

Supersonic gas jet fueling experiments on NSTX



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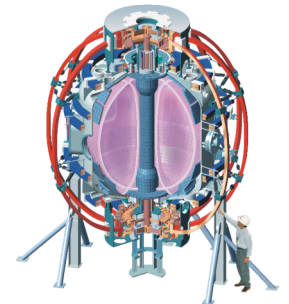
H. W. Kugel, R. Kaita, A. L. Roquemore

Princeton Plasma Physics Laboratory

Boundary Physics ET Meeting

9 February 2005

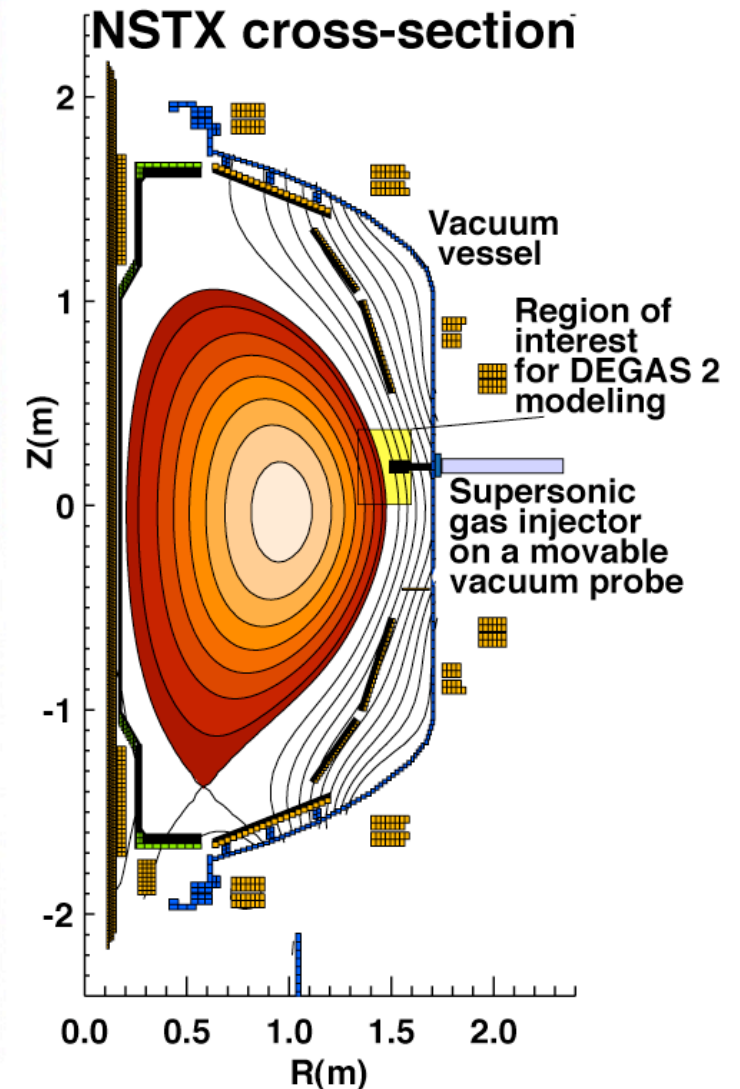
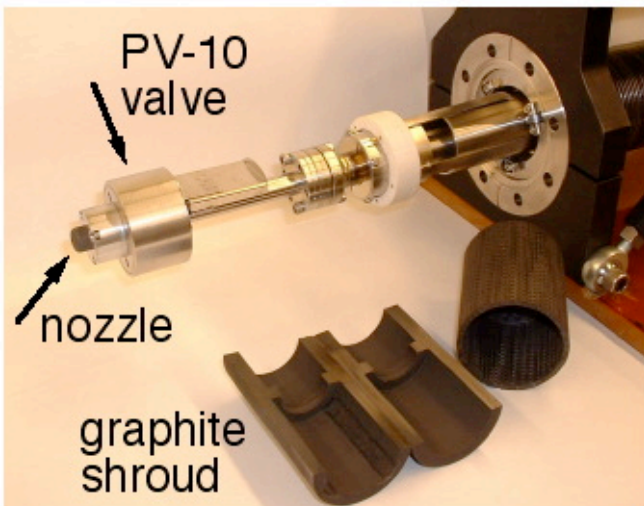
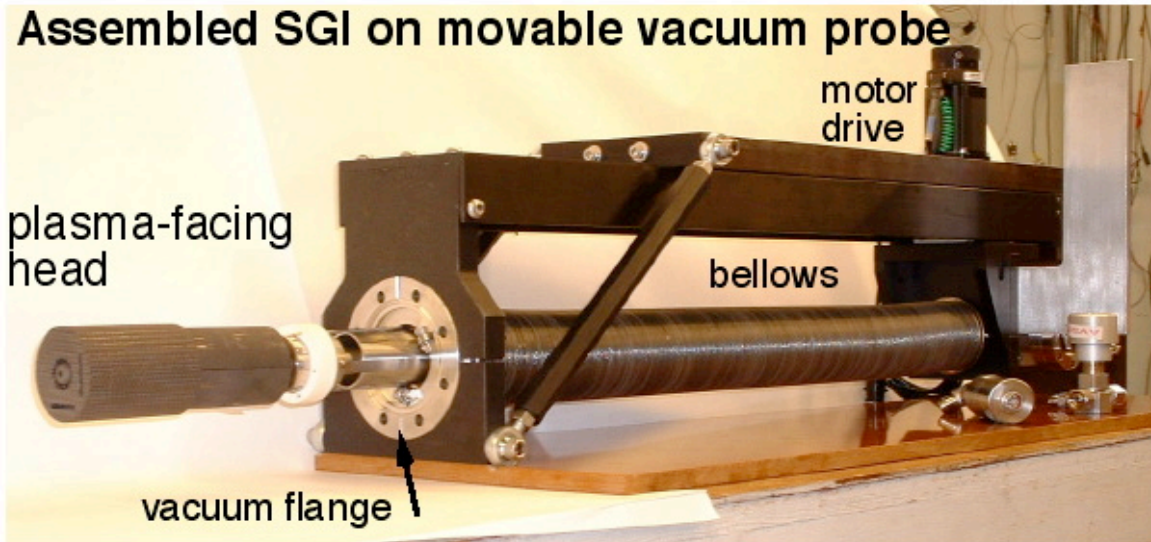
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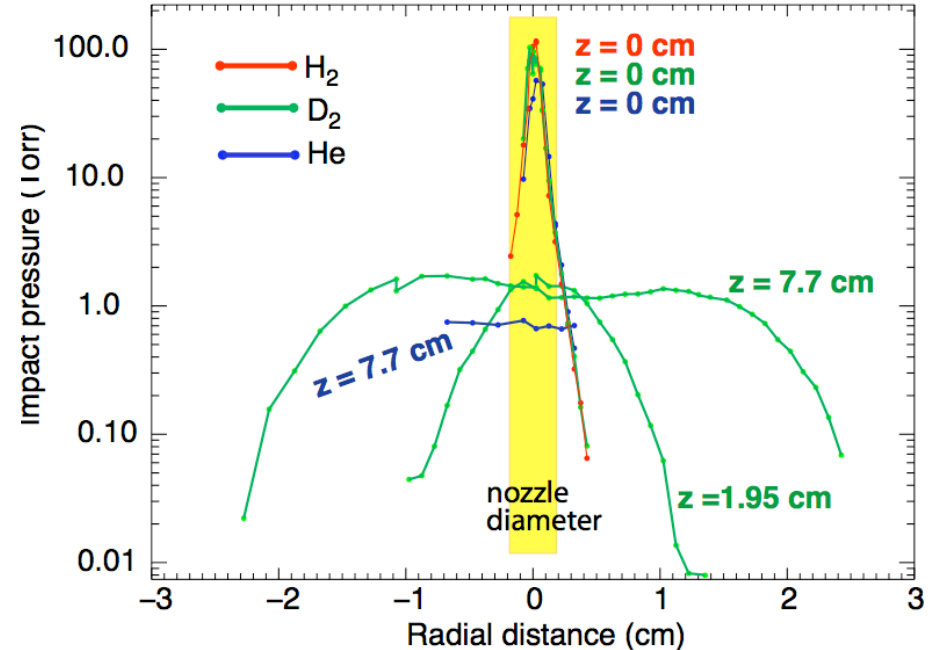
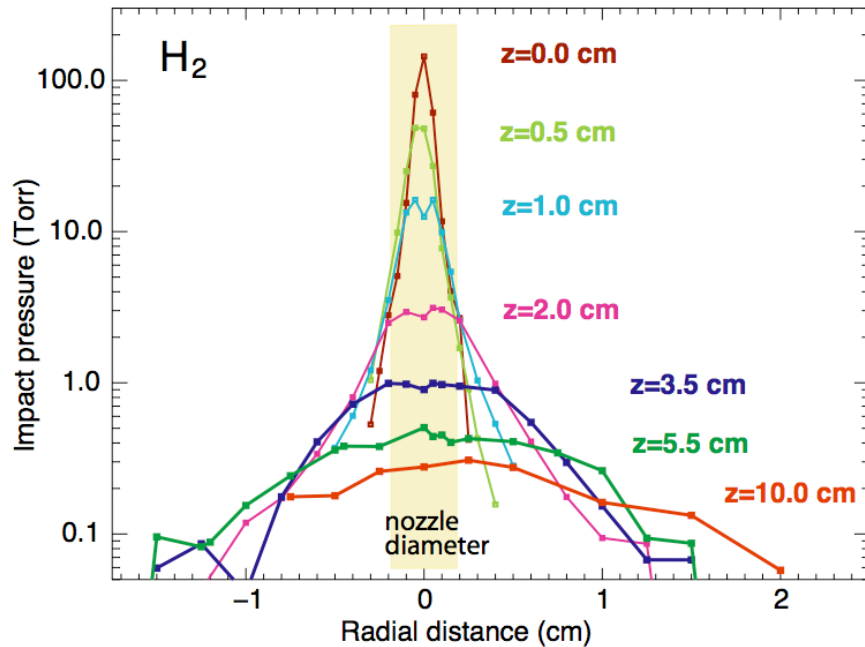
FY'04 status

