



# Role of plasma edge region in global stability on NSTX\*

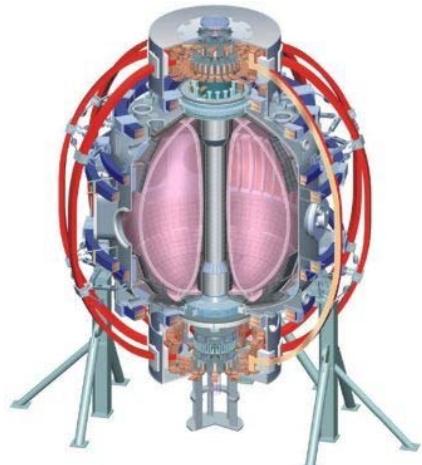
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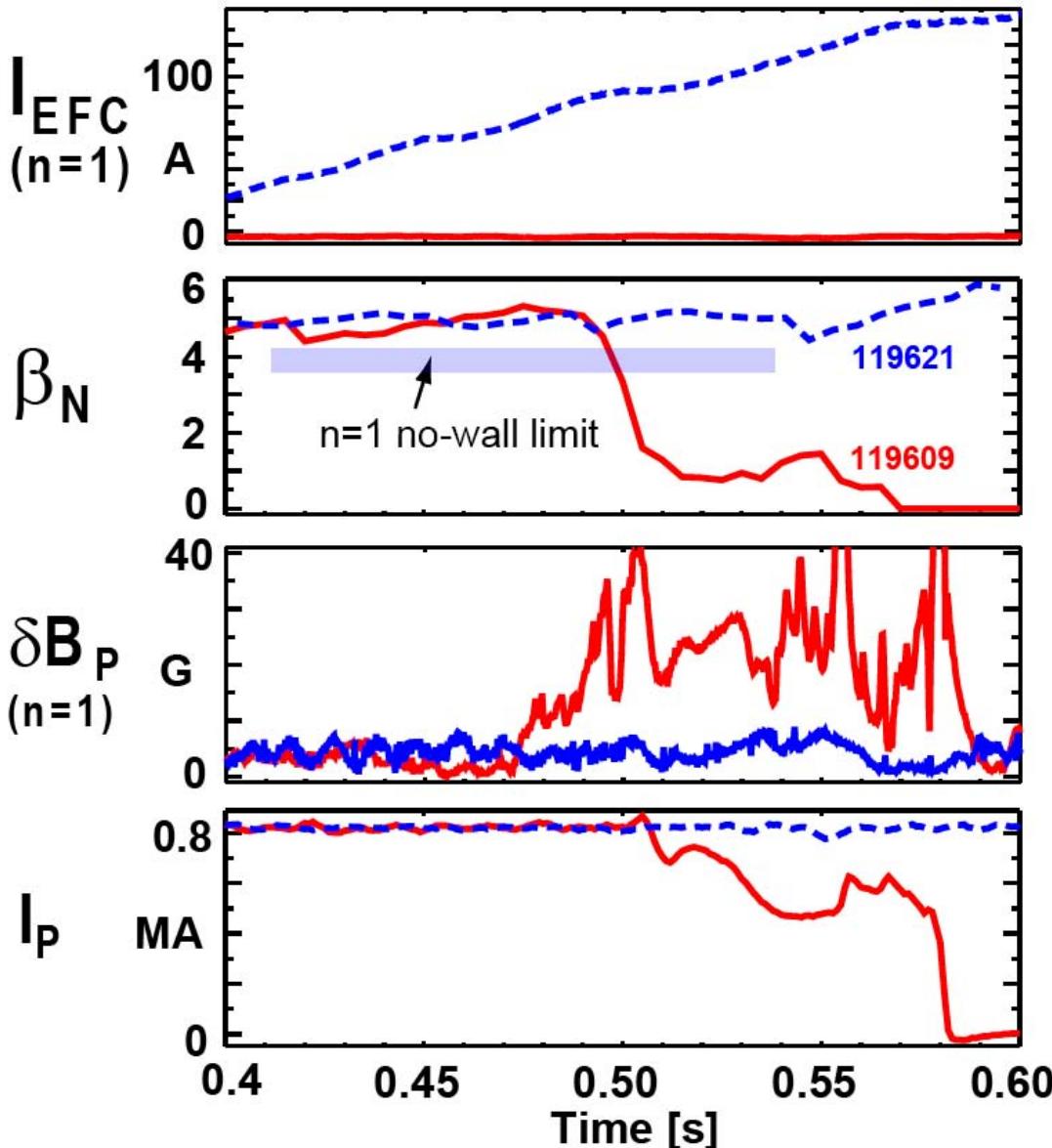
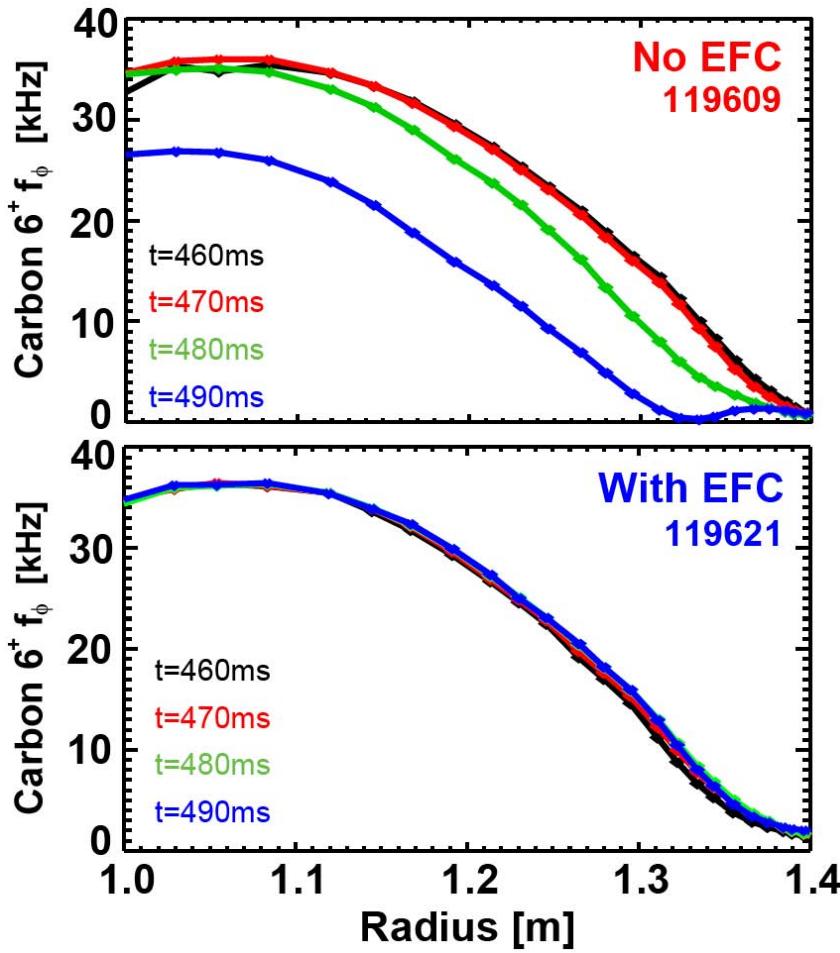
# Outline

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1. Experimental motivation
2. Role of  $E \times B$  drift frequency profile
3. Kinetic stability analysis using MARS code
  - Comparisons with experiment
  - Self-consistent vs. perturbative approach

# Error field correction (EFC) often necessary to maintain rotation, stabilize n=1 resistive wall mode (RWM) at high $\beta_N$

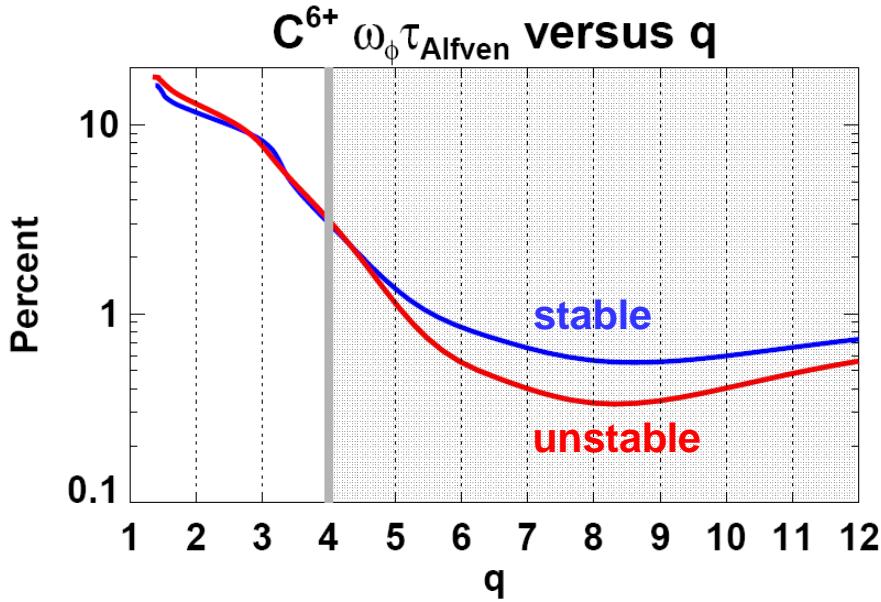
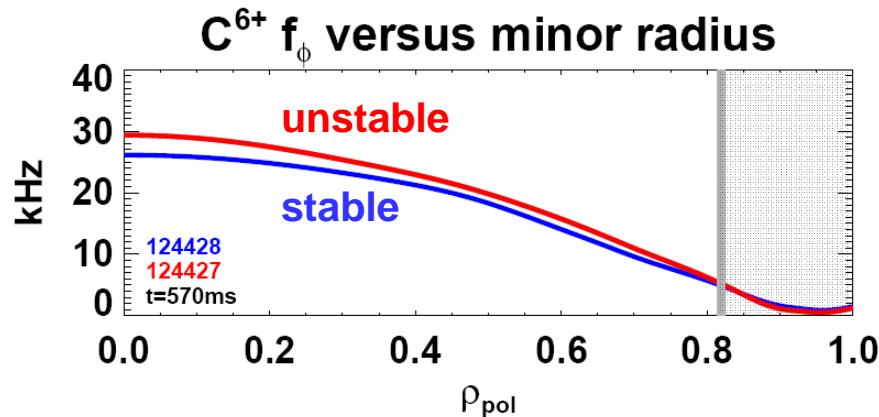
- No EFC  $\rightarrow$  n=1 RWM unstable
- With EFC  $\rightarrow$  n=1 RWM stable



