

Taming the Plasma-Material Interface with the Snowflake Divertor in NSTX

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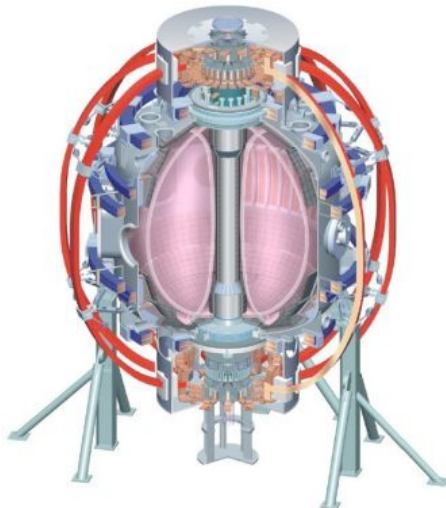
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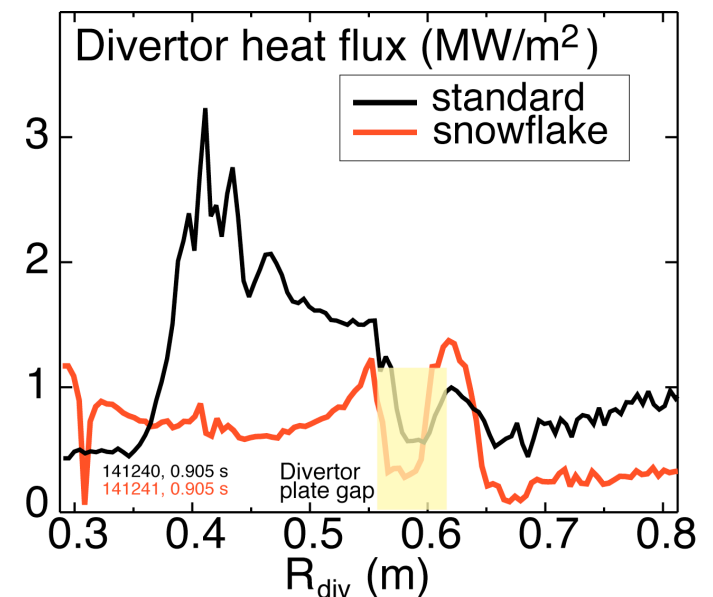
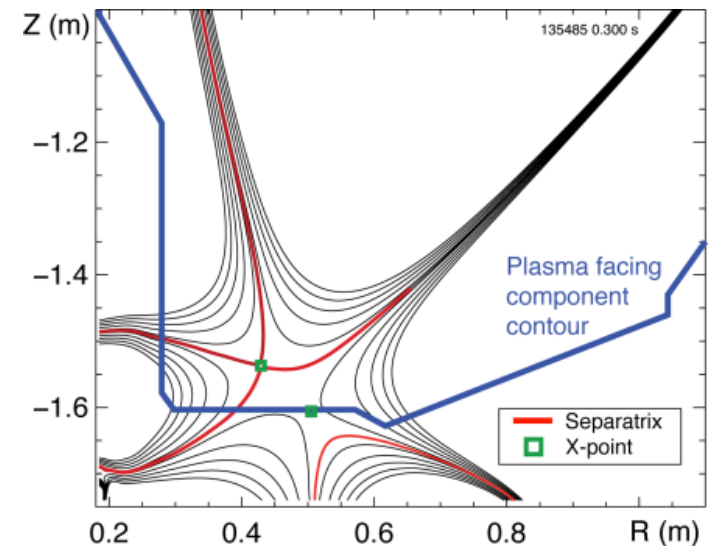
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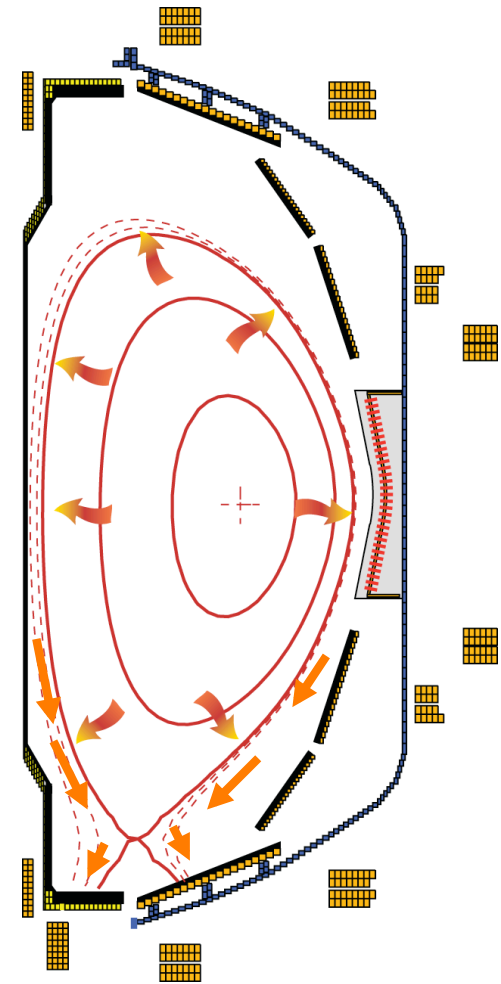
Outline: Experimental studies of snowflake divertor in NSTX

- Tokamak divertor challenge
- Snowflake divertor configuration
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 - Magnetic properties and control
 - Core and divertor plasma properties
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 - 2D transport model
- Conclusions



Poloidal divertor concept enabled progress in magnetic confinement fusion in the last 30 years

- Divertor challenge
 - Steady-state heat flux
 - present limit $q_{peak} \leq 10 \text{ MW/m}^2$
 - projected to $q_{peak} \leq 80 \text{ MW/m}^2$ for future devices
 - Density and impurity control
 - Impulsive heat and particle loads
 - Compatibility with good core plasma performance
- Spherical tokamak: additional challenge - compact divertor
- NSTX (Aspect ratio $A=1.4-1.5$)
 - $I_p \leq 1.4 \text{ MA}$, $P_{in} \leq 7.4 \text{ MW}$ (NBI), $P / R \sim 10$
 - $q_{peak} \leq 15 \text{ MW/m}^2$, $q_{||} \leq 200 \text{ MW/m}^2$
 - Graphite PFCs with lithium coatings



**National Spherical
Torus Experiment**

Various techniques developed for reduction of heat fluxes q_{\parallel} (divertor SOL) and q_{peak} (divertor target)

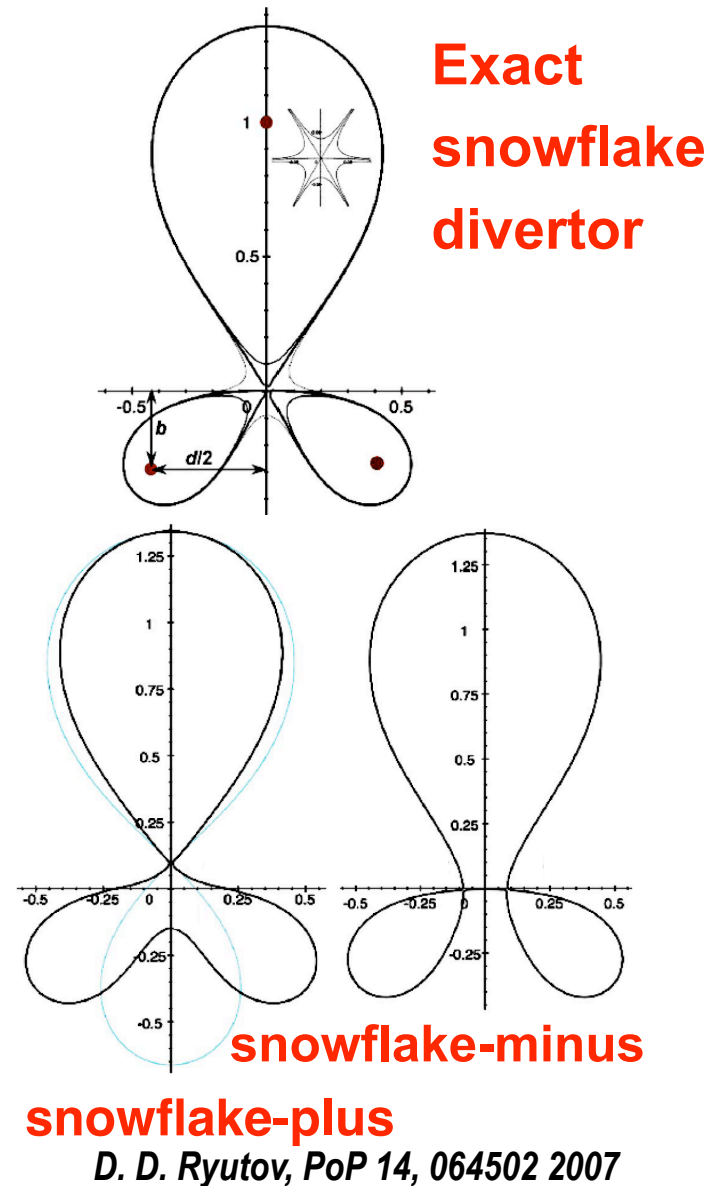
$$q_{peak} \simeq \frac{P_{SOL}(1 - f_{rad})f_{geo} \sin \alpha}{2\pi R_{SP} f_{exp} \lambda_{q_{\parallel}}} \quad A_{wet} = 2\pi R f_{exp} \lambda_{q_{\parallel}}$$

$$f_{exp} = \frac{(B_p/B_{tot})_{MP}}{(B_p/B_{tot})_{OSP}}$$

- Promising divertor peak heat flux mitigation solutions:
 - Divertor geometry
 - poloidal flux expansion
 - divertor plate tilt
 - magnetic balance
 - Radiative divertor
- Recent ideas to improve standard divertor geometry
 - X-divertor (M. Kotschenreuther *et. al*, IC/P6-43, IAEA FEC 2004)
 - Snowflake divertor (D. D. Ryutov, PoP 14, 064502 2007)
 - Super-X divertor (M. Kotschenreuther *et. al*, IC/P4-7, IAEA FEC 2008)