- XMP-35 “SGI commissioning” successfully completed
- No exp. time was allocated for a physics experiment
- Preliminary results are encouraging: higher fueling efficiency, high gas jet collimation (expect higher wall saturation limit), good SOL penetration, compatibility with H-mode edge

Supersonic gas injector has become operational in FY'04



Off-line pressure measurements confirm high Mach number and highly collimated gas jet shape



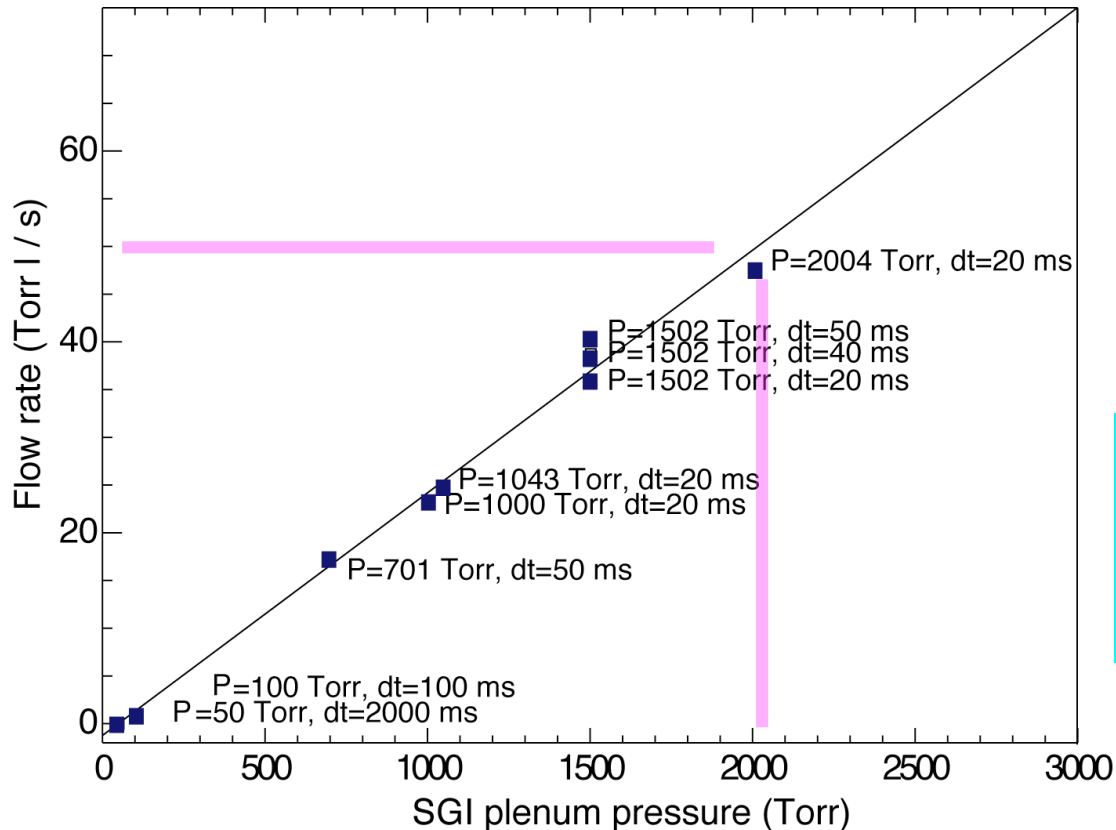
Jet divergence half-angle: 6° - 25°

D₂: $M = 4$, $T \sim 60 - 160 \text{ K}$, $\rho \sim 5 \times 10^{17} \text{ cm}^{-3}$, $Re = 6000$

D₂: $v_{therm} \sim 1100 \text{ m/s}$, $v_{flow} = 2400 \text{ m/s}$

$$u_{max} = \sqrt{\frac{2\gamma}{\gamma-1} \frac{kT_0}{m}}$$

Flow rate is measured *in situ* on NSTX



NSTX gas injector flow rates:

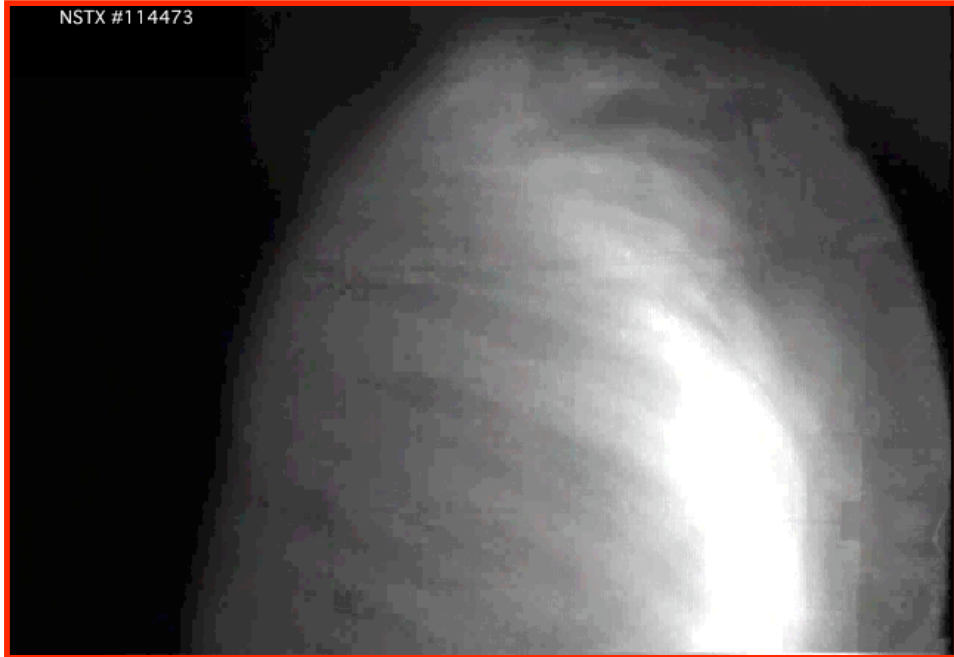
HFS: 10 - 50 Torr l/s

LFS: 20 - 150 Torr l/s

NSTX SGI will be operated at 50 Torr l/s
(= 3.5×10^{21} molecules/s)

