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Plasma performance improvements from optimized error field correction in NSTX

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Abstract

The active suppression of n=1 resonant field amplification (RFA) of intrinsic error fields was previously shown to lead to pulse length extension at high beta in NSTX. The correction of intrinsic n=3 error fields was also found to maintain/increase plasma rotation near the plasma boundary resulting in further pulse length extension for operation above the no-wall limit. More recently, the optimal n=3 error field correction (EFC) was determined as a function of plasma current indicating that n=3 intrinsic EF is most likely related to the PF or TF coil system rather than the OH coil as is the case for the n=1 intrinsic EF. Importantly, n=2 error fields were also investigated and measured to be small, indicating odd-n (n=1 and 3) EFs are most prominent in NSTX. Finally, the time response of the n=1 RFA suppression has been optimized by optimizing the low-pass filtering and proportional gain to more robustly control n=1 RFA and unstable n=1 RWMs. Overall, the combined n=3 EFC and n=1 RFA and RWM control has been instrumental in reliably increasing the duration of operation above the no-wall limit. This improved control was used in achieving record pulse-lengths on NSTX and is being applied to a wide range of operating scenarios in NSTX.

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Effective EF and RWM control relies heavily on robust detection of small (~1G) non-axisymmetric magnetic fields

- NSTX has powerful low-f mode detection capabilities:
 - -54 sensors, 2 components of B:
 - 30 radial (B_R) and 24 poloidal (B_P)
 - 6 B_R's are ex-vessel saddle coils
 - Toroidal mode-numbers n=1, 2, 3
 - Only n=1 used in real-time thus far
- Several RWM/EF sensor combinations used:
 - $-B_{P-U} + B_{P-L}$
 - $-B_{R-U} + B_{R-L}$
 - $-B_{P-U} + B_{P-L}$ with spatial offset
 - All sensors in combination
- $B_{P-U} + B_{P-L}$ described here



VALEN Model of NSTX (Columbia Univ.)

The NSTX low-frequency mode detection system has been instrumental in identifying vacuum error fields

Error field detection & correction timeline:

- 2001 Primary vertical field coil (PF5) identified as n=1 EF source, and was corrected in 2002 → sustained high β
- 2006 Determined force (from OH leads) at top of machine induces TF coil motion 1-2 mm at midplane relative to PF coils
 → n=1 B_R EF at outboard midplane
- 2007 shimmed TF w.r.t. OH to minimize relative motion of OH and TF
 - <u>n=1 EF reduced, but not eliminated</u>
- 2007-2008 identified n=3 intrinsic EF, find no evidence of significant n=2 EF





n=1 EF from TF coil motion is $\propto I_{OH} \times I_{TF}$, but has additional time lags and non-linearities which complicate correction





At high β , EF correction can aid sustainment of high toroidal rotation needed for passive (rotational) stabilization of the RWM



- Use real-time $I_{OH} \times I_{TF},$ incorporate observed time-lag and non-linearity of EF
- Empirically minimize rotation damping near q=2-3 for 100-200ms of reference shot
 - Extrapolate in time, balance m=2 against m=0 (*non-resonant!*) of EF from moving TF
 - Correction coefficients must be altered for different q(ρ,t), startup, shape, etc.



Optimized B_P sensor usage improves detection of low-f n=1 mode, enabling improved feedback suppression of RFA and RWMs



Optimal shift increases n=1 signal / baseline by 2-3 \times \rightarrow higher stable feedback gain

Using optimized B_P sensors in control system allows feedback to provide most/all n=1 error field correction at high β

- Previous n=1 EF correction required a priori estimate of intrinsic EF
- Additional sensors \rightarrow detect modes with RWM helicity \rightarrow increased signal to noise
- Improved detection → higher gain → EF correction using <u>only feedback on RFA</u>

EFC algorithm developed in FY07:

- Use time <u>with minimal intrinsic EF</u> and RWM stabilized by rotation
- Intrinsic Ω_φ collapse absent in 2007
 → purposely apply n=1 EF to reduce rotation, destabilize RWM
- Find corrective feedback phase that reduces applied EF currents
- Increase gain until applied EF currents are nearly completely nulled and plasma stability restored
- Then turn off applied error field (!)



