Measuring Error Fields in ITER Before Its First Plasma*

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Challenge to Meet Implicit ITER Requirement for Detecting Error Fields < 5 × 10⁻⁵B_T

Primary concern has been components with toroidal periodicity n = 1

$$B_{\text{TMEI}} \equiv \sqrt{0.2B_{1,1}^2 + 1.0B_{2,1}^2 + 0.8B_{3,1}^2} \le 5 \times 10^{-5} B_{\text{T0}} \text{ (at } q = 2 \text{ surface)}^*$$

Recent study shows higher poloidal harmonics may also be important[‡]

- Desirable to measure error fields in ITER *as-built* to characterize basic coil perturbations
 - Requires TF & PF coils at operating temperature and under EM loads
- Accurate positioning and alignment of sensors required to detect perturbations ~0.1 mT in presence of background fields 2 - 5 T
 - Ferromagnetic Inserts (FI) to reduce TF ripple affect local measurements
- Approach adopted depends on accuracy deemed necessary
 - Ensure 18 Correction Coils in ITER can provide first-order compensation
 - Plasma response can then reveal more subtle features of error fields

Measurements *Outside* TF Coil Could Identify Some Manufacturing and Assembly Defects

- Only field *errors* ($m,n \neq 0$) are present outside TF coil envelope
- Ripple (n = 18) component decays roughly as R⁻ⁿ so low-n components dominate at large R
- Model TF as 18 filamentary coils and apply low-order perturbations



Measure B_R, B_Z at well defined locations with Hall-effect sensors
 – Discriminate from background field by measuring with TF on and off

Measurements at 0.1mT Level Can Detect Low-*n* Errors at q = 2 Surface of Order $5 \times 10^{-4}B_{T0}$

• Decompose normal component from perturbed TF on q = 2 surface



- Assessed effects of FI by modeling them as discrete dipoles
 - n = 1 variation of M_{sat} by 5% only slightly affects sensitivity to n = 1
- Including |B| data from array of NMR sensors at inboard midplane of vacuum vessel improves separation of low-n components somewhat
- For higher accuracy, would need to perform electron beam mapping

Planned "Saddle" Coils in ITER Can Be Used to Characterize Field Errors from PF Coils

- Saddle Coils (SC or Partial Flux Loops) mounted on Vacuum Vessel inner wall, toroidally span all or part of a VV sector (40°)
- 22 SC span poloidal circumference in 6 of 9 VV sectors



- Conductor positions specified to be known to mm accuracy
 - Calculate changes in mutual inductance from perturbations (*e.g.* shifts, tilts) of PF coils and the SC themselves
 - Δψ_{max} ~ 2mWb typically for perturbations ~10⁻³R₀, I_{PF} = 10kA
 - To measure small changes in mutuals, take one sector as reference and difference equivalent coils in other sectors ⇒ 110 flux differences

Compensate for Coupling of SC to PF Coils Due to Nearby Ferromagnetic Inserts

- SC are close to FI between inner and outer shells
- Model FI as discrete dipoles (864) to calculate flux through each SC

$$\Delta \psi_{j} = \frac{\mu_{0}}{4\pi} \sum_{i} \oint_{C_{j}} \frac{\boldsymbol{m}_{i} \times \boldsymbol{r}_{ij}}{r_{ij}^{3}} \cdot d\boldsymbol{s}_{j}$$

Apply constant TF to saturate FI



- For $B_{\rm PF} << B_{\rm TF}$, change in coupling produced by FI $\Delta \psi_{\rm FI} \propto I_{\rm PF}/I_{\rm TF}$
- $\varDelta \psi_{\rm FI}$ can exceed that from prototypical PF coil perturbations $\varDelta \psi_{\rm PF}$
- If we measure coupling at same I_{PF} and two values of I_{TF} , then $\Delta \psi_1 = \mu I_{PF0}/I_{TF1} + \Delta \psi_{PF}$ and $\Delta \psi_2 = \mu I_{PF0}/I_{TF2} + \Delta \psi_{PF}$, so $\Delta \psi_{PF} = (I_{TF1} \Delta \psi_1 - I_{TF2} \Delta \psi_2)/(I_{TF1} - I_{TF2})$



Use Numerical Techniques to Extract Both Coil Displacements and Error Fields from Data

- Allow both perturbations of PF and SC from nominal geometry to be free parameters determined by data from excitation of *all* coils
- In-plane shifts (Δx , Δy) and tilts ($\Delta \alpha_x$, $\Delta \alpha_y$) of 12 PF coils and basic perturbations (ΔR , ΔZ , $\Delta \alpha_{\phi}$, ΔA) of 132 SC \Rightarrow 576 unknowns **X**
- 110 flux differences \times 12 PF coils \Rightarrow 1320 measurements **S**
- Calculate elements of (sparse) matrix \mathbb{M} relating **S** to **X**: **S** = \mathbb{M} **X**
- Use SVD to calculate condition of $\mathbb M$ and its pseudo-inverse
 - Matrix is reasonably well conditioned but solution degenerate w.r.t.
 displacements of reference SC sector
- Determine subset $\boldsymbol{X}_{\text{SC}}$ then recalculate \mathbb{M}_{PF} for coil displacements
- Displacements of each PF coil are well determined by data
 - predominantly from a few SC for each PF coil

Methods Used to Measure Basic Coil Displacements and Error Fields Depends on Accuracy Needed

- Proposed accuracy $(5 \times 10^{-5}B_T)$ difficult, time consuming and expensive, so
- It is critical to establish what components at what level are really important
- Relatively simple techniques can reveal errors which can be compensated with ITER's (external) Correction Coils
- For TF, arrays of Hall sensors (~100) accurately mounted outside cryostat can reveal errors leading to n = 1 components ~5 × 10⁻⁴ B_T at q = 2 surface
 - For higher sensitivity to TF errors, use electron-beam measurements
- For PF coil errors, measure mutual inductances to full set of Saddle Coils
 - Make measurements with TF applied to saturate Ferromagnetic Inserts and correct for effect on PF coupling by measuring at different TF levels
 - Ideally make use of accurate metrology of loops on inner VV surface, but
 - Can also refine flux loop geometry through analysis of full data set to determine coil perturbations responsible for errors $\sim 5 \times 10^{-4} B_{T}$