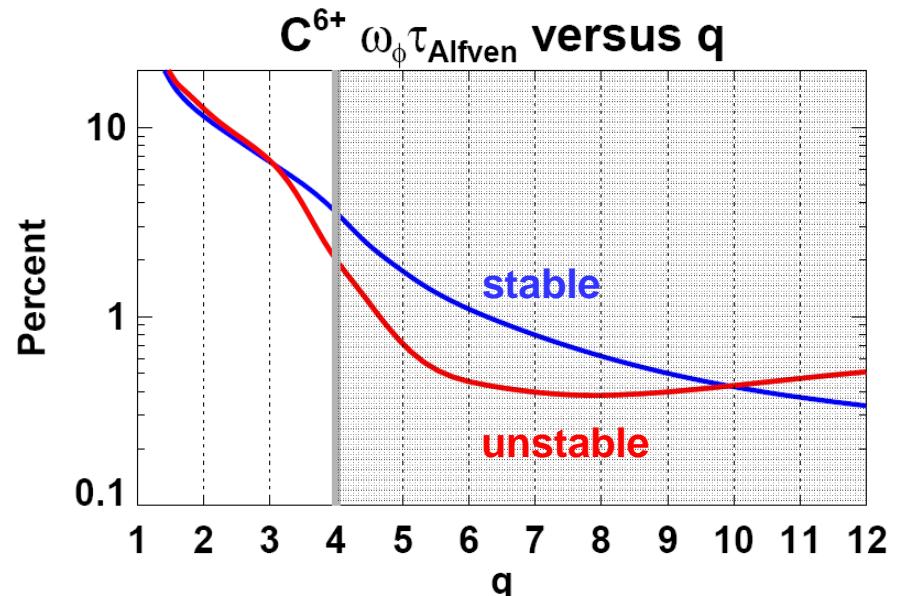
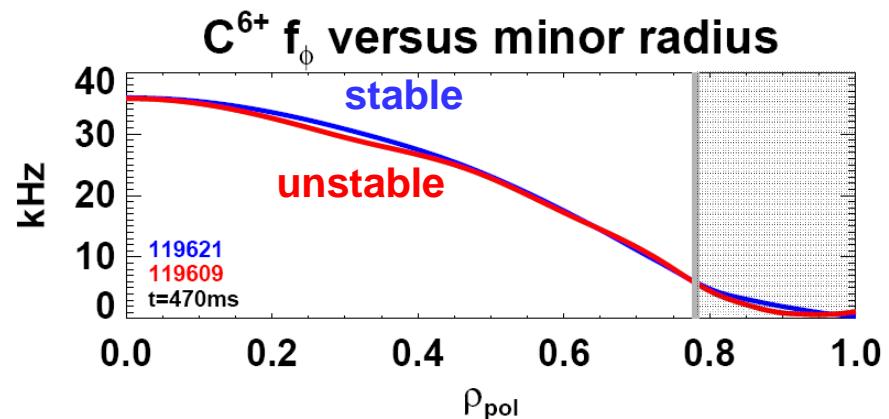
J.E. Menard et al, Nucl. Fusion 50 (2010) 045008

# EFC experiments show edge region with $q \geq 4$ and $r/a \geq 0.8$ apparently determine stability

- $n=3$  EFC  $\rightarrow$  stable
- No EFC  $\rightarrow$   $n=1$  RWM unstable



- $n=1$  EFC  $\rightarrow$  stable
- No EFC  $\rightarrow$   $n=1$  RWM unstable



# MARS is linear MHD stability code that includes toroidal rotation and drift-kinetic effects

- Single-fluid linear MHD

$$(\gamma + in\Omega)\xi = \mathbf{v} + (\xi \cdot \nabla \Omega)R^2 \nabla \phi$$

$$\rho(\gamma + in\Omega)\mathbf{v} = -\nabla \cdot \mathbf{p} + \mathbf{j} \times \mathbf{B} + \mathbf{J} \times \mathbf{Q}$$

$$- \rho[2\Omega \hat{\mathbf{Z}} \times \mathbf{v} + (\mathbf{v} \cdot \nabla \Omega)R^2 \nabla \phi]$$

$$(\gamma + in\Omega)\mathbf{Q} = \nabla \times (\mathbf{v} \times \mathbf{B}) + (\mathbf{Q} \cdot \nabla \Omega)R^2 \nabla \phi$$

$$(\gamma + in\Omega)p = -\mathbf{v} \cdot \nabla P, \quad \mathbf{j} = \nabla \times \mathbf{Q}$$

*Y.Q. Liu, et al., Phys. Plasmas 15, 112503 2008*

- Mode-particle resonance operator:

**MARS-K:**

$$\lambda_{ml} = \frac{n[\omega_{*N} + (\hat{\epsilon}_k - 3/2)\omega_{*T} + \omega_E] - \omega}{n(\langle \omega_d \rangle + \omega_E) + [\alpha(m + nq) + l]\omega_b - i\nu_{\text{eff}} - \omega}$$

**MARS-F:**

$$\lambda_{ml} = \frac{n[\cancel{\omega_{*N}} + (\hat{\epsilon}_k - 3/2)\cancel{\omega_{*T}} + \cancel{\omega_E}] - \omega}{n(\cancel{\langle \omega_d \rangle} + \cancel{\omega_E}) + [\alpha(m + nq) + l]\cancel{\omega_b} - i\nu_{\text{eff}} - \omega}$$

+ additional approximations/simplifications in  $f_L^1$

- Fast ions: MARS-K: slowing-down  $f(v)$ , MARS-F: lumped with thermal

- Kinetic effects in perturbed  $p$ :

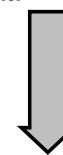
$$\mathbf{p} = p\mathbf{I} + p_{\parallel}\hat{\mathbf{b}}\hat{\mathbf{b}} + p_{\perp}(\mathbf{I} - \hat{\mathbf{b}}\hat{\mathbf{b}})$$

$$p_{\parallel}e^{-i\omega t + in\phi} = \sum_{e,i} \int d\Gamma M v_{\parallel}^2 f_L^1$$

$$p_{\perp}e^{-i\omega t + in\phi} = \sum_{e,i} \int d\Gamma \frac{1}{2} M v_{\perp}^2 f_L^1$$

$$f_L^1 = -f_{\epsilon}^0 \epsilon_k e^{-i\omega t + in\phi} \sum X_m^u H_{ml}^u \lambda_{ml} e^{-in\tilde{\phi}(t) + im\langle \dot{\chi} \rangle t + il\omega_b t}$$

$$H_L = \frac{1}{\epsilon_k} [M v_{\parallel}^2 \vec{\kappa} \cdot \xi_{\perp} + \mu(Q_{L\parallel} + \nabla B \cdot \xi_{\perp})]$$



# Sensitivity of stability to rotation motivates study of all components of $\mathbf{E} \times \mathbf{B}$ drift frequency $\omega_E(\psi)$

- Decompose flow of species  $j$  into poloidal + toroidal components:  

$$\vec{u}_j = u_{\theta j}(\psi) \vec{B}_P + \Omega_{\phi j}(\psi, \theta) R^2 \nabla \phi \quad \text{satisfying } \nabla \cdot \vec{u}_j = 0$$
- Orbit-average  $\mathbf{E} \times \mathbf{B}$  drift frequency:  $\omega_E \equiv \langle \langle \vec{v}_E \cdot \nabla(\phi - q\theta) \rangle \rangle$   
 Bounce average:  $\langle \langle X \rangle \rangle \equiv \frac{1}{\tau_b} \oint X d\tau \quad \vec{v}_E = \mathbf{E} \times \mathbf{B} \text{ drift velocity}$   
F. Porcelli, et al., Phys. Plasmas 1 (1994) 470
- Ignoring centrifugal effects (ok in plasma edge),  $\omega_E$  reduces to:

$$\omega_E(\psi) = \frac{\langle \vec{u}_j \cdot \vec{B} \rangle}{F} - \omega_{*j} - u_{\theta j}(\psi) \frac{\langle B^2 \rangle}{F}$$

1. parallel/toroidal    2. diamagnetic    3. poloidal

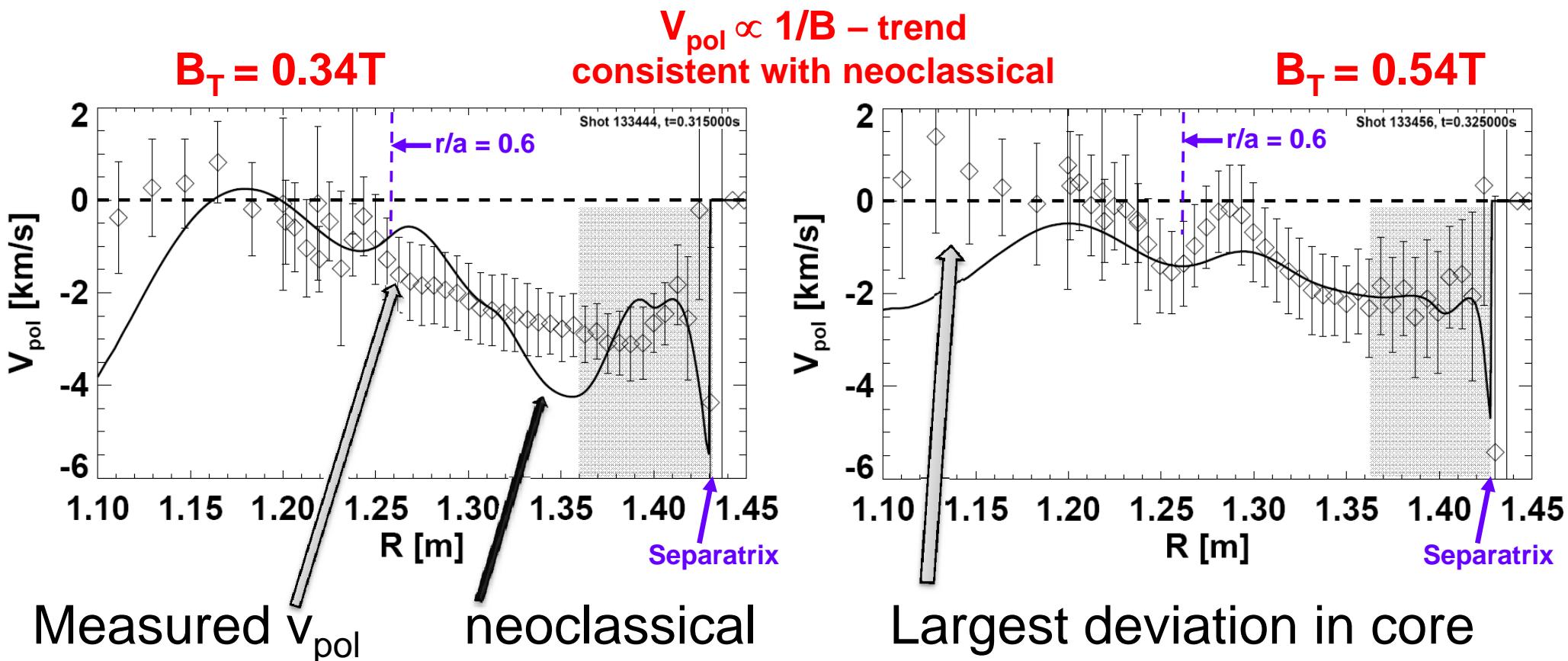
$\frac{\langle \vec{u}_j \cdot \vec{B} \rangle}{F}$       measured      measured or neoclassical theory  
 $\frac{\langle B^2 \rangle}{F}$       reconstructions

$$\frac{\langle \vec{u}_j \cdot \vec{B} \rangle}{F} = \Omega_{\phi j}(\psi, \theta) + \frac{u_{\theta j}(\psi)}{F} \left[ \langle B^2 \rangle - \frac{F^2}{R^2} \right]$$

flux function      measured

Y.B. Kim, et al., Phys. Fluids B 3 (1991) 2050  
 Flux-surface average:  
 $\langle X \rangle \equiv \oint J X d\theta / \oint J d\theta$   
 $F(\psi) \equiv R B_\phi$

