Identify disruption event chains and elements
- Predict events in disruption chains
- Cues disruption avoidance systems to break event chains
 - Attack events at several places with active control
- Synergizes and builds upon both physics and control successes of NSTX

New Disruption Event Characterization and Forecasting (DECAF) code created

Disruption Event Characterization And Forecasting Code (DECAF) yielding initial results (pressure peaking example)



J.W. Berkery, S.A. Sabbagh, Y.S. Park (Columbia U.) and the NSTX-U Disruption PAM Working Group

- 10 physical events presently defined in code with quantitative warning points
 - Builds on manual analysis of de Vries
 - P.C. de Vries et al., Nucl. Fusion 51 (2011) 053018
 - Builds on warning algorithm of Gerhardt

S.P. Gerhardt et al., Nucl. Fusion 53 (2013) 063021

- New code written (in Python), easily expandable, portable to other tokamaks (recent capability to process DIII-D data)
- <u>Example</u>: Pressure peaking (PRP) disruption event chain identified by code before disruption
 - 1. (PRP) Pressure peaking warnings identified first
 - 2. (VDE) VDE condition subsequently found 19 ms after last PRP warning
 - 3. (IPR) Plasma current request not met
 - 4. (SCL) Shape control warning issued

DECAF is structured to ease parallel development of disruption characterization, event criteria, and forecasting



Initial DECAF results detect disruption chain events when applied to dedicated 44 shot NSTX RWM disruption database

Several events detected for all shots

- RWM: RWM event warning
- SCL: Loss of shape control
- IPR: Plasma current request not met
- DIS: Disruption occurred
- LOQ: Low edge q warning
- □ VDE: VDE warning (40 shots)

Others:

- PRP: Pressure peaking warning
- GWL: Greenwald limit
- LON: Low density warning
- LTM: Locked tearing mode



Initial DECAF results detects disruption chain events when applied to dedicated 44 shot NSTX RWM disruption database



Initial DECAF analysis already finding common disruption event chains (44 shot NSTX disruption database)

Common disruption event chains (52.3%)

 $\mathsf{RWM} \rightarrow \mathsf{VDE} \rightarrow \mathsf{SCL} \rightarrow \mathsf{IPR} \rightarrow \mathsf{DIS}$

- Related chains
 - RWM → SCL → VDE → IPR → DIS
 - VDE → RWM → SCL → IPR → DIS
 - VDE → RWM → IPR → DIS → SCL
 - RWM → SCL → VDE → GWL → IPR → DIS
- Disruption event chains w/o VDE (11.4%)
- New insights being gained
 - Chains starting with GWL are found that show rotation and β_N rollover before RWM (6.8%)
 - Related chains
 - GWL \rightarrow VDE \rightarrow RWM \rightarrow SCL \rightarrow IPR \rightarrow DIS
 - GWL → SCL → RWM → IPR → DIS





First DECAF results for NSTX-U replicate the triggers found in new real-time state machine shutdown capability

- Important capability of DECAF to compare analysis using offline vs. real-time data
 - □ Simple, initial test
- PCS Shut-down conditions are analogous to DECAF events
 - PCS loss of vertical control
 DECAF VDE

DECAF comparison:VDE event

- Matches PCS when r/t signal used (1 criterion)
- VDE event 13 ms earlier using offline EFIT signals (3 criteria)



See talk by S. Gerhardt (next) for detail of new NSTX-U automated shutdown capability

Disruption Avoidance

NSTX-U is building on past strength, creating an arsenal of capabilities for disruption avoidance

Predictor/Sensor (CY available)	Control/Actuator (CY available)	Modes	REFER TO
Rotating and low freq. MHD (n=1,2,3) 2003	Dual-component RWM sensor control (closed loop 2008)	NTM RWM	 Menard NF 2001 Sabbagh NF 2013; + backup slides
Low freq. MHD spectroscopy (open loop 2005); Kinetic RWM modeling (2008)	Control of β _N (closed loop 2007)	Kink/ball RWM	- Sontag NF 2007 - Berkery (2009–15) - Gerhardt FST 2012
r/t RWM state-space controller observer (2010)	Physics model-based RWM state-space control (2010)	NTM, RWM Kink/ball, VDE	- THIS TALK - Sabbagh NF 2013; + backup slides
Real-time V _o measurement (2016)	Plasma V _o control (NTV 2004) (NTV + NBI rotation control closed loop ~ 2017)	NTM Kink/ball RWM	 Podesta RSI 2012 Zhu PRL 06 +backup THIS TALK
Kinetic RWM stabilization real-time model (2016-17)	Safety factor, l _i control (closed loop ~ 2016-17)	NTM, RWM Kink/ball, VDE	- Berkery, NF 2015 - D. Boyer's TALK
MHD spectroscopy (real-time) (in 5 Year Plan)	Upgraded 3D coils (NCC): improved V_{ϕ} and mode control (in 5 Year Plan)	NTM, RWM Kink/ball, VDE	- NSTX-U 5 Year Plan - THIS TALK