- Flow rate (Torr l / s): $\Gamma = V_{NSTX} \Delta P / \Delta t$
- Future SGI may require $P_{plenum} > 2000$ Torr

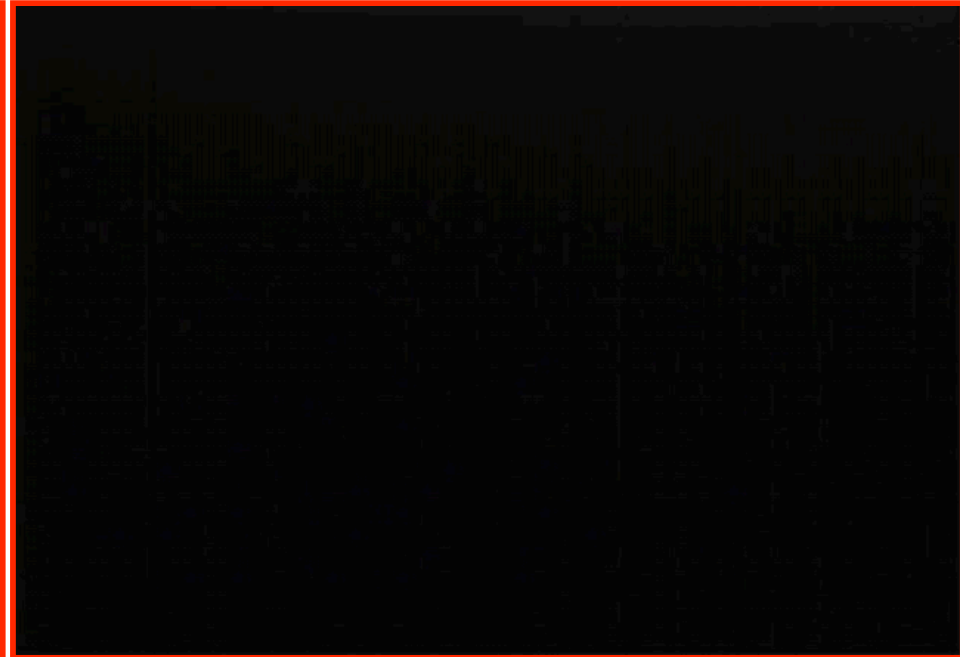
D₂ injections in 4-6 MW NBI heated plasmas (movies)



Shot 114473:

6 MW **high** β plasmas, injection at
 $t=180$ ms

$R_{SGI}=1.604$ m, $Z_{SGI}=0.198$ m
 $R_{sep}=1.49-1.52$ m

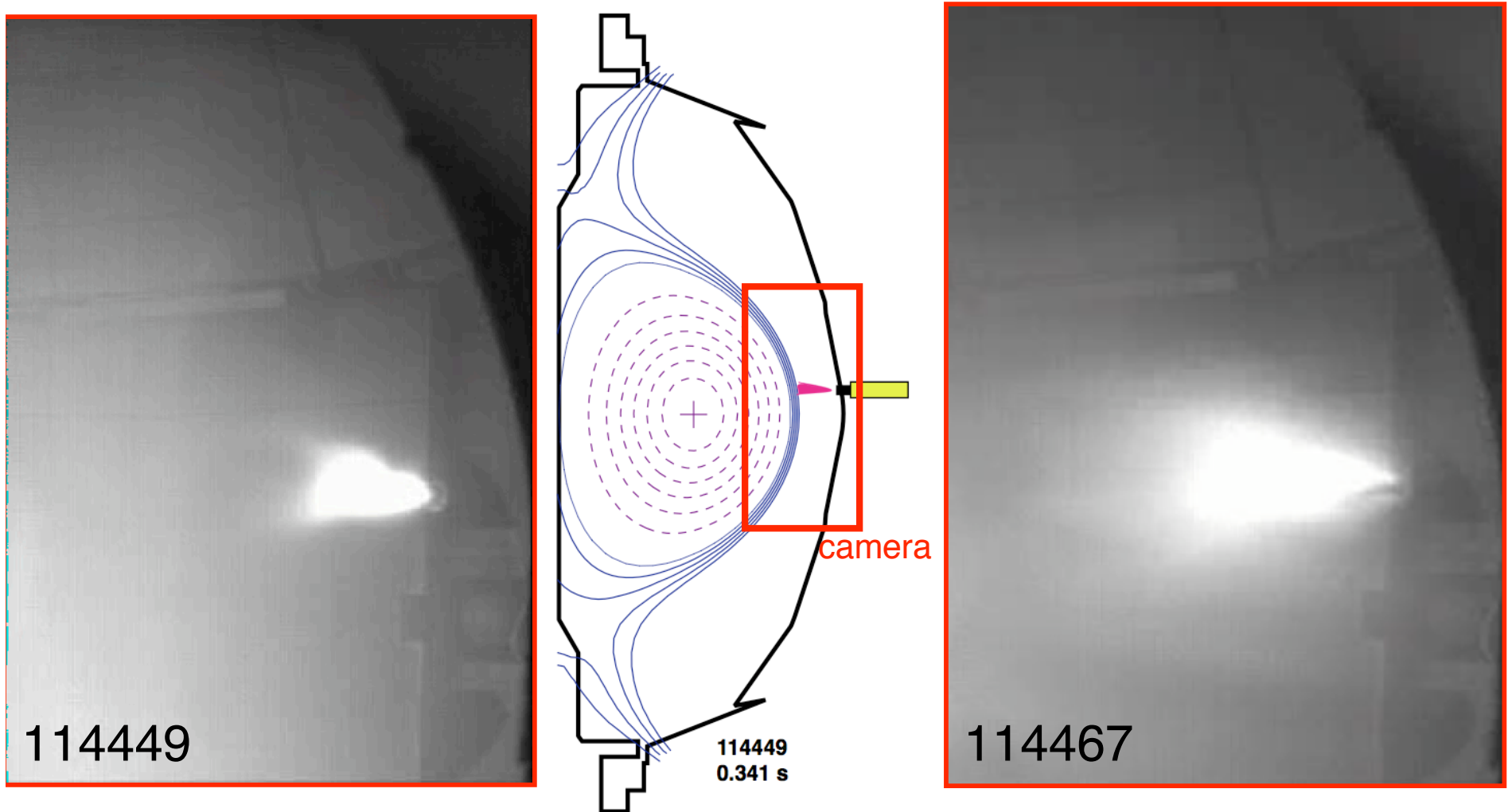


Shot 114475:

4 MW **H-mode** with type 1 ELMs,
injection at $t=300$ ms

$R_{SGI}=1.604$ m, $Z_{SGI}=0.198$ m
 $R_{sep}=1.50-1.52$ m

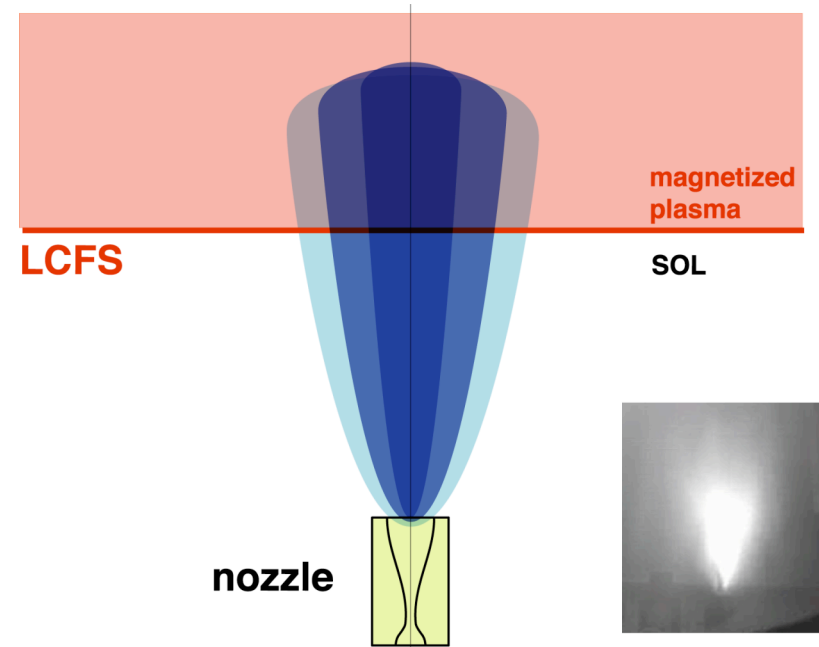
Supersonic gas jet penetrates well through a wide scrape-off layer



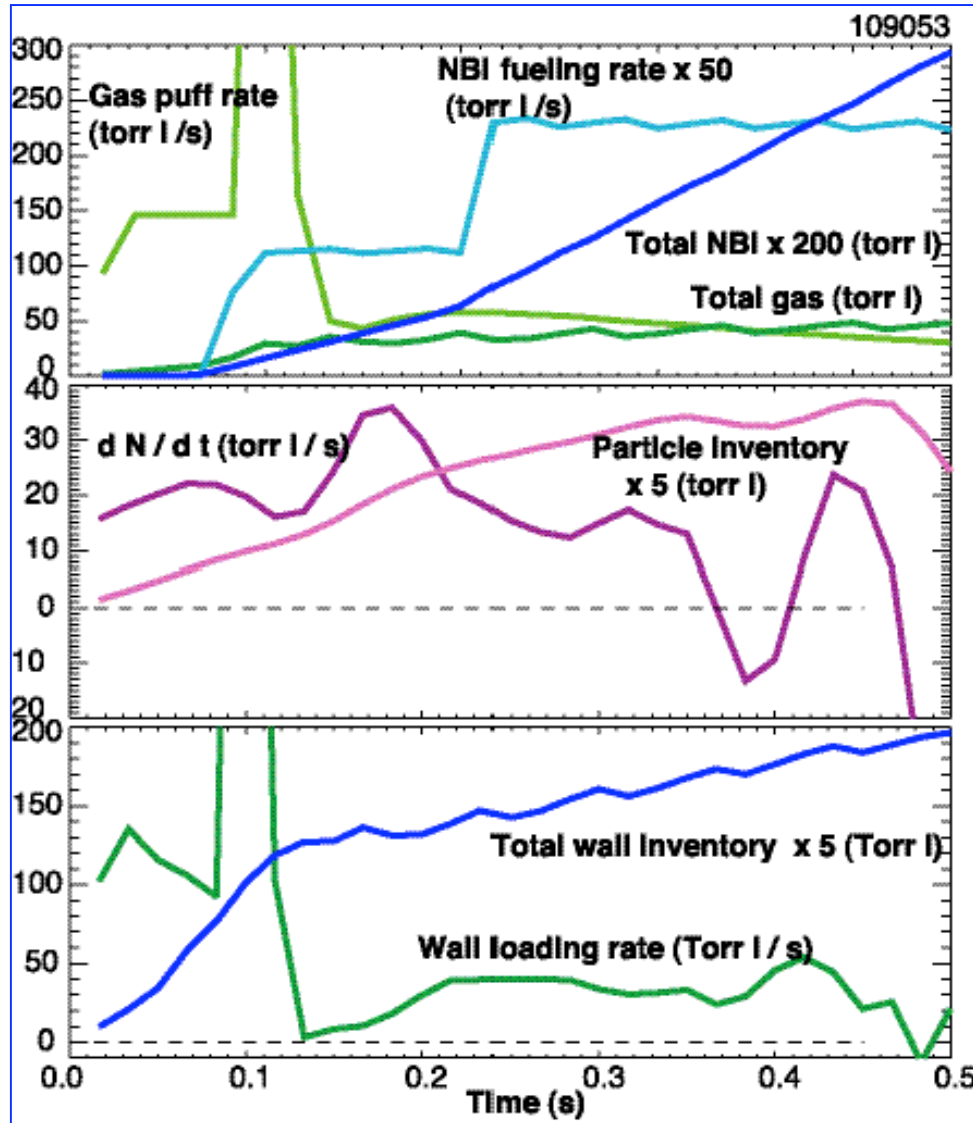
Injection in the end of discharge into a 25 cm SOL
with $T_e < 5$ eV, $n_e < 5 \times 10^{12}$ cm⁻³ plasma

