

# Divertor heat flux scaling with heating power and plasma current in H-mode discharges in the national spherical torus experiment

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## Abstract

We present the first results of lower divertor heat flux scaling with input power ( $P_{\text{NBI}}$ ) and plasma current ( $I_p$ ) in H-mode discharges in the National Spherical Torus Experiment. These experiments were conducted with  $0.6 \leq I_p \leq 0.9$  MA,  $1 < P_{\text{NBI}} < 6$  MW, on-axis toroidal field  $B_t = 0.45$  T, in a lower-single null discharge shape with elongation  $\kappa \sim 2.0$ , triangularity  $\delta \sim 0.45$ , and the ion grad- $B$  drift toward the  $X$ -point. As  $P_{\text{NBI}}$  was raised from 1 MW to 6 MW, the outer divertor peak heat flux was observed to increase up to 6 MW/m<sup>2</sup>. A break in the slope of peak heat flux vs. power was observed at heating power  $\sim 3$  MW, which we interpret as the transition of the divertor toward the high recycling regime and well away from the detachment threshold. The peak heat flux was also observed to increase strongly with  $I_p$ .

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## 1. Introduction

Heat flux management is an important concern in high power density systems. Owing to their compact nature, spherical tori (ST) have the potential for high heat flux at divertor target plates because of the large ratio of  $P/R$ , where  $P$  is the heating

power and  $R$  is the major radius of the device. High heat fluxes can be intensified by the relatively short outboard connection length in STs. Fortunately, the ST scrape-off layer (SOL) can be designed to have high poloidal flux expansion at the target, which has been shown to reduce the peak heat flux [1]. While substantial experimental work has been done in heat flux scaling for higher aspect ratio tokamaks such as DIII-D [2], there are far fewer published reports from lower aspect ratio, spherical tokamaks [3–5].

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In this paper, we present the first results of outer divertor heat flux scaling with neutral beam heating power ( $P_{\text{NBI}}$ ) and plasma current ( $I_p$ ) in H-mode discharges in the National Spherical Torus Experiment (NSTX). This work builds upon previous NSTX reports of the peak heat flux scaling in L-mode discharges [6], and power accountability [7] and initial surveys of the heat flux characteristics [8] in H-mode discharges, as well as studies of heat flux management through radiation and detachment [9]. We focus on the outer divertor because the inner divertor remains detached through most of the operational window in NSTX [10].

## 2. Experiment setup and results of scaling studies

The heat flux profile is measured in NSTX with infrared cameras; the basic method is described here and details are provided elsewhere [11]. The camera is a commercial 12-bit, 30 Hz micro-bolometer camera with sensitivity in the 8–12  $\mu\text{m}$  range and a measured thermal response time constant of  $\sim 20$  ms. The lower divertor tile infrared emission is calibrated during in situ high temperature bakes, and the heat flux profile is computed from a 1-D conduction model into a semi-infinite solid [2], i.e. neglecting thermal transport along the surface of the tile.

The lower single-null diverted discharges used in this study had the following parameters:  $0.6 \leq I_p \leq 0.9$  MA,  $1 \leq P_{\text{NBI}} \leq 6$  MW, toroidal field on-axis  $B_t = 0.45$  T, elongation  $\kappa = 2.0$ , average triangularity  $\delta \sim 0.45$ , and a large inner-wall gap between 6 and 10 cm. The temporal evolution of the highest power discharge used in the  $P_{\text{NBI}}$  scan is shown in Fig. 1. Neutral beam heating during the  $I_p$  ramp was used to minimize volt-second consumption during the ramp-up. As in most NSTX H-mode discharges, the line-average density ( $n_e^{\text{FIR}}$ ) ramped throughout the discharge, owing partly to continuous gas fueling from the high-field side gas injector which improves the reliability of H-mode access in STs [12,13]. The stored energy ( $W_{\text{MHD}}$ ) continued to increase slowly after the L–H transition at 0.22 s, until it was clamped at the onset of Type I edge-localized modes (ELMs) at  $t = 0.345$  s.