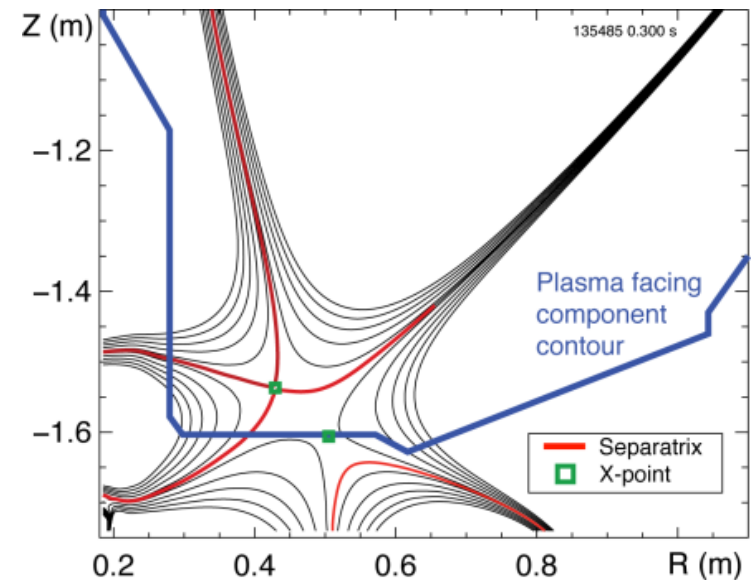
Attractive divertor geometry properties predicted by theory in snowflake divertor configuration

- Snowflake divertor
 - Second-order null
 - $B_p \sim 0$ and $\text{grad } B_p \sim 0$; $B_p \sim r^2$
(Cf. first-order null: $B_p \sim 0$; $B_p \sim r$)
 - Obtained with existing divertor coils (min. 2)
 - Exact snowflake topologically unstable
- Predicted properties (cf. standard divertor)
 - Larger low B_p region around X-point
 - Larger plasma wetted-area A_{wet} (flux expansion f_{exp})
 - Larger X-point connection length L_x
 - Larger effective divertor volume V_{div}
 - Increased edge magnetic shear
- Experiments
 - TCV (F. Piras *et. al*, PRL 105, 155003 (2010))



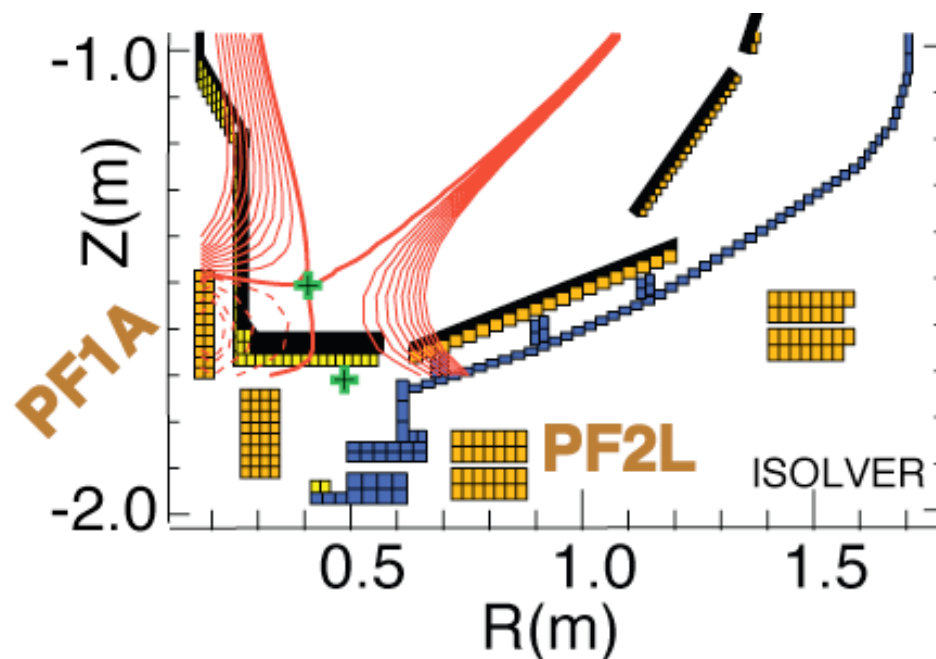
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 - 2D transport model
 - **Conclusions**



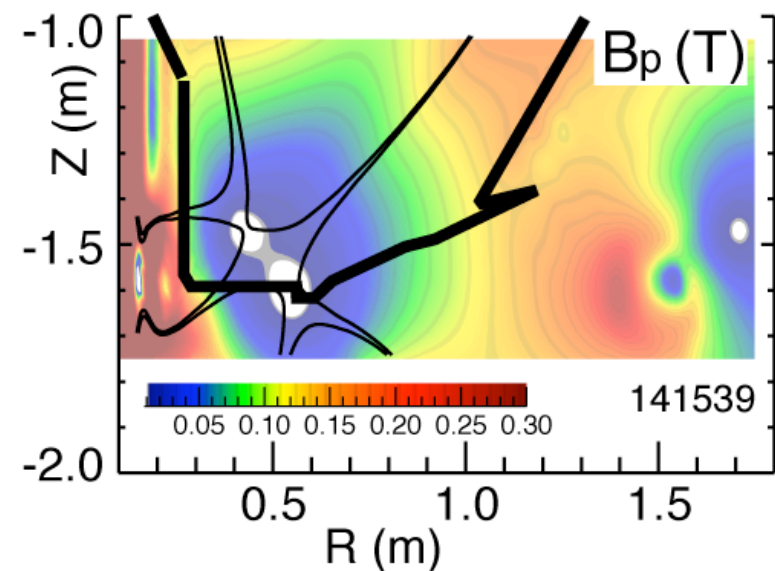
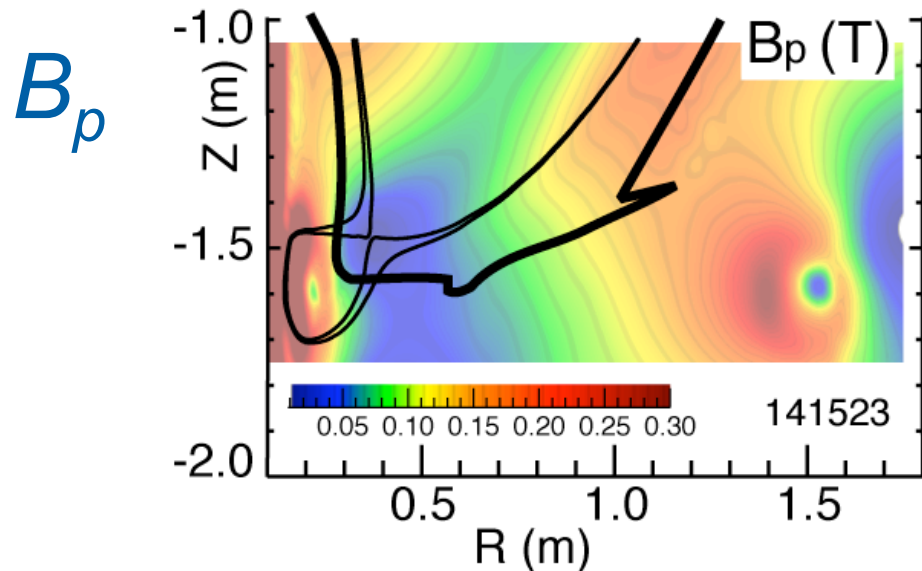
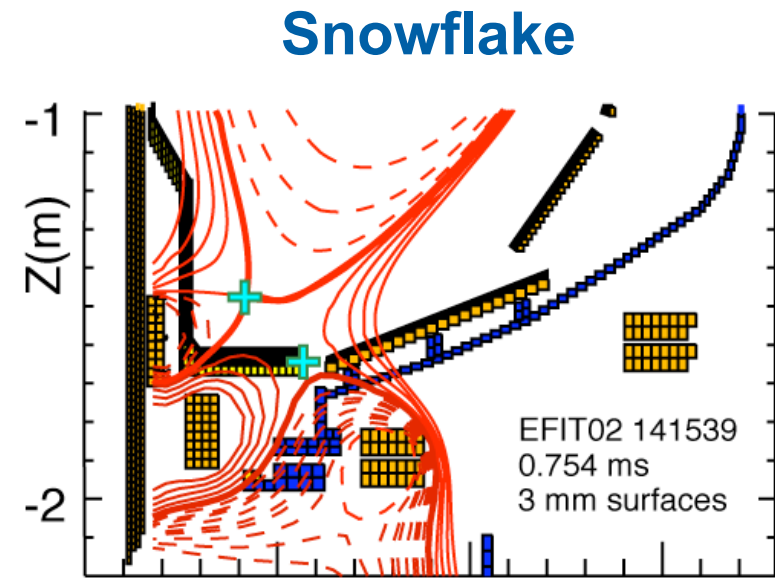
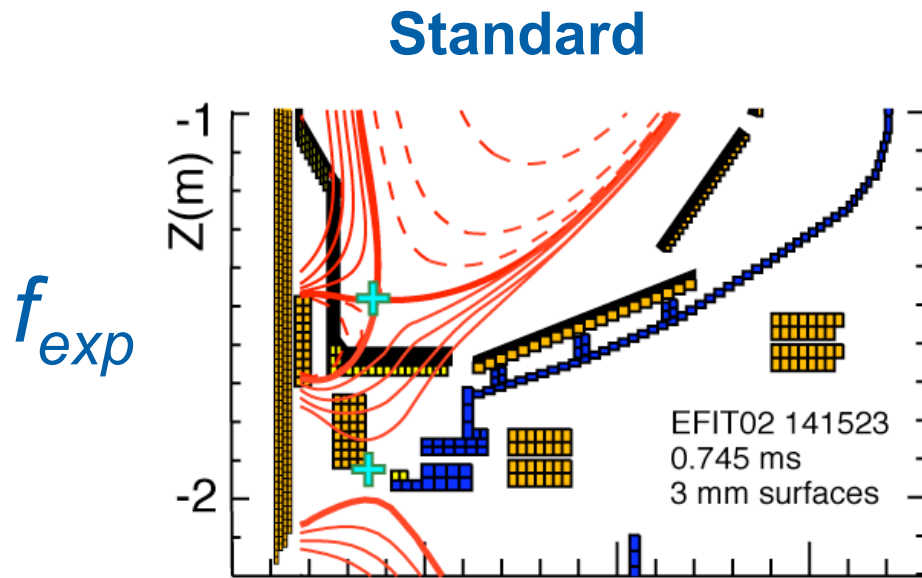
Possible snowflake divertor configurations were modeled with ISOLVER code

- ISOLVER - predictive free-boundary axisymmetric Grad-Shafranov equilibrium solver
 - Input: normalized profiles (P , I_p), boundary shape
 - Match a specified I_p and β
 - Output: magnetic coil currents
- ✓ Standard divertor discharge below:
 - $B_t=0.4$ T, $I_p=0.8$ MA, $\delta_{bot}\sim 0.6$, $\kappa\sim 2.1$