# NSTX edge $v_{\text{pol}}$ $\approx$ neoclassical (within factor of $\sim 2$ )

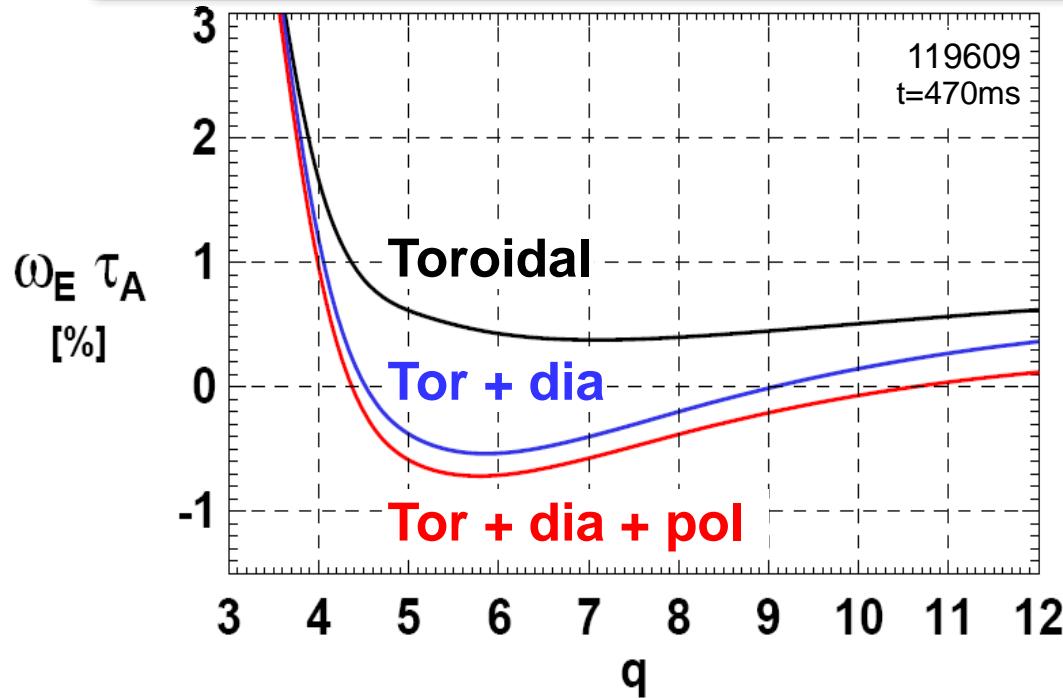


**Subsequent MARS calculations use  
neoclassical  $v_{\text{pol}}$ , but  $v_{\text{pol}} = 0$  for  $r/a < 0.6$**

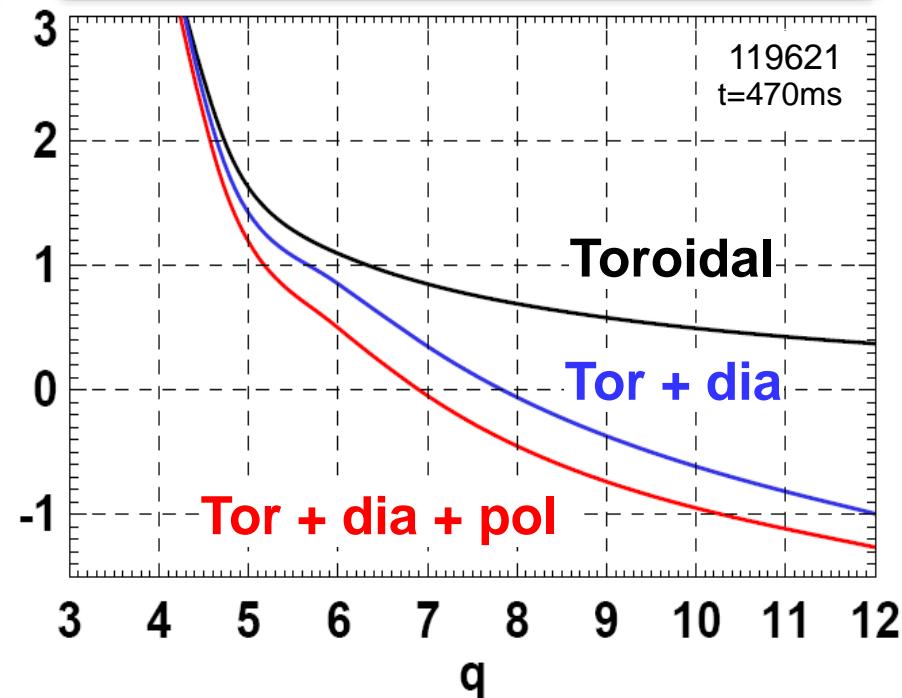
**NSTX results:** R. E. Bell, et al., Phys. Plasmas 17, 082507 (2010)  
**Neoclassical:** W. Houlberg, et al., Phys. Plasmas 4, 3230 (1997)

# $n=1$ EFC profiles show impurity C diamagnetic and poloidal rotation modify $|\omega_E \tau_A| \sim 1\%$ in edge $\rightarrow$ potentially important

$n=1$  RWM unstable (no  $n=1$  EFC)



$n=1$  RWM stable ( $n=1$  EFC)



$\text{C}^{6+}$  Toroidal rotation only:  $\omega_E = \Omega_{\phi-\text{C}}(\psi)$

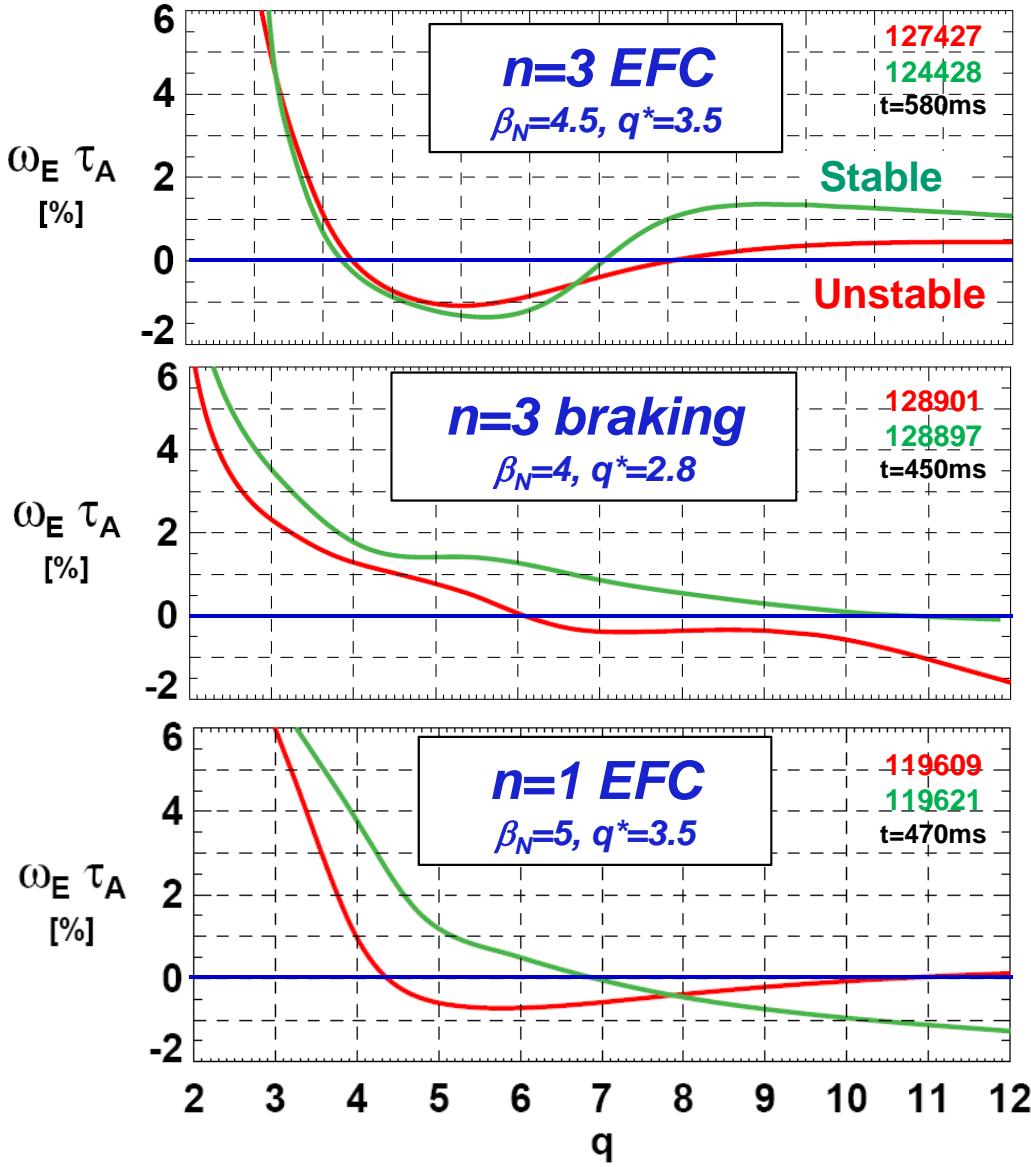
Toroidal + diamagnetic:  $\omega_E = \Omega_{\phi-\text{C}}(\psi) - \omega_{*\text{C}}$

Toroidal + diamagnetic + poloidal:  $\omega_E = \langle \mathbf{u}_C \cdot \mathbf{B} \rangle / F - \omega_{*\text{C}} - u_{\theta-\text{C}} \langle \mathbf{B}^2 \rangle / F$

- Diamagnetic contribution to  $\omega_E \tau_A$   $\approx -0.5$  to  $-1.0\%$
- Neoclassical  $v_{\text{pol}}$  contribution to  $\omega_E \tau_A$   $\approx -0.2$  to  $-0.4\%$

