

Institute for Plasma Physics Rijnhuizen

Topic: Millimeter wave technologies for ECE and ECRH



Fourier Transform based ECE systems for Real Time Tearing Mode Control* in Tokamaks[©]

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[©]*This presentation is based on: "FFT based flexible high dynamic range ECE systems for Real Time Tearing Mode Control in Tokamaks" to be published in Review Scientific instruments 2010*

*See also talk B. Hennen et al., "Feedback control of tearing modes through ECRH with launcher mirror steering and power modulation using a line-of-sight ECE diagnostic" at Wednesday 14:00

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Fourier Transform (FT) based ECE systems for Real Time Tearing Mode Control* in Tokamaks

- Definition: FT based ECE system
- Motivation for FT based ECE systems
- Theoretical Characteristics
- Challenge and solution
 - ✓ Implementation of the line-of-sight conventional- and FT-ECE systems on TEXTOR*
 - Proof of principle on TEXTOR, measured by pilot FT System:
 - 1) ECRH scattering
 - 2) ECE emission
- Conclusion and Outlook

*See also talk B. Hennen et al., "Feedback control of tearing modes through ECRH with launcher mirror steering and power modulation using a line-of-sight ECE diagnostic" at Wednesday 14:00.





Frontend at all ECE systems:

ECE RF signal from USB or LSB (by HP or LP filter) down converted by mixers and LO to one or several IF bands and amplified

Conventional ECE system:

IF bands splitted in several smaller 2nd IF frequency bands and fed to video detectors with amplifiers connected to slow ADCs

Fourier Transform ECE system: IF bands are directly digitized by Fast Giga sample ADC's (no video detection and conservation of ECE frequency phase)

✓ Real-time or off-line data processing to extract spectra as function of time









Definition Fourier Transform ECE systems

Example Equivalent **Conventional ECE system: Fourier Transform ECE system:** Local oscillator Local oscillator Corrugated Horn antenna @ 126.6 GHz Corrugated Horn antenna @ 132.25 GHz PIN Notch HP-filter PIN Notch HP-filter Switch 140 GHz 125 GHz Switch 140 GHz 130 GHz Mixer Mixeı 147.5 GHz 2 8~8 144.5 GHz IF: 5.7-21.2 GHz IF: 0-15.5 GHz 141.5 GHz ~ ₩ Notch 3.4 GHz Equalizer Notch ADC FFT 828 .75 GHz 138.5 GHz Ð one ADC æ 0135.5 GHz ~ > 31 Gsample e.g. or alternatively ۲ مر 132.5 GHz 4 ADCs of 8 Gsample and quad splitter, **BPF** Video 3 mixers, amplifiers & B=Detectors LOs 500 MHz & Amplifiers **Only limited nr. of Channels Thousands of Channels** Technische Universiteit iter-n Dr. Waldo Bongers, 16th Joint Workshop FOM DRSCHUNCSZENTRUM

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Conventional ECE:

- With limited channels) Works fine with fixed spatial and temporal resolution
- Observed anomalous ECRH scattering in specific phases of magnetic islands

FT ECE system (to study phenomenon in detail):

- Frequency resolution can be exchanged in trade-off with time resolution of plasma. Possible within the system bandwidth to:
 - ✓ Have flexible time/spatial resolution
 - ✓ Dynamically zoom in on certain plasma positions or plasma events
- ✓ Became possible by recent development of Gsample/s ADCs
- Example: Real time FT spectrometer ECE systems could be used as an adaptive sensor for MHD stability control







Qualifiers of ECE System

$$T_{rec} = T_1 + \frac{T_2}{G_1} + \frac{T_3}{G_1 G_2} + \dots$$

$$T_{sys} = \left(L_{wg} - 1\right) T_0 + L_{wg} T_{rec}$$

$$P_{\min sys} = k_B B_{IF} T_{sys} \sqrt{\frac{2B_{vid}}{B_{IF}}}$$

$$\frac{\Delta T_{ECE}}{T_{av ECE}} = \sqrt{\frac{2B_{vid}}{B_{IF}}}$$

 \succ Video Bandwidth: B_{vid}

Thermal- (& wave)-noise ratio on ECE signal (eg ~few %)

► Relative fluctuation ratio to average ECE: $\sqrt{2B_{vid}} / B_{IF}$

Spatial resolution and range :

 \succ IF Bandwidth: B_{IF}

Total ECE receiver frequency range gives number of channels





Conventional ECE system

Fourier Transform ECE system



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Fourier Transform ECE system



