

NO1.7 - Error field identification and correction at high β_N in NSTX

College W&M
Colorado Sch Mines
Columbia U
Comp-X
General Atomics
INEL
Johns Hopkins U
LANL
LLNL
Lodestar
MIT
Nova Photonics
New York U
Old Dominion U
ORNL
PPPL
PSI
Princeton U
SNL
Think Tank, Inc.
UC Davis
UC Irvine
UCLA
UCSD
U Colorado
U Maryland
U Rochester
U Washington
U Wisconsin

**J.E. Menard, D.A. Gates, C. Ludescher,
D. Mastrovito, C. Neumeyer, S.A. Sabbagh,
A. Sontag and the NSTX Research Team**

**48th Annual Meeting of the APS-DPP
Wednesday, November 1, 2006
Philadelphia, PA**

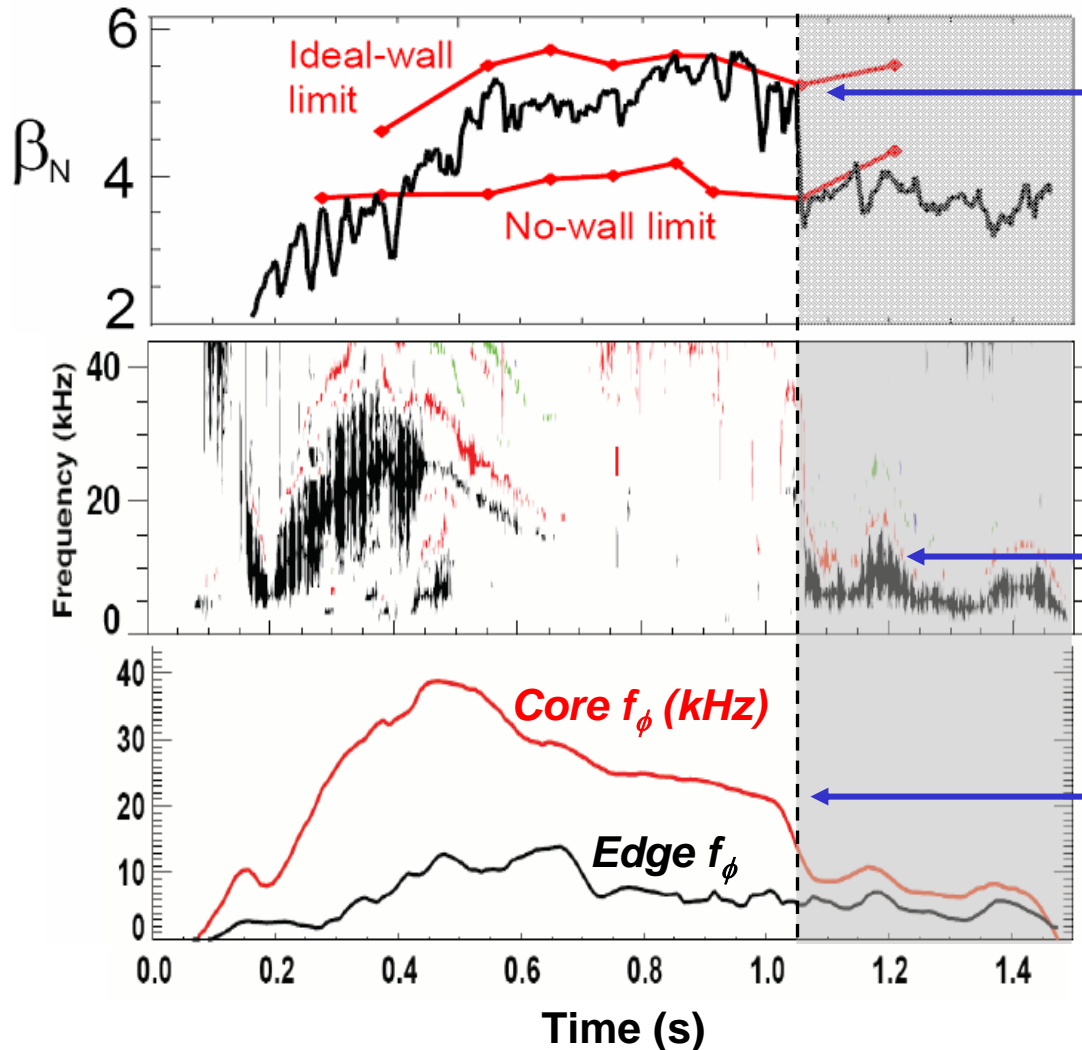
Culham Sci Ctr
U St. Andrews
York U
Chubu U
Fukui U
Hiroshima U
Hyogo U
Kyoto U
Kyushu U
Kyushu Tokai U
NIFS
Niigata U
U Tokyo
JAERI
Hebrew U
Ioffe Inst
RRC Kurchatov Inst
TRINITY
KBSI
KAIST
ENEA, Frascati
CEA, Cadarache
IPP, Jülich
IPP, Garching
ASCR, Czech Rep
U Quebec