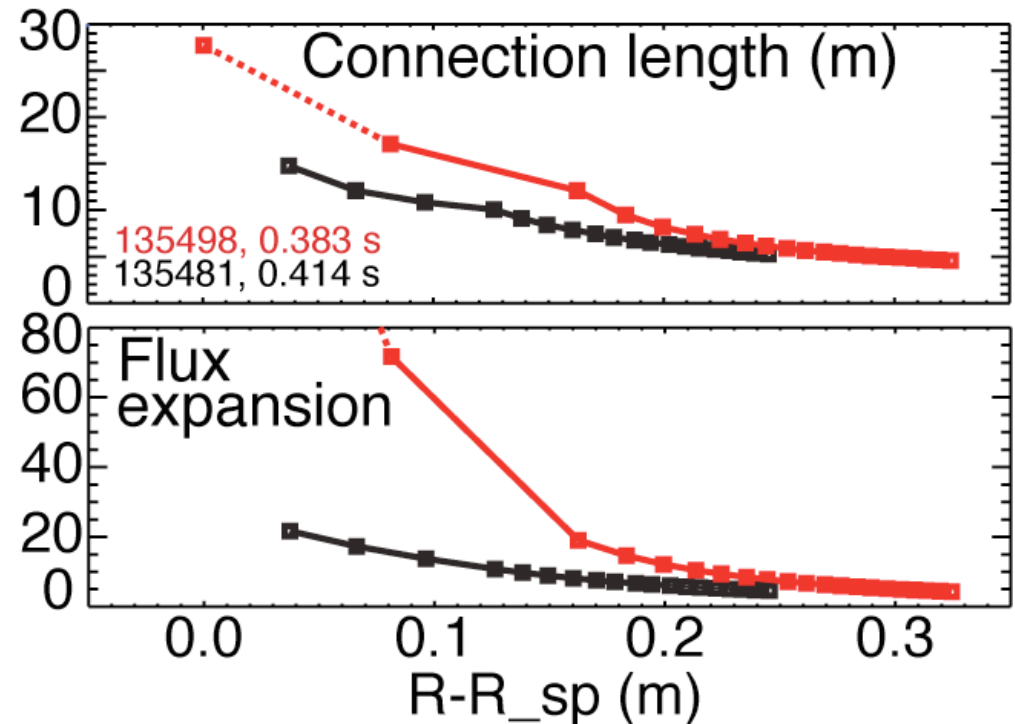
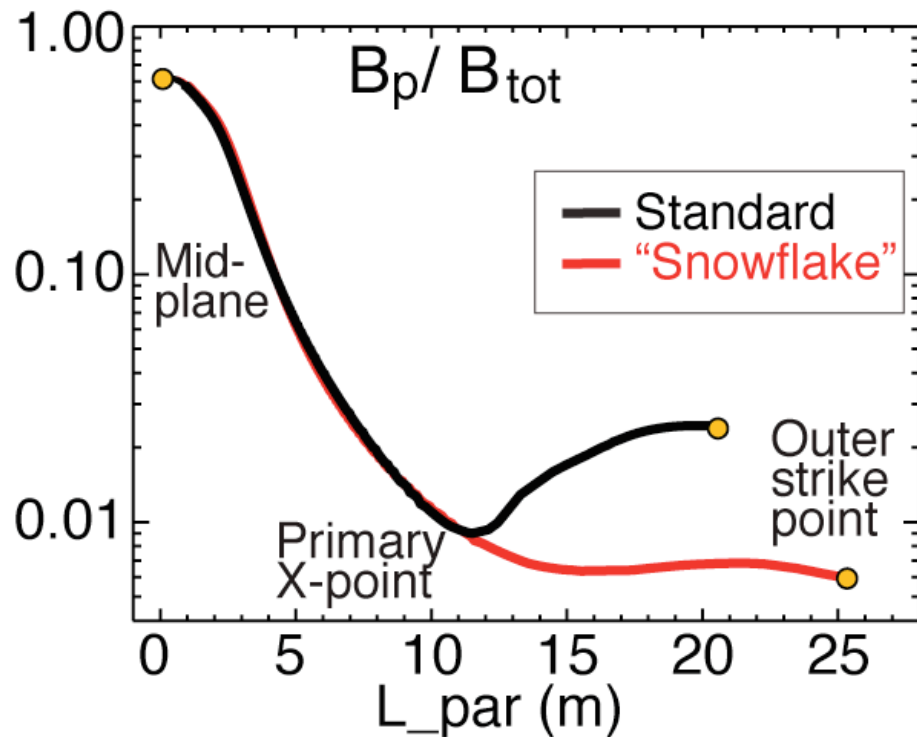


Quantity	Standard divertor	Simulated snowflake
X-point to target parallel length L_x (m)	5-10	10
Poloidal magnetic flux expansion f_{exp} at outer SP	10-24	60
Magnetic field angle at outer SP (deg.)	1-2	~ 1
Plasma-wetted area A_{wet} (m ²)	≤ 0.4	0.95

Snowflake divertor configurations obtained in NSTX confirm analytic theory and modeling



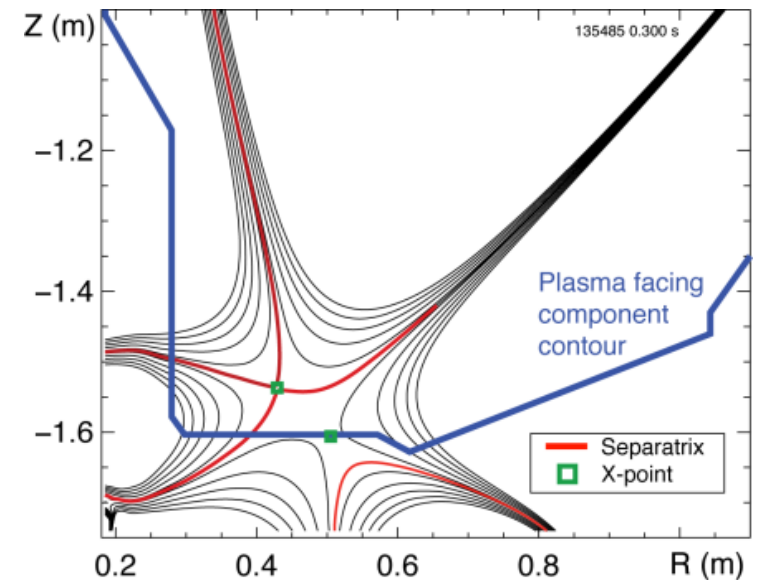
Plasma-wetted area and connection length are increased by 50-90 % in snowflake divertor



- These properties observed in first 2-3 mm of SOL $\lambda_q \sim 6-7$ mm when mapped to midplane
- Magnetic characteristics derived from EFIT and LRDFIT equilibria

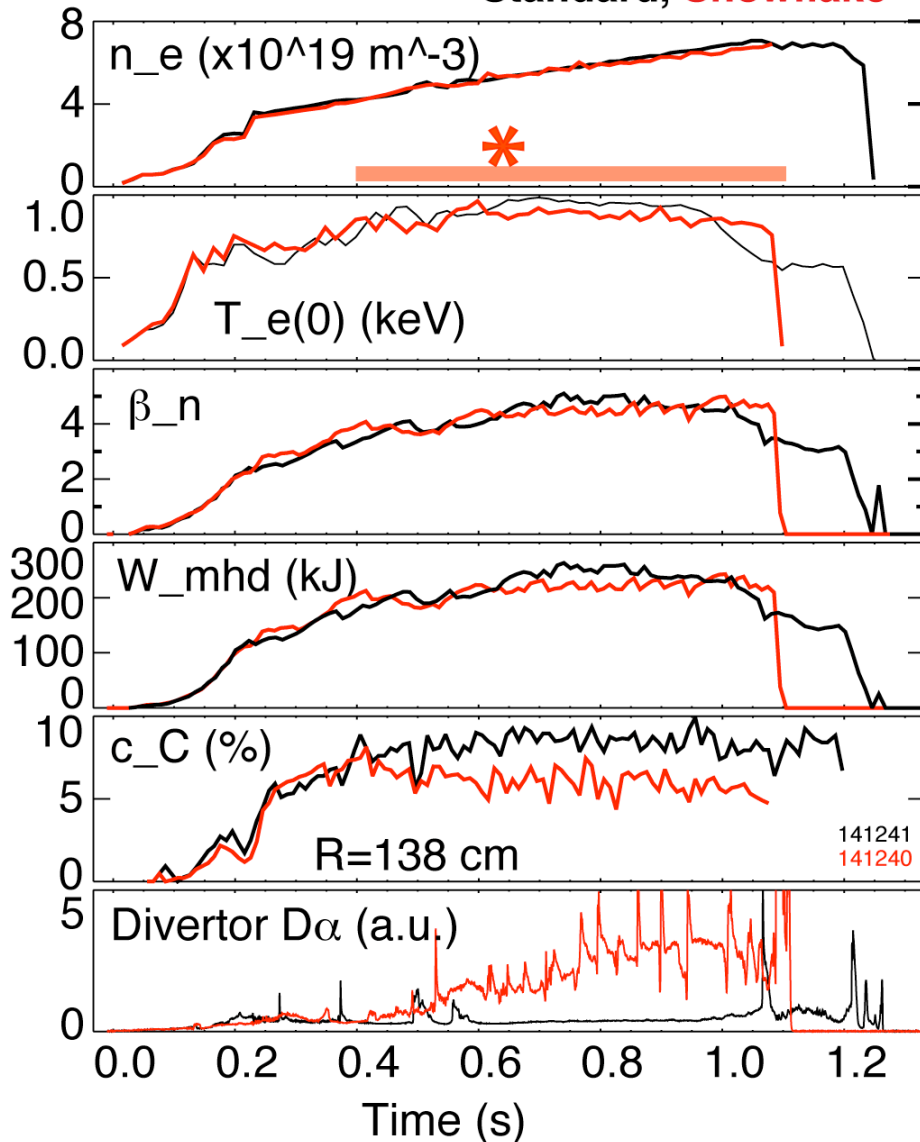
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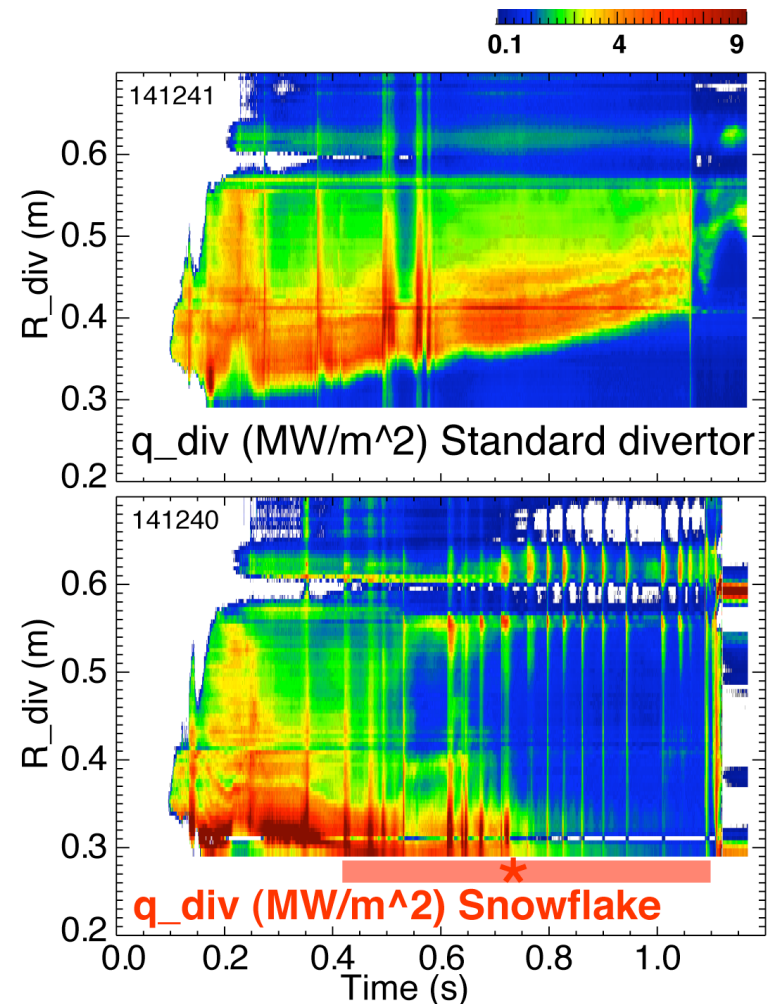
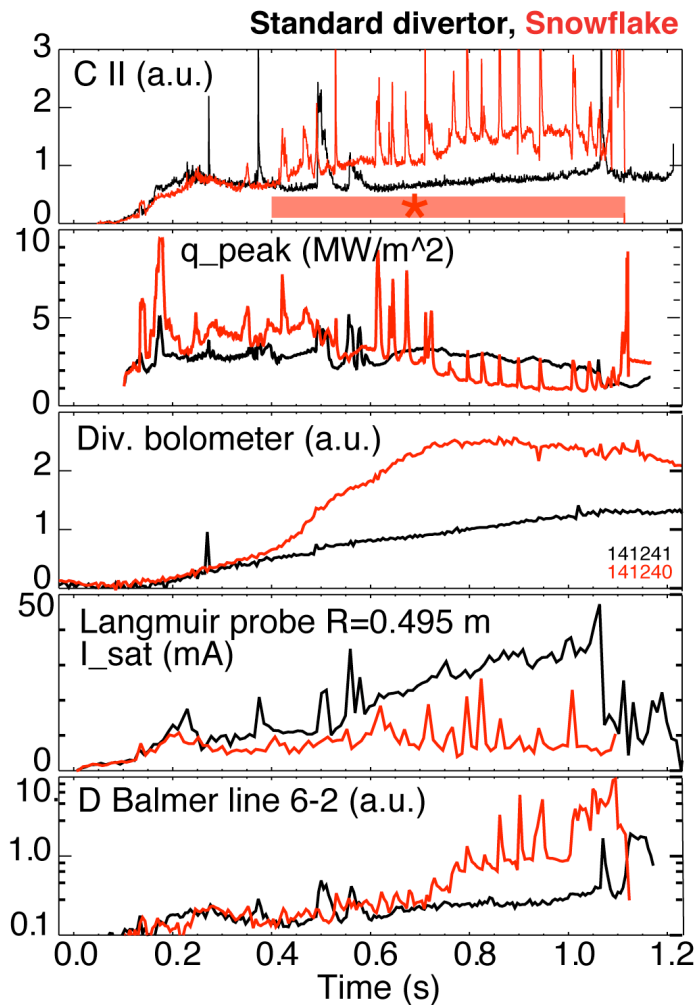
Significant core impurity reduction and good H-mode confinement properties with snowflake divertor