Gas jet penetration mechanism

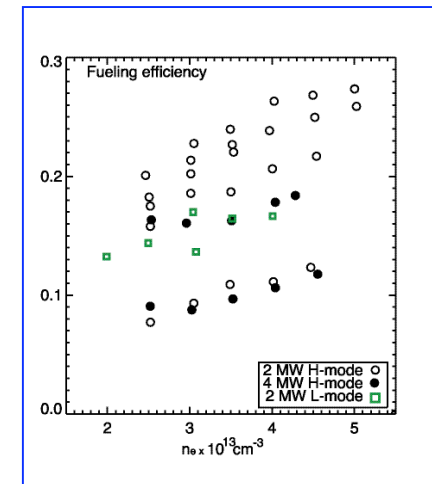
- Single particle model is inapplicable
- Gas jet retains shape due to compressible flow considerations
- Gas jet eventually ionizes and creates a plasmoid
- Gas jet retains cluster-molecular-atomic-ion structure
- SOL/edge electrons with low T_e do not fully penetrate gas jet
- Plasmoid can not penetrate into the magnetized plasma due to insufficient velocity and high plasma kinetic and magnetic pressure
- Modeling must include particle, momentum, energy balance (Braginskii) equations with detailed reaction rates and neutral transport



SGI is an important element in the NSTX density control program



- Conventional gas injector fueling efficiency low (< 0.15)
- High efficiency fueling will help control density in plasmas with recycling control (cryopump or lithium)
- At present recycling flux is $\Gamma_{div} < 5 \times 10^{23}$, $\Gamma_{MC} < 5 \times 10^{22}$ i/s



$$\frac{dN_p}{dt} = \Gamma_{gas} + \Gamma_{NBI} + \Gamma_{NBI_cold} + \Gamma_{NBI_cryo} + \Gamma_{wall} + \Gamma_{pump} + \frac{dN_n}{dt}$$

What we would like to *do* with SGI

- Start-up fueling
- Development of long-pulse fueling scenario -
 - L-mode flat-top fueling
 - H-mode access and flat-top fueling
- ELM control

What we would like to *measure* with D_2

- Fueling efficiency as a function of SGI - LCFS distance

$$\eta = \frac{dN_i / dt}{\Gamma}$$

- Characterize edge plasma conditions (T_e , n_e , n_0 , magnetics, plasma rotation, impurities)
- Determine impact on core plasma performance (τ_e , τ_p , E_{stored})
- Determine impact on wall saturation limit

Fueling experiments with D₂

Ohmic L-mode plasmas

- Set-up an LSN (PF2L) shot (2-3 shots)
 $\kappa=1.8-1.9$, $\delta=0.5$, $drsep=-2$, outer gap 7-10 cm
($R_{LCFS} = 150-154$ cm)
- Scan SGI-LCFS distance by 1 cm (5-8 shots). SGI setup:
100 ms pulse, start at 200 ms
- Do 10 min GDC between shots
- Use SGI instead of Inj#1, #2 for start-up (5 shots)

Aux. Heated L- and H-mode plasmas

- Do a small scan around optimal SGI position
- Do injections into ELM-free H-mode flat-top
- Do injections into ELM-y H-mode