Stable operation above the ideal no-wall limit is routinely achieved without any error field correction or feedback control



Co-injected NBI heating up to 7MW $\rightarrow v_\phi / v_A$ up to 0.5 on axis
 \Rightarrow Rotational stabilization of the n=1 RWM

Sontag, PoP **12** (2005) 056112
 Sabbagh, NF **46** (2006) 635
 Reimerdes, PoP **13** (2006) 056107



MSE \Rightarrow repeated excursions above ideal wall limit can trigger saturated core n=1 quasi-interchange modes

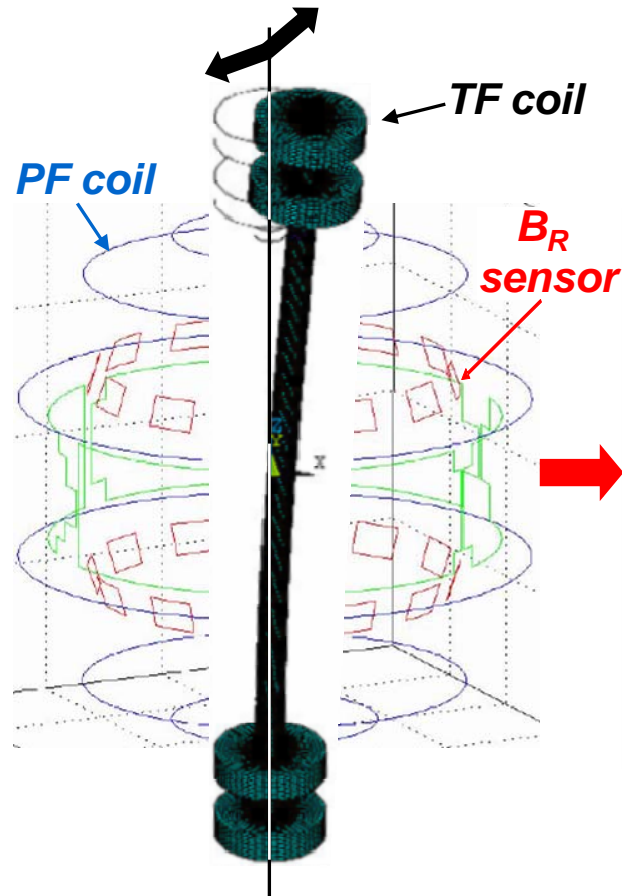
Menard, PRL **97** (2006) 095002

Central rotation is maintained until saturated core n=1 mode flattens the core rotation profile via Neoclassical Toroidal Viscosity

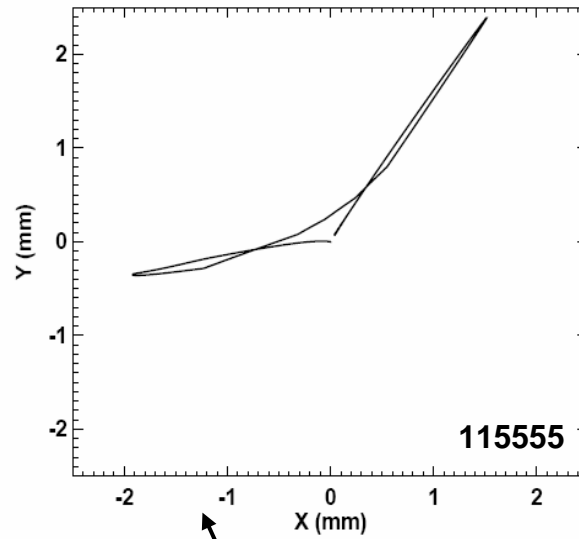
Menard, NF **45** (2005) 539
 Zhu, PRL **96** (2006) 225002

Why bother with error field identification and control for NSTX?