Standard, **Snowflake**



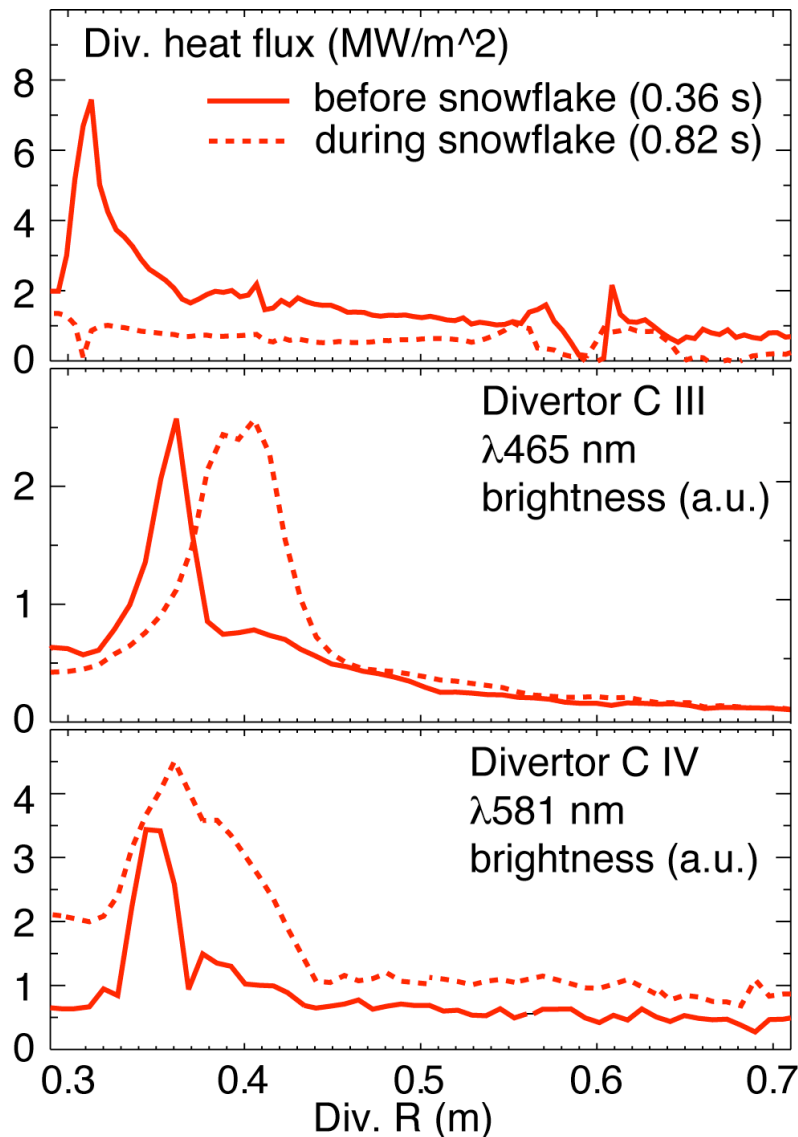
- 0.8 MA, 4 MW H-mode
- $\kappa=2.1$, $\delta=0.8$
- Core $T_e \sim 0.8\text{-}1$ keV, $T_i \sim 1$ keV
- $\beta_N \sim 4\text{-}5$
- Plasma stored energy ~ 250 kJ
- $H_{98}(y,2) \sim 1$ (from TRANSP)
- Core carbon reduction due to
 - Medium-size Type I ELMs
 - Edge source reduction

Strong signs of partial strike point detachment are observed in snowflake divertor



- Heat and ion fluxes in the outer SP region decreased
- Divertor recombination rate and radiated power are increased

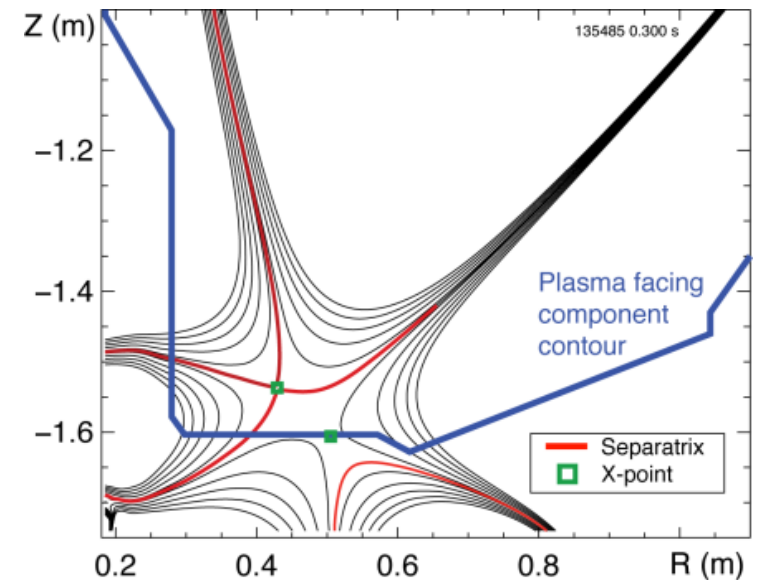
Divertor profiles show low heat flux, broadened C III and C IV radiation zones in the snowflake divertor phase