Joint NSTX / DIII-D experiments and analysis gives unified kinetic RWM physics understanding for disruption avoidance

RWM Dynamics

- RWM rotation and mode growth observed
- No strong NTM activity
- Some weak bursting MHD in DIII-D plasma

Alters RWM phase No bursting MHD in NSTX plasma



<u>NSTX ($\beta_N = 4.4$)</u>



S. Sabbagh et al., APS Invited talk 2014

2.98

20

15 E

10

5

0

4

3

2

(arb)

 D_{α}

2.96 2.97

Evolution of plasma rotation profile leads to kinetic RWM instability as disruption is approached



Kinetic RWM stabilization occurs from broad resonances between plasma rotation and particle precession drift, bounce/circulating, and collision frequencies

S. Sabbagh et al., APS Invited talk 2014

State space rotation controller designed for NSTX-U using non-resonant NTV and NBI to maintain stable profiles

• Momentum force balance – ω_{ϕ} decomposed into Bessel function states $\sum_{i} n_{i} m_{i} \langle R^{2} \rangle \frac{\partial \omega}{\partial t} = \left(\frac{\partial V}{\partial \rho}\right)^{-1} \frac{\partial}{\partial \rho} \left[\frac{\partial V}{\partial \rho} \sum_{i} n_{i} m_{i} \chi_{\phi} \langle (R \nabla \rho)^{2} \rangle \frac{\partial \omega}{\partial \rho}\right] + T_{NBI} + T_{NTV}$

NTV torque:

$$T_{NTV} \propto K \times f\left(n_{e,i}^{K1} T_{e,i}^{K2}\right) g\left(\delta B(\rho)\right) \left[I_{coil}^{2} \omega\right]$$

I. Goumiri, et al., submitted to NF (2016)



State space rotation controller designed for NSTX-U using non-resonant NTV and NBI to maintain stable profiles

• Momentum force balance – ω_{ϕ} decomposed into Bessel function states $\sum_{i} n_{i} m_{i} \langle R^{2} \rangle \frac{\partial \omega}{\partial t} = \left(\frac{\partial V}{\partial \rho}\right)^{-1} \frac{\partial}{\partial \rho} \left[\frac{\partial V}{\partial \rho} \sum_{i} n_{i} m_{i} \chi_{\phi} \langle (R \nabla \rho)^{2} \rangle \frac{\partial \omega}{\partial \rho} \right] + T_{NBI} + T_{NTV}$

NTV torque:

$$T_{NTV} \propto K \times f\left(n_{e,i}^{K1} T_{e,i}^{K2}\right) g\left(\delta B(\rho)\right) \left[I_{coil}^{2} \omega\right]$$

I. Goumiri, et al., submitted to NF (2016)



State space rotation controller designed for NSTX-U can evolve plasma rotation profile toward global mode stability



I. Goumiri (Princeton student), S.A. Sabbagh (Columbia U.), C. Rowley (P.U.), D.A. Gates, S.P. Gerhardt (PPPL)

With planned NCC coil upgrade, rotation controller can reach desired rotation profile faster, with greater fidelity



I. Goumiri (Princeton student), S.A. Sabbagh (Columbia U.), C. Rowley (P.U.), D.A. Gates, S.P. Gerhardt (PPPL)

Active RWM control design study for proposed NSTX-U 3D coil upgrade (NCC coils) shows superior capability



NSTX RWM state space controller sustains high β_N , low I_i plasma – available for NSTX-U with independent coil control



Run time has been allocated for continued experiments on NSTX-U in 2016

S. Sabbagh et al., Nucl. Fusion 53 (2013) 104007

In addition to active mode control, the NSTX-U RWM state space controller can be used for real-time disruption warning

- The controller "observer" produces a physics modelbased calculation of the expected sensor data – <u>a</u> <u>synthetic diagnostic</u>
- If the real-time synthetic diagnostic doesn't match the measured sensor data, a r/t disruption warning signal can be triggered
 - Technique will be assessed using the DECAF code

Effect of 3D Model Used



Disruption Mitigation

NSTX-U Disruption Mitigation Research Aims to Develop MGI and EPI Technologies in Support ITER and FNSF