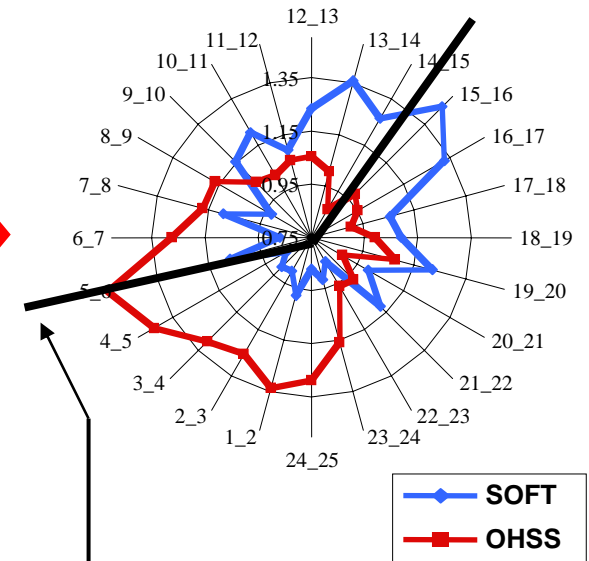
- Some scenarios with lower κ , δ exhibit Ω_ϕ and β_N collapse when $\beta_N > \beta_N$ (no-wall)
- Measure 2-3 Gauss $B_\perp^{2/1}$ EF in LM experiments... what is EF source?
- **Present picture of EF Source:** EF from/near OH leads at top of machine induces TF coil motion relative to B_R sensors (plates, vessel) and thus **the PF coils**