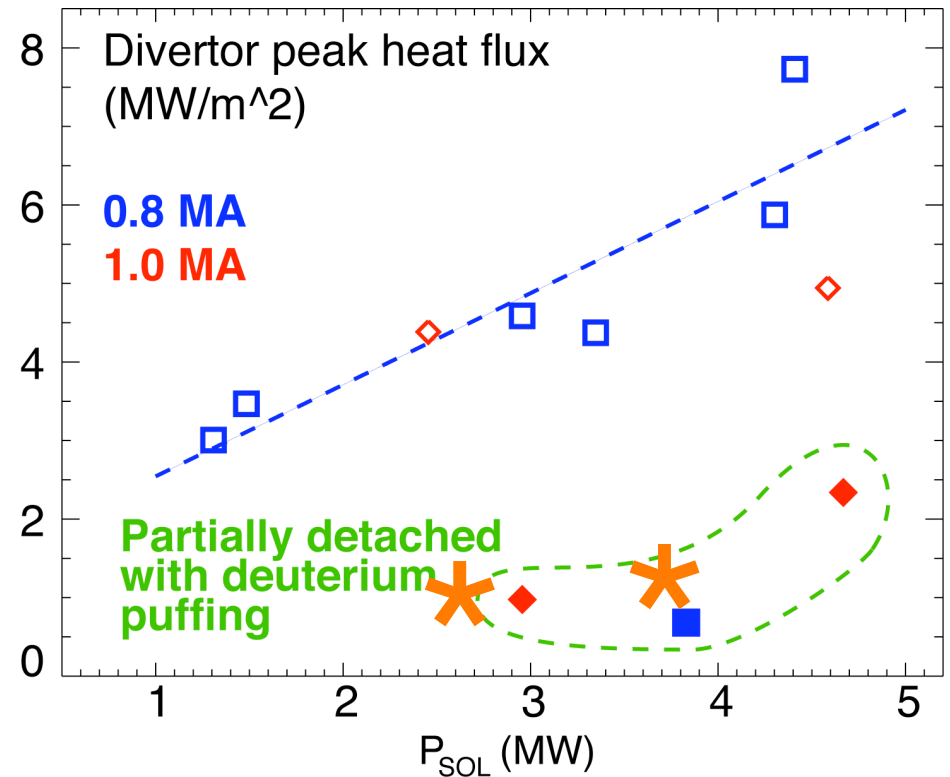
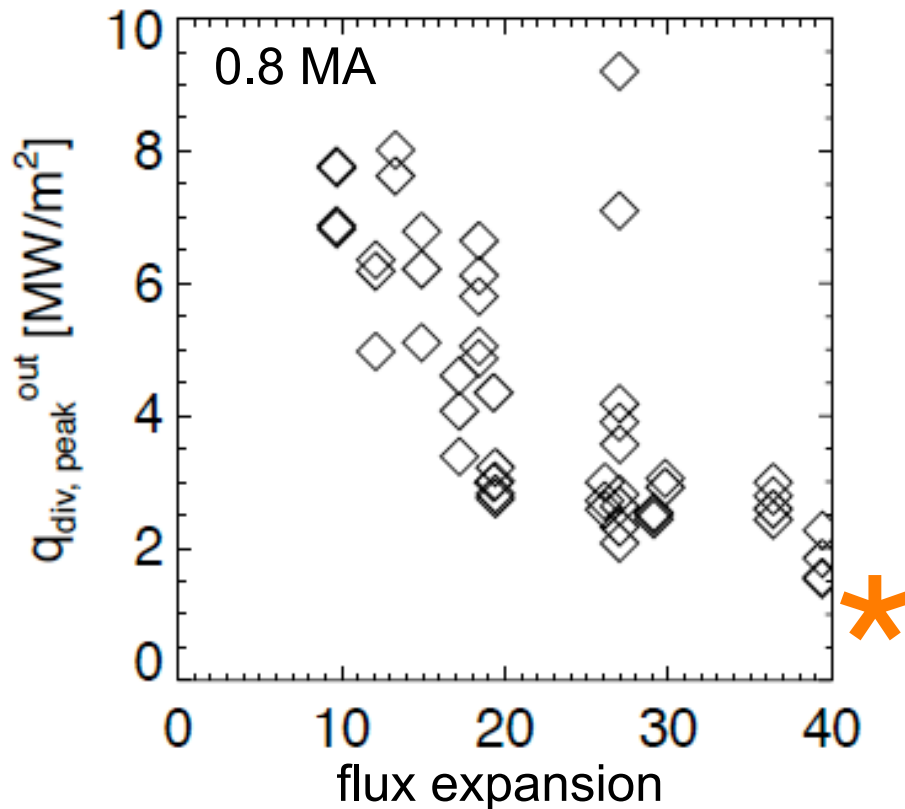
- Heat flux profiles reduced to nearly flat low levels, characteristic of radiative heating
- C III and C IV emission profiles broaden
- High- n Balmer line spectroscopy and CRETIN code modeling confirm outer SP detachment with $T_e \leq 1.5$ eV, $n_e \leq 5 \times 10^{20}$ m⁻³
 - Also suggests a reduction of carbon physical and chemical sputtering rates

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Snowflake divertor heat flux consistent with NSTX divertor heat flux scalings



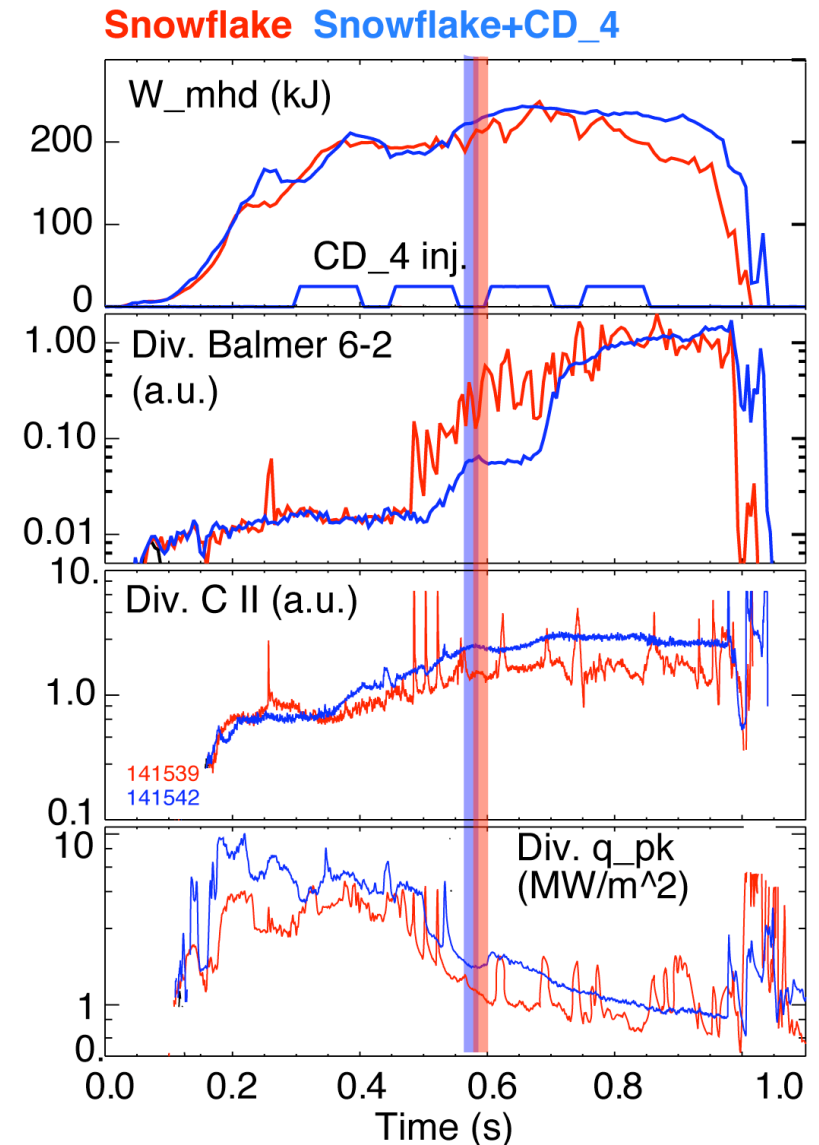
- Snowflake divertor (*): $P_{SOL} \sim 3-4$ MW, $f_{exp} \sim 40-80$, $q_{peak} \sim 0.5-1.5$ MW/m²

T. K. Gray et. al, EX/D P3-13, IAEA FEC 2010

V. A. Soukhanovskii et. al, PoP 16, 022501 (2009)

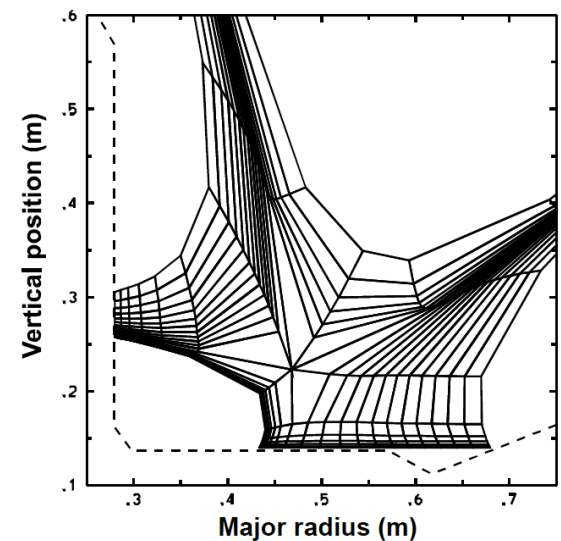
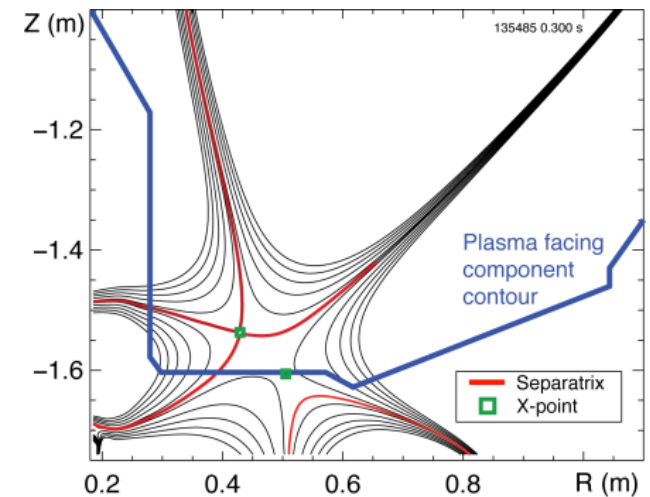
Snowflake divertor with CD_4 seeding leads to increased divertor carbon radiation

- $I_p=0.9$ MA, $P_{NBI}=4$ MW, $P_{SOL}=3$ MW
- Snowflake divertor (from 0.6 ms)
 - Peak divertor heat flux reduced from 4-6 MW/m² to 1 MW/m²
- Snowflake divertor (from 0.6 ms) + CD_4
 - Peak divertor heat flux reduced from 4-6 MW/m² to 1-2 MW/m²
 - Divertor radiation increased further