□ <u>Massive Gas Injection (MGI)</u>: (starting 2016)

- ITER-type MGI valve will be used on NSTX-U in a configuration to do nearly exact comparison experiments
- □ Experimental results to be studied using M3D-C¹ (A. Fil, S. Jardin, et al.)
 - Develop understanding of gas assimilation fraction by the plasma
 - Use to project to ITER plasmas
- Similar plasma poloidal size, shape of DIII-D and NSTX-U allows multimachine comparison studies

□ <u>Electromagnetic Particle Injector (EPI)</u>: (in 5 Year Plan)

- Motivation: Handle fast disruptions
 - For warning times < 10 ms, MGI may not be a viable option
- Rapid delivery of impurities deeper into plasma with fast time-response
 - Under 5ms from trigger to delivery at 7m from plasma
 - Efficiency of system improves in a magnetic field environment

New double solenoid valve design (zero net JxB torque) pass tests for reliability and magnetic field limits



NSTX-U MGI will study poloidal injection location variation using identical MGI valves and gas transit piping



- Assess benefits of injection into the private flux region & the high-field side vs.
 LFS midplane
- Quantify MGI gas assimilation fractions and extend model to larger machines
- Model gas penetration and assimilation results using 3D MHD codes (incl. M3D-C¹)

First plasma tests April, experiment May 2016

DPAM Working Group is fulfilling DOE Joint Research Target JRT-16 milestones to start NSTX-U 5 YP research goals

□ FY16 DOE Joint Research Target summary (1 page)

http://nstx.pppl.gov/DragNDrop/Working_Groups/DPAM/Repository/JRT 16QuarterlyMilestones-V9.pdf

Culminating Milestones for 2016

Prediction / Avoidance

- Use disruption prediction algorithm to characterize the reliability of predicting a few types of common disruptions from at least two devices
- Report on capability to reduce disruption rate through active improvement of plasma stability
- Test on at least one facility to detect in real time an impending disruption and take corrective measures to safely terminate the plasma discharge

Mitigation

Test newly-designed ITER-type massive gas injection value to study benefits of private flux region massive gas injection vs. mid-plane inj.

NSTX-U Research is building upon physics understanding and synergizing control for disruption PAM in tokamaks

Disruption PAM Working Group Mission

- □ Satisfy gaps in understanding disruption prediction, avoidance, mitigation
- Apply knowledge to demonstrate acceptable levels of disruption frequency/severity using quantified metrics

PAC charges are directly addressed

- FESAC/FES Initiatives: NSTX-U DPAM Working group effort was born from 2015 FES effort - is identically aligned with it. Urgent ITER need.
- <u>Research</u>: Disruption Event Characterization And Forecasting effort started to unify physics understanding for disruption avoidance (5 YP Committee member recommendation); MGI to start in 2016.
- Facility enhancements: Quantified disruptivity metrics will assess new capabilities (e.g. plasma rotation, q, active mode control) and guide future improvements (e.g. planned NCC 3D coil upgrade, et al.)
- PPPL Theory partnership: Is highly leveraged in this effort (10 members) (see talk by A. Bhattacharjee)

Supporting Slides Follow

NSTX is a spherical torus equipped to study passive and active global MHD control

□ High beta, low aspect ratio

□ R = 0.86 m, A > 1.27

- □ $\beta_t < 40\%, \beta_N > 7$
- Copper stabilizer plates for kink mode stabilization

Midplane control coils

- n = 1 3 field correction, magnetic braking of ω_φ by NTV
 n = 1 PWM control
- $\square n = 1 \text{ RWM control}$

Combined sensor sets now used for RWM feedback

□ 48 upper/lower B_p, B_r



Modification of Ideal Stability by Kinetic theory (MISK code) is used to determine proximity of plasmas to stability boundary

- □ Initially used for NSTX since simple critical scalar ω_{ϕ} threshold stability models did not describe RWM stability Sontag, et al., Nucl. Fusion **47** (2007) 1005
- Kinetic modification to ideal MHD growth rate
 - Trapped / circulating ions, trapped electrons, etc.
 - Energetic particle (EP) stabilization
- Stability depends on

$$\gamma \tau_{w} = -\frac{\delta W_{\infty} + \delta W_{K}}{\delta W_{wall} + \delta W_{K}}$$

Hu and Betti, Phys. Rev. Lett **93** (2004) 105002

Some NSTX / MISK

analysis references

 ω_{ϕ} profile (enters through ExB frequency)

- Integrated $\underline{\omega}_{\phi}$ profile: resonances in δW_{κ} (e.g. ion precession drift)
- Particle <u>collisionality</u>, EP fraction