TF coil shift at mid-plane
inferred from B_R sensors
during OH+TF vacuum shot



Normalized TF bottom joint voltage drop from OH+TF test

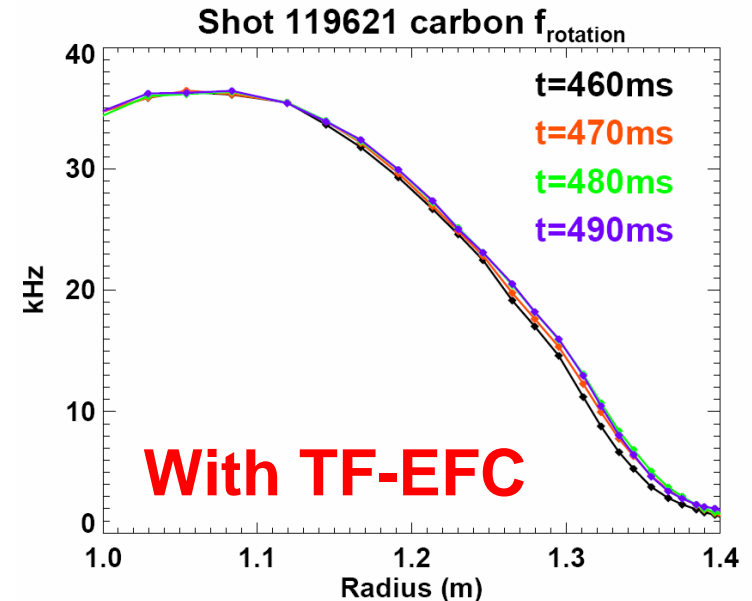
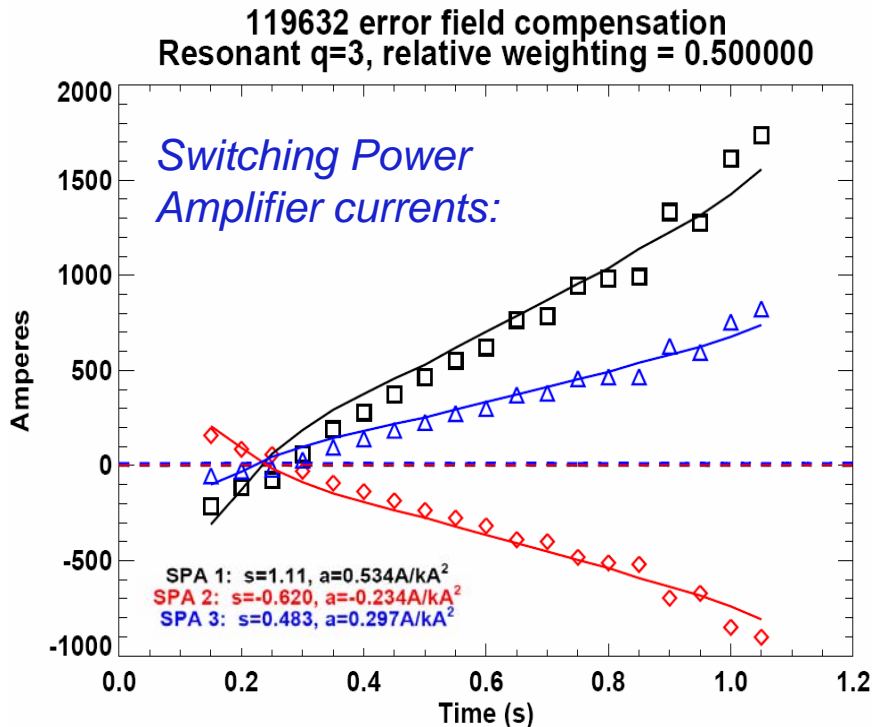
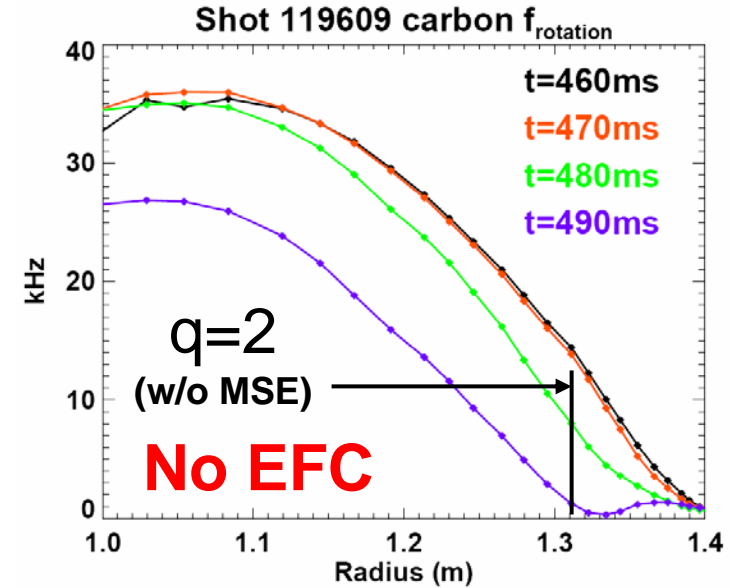


TF flag-joint voltage variation direction consistent with magnetics

Methodology for real-time TF error field correction (TF-EFC)



- Use real-time $I_{OH} \times I_{TF}$, incorporate observed rectification and time-lag of EF
- Empirically minimize rotation damping near $q=2-3$ for 100-200ms of reference shot \rightarrow
 - Extrapolate in time, balance $m=2$ against $m=0$ (**non-resonant!**) of EF from moving TF
 - Correction coefficients must be altered for different $q(\rho, t)$, startup, shape, etc.