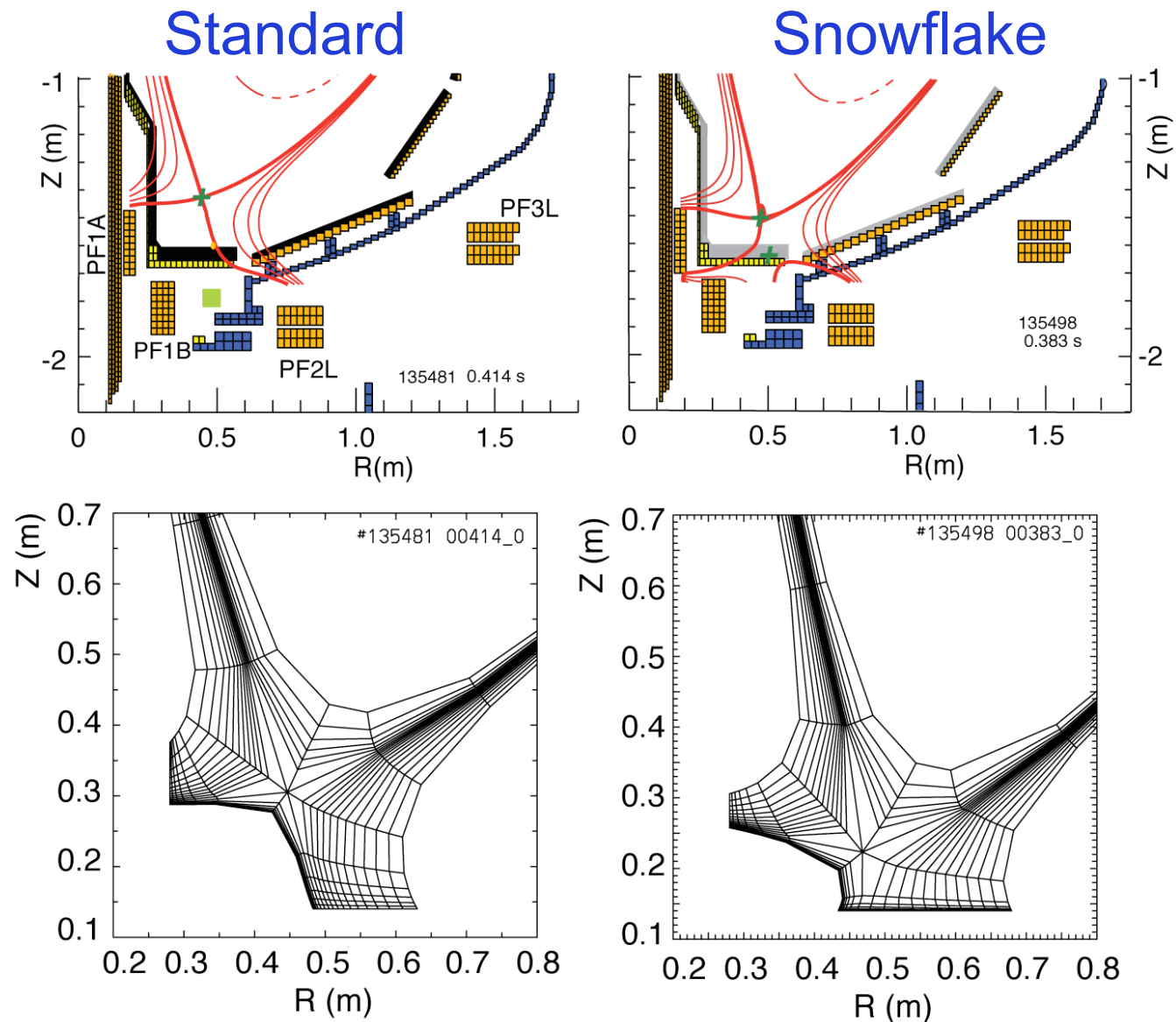
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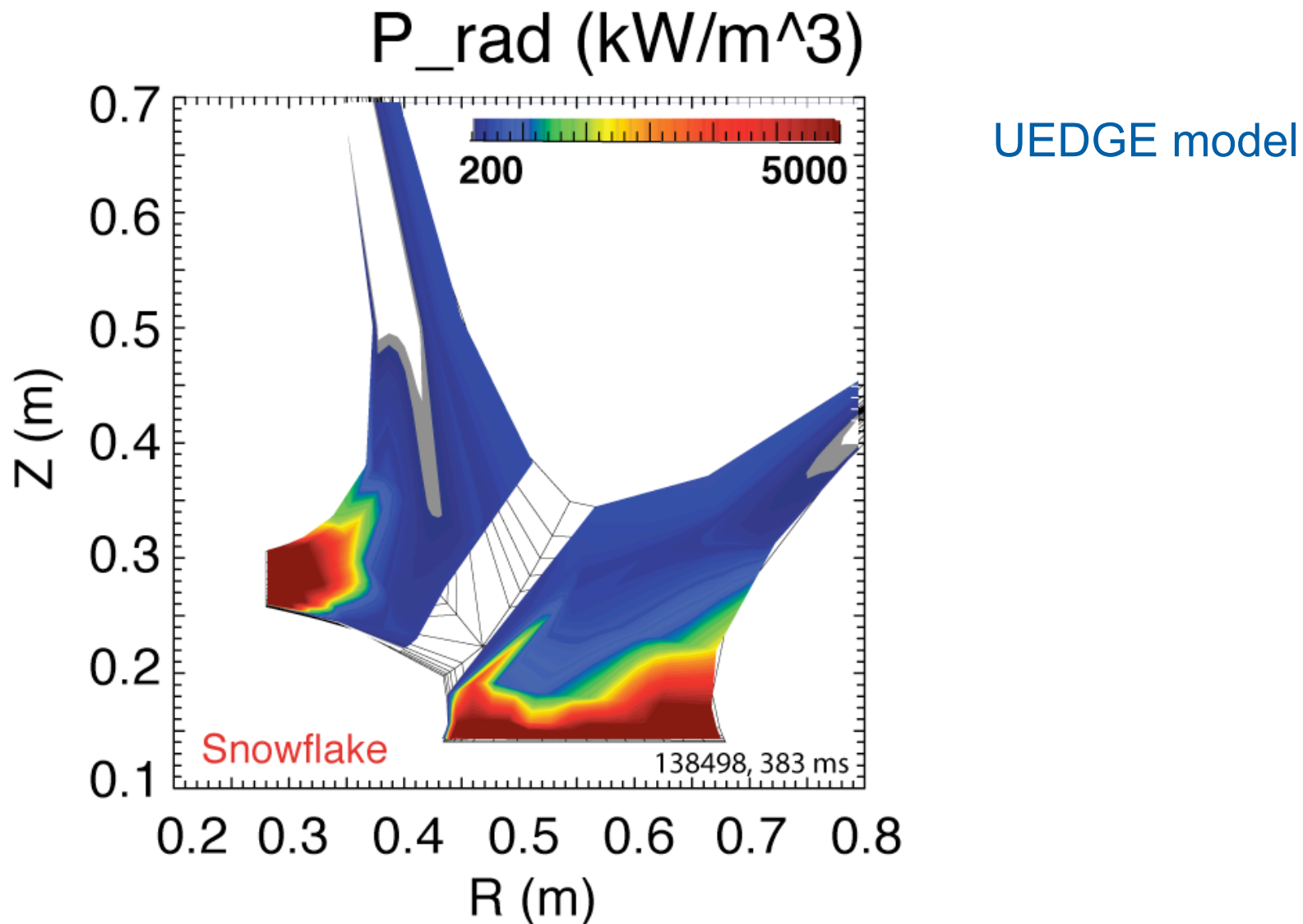


2D multi-fluid edge transport code UEDGE is used to study snowflake divertor properties

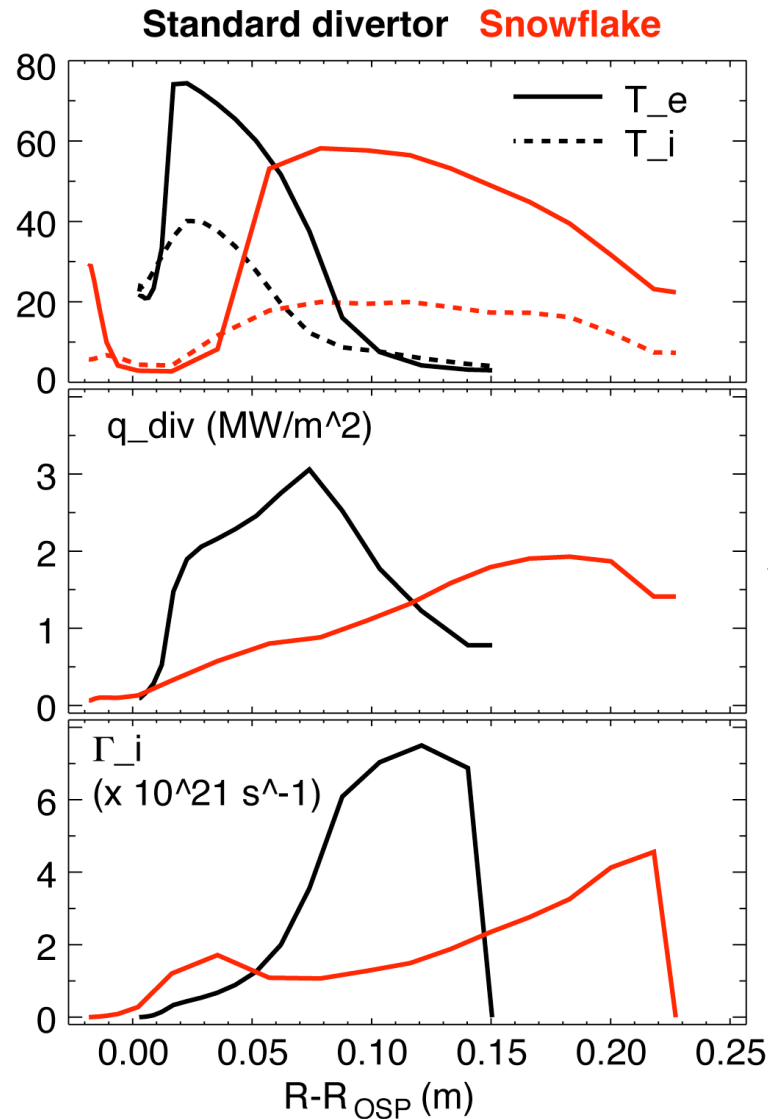
- Fluid (Braginskii) model for ions and electrons
- Fluid for neutrals
- Classical parallel transport, anomalous radial transport
- Core interface:
 - $T_e = 120$ eV
 - $T_i = 120$ eV
 - $n_e = 4.5 \times 10^{19}$
- $D = 0.25$ m²/s
- $\chi_{e,i} = 0.5$ m²/s
- $R_{recy} = 0.95$
- Carbon 3 %



Radiated power is broadly distributed in the outer leg of snowflake divertor



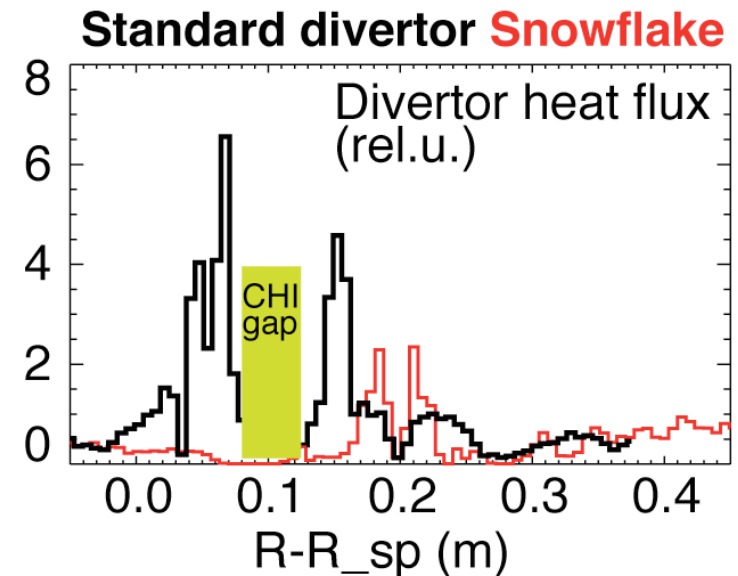
UEDGE model shows a trend toward detachment in snowflake divertor outer leg (cf. standard divertor)