H-mode access with SGI fueling

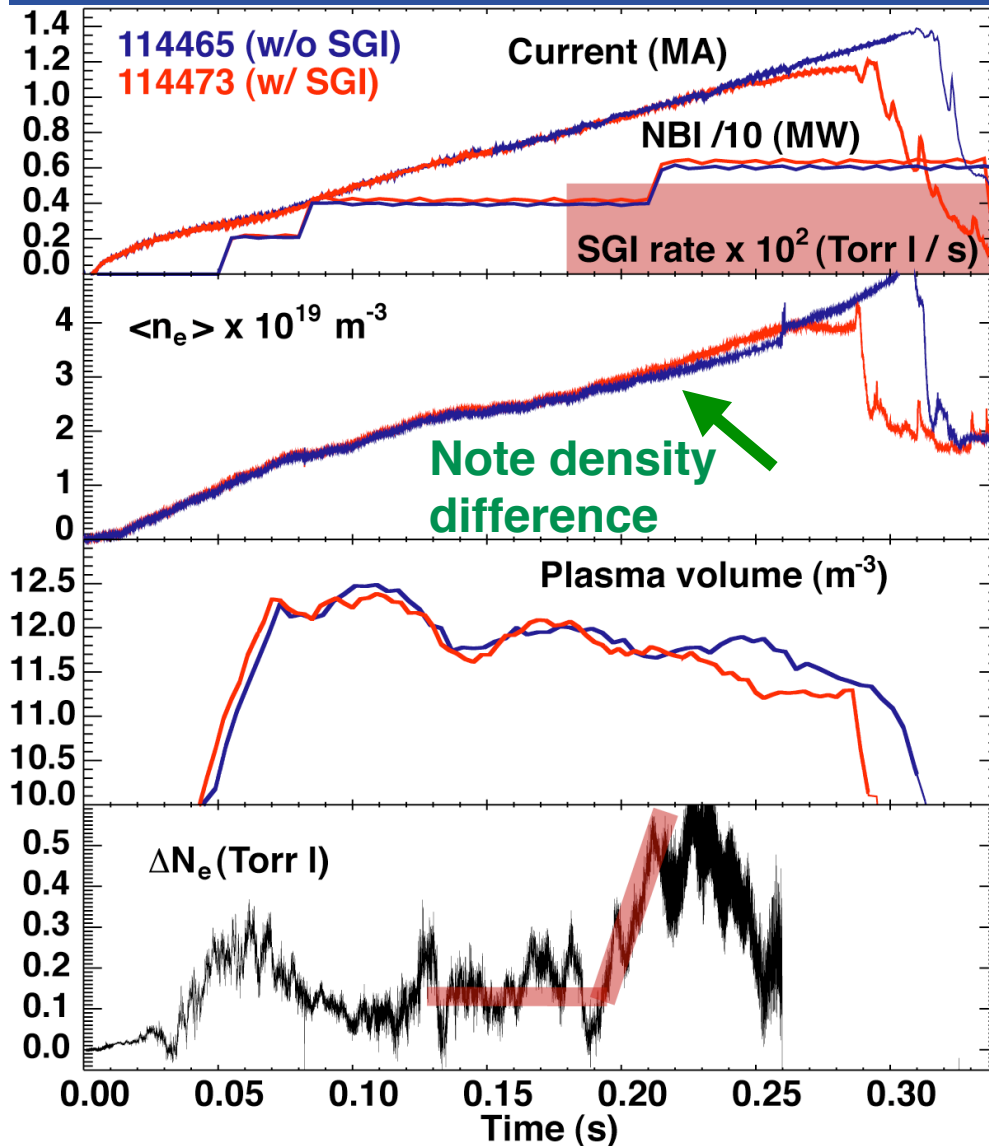
- Poloidal fueling location matters for the historically developed H-mode access scenarios on NSTX (R. Maingi)
- HFS-fueled LSN H-modes are most reproducible, L-H threshold lower (R. Maingi)
- XP 440 “Early H-mode” produced long H-mode plasmas with LFS fueling only. Required every 2nd He conditioning shot and 5+5 min He GDC.
- Use the XP 440 template (112548) and replace the conventional LFS injector with SGI, attempt to reach higher n_e with less gas and less wall saturation
- Inject D₂ in an HFS-fueled LSN H-mode to obtain higher density

ELM control with SGI

- ELM Type I, III, V have been observed on NSTX
- Gas and pellet injection is a proven ELM mitigation technique (change ELM type from I to III, change frequency and amplitude of type III by means of increasing power flow through the edge)
- Use SGI to inject D_2 and/or He to control edge power flow and/or pedestal T_e , n_e , p_e to delay ELMs, or change ELM type

Backup

Supersonic gas jet fueling efficiency η is 3-4 times higher than η of a conventional gas puff



- Compare two 6 MW NBI high- β pulses with and without supersonic gas injection

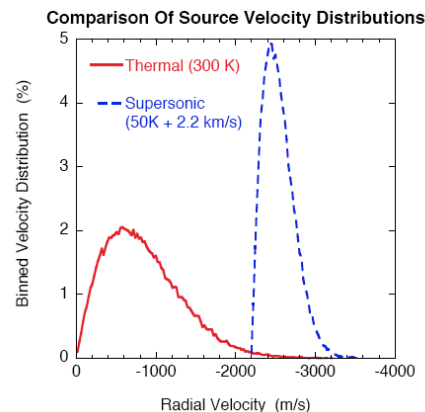
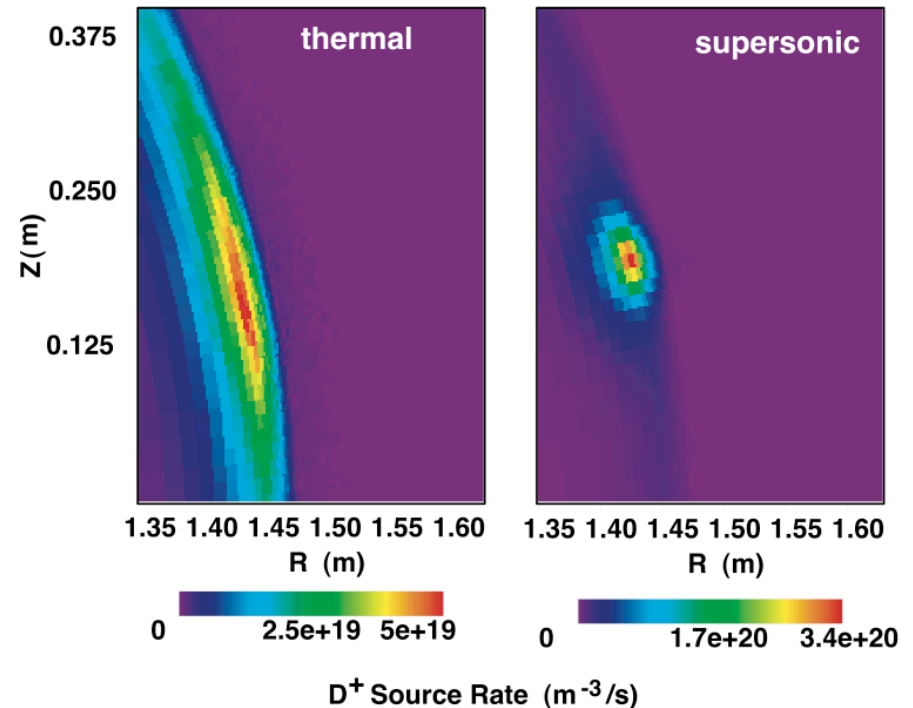
- Fueling efficiency