Rotation sustainment is a sensitive function of TF-EFC gain

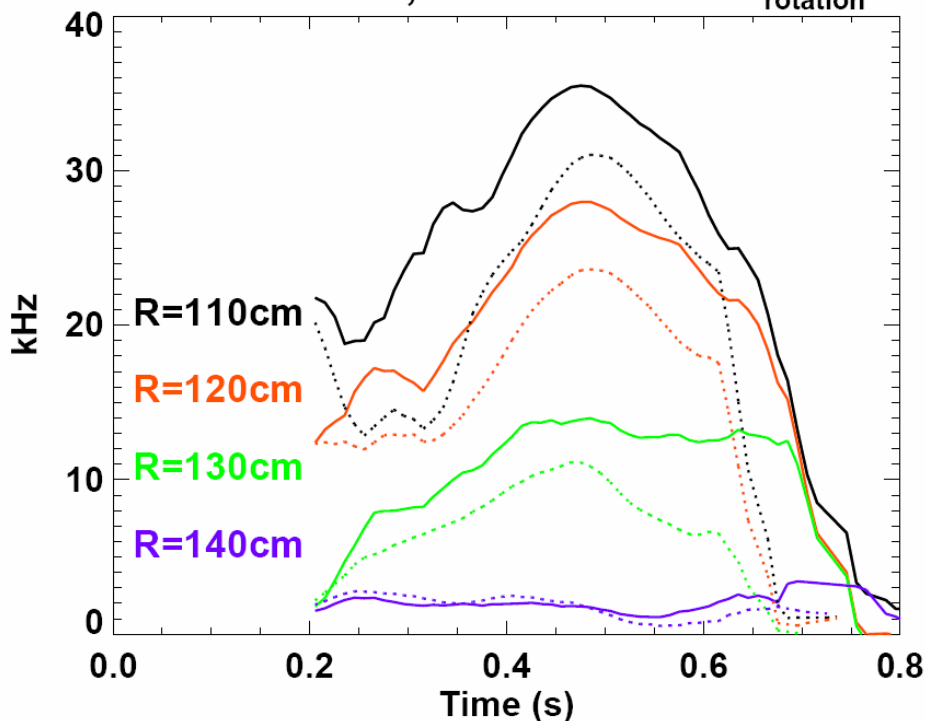


Solid: Optimized TF-EFC gains

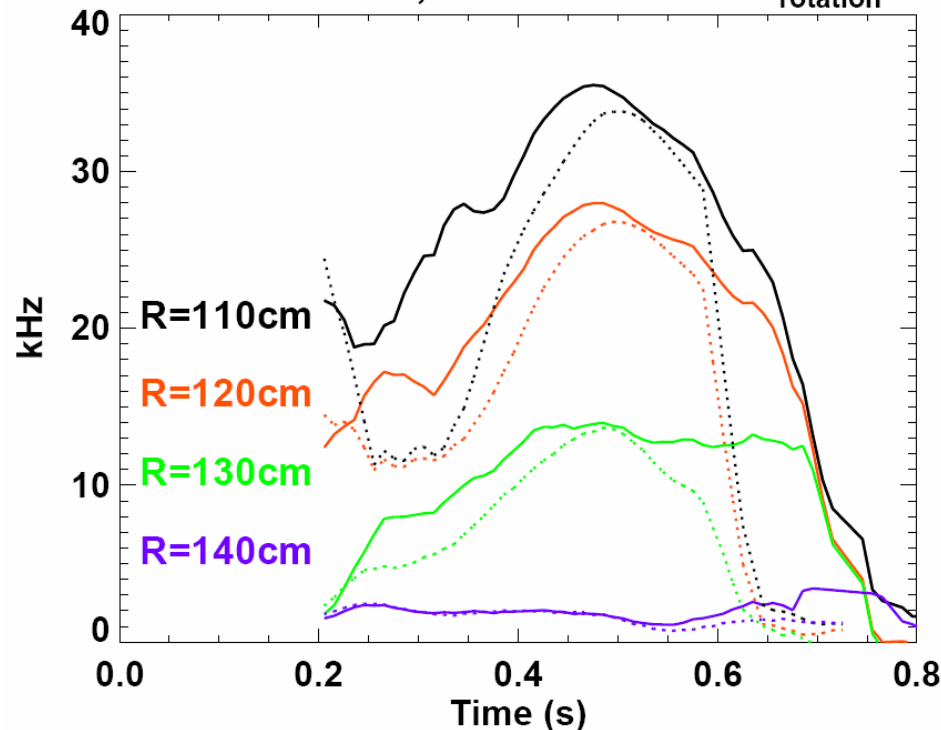
Dashed: Proportional gain
increased 20% above optimum