<u>Trapped ion component of δW_{κ} (plasma integral over energy)</u>

$$\delta W_{K} \propto \int \left[\frac{\omega_{*N} + \left(\hat{\varepsilon} - \frac{3}{2}\right)\omega_{*T} + \omega_{E} - \omega - i\gamma}{\langle \omega_{D} \rangle + l\omega_{b} - i\nu_{eff}} + \omega_{E} - \omega - i\gamma \right] \hat{\varepsilon}^{\frac{5}{2}} e^{-\hat{\varepsilon}} d\hat{\varepsilon} \qquad \text{J. Berkery et al., PRL 104, 035003 (2010)} \\ \text{J. Berkery et al., NF 50, 025020 (2010)} \\ \text{J. Berkery et al., NF 53, 104007 (2013)} \\ \text{J. Berkery et al., NF 53, 104007 (2013)} \\ \text{J. Berkery et al., POP 21, 056112 (2014)} \\ \text{J. Berkery et al., NF 55, 123007 (2015)} \end{cases}$$

Kinetic RWM stability evaluated for DIII-D and NSTX plasmas, reproduces experiments over wide rotation range

Summary of results

- Plasmas free of other MHD modes can reach or exceed linear kinetic RWM marginal stability
- Bursting MHD modes can lead to non-linear destabilization before linear stability limits are reached

 Extrapolations of DIII-D plasmas to different V_o show marginal stability is bounded by 1.6 < q_{min} < 2.8

Extensive NSTX / MISK analysis references spanning ~ 7 years (8 references given in supporting slides)



S. Sabbagh et al., APS Invited talk 2014 J.W. Berkery, J.M. Hanson, S.A. Sabbagh (Columbia U.)

JET disruption event characterization provides framework to follow for understanding / quantifying DPAM progress

JET disruption event chains

Related disruption event statistics



- □ JET disruption event chain analysis performed by hand, desire to automate
- General code written (DECAF) to address the <u>first step</u> initial analysis started using NSTX data

Disruption Characterization Code now yielding initial results: disruption event chains, with related quantitative warnings (2)



- This example: Greenwald limit warning during I_p rampdown
 - 1. (GWL) Greenwald limit warning issued
 - (VDE) VDE condition then found
 0.6 ms after GWL warning
 - (IPR) Plasma current request not met

J.W. Berkery, S.A. Sabbagh, Y.S. Park

NTV physics studies for rotation control: measured **NTV** torque density profiles quantitatively compare well to theory



 $\Box T_{NTV}$ (theory) scaled to match *peak* value of measured *-dL/dt*

□ Scale factor $((dL/dt)/T_{NTV}) = 1.7$ and 0.6 for cases shown above - O(1) agreement

KSTAR n = 2 NTV experiments <u>do not</u> exhibit hysteresis
 See recent NTV review paper: K.C. Shaing, K. Ida, S.A. Sabbagh, et al., Nucl. Fusion 55 (2015) 125001

Active RWM control: dual $B_r + B_p$ sensor feedback gain and phase scans produce significantly reduced n = 1 field



Model-based RWM state space controller including 3D model of plasma and wall currents used at high β_N



t (s)

State Derivative Feedback Algorithm needed for Current Control

• State equations to advance $\vec{x} = A\vec{x} + B\vec{u}$ $\vec{u} = -K_c\vec{x} = \dot{I}_{cc}$ $\vec{y} = C\vec{x} + D\vec{u}$ Control vector, u; controller gain, K_c

Observer est., y; observer gain, K_o

 K_c , K_o computed by standard methods (e.g. Kalman filter used for observer)

- Previously published approach found to be formally "uncontrollable" when applied to current control
- State derivative feedback control approach

$$\dot{\vec{x}} = A\vec{x} + B\vec{u}$$
 $\vec{u} = -\hat{K}_c\dot{\vec{x}}$ \longrightarrow $\vec{I}_{cc} = -\hat{K}_c\vec{x}$

 $\dot{\vec{x}} = ((\mathbf{I} + B\hat{K}_c)^{-1}A)\vec{x}$ e.g. T.H.S. Abdelaziz, M. Valasek., Proc. of 16th IFAC World Congress, 2005

new Ricatti equations to solve to derive control matrices – still "standard" solutions for this in control theory literature

Advance discrete state vector

$$\hat{\vec{x}}_t = A\vec{x}_{t-1} + B\vec{u}_{t-1}; \quad \hat{\vec{y}}_t = C\hat{\vec{x}}_t$$
 (time update)
 $\vec{x}_{t+1} = \hat{\vec{x}}_t + A^{-1}K_o(\vec{y}_{sensors(t)} - \hat{\vec{y}}_t)$ (measurement update)