→ Use same gain/phase settings to suppress RFA from intrinsic EF **and** any unstable RWMs

2008: n=1 feedback gain and low-pass filter time-constant optimized at high current I_P= 1.1MA

- Instead of applying known n=1 EF, used OHxTF EF
 - 1.1MA uses full OH swing
- Use B_P U/L averaging and include n=3 EFC
- Increased gain scan by factor of 3: from 0.7 → 2
 - Response to n=1 RFA from OH×TF error field changes very little for $G_P > 1$
 - System marginally stable at G_P = 2 for τ_{LPF} as low as 1-2ms
- Optimal control parameters:
- $G_P = 1-1.5, \tau_{LPF} = 2-5ms$

$G_{P} = 1.5, \tau_{LPF} = 50ms$ $G_{P} = 2.0, \tau_{LPF} = 5ms$



Correction of intrinsic n=3 error fields important at high β_N



- Pulse-length depends on polarity of applied n=3
 - Anti-corrective polarity disrupts I_P and β
- Plasmas operate above n=1
 no-wall limit → RFA

– slows rotation \rightarrow

- destabilizes n=1 RWM
- Correction current magnitude for n=3 similar to that for n=1 correction
 - Applied n=3 $|B_R|$ is \approx 6G at outboard midplane
 - Fortuitous phase match between intrinsic n=3 EF and field coils can apply
- Assessing n=3 EF sources...

• n > 1 error fields not commonly addressed in present devices, or in ITER

2008: Attempt to determine source of n=3 error field

Method: Assess n=3 error field vs. vertical field (PF5 coil), toroidal field



Pulse length is unreliable guide for optimal EF correction





Method utilized to determine optimal n=3 correction

- Compute total plasma angular momentum
 Use up to 5 kinetic profile time-slices before collapse
- Fit angular momentum data vs. correction coil current – Fit to quadratic and cubic function of correction coil current

Total plasma angular momentum:

 $\mathcal{L}_{plasma} \equiv \int \rho_{mass}(\psi) \,\Omega_{\phi}(\psi) \,R^2 \,dV$



Optimal n=3 error field correction fit for lower I_P, lower B_T



()) NSTX

Optimal n=3 error field correction fit for lower I_P, higher B_T



Optimal n=3 error field correction fit for higher I_P, higher B_T



Assessment of most probable n=3 error field source



- Conclusions:
 - Most probable source of n=3 EF is vertical field (PF5), but TF is also possible source
 - Phase of intrinsic n=3 EF cannot be determined further EFC optimization possible
 - Torque variation with I_{RWM} consistent with δB^2 dependence \rightarrow consistent with NTV

No significant n=2 intrinsic error field identified

- Shot duration and duration of high β_N and rotation reduced with applied n=2
- Results independent of phase & amplitude for 0.5kA, 1kA \rightarrow n=2 intrinsic EF < 500A



() NSTX

APS-DPP 2008 - Optimized EFC in NSTX (J. Menard)



n=3 EFC + n=1 feedback was successfully applied to wide range of plasma current = 0.75-1.1MA

• Pulses run reliably until nearly all OH flux is consumed



Optimized n=3 EFC + n=1 feedback + Lithium → record NSTX pulse-lengths

- Flux consumption reduced following LITER experiments
 - Lower V_{LOOP} at lower P_{NBI}

- Li + optimized EFC \rightarrow
 - Avoid late n=1 rotating mode
 - Rotation sustained
 - $\beta_{\text{N}} \geq$ 5 sustained 3-4 τ_{CR}
 - record pulse-length = 1.8s





n=3 error correction combined with n=1 RFA/RWM feedback control increases β and rotation, and extends pulse



- Non-axisymmetric feedback algorithm has been developed using unique feedback training scheme
 - Prevents onset of MHD modes
 - Plasma rotation is maintained throughout discharge
 - Control statistically raises β and increase pulse length

Pulse averaged β_N vs. current flat-top





Probability of long pulse and <β_N>_{pulse} increases significantly with active RWM control and error field correction



- Standard H-mode operation shown
 - I_p flat-top duration > 0.2s (> 60 RWM growth times)
- Control allows $<\beta_N >_{pulse} > 4$ - β_N averaged over I_p flat-top

Conclusions

- Extensive non-axisymmetric magnetic sensor array useful for detecting and correcting intrinsic n=1 error fields
- Dominant n=1 error field results from TF bundle motion from electromagnetic interaction between OH and TF coils
- Gain and low-pass filter optimization of n=1 active feedback control successfully suppresses resonant field amplification (RFA) of n=1 EF and unstable RWMs
- n=3 intrinsic error field adversely impacts high-beta operation, and is most likely associated with vertical field coil
- No evidence (yet) of significant n=2 intrinsic error field
- Combination of n=3 EF correction + n=1 active feedback control improves plasma performance for a wide range of conditions: sustained high rotation, $\beta \rightarrow$ record pulse duration



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