Dashed: Proportional gain
decreased 20% below optimum

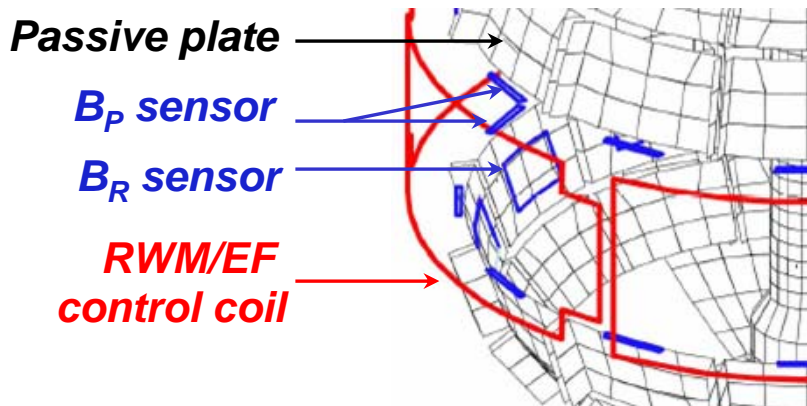
Shot 119649, 119645 carbon f_{rotation}



Shot 119649, 119647 carbon f_{rotation}

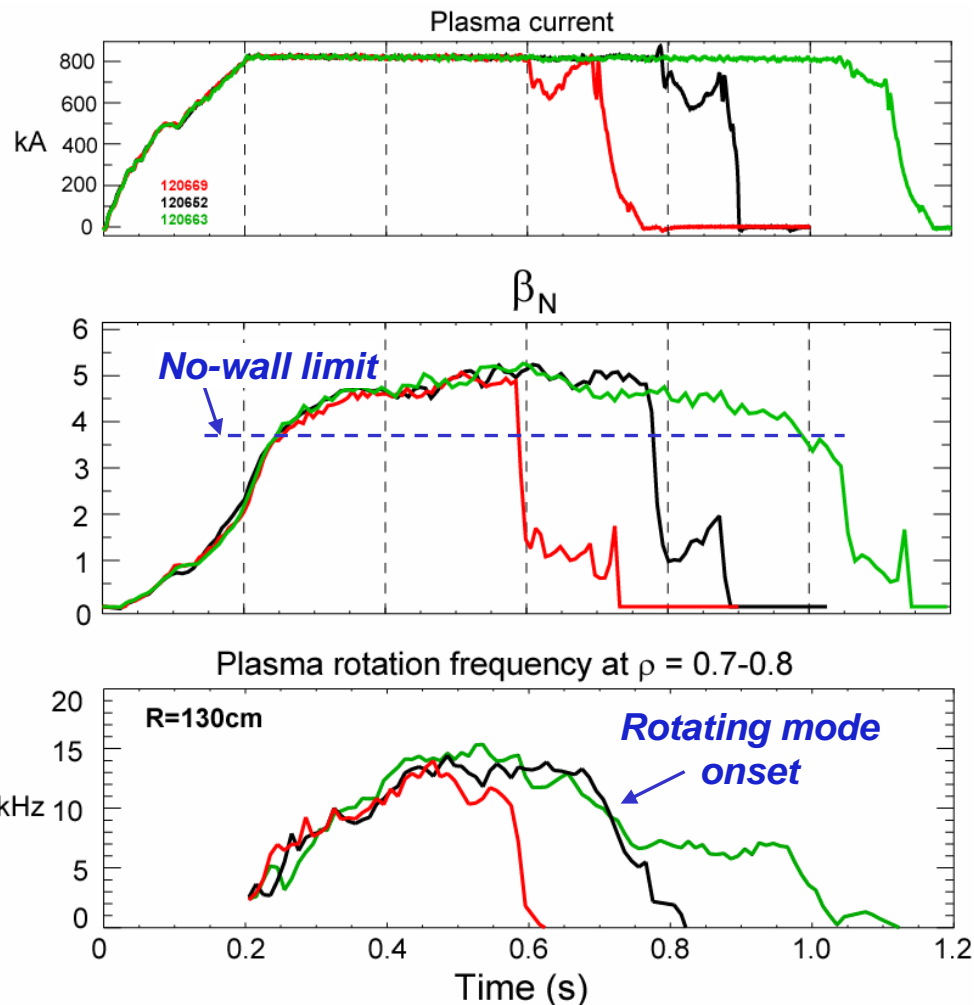


Combination of TF error field correction and n=1 feedback driven by B_p sensors optimizes plasma performance