UEDGE model

In the snowflake divertor outer strike point region:

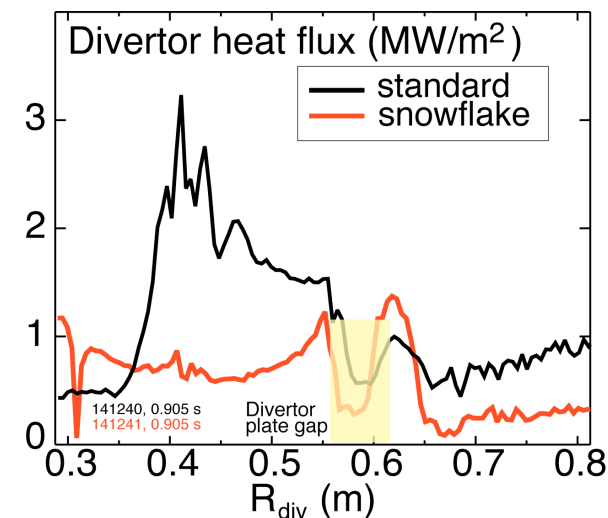
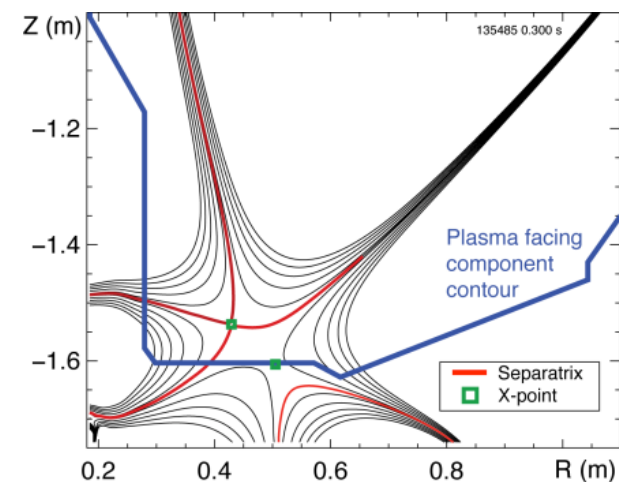
- T_e and T_i reduced
- Divertor peak heat flux reduced
- Particle flux low



Experiment

NSTX studies suggest the snowflake divertor configuration may be a viable divertor solution for present and future tokamaks

- Steady-state snowflake (up to 600 ms, many τ_E 's)
- Good H-mode confinement
- Reduced core carbon concentration
- Significant reduction in peak divertor heat flux
- Potential to combine with radiative divertor for increased divertor radiation
- This talk focused on divertor results. Planned future efforts with the snowflake divertor:
 - Improved magnetic control
 - Pedestal peeling-ballooning stability
 - ELM heat and particle deposition profiles
 - Divertor impurity source distribution
 - Divertor and upstream turbulence (blobs)



Session PP9: Poster Session VI, 10 November, Wednesday PM - Snowflake divertor presentations

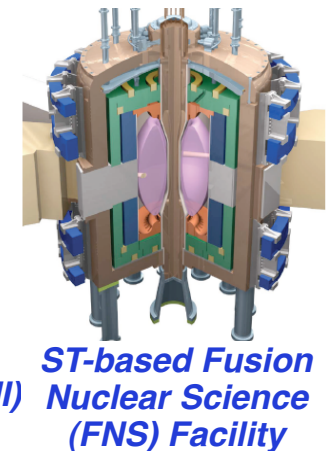
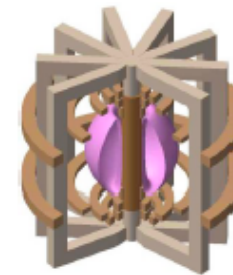
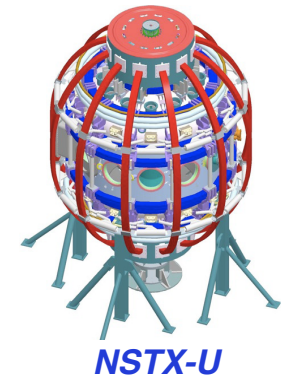
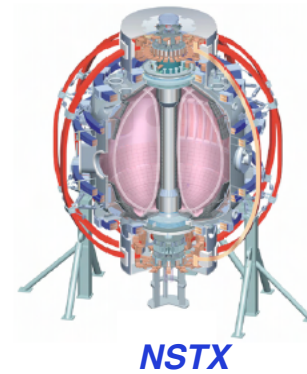
- PP9.00149 : D. D. Ryutov et. al, General properties of the magnetic field in a snowflake divertor
- PP9.00152 : M. V. Umansky et. al, Ion orbit loss effects on radial electric field in tokamak edge for standard and snowflake divertor configurations
- PP9.00136 : F. Piras et. al, H-mode Snowflake Divertor Plasmas on TCV



Backup slides

Divertor heat flux mitigation is key for present and future fusion plasma devices

- ST / NSTX goals:
 - Study high beta plasmas at reduced collisionality
 - Access full non-inductive start-up, ramp-up, sustainment
 - Prototype solutions for mitigating high heat & particle flux
- In an ST, modest q_{\parallel} can yield high divertor q_{pk}
 - in NSTX, $q_{\parallel} = 50\text{-}100 \text{ MW/m}^2$ and $q_{pk} = 6\text{-}15 \text{ MW/m}^2$
 - Large radiated power and momentum losses are needed to reduce q_{\parallel}
- In NSTX, partially detached divertor regime is accessible only
 - in highly-shaped plasma configuration with high flux expansion divertor (high plasma plugging efficiency, reduced q_{\parallel})
 - modest divertor D_2 injection still needed



Heat flux mitigation is more challenging in compact divertor of spherical torus

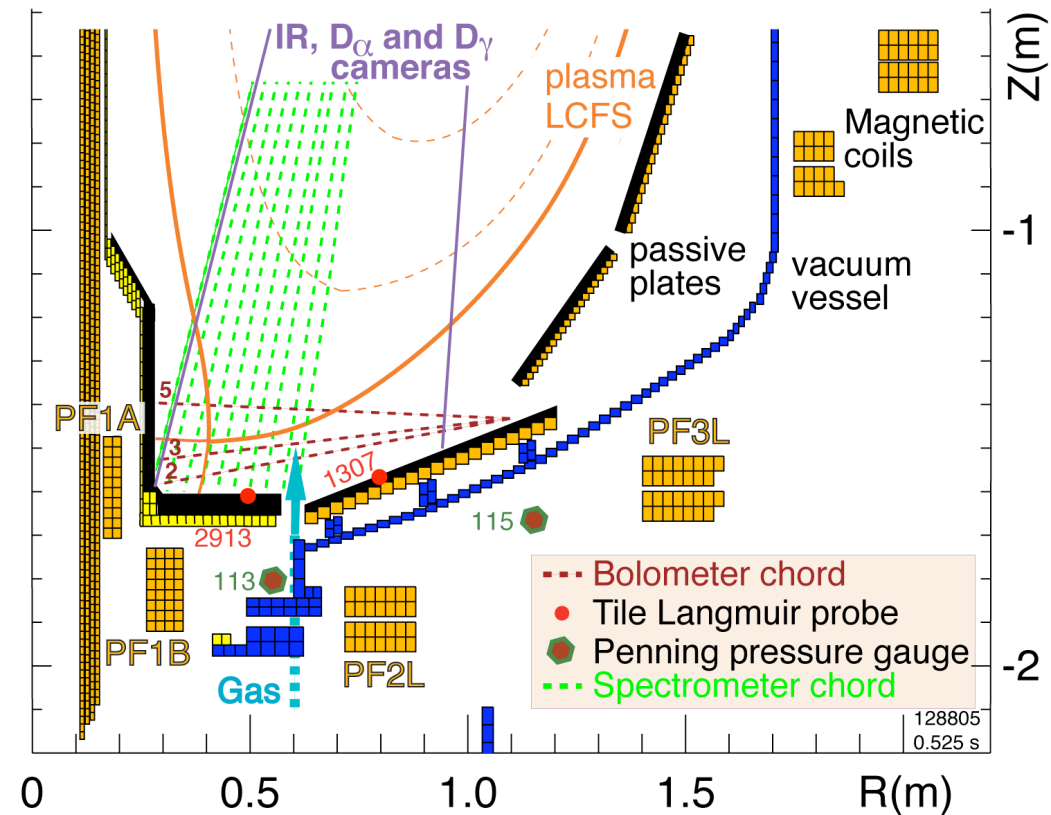
- NSTX

- $I_p = 0.7-1.4$ MA, $t_{\text{pulse}} < 1.5$ s, $P_{in} \leq 7.4$ MW (NBI)
- ATJ and CFC graphite PFCs
- $P / R \sim 10$
- $q_{pk} \leq 15$ MW/m²
- $q_{||} \leq 200$ MW/m²