# A range of edge $\omega_E$ profile shapes can be stable, but unstable profiles can often be nearby

Toroidal + diamagnetic + poloidal



- Separation between **stable** and **unstable** profiles typically small:  $\Delta(\omega_E \tau_A) \leq 1\%$
- $\omega_E \approx 0$  over most of edge may correlate with instability
- Edge  $\omega_E(r)$  control could potentially provide RWM stabilization technique
- Motivation for RWM active feedback control remains

# Kinetic stability analysis using MARS-F

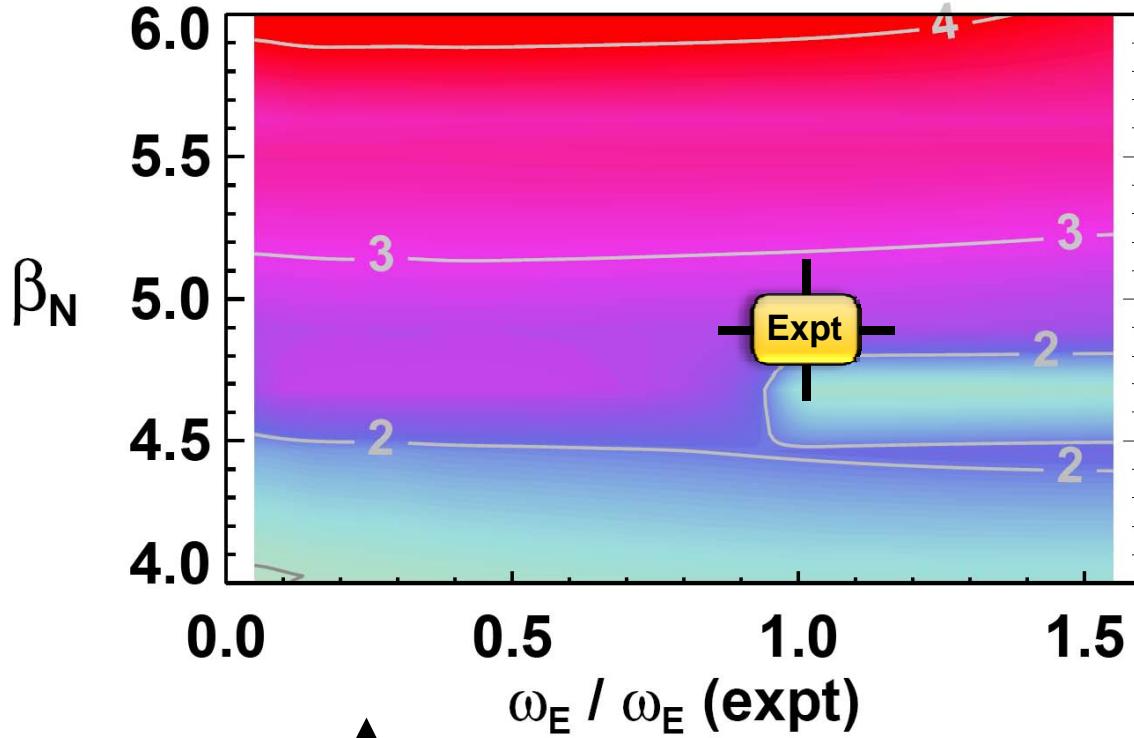


- Experimentally unstable case
- Experimentally stable case
- Comparison of unstable and stable cases

# MARS-F using marginally unstable $\omega_E = \Omega_{\phi,C}$ predicts n=1 RWM to be robustly unstable → inconsistent with experiment

**Calculated n=1  $\gamma\tau_{\text{wall}}$**

Using experimentally marginally unstable profiles

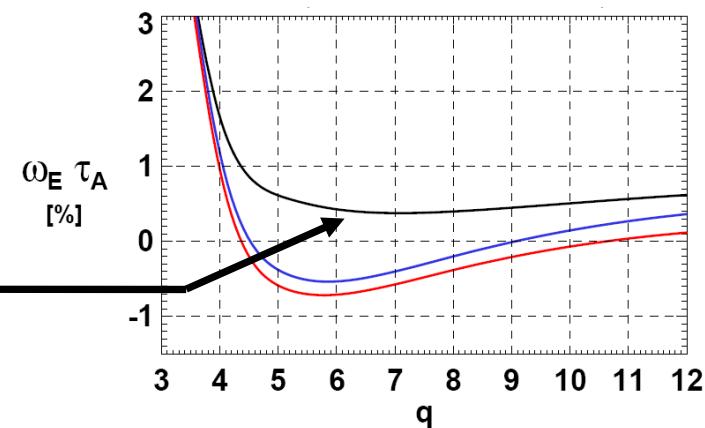


$$C_\beta \equiv \frac{\beta_N - \beta_N(\text{no-wall})}{\beta_N(\text{wall}) - \beta_N(\text{no-wall})}$$

$$C_\beta = 1$$

- $\gamma$  depends only weakly on rotation
- $\gamma$  increases with  $\beta_N$

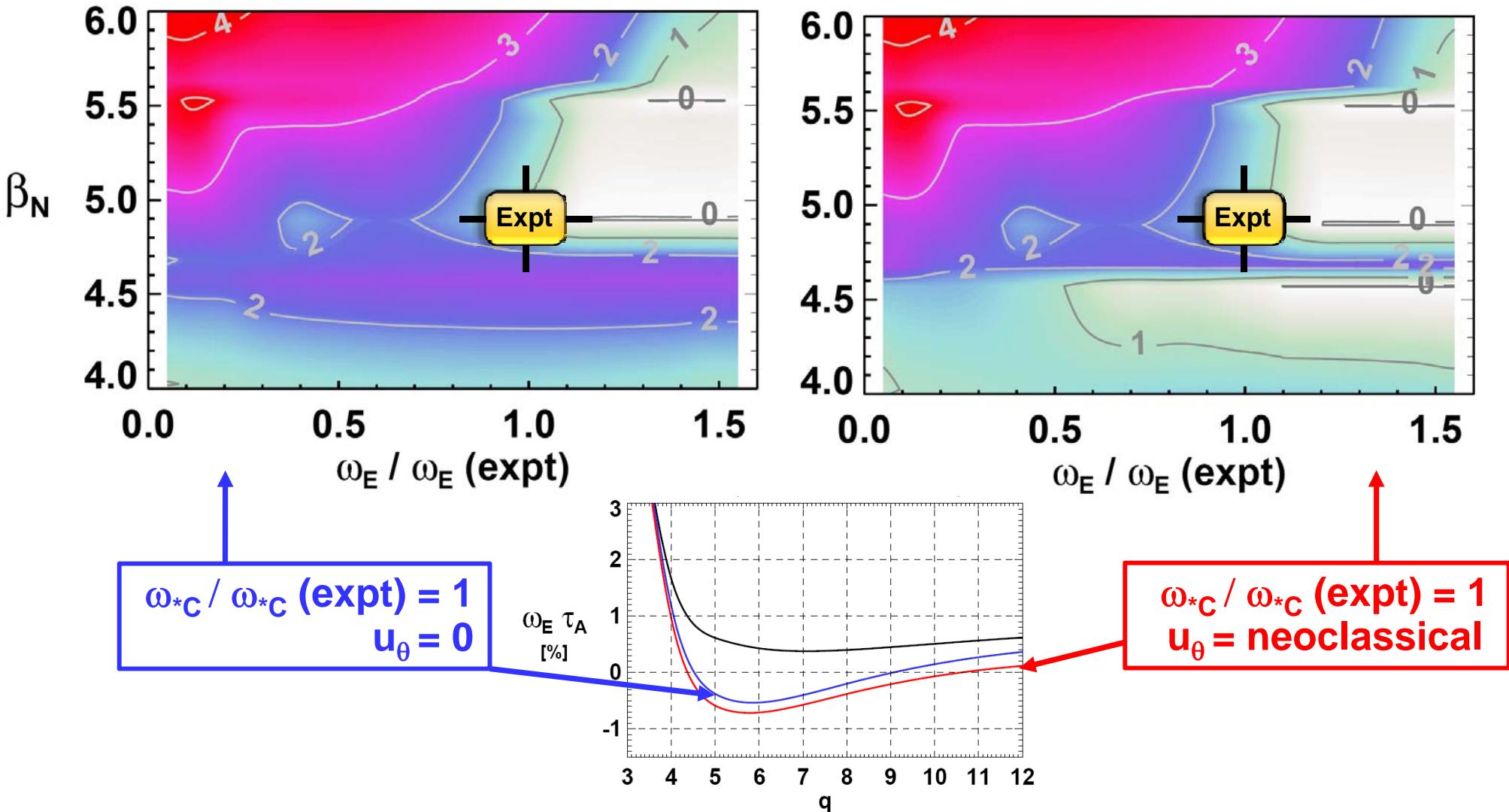
$$C_\beta = 0$$



$$\omega_{*C} / \omega_{*C} (\text{expt}) = 0, u_\theta = 0$$

MARS-F using marginally unstable full  $\omega_E$  predicts n=1 RWM to be marginally unstable → more consistent with experiment