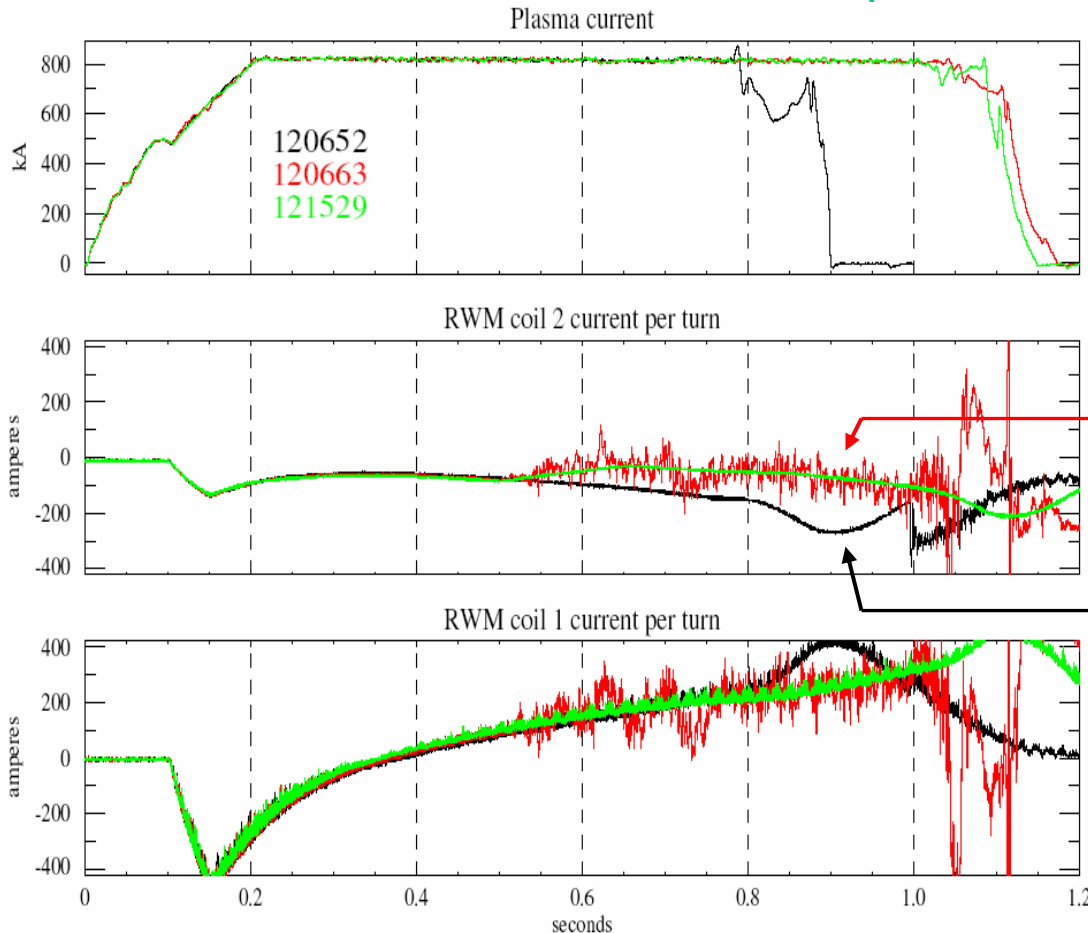
- Mode detection
 - Linear compensation: PF, TF, OH
 - Assume $n=1$ thru 2 modes present
- RWM/EF coil current driven by:
 - Pre-programmed (braking, spectr.)
 - Correction of OHxTF EF
 - Feedback on $n=1$ component of B_p
- Feedback control optimization:
 - Scan phase of $n=1$ B_p wrt coil B_R
 - Scan proportional gain (0.7 optimal)

- No error field control during high β_N phase
- TF-EFC
- TF-EFC + active $n=1$ B_p feedback



Plasma performance from time-averaged SPA currents from feedback equivalent to non-time-averaged currents

- **TF-EFC**
- **TF-EFC + active n=1 B_p feedback**
- **TF-EFC + time-averaged active n=1 B_p feedback**



- β_N , rotation (not shown) similar with and w/o time-averaging of coil currents
 - Green shot EFC currents pre-programmed \Rightarrow
 - n=1 RWM is stable
 - Stabilized by sustained Ω_ϕ
- **Feedback on n=1 B_p changes EFC amplitude and phase relative to TF-EFC alone**
 - TF EF model known to lose accuracy late in shot
 - Modification of RFA (and hence EFC) from β variation also possible