$$\eta = \frac{dN_i/dt}{\Gamma_{gas}}$$

- $\Gamma_{gas} \sim 50 \text{ Torr l / s}$
- $dN_e/dt = 0.4 / 0.025 = 16 \text{ T l / s}$
- $\eta = 0.3-0.4$
- **Preliminary result - based on one shot**

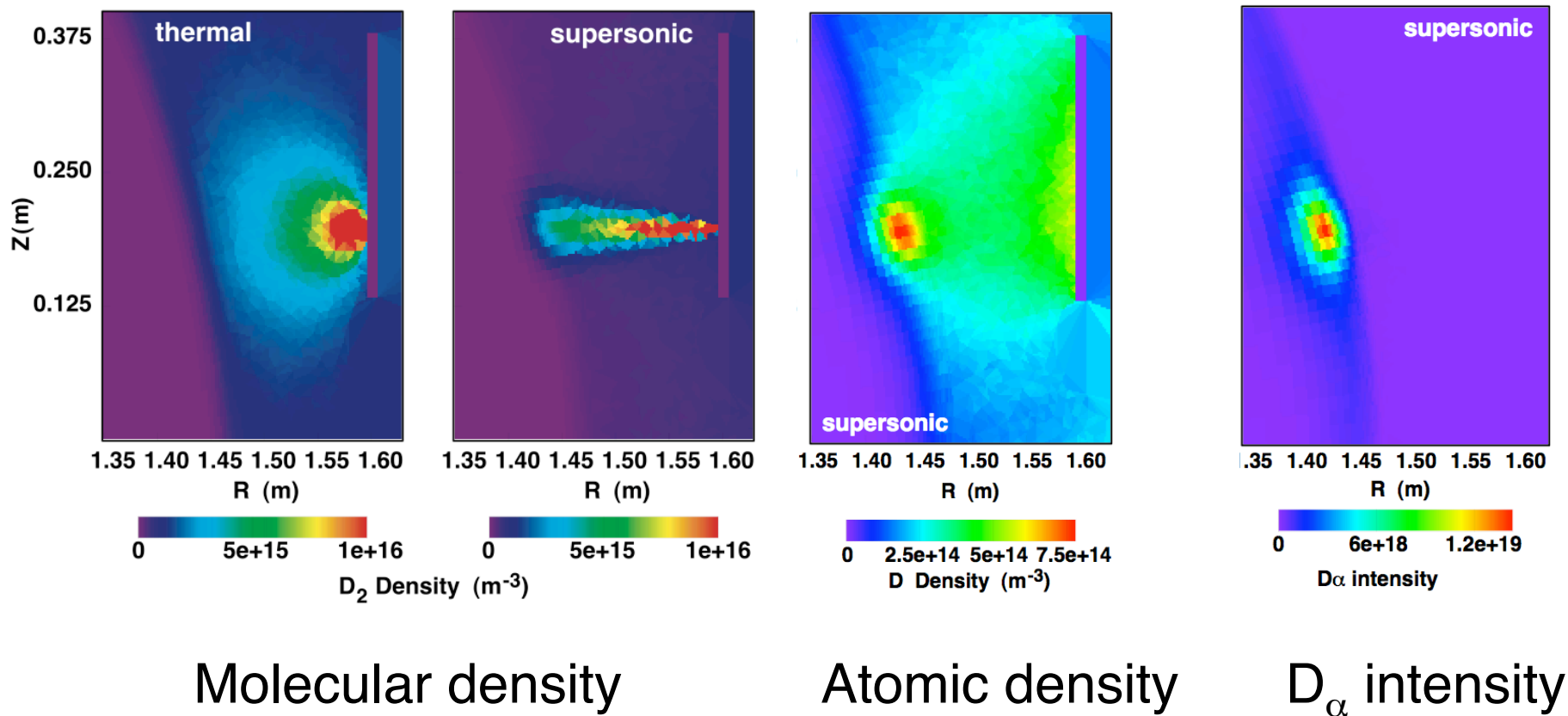
DEGAS 2 neutral transport modeling consistent with general features of supersonic gas injection

- DEGAS 2 neutral transport model
- Conventional D_2 injection:
 $T = 300\text{ K}$
- Supersonic D_2 injector:
 $T = 50\text{ K}$, $v_{flow} = 2200\text{ m/s}$
- Not self-consistent: fixed T_e , n_e are used
- D_2 injected from a 5 mm nozzle
- **Good starting point for experiment interpretation**



DEGAS 2
D. P. Stotler

DEGAS 2 neutral transport modeling consistent with observed features of supersonic gas injection



DEGAS 2
D. P. Stotler