Acquisition for plasma control of FT ECE only feasible through reduction of data flow by blockwise data acquisition: In practice: $N_{aq} < N_{max}$ because idling time, $\tau_i > 0$, is introduced

$$B_{vid} = \frac{1}{2 \tau_{sampling}} \qquad B_{IF} \ge \Delta f = \frac{f_{sample}}{N_{aq}} \qquad P_{\min FTECE} = \frac{k_B f_{sample}}{N_{aq}} \frac{T_{sys}}{N_{aq}} \qquad B_{IF} = n \Delta f \qquad \qquad \frac{\Delta T_{ece}}{T_{av ECE}} = \frac{1}{\sqrt{n}} \qquad \qquad \frac{\Delta T_{ece}}{T_{av ECE}} = \frac{1}{\sqrt{n}} \qquad \qquad \frac{P_{\min FTECE}}{P_{ini conv ECE}} = \frac{\sqrt{T_{sampling}}}{T_{sampling}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min FTECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \frac{1}{2(\tau_{sampling}} + \tau_{idle})} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{N_{aq}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{sampling}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{min Conv ECE}}{T_{sampling}}} = \sqrt{\frac{N_{max}}{T_{sampling}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{min Conv ECE}}{T_{sampling}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} \qquad \qquad P_{min Conv ECE} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}} = \sqrt{\frac{T_{min Conv ECE}}{T_{min Conv ECE}}}} = \sqrt{\frac{T_{min Conv ECE}}{T$$

Practical ECE FT 8 Gsample/s system ADC properties with current proven technology

Time domain samples	Frequency Resolution [MHz]	Spectrum Acquisition time [ns]	Video Bandwidth [kHz]	Maximum Retrigger Frequency [kHz]	ldle Time [ns]	Minimal Power conv. ECE [dB]	Data Transfer [Msample/s]	ΔT _{ECE} T _{av ECE} B _{IF} =250 MHz
80	100	10	50,000	200	4990	-13.5	16	63%
800	10	100	5,000	66.25	14994	-10.9	53	20%
4,000	2	500	1,000	18.75	52833	-10.1	75	8.9%
8,000	1	1,000	500	10	99000	-10.0	80	6.3%
60,000	0.13	7,500	67	1.083	915577	-10.5	65	2.3%
160,000	0.05	20,000	25	0.313	3180000	-11.0	50	1.4%
320,000	0.025	40,000	13	0.125	7960000	-11.5	40	1.0%

interpolated

✓Example:

Suppose NTM rotation 1 kHz Design: B_{IF} = 500 MHz and B_{vid} > 5 kHz

✓ Best Solution:

► Retrigger rate=10 kHz B_{vid} =500 kHz and sum 500 frequency domain samples results $\Delta T_{ECE}/T_{av ECE}$ = 4%

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Noise temperature of ADC

Dependent on:

FT Block size, N (dynamical gain)
Effective number of bits, b (dc)
Sampling window Jitter time, σ
ADC internal amplifier/buffer

SNR (f) = 10 log
$$\left\{ \frac{3 2^{2b}}{2 + 3 (2^{b} 2 \pi f \sigma)^{2}} \frac{N}{2} \right\}$$

$$P_{\min ADC}(f) = \left\{10^{\binom{P_{clip} - SNR(f)}{10}}\right\} / 1000$$

$$T_{ADC}(f) = \frac{P_{\min ADC}(f)}{k_B B_{IF}}$$

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Measurement of Agilent 8 Gsample/s ADC



Effective number of bits is 6.6 of 10 (dc) and the RMS jitter time is about 0.2 ps ADC amplifier/buffer has significant influence at maximum outer frequency limit

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Implementation

In-Line ECE ON TEXTOR



- In line ECE implemented on TEXTOR as sensor for MHD feedback control:
 - ECE is coming from the exact position where the ECRH is deposited: actuator and sensor always aligned
- Anomalous ECRH scattering observed in specific phases of magnetic islands
 - ✓ FT ECE system implemented to study phenomenon in detail: test case for flexible resolution

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Final design of in-line ECE



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Implementation

Diagnostic: New high dynamic range FT receiver system (Double Sideband)



To ADC 8 Gs/s (4 GHz Bandwidth)

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Proof of principle: results measured on TEXTOR Time resolved ECRH Scattered radiation: slow movement of island by Dynamic Ergodic Divertor (DED) Gyrotron IF Frequency [GHz] (LO=140 GHz, B_{lF}=16.53 MH<mark>z</mark>) **I**DED 0.5 signal(s) -5 $> 120 \, dB$ -10 1.5 [dBm] 8k freq -15 domain Power -20 samples 2.5 -25 33 summed 3 -30 3.5 -35 40 0.2 1.6 1.8 0.4 0.6 0.8 1.2 1.4 Time [s] (AT = 1.00 ms)

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Proof of principle: results measured on TEXTOR





Signal quality marginal caused by high conversion loss of the mixer of the FT frontend and TEXTOR operational conditions of the day

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Conclusion and Outlook

New ECE system with direct IF digitization: Fourier Transform ECE

✓ Advantages:

- Flexible time/spatial resolution with optional dynamic zoom on certain plasma positions or events: possible application to adaptive sensing for MHD control
- ✓ Wavelets analysis instead of FT is possible
- ✓ By block-wise data acquisition a reduced minimal detected power compared to conventional systems (~10 dB)
- Limited range (4 GHz) FT system is tested on TEXTOR in line-of-sight concept
 - ✓ Good ECRH scattering
 - Marginal ECE emission measured (due to frontend and operational conditions)
- > Next step to develop full range FT ECE/scatter system for control
 - Minimize idling time and high performance frontend