Summary

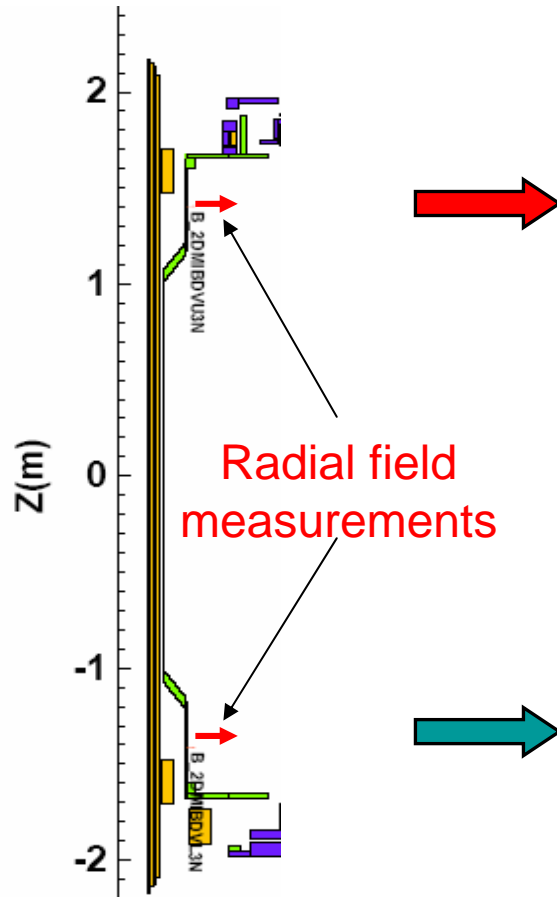


- OH lead-area EF tilts TF bundle several mm → $n=1$ EF in vessel
- TF-EFC yields 50% increase in duration above no-wall limit
- Implemented real-time low-f mode-ID and $n=1$ B_p feedback
- Optimized phase and gain, compared and added to TF-EFC
 - **$n=1$ feedback alone not (yet) robust**
 - **$n=1$ feedback + TF-EFC doubles flat-top duration above no-wall limit**
 - Time-averaged control currents give same response → RFA suppression
- Future work:
 - Attempt to reduce OH error field and/or better constrain TF motion
 - Incorporate non-linear TF motion to improve TF-EFC late in discharge
 - Incorporate up + down and $B_R + B_p$ sensors for improved mode-ID
 - Study full plasma response to EF with DCON/IPEC (**J. Park – QP1.29**)

Backup Slides

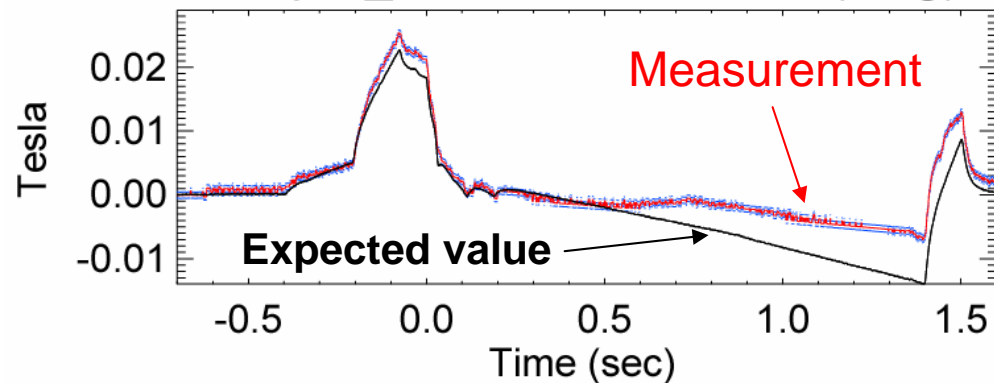
Radial field measurements at ends of solenoid imply TF tilts and is approximately fixed at bottom of machine

- Vacuum shot: OH waveform from 800kA discharge (constant TF)
- **Upper field significantly different than expected \Rightarrow 50-70G local EF**
- **Field at bottom close to expected value \rightarrow small relative motion**



Radial field measurements

B-loop B_2DMIBDVU3N field (tang)



B-loop B_2DMIBDVL3N field (tang)