### 2.1. Outer divertor heat flux scaling with $P_{\text{NBI}}$

The scaling of peak divertor heat flux with  $P_{\text{NBI}}$  was conducted with constant  $I_p = 0.8$  MA over a range of  $1 \leq P_{\text{NBI}} \leq 6$  MW. To insure reliable H-

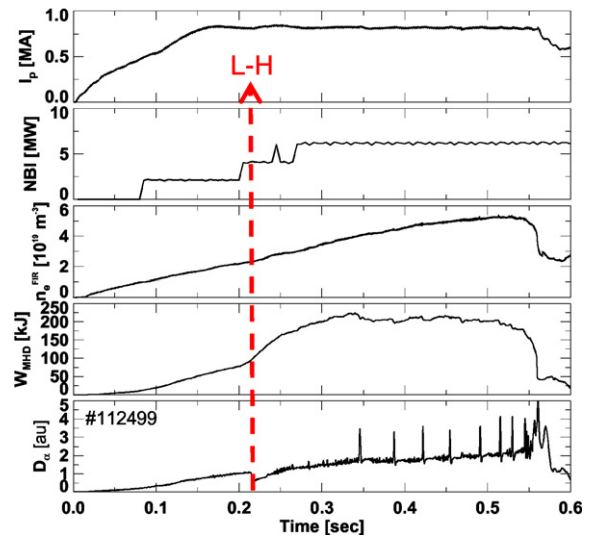


Fig. 1. Time traces of highest heating power discharge. Density ramps throughout the discharge, due partly to continuous gas fueling from the center stack region. Note that the stored energy comes into equilibrium, and the discharge exhibits both small Type V ELMs and large Type I ELMs.

mode transitions, all discharges had  $P_{\text{NBI}} = 4$  MW until  $\sim 0.23$  s, after which the power was changed to the desired level by 0.26 s. As previously reported [14], the ELM character changed substantially during the  $P_{\text{NBI}}$  scan upon reaching a critical value of normalized beta  $\beta_N \sim 5$  [ $\beta_N \equiv (\beta_t a B_t / I_p)$  where toroidal beta  $\beta_t = 2\mu_0 W_{\text{MHD}} / B_t^2$ ,  $a$  is the minor radius, and  $W_{\text{MHD}}$  is the plasma stored energy]. Fig. 2 shows that below 4 MW of heating power, the discharges had only small, Type V ELMs [15] and no Type I ELMs. For  $P_{\text{NBI}} \geq 4$  MW, a mixture of Type V and Type I ELMs were observed, with the Type I ELM frequency increasing with  $P_{\text{NBI}}$ . These Type I ELMs individually resulted in a stored energy drop between 4% and 10%, consistent with previous NSTX Type I ELM scaling studies [16]. The impact of the large ELMs on the heat flux profile was modest, however, owing to the long frame integration time of 33.3 ms relative to the typical ELM time scale of 1–2 ms. An analysis window of 110 ms (four camera frames) was used to minimize the impact of the large ELMs on the heat flux profiles. During this time window, it should be noted that the line-averaged density typically increased by 20–25%.

As shown in Fig. 3, the peak heat flux  $Q_{\text{peak}}$  increased with the power flowing into the SOL,  $P_{\text{loss}}$ . Here loss power is defined as  $P_{\text{loss}} = P_{\text{OH}} + P_{\text{NBI}} - dW_{\text{MHD}}/dt - P_{\text{rad}}^{\text{core}} - P_{\text{loss}}^{\text{fast ion}}$ , where  $P_{\text{OH}}$  is

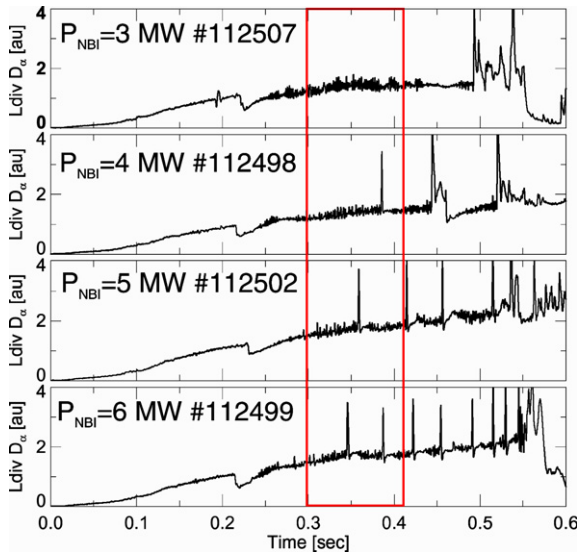


Fig. 2. Dependence of ELM activity on heating power at constant  $I_p = 0.8$  MA. At low heating power, only Type V ELMs are observed. The frequency of type I ELMs increased with the heating power. The time window of the analysis is shown by the red box. (For interpretation of the references in colour in this figure legend, the reader is referred to the web version of this article.)