Written into the PCS

- General (portable) matrix output file for operator

NSTX RWM state space controller sustains high β_N , low I_i plasma – available for NSTX-U with independent coil control



Run time has been allocated for continued experiments on NSTX-U in 2016

S. Sabbagh et al., Nucl. Fusion 53 (2013) 104007

RWM state space controller sustains otherwise disrupted plasma caused by DC n = 1 applied field



- n = 1 DC applied field test
 - Generate resonant field amplication, disruption
 - Use of RWM state space controller sustains discharge
- RWM state space controller sustains discharge at high β_N
 - Best feedback phase produced long pulse, β_N = 6.4, β_N/l_i = 13

S. Sabbagh et al., Nucl. Fusion **53** (2013) 104007

Open-loop comparisons between measurements and RWM state space controller show importance of states and model



Improved agreement with sufficient number of states (wall detail) 3D detail of model important to improve agreement

In addition to active mode control, the NSTX-U RWM state space controller can be used for r/t disruption warning

- The controller "observer" produces a physics modelbased calculation of the expected sensor data – <u>a</u> <u>synthetic diagnostic</u>
- If the real-time synthetic diagnostic doesn't match the measured sensor data, a r/t disruption warning signal can be triggered
 - Technique will be assessed using the DECAF code

Effect of 3D Model Used





In addition to active mode control, the NSTX-U RWM state space controller can be used for real-time disruption warning

- The controller "observer" produces a physics modelbased calculation of the expected sensor data – <u>a</u> <u>synthetic diagnostic</u>
- If the real-time synthetic diagnostic doesn't match the measured sensor data, a r/t disruption warning signal can be triggered
 - Technique will be assessed using the DECAF code

Effect of 3D Model Used



Bounce resonance stabilization dominates for DIII-D vs. precession drift resonance for NSTX at similar, high rotation

 $|\delta W_{K}|$ for trapped resonant ions vs. scaled experimental rotation (MISK)



Increased RWM stability measured in DIII-D plasmas as q_{min} is reduced is consistent with kinetic RWM theory

 $|\delta W_{K}|$ for trapped resonant ions vs. scaled experimental rotation (MISK)



When T_i is included in NTV rotation controller model, 3D field current and NBI power can compensate for T_i variations



<u>NSTX-U</u>: RWM active control capability increases as proposed 3D coils upgrade (NCC coils) are added



ITER High Priority need: What levels of plasma disturbances (δB_p ; $\delta B_p/B_p(a)$) are permissible to avoid disruption?

- NSTX RWM-induced disruptions analyzed
 - Same database analyzed by DECAF in prior slides
- Compare maximum δB_p (n = 1 amplitude) causing disruption vs I_p

Max $\delta B^{n=1 \text{ lower RWM}}$ vs. Plasma Current



- Maximum δB_p increases with I_p
- Next step: add results from other devices

the way to new ene

f (a)

<u>Maximum δB_p might follow a de Vries-style engineering</u> scaling $I_p^{p1}I_i^{p2}/a^{p3}q_{95}^{p4}$

- NSTX RWMinduced disruptions
- Compare maximum δB_p causing disruption to de Vries locked NTM scaling
 - engineering parameters
 - Data shows significant scatter (as does de Vries' analysis for NTM)

Max δBn=1 lower RWM (G)



Max $\delta B^{n=1 \text{ lower RWM}}$ vs. engineering scaling

the way to new end

T C

<u>Maximum $\delta B_p / \langle B_p(a) \rangle$ might follow a de Vries-style</u>

scaling l_i^{p1}/q₉₅^{p2}

- NSTX RWMinduced disruptions
- Compare maximum δB_p causing disruption vs. de Vries locked (m) NTM scaling
 - Normalized parameters
- NSTX analysis uses kinetic EFIT reconstructions

 \Box I_i instead of I_i(3)

□ <B_p(a)>_{fsa} used

Max $\delta B^{n=1 \text{ lower RWM}} < B_p(a) > vs. norm. scaling$



the way to new ene

In contrast, maximum $\delta B_p/\langle B_p(a) \rangle$ seems independent of scaling on (I_i) or (F_p) (or (F_p/I_i))



- $F_p = p_{tot}(0)/\langle p_{tot} \rangle_{vol}$ (from kinetic equilibrium reconstructions)
- Dependence on I_i, F_p expected for RWM marginal stability points

the way to new ene

her