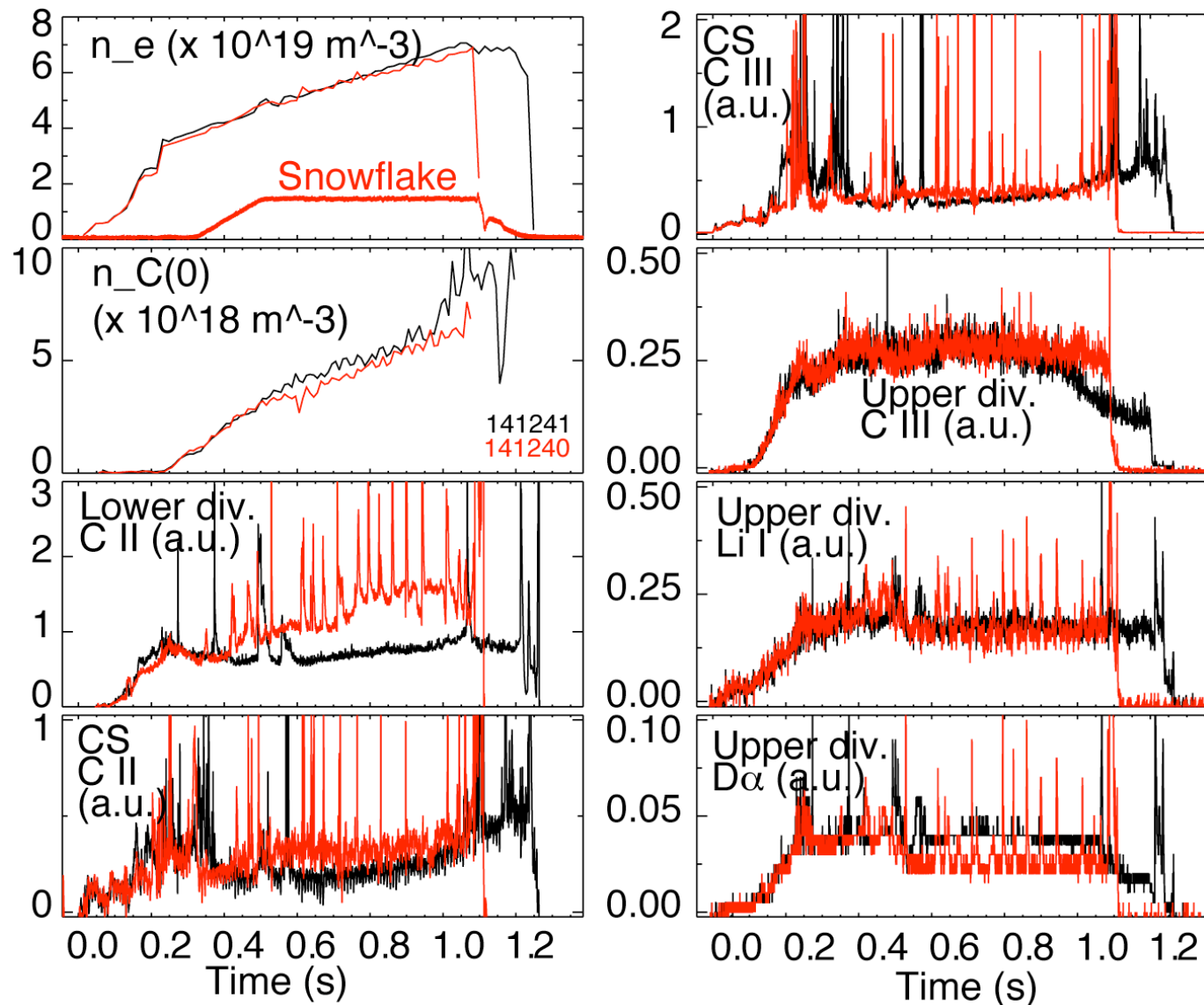
Quantity	NSTX	DIII-D
Aspect ratio	1.4-1.5	2.7
In-out plasma boundary area ratio	1:3	2:3
X-point to target parallel length L_x (m)	5-10	10-20
Poloidal magnetic flux expansion f_{exp} at outer SP	5-30	3-15
Magnetic field angle at outer SP (deg.)	1-10	1-2

Open divertor geometry, three existing divertor coils and a good set of diagnostics enable divertor geometry studies in NSTX

- $I_p = 0.7\text{-}1.4$ MA
- $P_{in} \leq 7.4$ MW (NBI)
- ATJ and CFC graphite PFCs
- Lithium coatings from lithium evaporators
- Three lower divertor coils with currents 1-5, 1-25 kA-turns
- Divertor gas injectors (D_2 , CD_4)
- Extensive diagnostic set

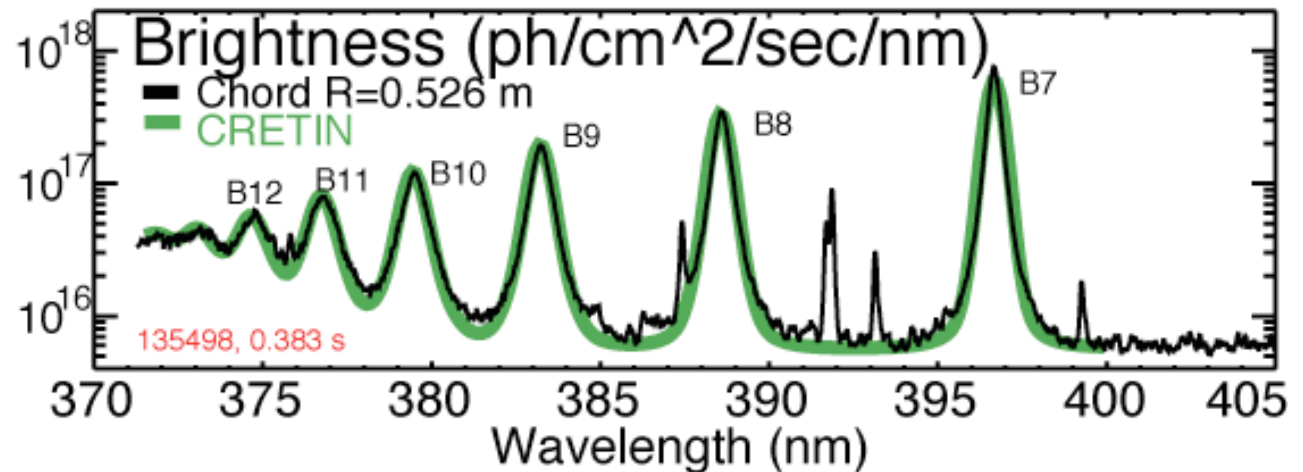
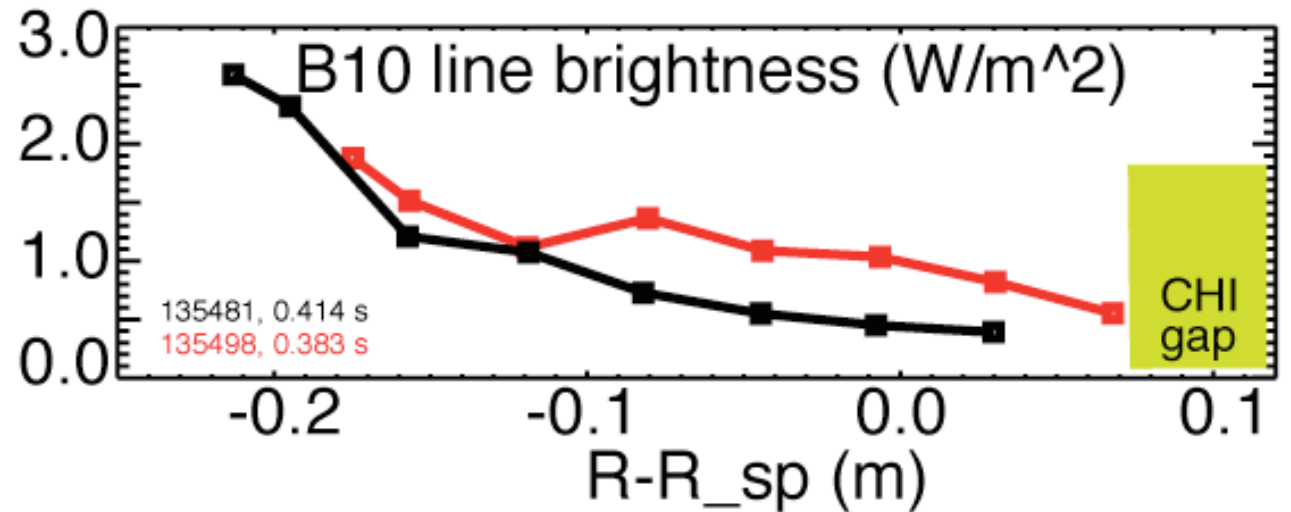


Upper divertor is unaffected by lower divertor snowflake configuration



High- n Balmer line emission measurements suggest high divertor recombination rate, low T_e and high n_e

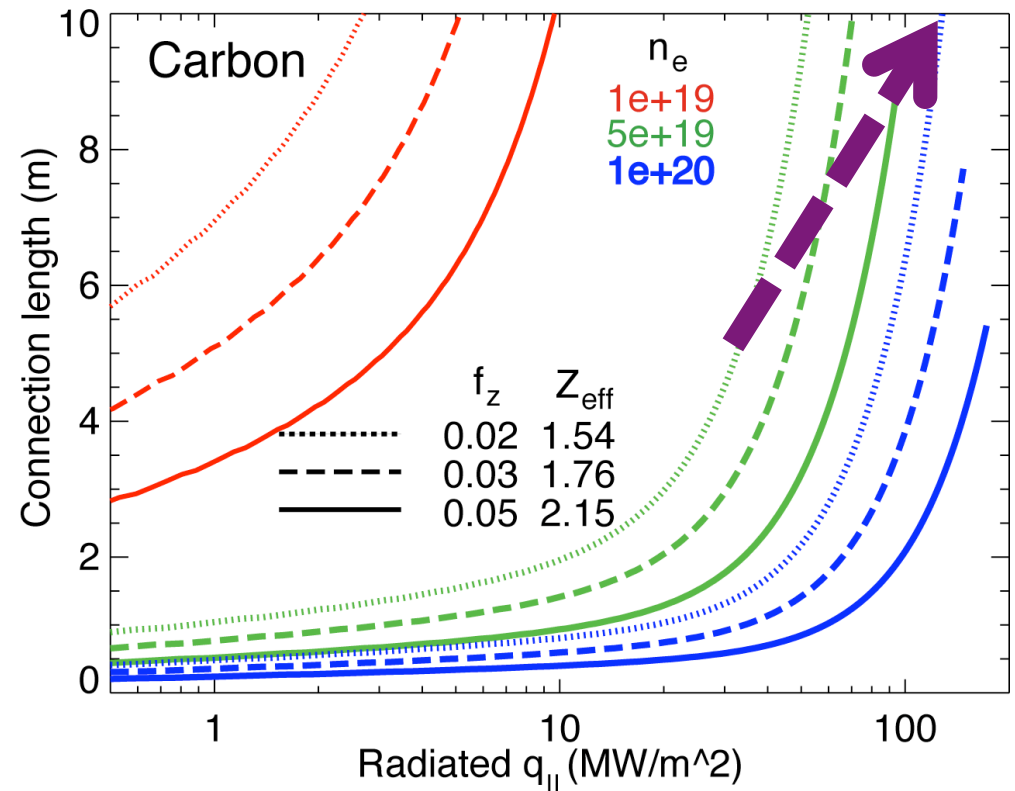
- Balmer series spectra modeled with CRETIN; Spectra sensitive to
 - Line intensity \leftrightarrow Recombination rate
 - $T_e \leftrightarrow$ Boltzman population distribution
 - $n_e \leftrightarrow$ Line broadening due to linear Stark effect from ion and electron microfield



- $T_e=0.8-1.2$ eV, $n_e=2-7 \times 10^{20} m^{-3}$ inferred from modeling

1D estimates indicate power and momentum losses are increased in snowflake divertor

- 1D divertor detachment model by Post
 - Electron conduction with non-coronal carbon radiation
 - Max $q_{||}$ that can be radiated as function of connection length for range of f_z and n_e
- Three-body electron-ion recombination rate depends on divertor ion residence time
 - Ion recombination time: $\tau_{ion} \sim 1-10$ ms at $T_e = 1.3$ eV
 - Ion residence time: $\tau_{ion} \leq 3-6$ ms in standard divertor, x 2 in snowflake



$$q_{||} = -\kappa_0 T_e^{5/2} \frac{\partial T_e}{\partial x}$$

$$\frac{\partial q_{||}}{\partial x} = -n_e n_z L_Z(T_e)$$