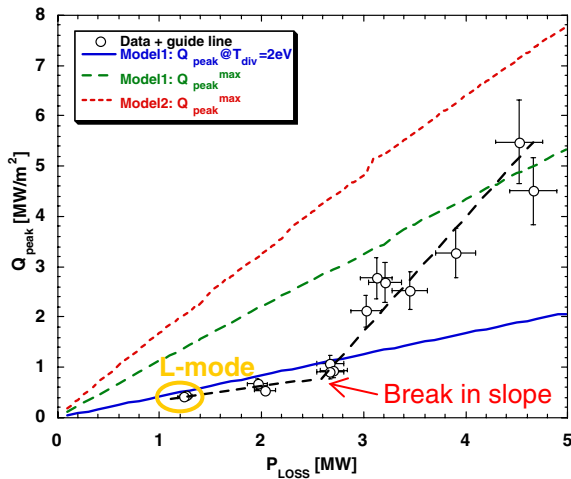


Fig. 3. Dependence of outer divertor peak heat flux (open circles) on SOL loss power. The dashed black lines are lines to guide the eye, and the other lines are predictions from the Borass model (see the text).

the ohmic heating power,  $P_{\text{rad}}^{\text{core}}$  is the core radiated power, and  $P_{\text{loss}}^{\text{fast ion}}$  is the fast ion loss. From our power accounting study [7], we use that  $P_{\text{rad}}^{\text{core}} \sim 0.1(P_{\text{OH}} + P_{\text{NBI}})$  and  $P_{\text{loss}}^{\text{fast ion}} \sim 0.2(P_{\text{OH}} + P_{\text{NBI}})$ . A change in the slope is evident for  $P_{\text{loss}}$  between

2.5 and 3 MW, i.e.  $Q_{\text{peak}}$  began to increase much more quickly. We note that the discharges reverted back to L-mode at the very lowest  $P_{\text{loss}}$  as it was below the H–L threshold at the operating densities in those discharges.

To obtain insight into the experimental trends, these data were simulated with a two-point model of the SOL derived by Borass et al. [17]. While this model was originally proposed to simulate SOL induced density limits in tokamaks, it nevertheless provides a useful framework for the operating window in tokamak and ST SOLs. The model was previously used for DIII-D detachment studies with only minor modifications [18], and the basic implementation for NSTX follows along the lines of that study. In the model equations, the heat flux can be parameterized as a function of assumed divertor temperature, either for a fixed SOL power flux width at the outer midplane or one computed from a cross-field transport scaling, such as Bohm transport. The relevant model inputs used for NSTX are given in Table 1.

Three curves from the two-point model calculations are shown in Fig. 3. The solid blue line<sup>1</sup> corresponds to a fixed SOL upstream heat flux width of 1.5 cm for an assumed divertor temperature of 2 eV, i.e. just above the onset of partial detachment observed in tokamaks [19]. The dashed green line corresponds to the maximum heat flux computed for the entire range of divertor temperatures considered, with the upstream SOL width fixed at 1.5 cm as above. Finally the dotted red line corresponds to the maximum heat flux computed for the range of divertor temperatures considered, with the assumption of Bohm level cross-field transport to self consistently compute the SOL width.

The main difference between the solid green and dashed blue curves originates from the enhanced carbon divertor radiation computed at a divertor temperature of 2 eV, as compared with higher temperatures typically between 20 and 40 eV, where the maximum heat flux is predicted to occur. Practically this difference is realized by variation of the upstream density through fueling variations. The main difference between the dashed green line and the dotted red line is that the SOL width is typically narrowed as the SOL temperature increases, i.e. the predicted SOL heat flux width for Bohm transport

<sup>1</sup> For interpretation of color in Fig. 3, the reader is referred to the web version of this article.

Table 1

NSTX input parameters used for the two-point model results shown in Fig. 3

Major radius (m)	0.86
Minor radius (m)	0.63
Elongation	2.0
Field on axis (T)	0.45
Plasma current (MA)	0.8
Carbon impurity fraction in divertor	0.05
$\alpha_{qL}$ , $\alpha_{DBohm}$	1.1
$q_{cyl}$ (for connection length)	2.0
$\eta$ (fraction of SOL power to low field side)	0.75

shrunk to 1.1–1.3 cm from the assumed fixed width of 1.5 cm in the other cases.

From these calculations, we can judge that the outer divertor was probably close to detachment at the lowest power levels, and that the sharp change in slope corresponds to the onset of the high recycling conduction-limited regime [20], as the SOL moves toward the sheath limited regime. Indeed the peak heat flux was measured to be  $<1 \text{ MW/m}^2$  at the lower power levels, approaching the values observed in radiative and detached divertor studies in NSTX [9]. The fact that the data lie *below* the solid blue line, which represents detachment onset, is perhaps not surprising, given that the power accountability in these discharges was 70% at the higher power levels and down to 60% at the lowest power levels [7]. Including an anomalous power loss of 30–40%, the solid blue line would shift below the data, representing a lower bound as expected.