### Calculated n=1 $\gamma\tau_{\text{wall}}$ using experimentally marginally unstable profiles



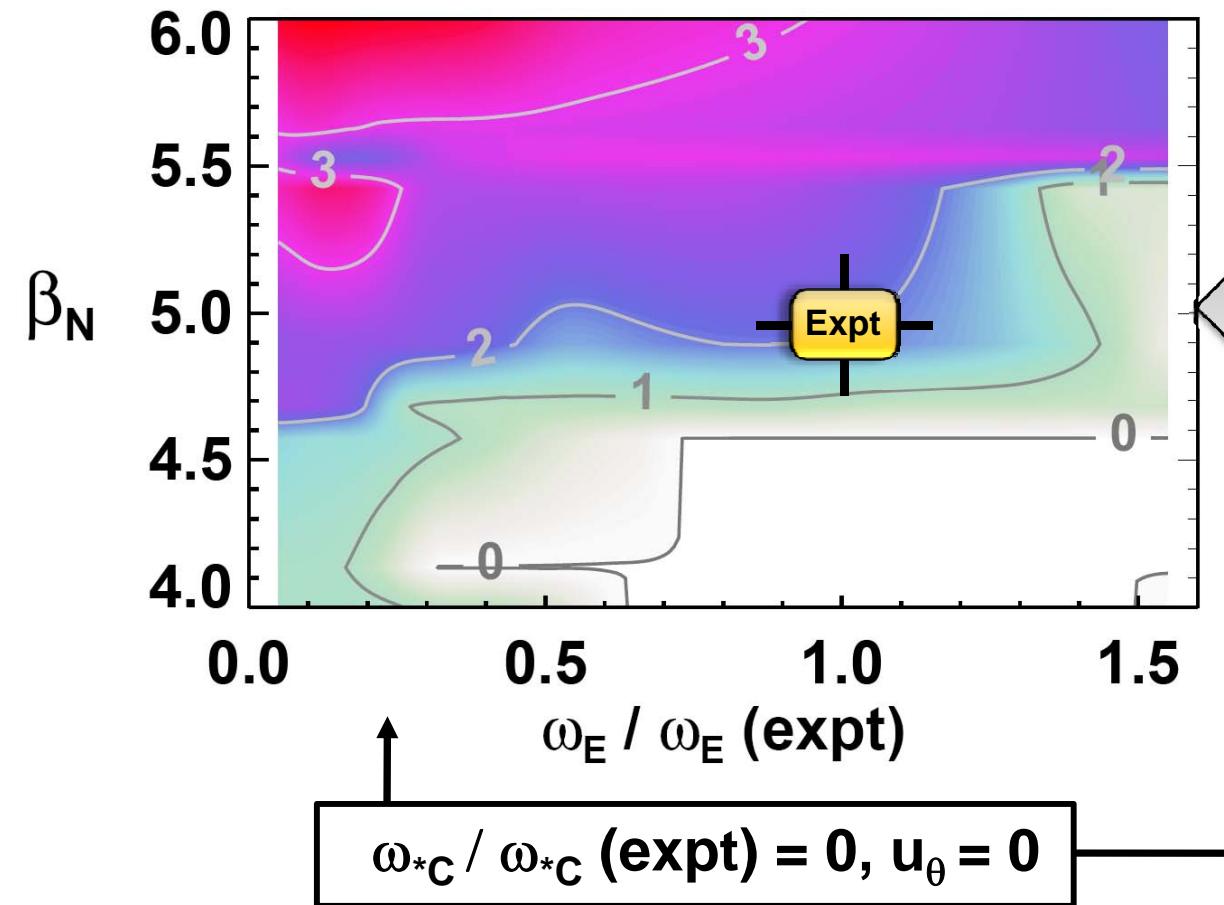
# Kinetic stability analysis using MARS-F

- Experimentally unstable case
- ■ Experimentally stable case
- Comparison of unstable and stable cases

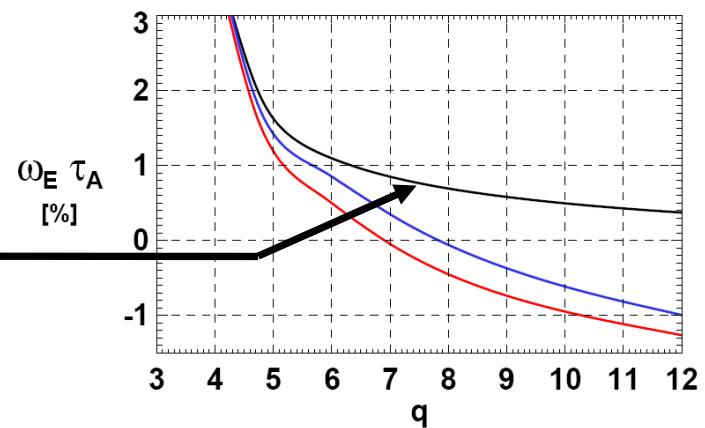
# MARS-F using stable $\omega_E = \Omega_{\phi-C}$ profile predicts n=1 RWM to be unstable → inconsistent with experiment

Calculated n=1  $\gamma\tau_{\text{wall}}$

using experimentally stable profiles

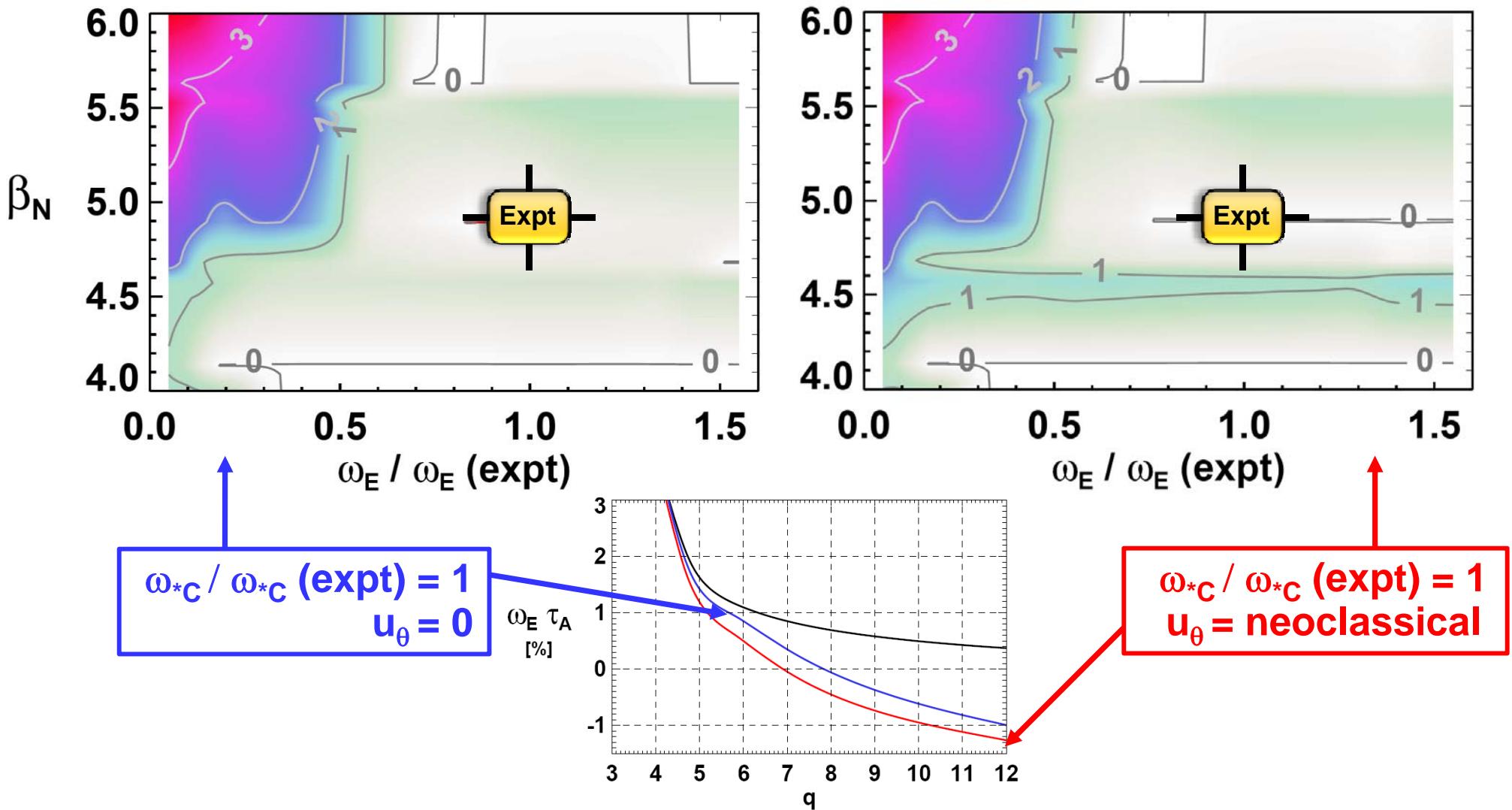


- $n=1$  RWM predicted to be unstable for  $\beta_N > 4.6$ , but actual plasma operates stably at  $\beta_N \geq 5$



# MARS-F using stable full $\omega_E$ profile predicts wide region of marginal stability → more consistent with experiment

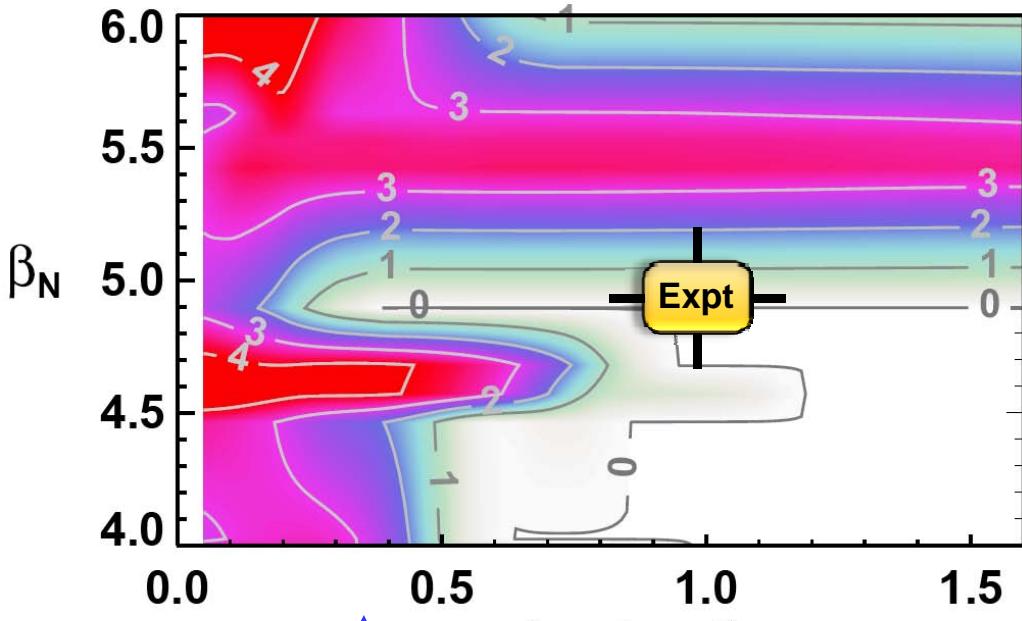
**Calculated  $n=1 \gamma\tau_{\text{wall}}$   
using experimentally stable profiles**