## 2.2. Outer divertor heat flux scaling with plasma current

The scaling of peak divertor heat flux with plasma current was conducted with constant  $P_{NBI} = 4 \text{ MW}$  over a range of  $0.6 \leq I_p \leq 0.9 \text{ MA}$ . Small variations in  $P_{OH}$  and  $dW_{MHD}/dt$  resulted in a  $P_{loss}$  range between 3.0 and 3.5 MW during the scan. As in the  $P_{NBI}$  scan, all discharges had a secular density ramp during the analysis time window of 0.3–0.41 s.

The time evolution of the lower divertor  $D_\alpha$  is shown in Fig. 4 for representative discharges of the  $I_p$  scan. A tendency toward large ELMs was observed as the  $I_p$  was increased at fixed  $P_{NBI}$ . Small Type V ELMs were also present in all of the discharges.

The outer divertor peak heat flux increased strongly with  $I_p$  from 0.6 to 0.9 MA, as shown in Fig. 5. Correspondingly the heat flux profile width (full-width at half-max value) decreased with

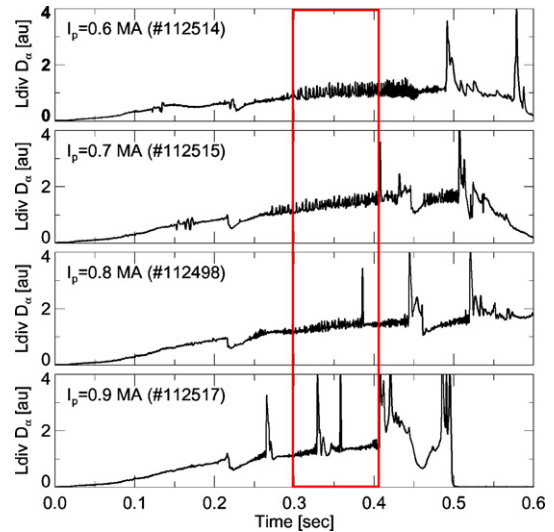


Fig. 4. Dependence of ELM activity on  $I_p$  at constant  $P_{NBI} = 4 \text{ MW}$ . Type I ELMs are observed at  $I_p \geq 0.7 \text{ MA}$ . The time window of the analysis is shown by the red box. (For interpretation of the references in colour in this figure legend, the reader is referred to the web version of this article.)

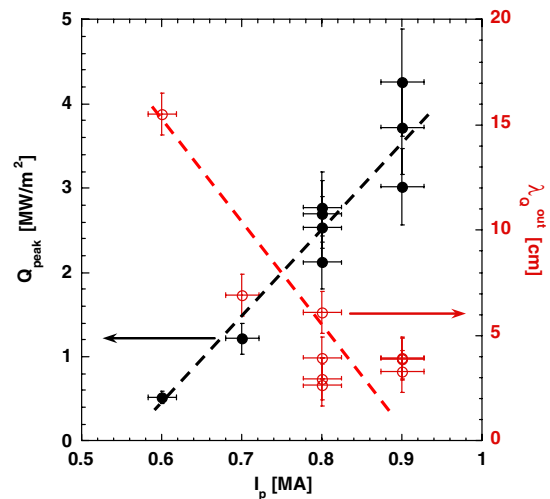


Fig. 5. Dependence of outer divertor peak heat flux and profile width on  $I_p$ . The peak heat flux (width) increases (decreases) rather strongly with  $I_p$ . The black and red dashed lines are placed solely to guide the eye and should not be used to extrapolate the dependencies outside of the dataset ranges. (For interpretation of the references in colour in this figure legend, the reader is referred to the web version of this article.)

increasing  $I_p$  from 0.6 to 0.8 MA. More data are required to determine if the width dependence extends to  $I_p \geq 0.9 \text{ MA}$ . This observed dependence of the peak heat flux and width on  $I_p$  is stronger than suggested by the simple two-point model

discussed above. We note, however, that a strong increase of  $Q_{\text{peak}}$  with  $I_p$  has been previously observed experimentally and reproduced with a model which predicted that the cross-field SOL width would decrease with increasing  $I_p$ , leading to a more peaked profile [21].

### 3. Summary and conclusions

We have presented the first measurements of the scaling of the outer divertor peak heat flux with input power and plasma current in the NSTX. We find that peak heat flux increased with heating power, and that the rate of increase accelerated at the higher power levels. A two-point model was used to simulate the data, from which we conclude that the sharp increase in the dependence can be attributed to the divertor plasma movement into the high recycling regime away from the detachment threshold.

We have also shown that the peak heat flux increased strongly with  $I_p$ , and that the width decreased over most of the available  $I_p$  scan. The dependence is stronger than that predicted by the two-point model if the sole impact of  $I_p$  is on the SOL connection length. More work is required to quantify the impact of the higher  $I_p$  on reducing the SOL cross-field transport, which would naturally lead to a smaller heat flux width.

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