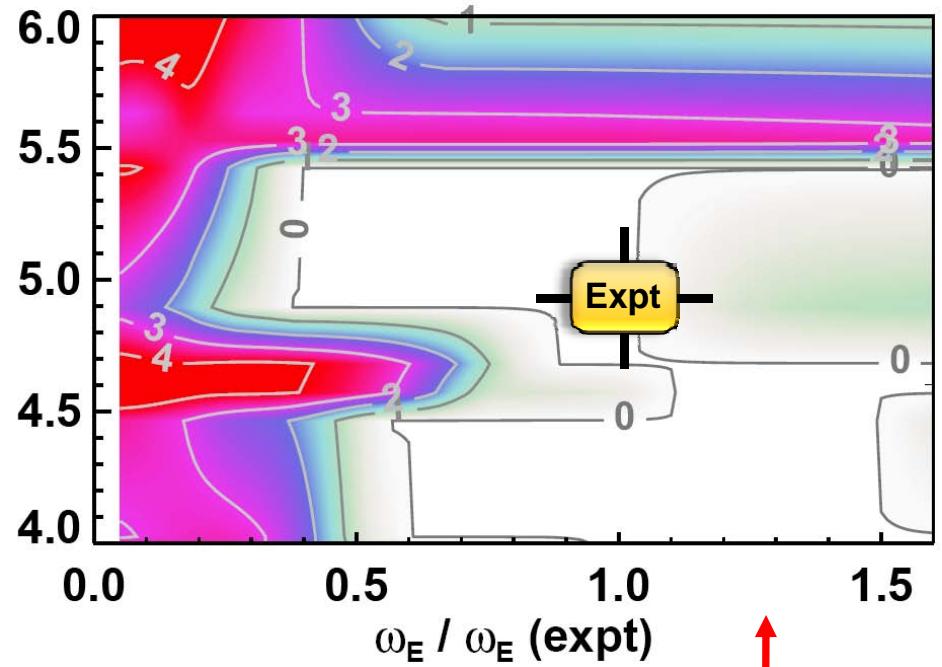
# Inclusion of $v_{pol}$ in $\omega_E$ can sometimes modify marginal stability boundary – example: wall position variation

Calculated  $n=1 \gamma\tau_{wall}$

experimentally stable profiles and  $b_{wall}$  / a artificially increased  $\times 1.1$



$\omega_{*C} / \omega_{*C} (\text{expt}) = 1$   
 $u_\theta = 0$



$\omega_{*C} / \omega_{*C} (\text{expt}) = 1$   
 $u_\theta = \text{neoclassical}$

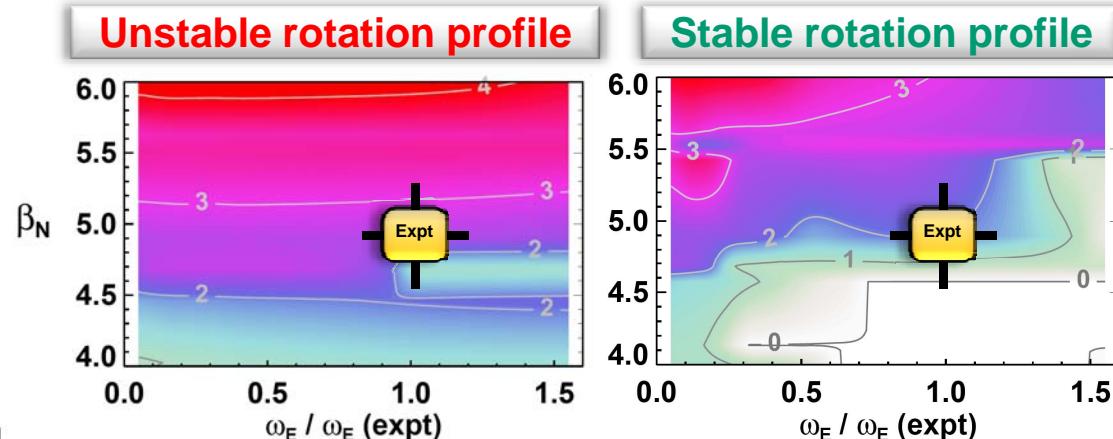
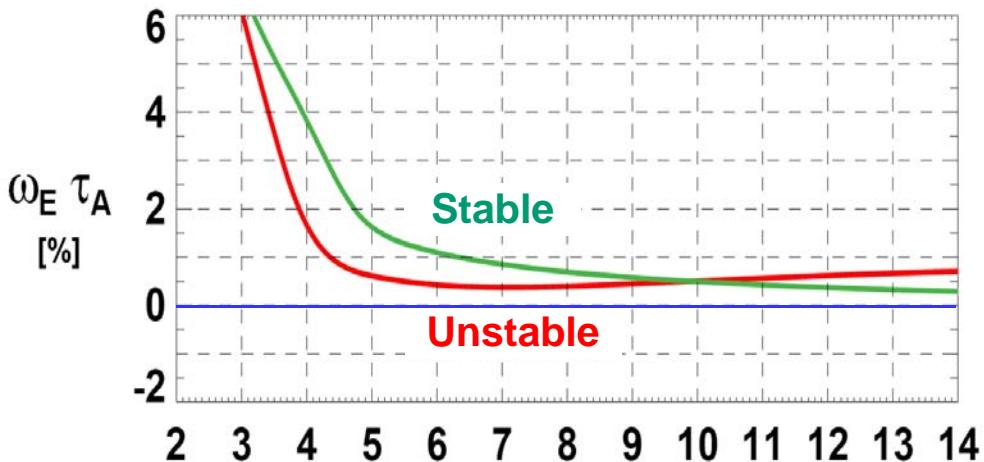
- Increased wall distance lowers with-wall limit to  $\beta_N \sim 5.5$
- Case with  $u_\theta=0$  has lower marginal stability limit  $\beta_N \sim 5$

# Kinetic stability analysis using MARS-F

- Experimentally unstable case
- Experimentally stable case
- ■ Comparison of unstable and stable cases

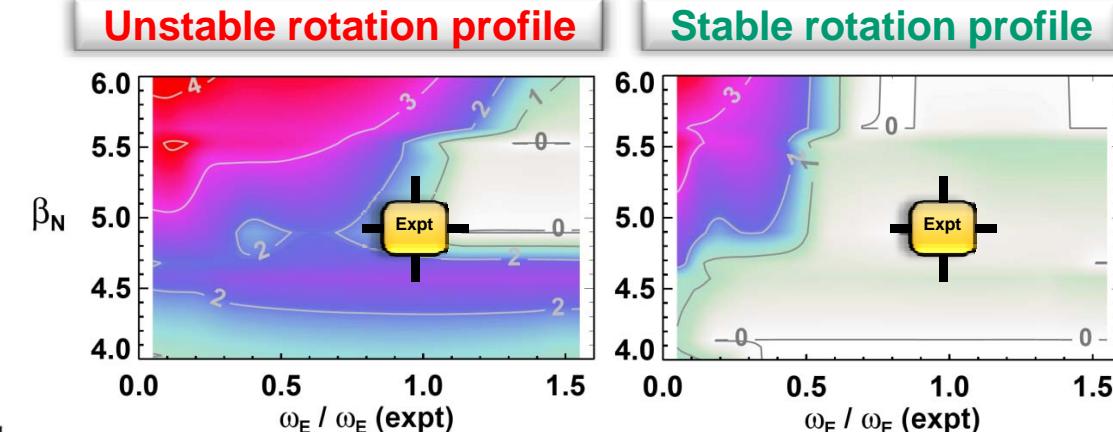
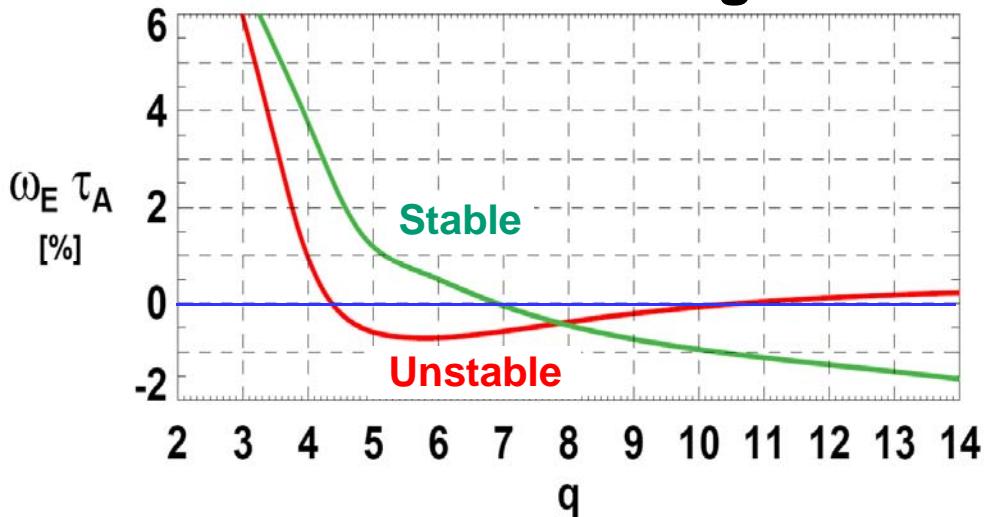
Inclusion of  $\omega_{*c}$  in  $\omega_E$  increases separation between stable and unstable  $\omega_E(\psi)$  and provides consistency w/ experiment

### Toroidal rotation only



*Predictions inconsistent with experiment*

### Toroidal + diamagnetic



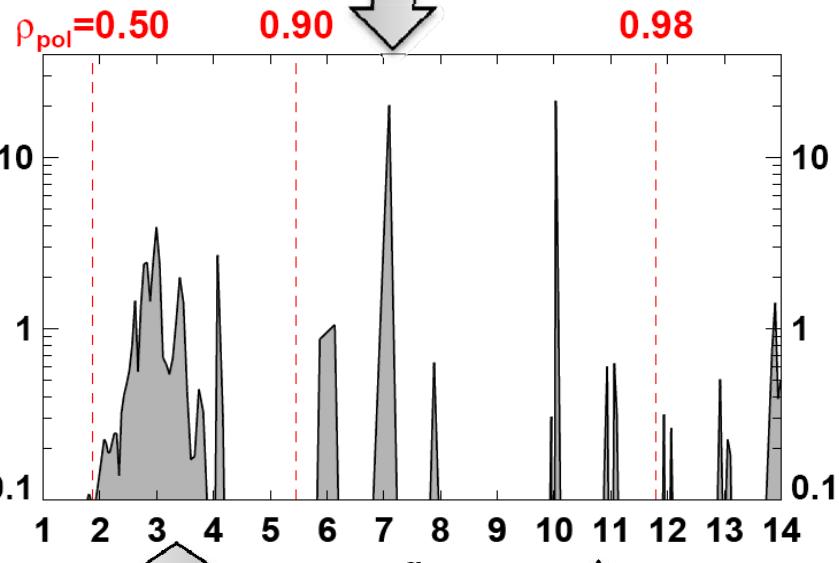
*Predictions more consistent with experiment*

# Mode damping in last 10% of minor radius calculated to determine stability of RWM in n=1 EFC experiments

Toroidal + diamagnetic

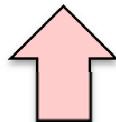
$\omega_E / \omega_E (\text{expt}) = 0.5$  used so unstable modes can be identified and local damping computed

Unstable rotation profile

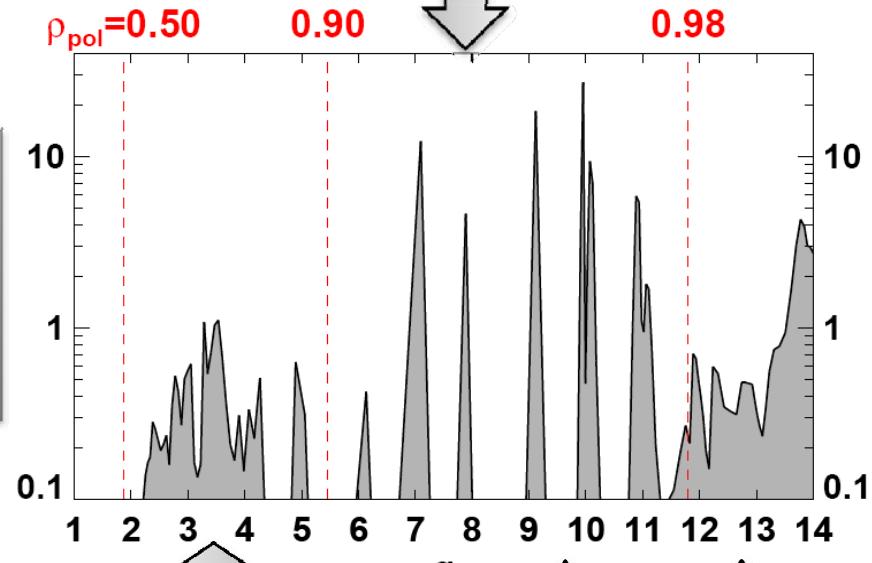


$$\text{Local mode damping} \propto \frac{\partial(\delta W_{K-\text{imag}})}{\partial V}$$

Higher core damping



Lower edge damping



Lower core damping



Higher edge damping

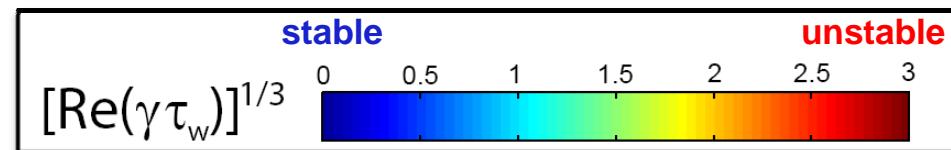
# Kinetic stability analysis using MARS-K

- Comparison with experiment
- Self-consistent vs. perturbative approach
- Modifications of RWM eigenfunction

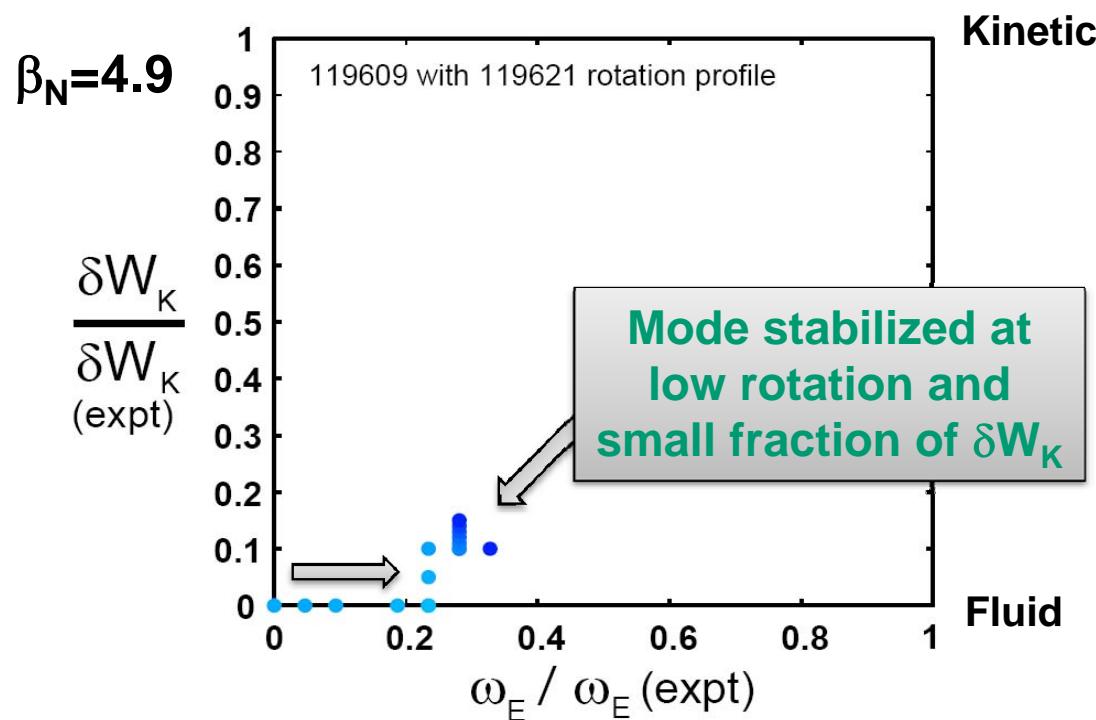
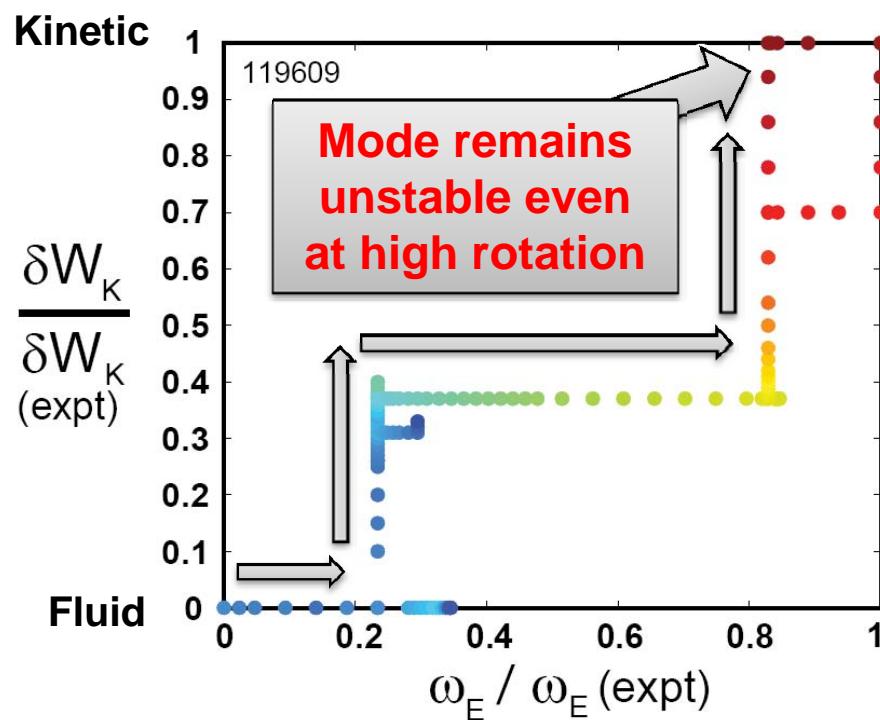
# MARS-K consistent with EFC results and MARS-F trends

- MARS-K full kinetic  $\delta W_K \rightarrow$  multiple modes can be present
  - Mode identification and eigenvalue tracking more challenging
- Track roots by scanning fractions of experimental  $\omega_E$  and  $\delta W_K$ :

Experimentally unstable case

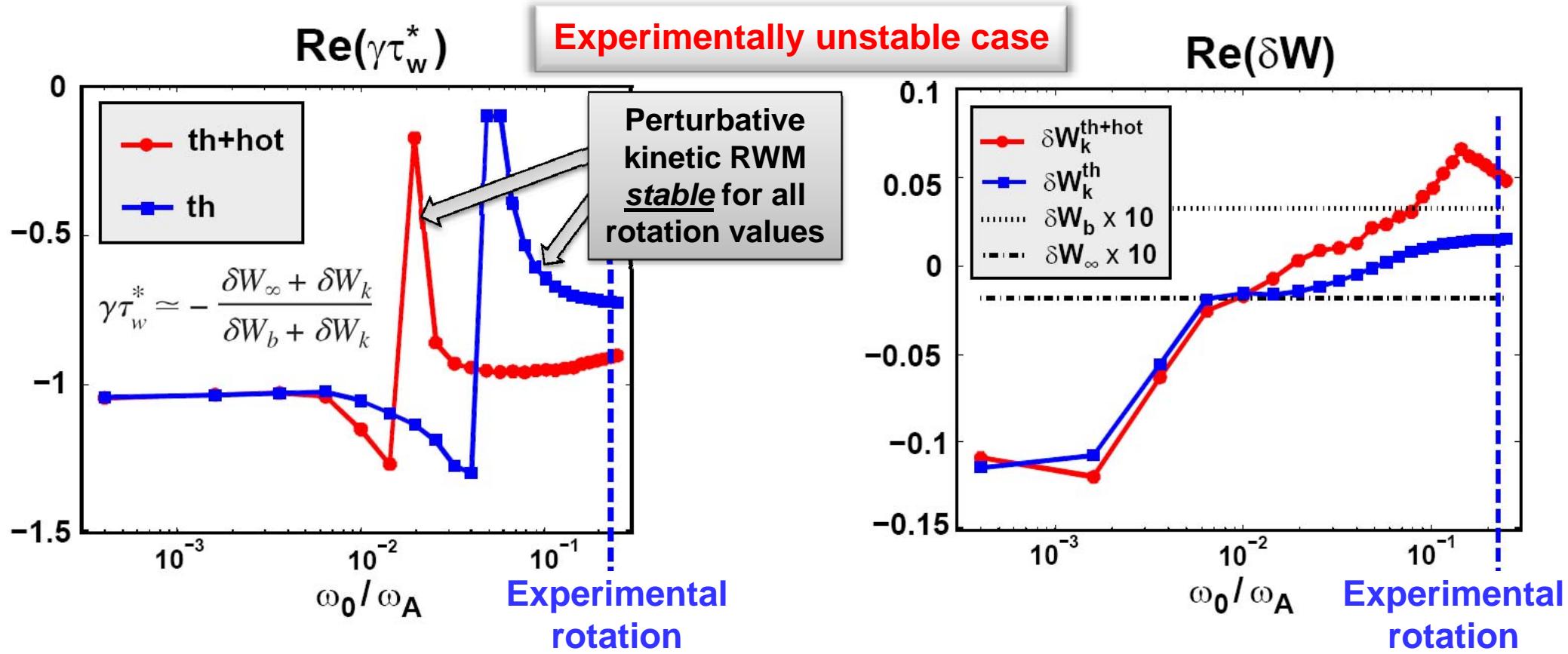


Experimentally stable case

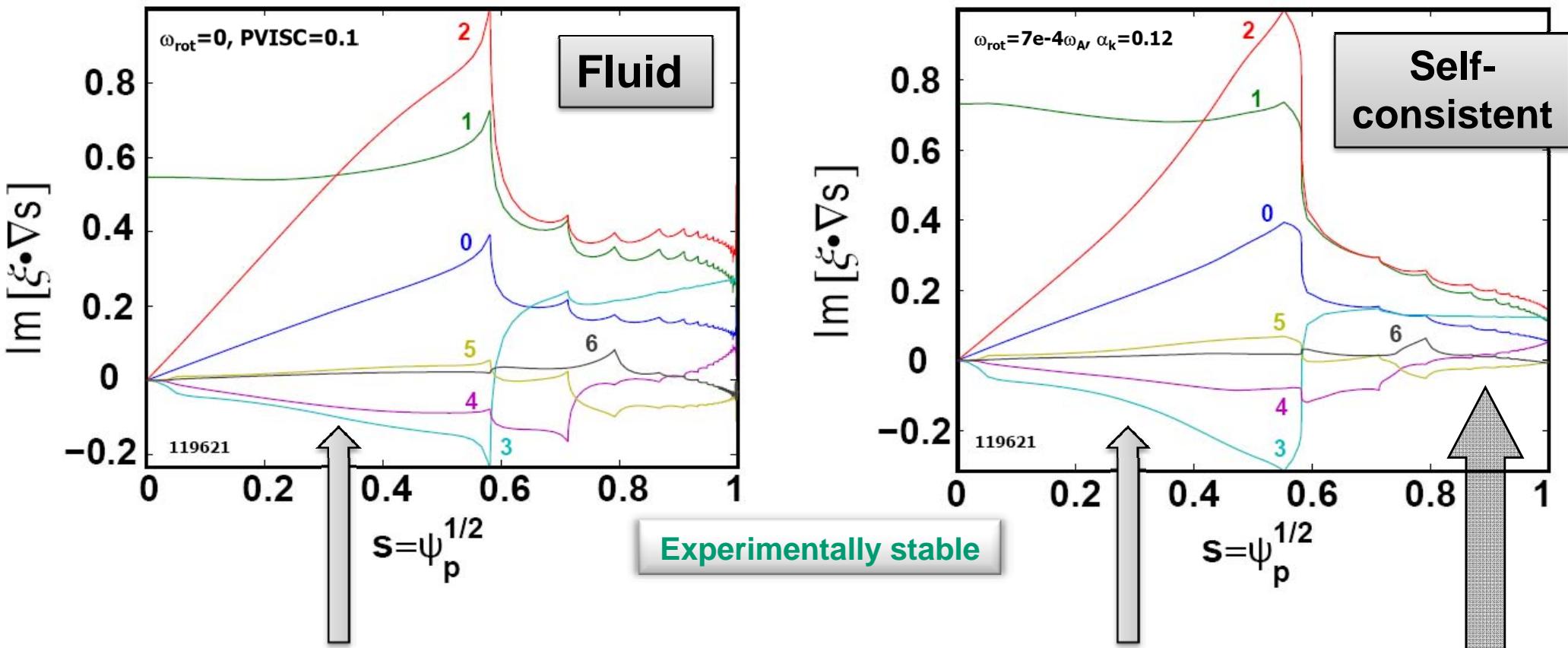


# Perturbative approach predicts unstable case to be stable → inconsistent with self-consistent treatment and experiment

- Perturbative approach uses marginally unstable fluid eigenfunction at zero rotation in limit of no kinetic dissipation
- For cases treated here,  $|\delta W_k|$  can be  $\gg |\delta W_\infty|$  and  $|\delta W_b|$ 
  - Possibility that rotation/dissipation can modify eigenfunction & stability

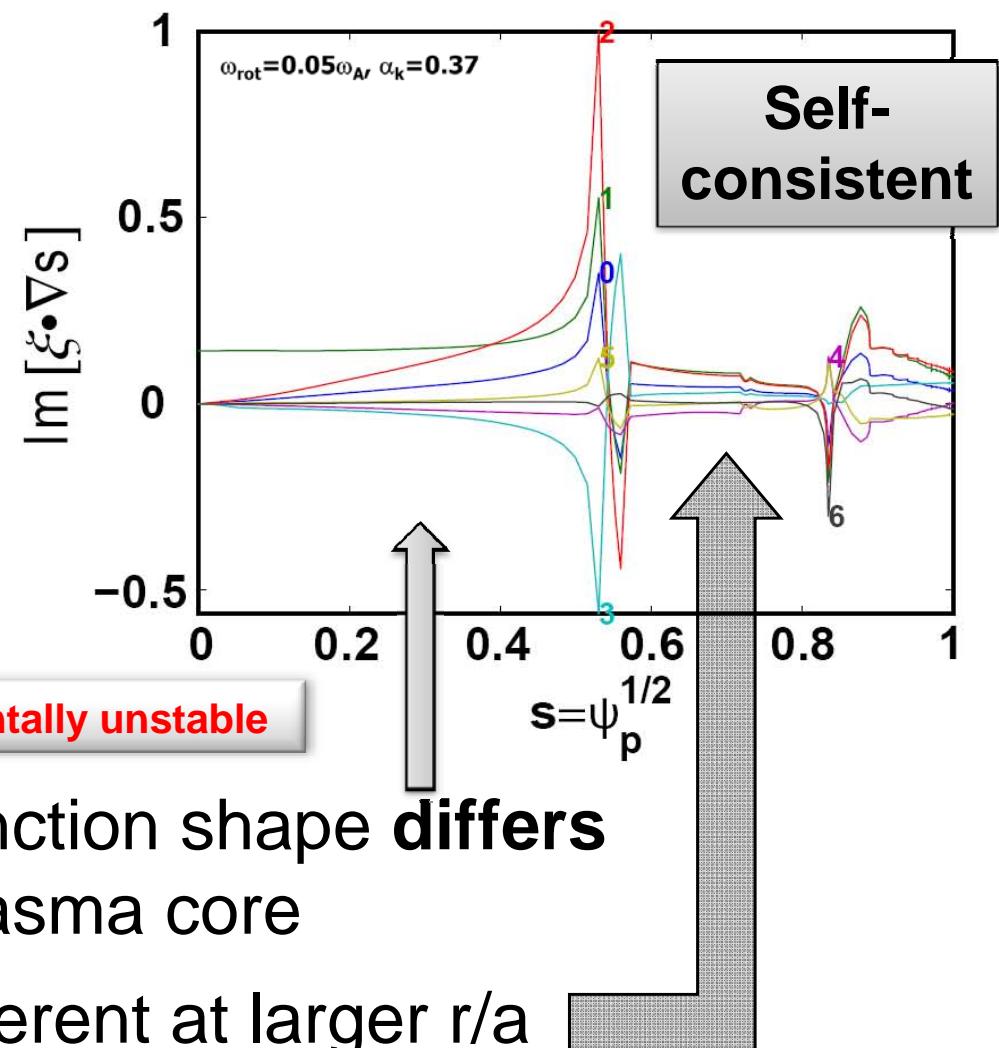
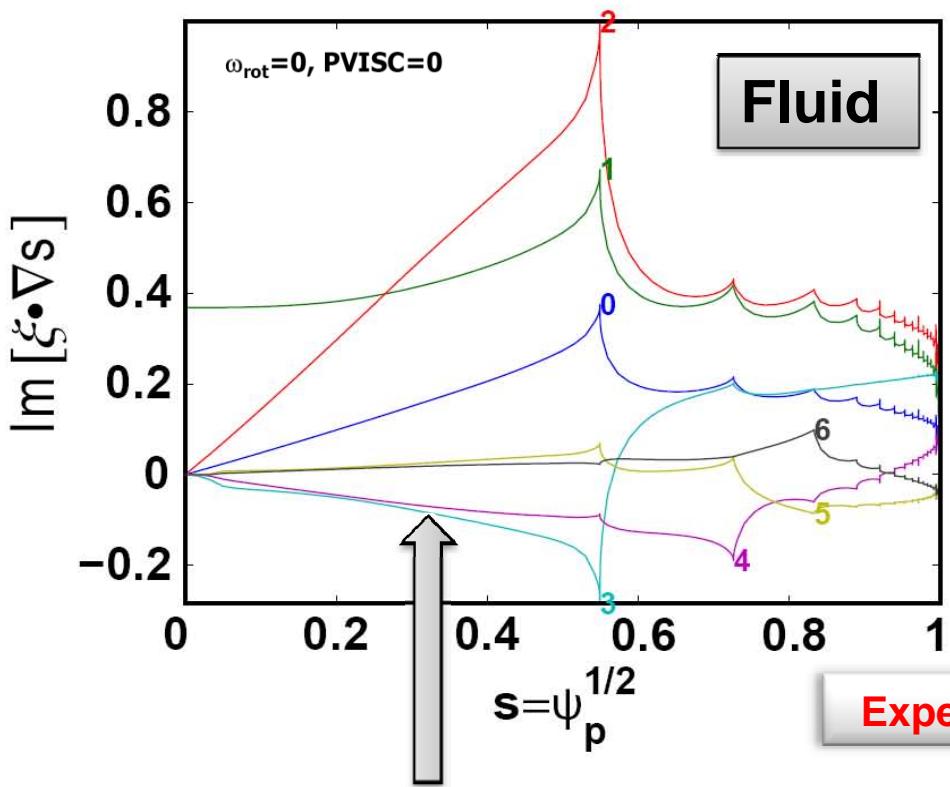


# MARS-K self-consistent calculations for stable case indicate modifications to eigenfunction begin to occur at low rotation



- Self-consistent (SC) eigenfunction qualitatively similar to fluid eigenfunction in plasma core
- SC RWM  $\xi_{\perp}$  amplitude reduced at larger r/a
  - Low  $\omega_E / \omega_E$  (expt) = 0.3%,  $\delta W_K / \delta W_K$  (expt) = 12%
  - Reduced amplitude could reduce dissipation, stability

# MARS-K self-consistent calculations indicate expt. rotation and dissipation can strongly modify RWM eigenfunction



- Self-consistent (SC) eigenfunction shape **differs** from fluid eigenfunction in plasma core
- SC RWM  $\xi_{\perp}$  substantially different at larger r/a
  - Moderate  $\omega_E / \omega_E$  (expt) = 22%,  $\delta W_K / \delta W_K$  (expt) = 37%
  - Differences could be even larger at full rotation and  $\delta W_K$
  - Does reduced edge  $\xi_{\perp}$  amplitude explain reduced stability?

# Summary

- Edge rotation ( $q \geq 4$ ,  $r/a \geq 0.8$ ) important for RWM
  - Trends consistent with stability calculations using MARS-F
  - Provides insight, method for optimal error field correction
- Stability quite sensitive to edge  $\omega_E$  profile
  - Essential to include accurate edge  $\nabla p$  in  $E_r$  profile
  - Poloidal rotation can also influence marginal stability
- Full kinetic stability (MARS-K) consistent w/ experiment
- Perturbative treatment inconsistent – overly stable
  - Edge eigenfunction strongly modified by rotation/dissipation
  - Reduction in  $\xi_\perp$  amplitude may reduce kinetic stabilization