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Compositional changes of lithium coatings on TZM molybdenum during plasma bombardment

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Abstract

The Titanium-Zirconium-Molybdenum alloy TZM has previously been used as a metallic plasma-facing component in Alcator C-Mod is being considered for use in NSTX-Upgrade. The time evolution of lithium (Li) coatings on TZM are studied in Magnum-PSI, a linear plasma device capable of ion fluxes up to 10²⁵ m⁻²s⁻¹ at electron temperatures < 5 eV. A series of 5 s exposures to a D^+ plasma were run on a bare TZM sample then repeated after an evaporation of 100 nm of Li. The temporal and spatial variation of neutral Li and oxygen (O) radiation were monitored using optical emission spectroscopy (OES) and a fast camera with a Li-I (671 nm) filter. The O-I (777 nm) line intensity decreased during discharges while the Li-I line intensity increased. The ionization mean free path (MFP) of Li was calculated and validations against the ADAS collisional-radiative model (CRM) will be reported. Separate measurements of physical sputtering rates with a 100-1000 eV D⁺ ion beam incident on Li-coated TZM were also obtained and compared with theoretical predictions.

Local material migration in the divertor occurs at fast gross rate but slower net rate



Adapted from P. Stangeby, PSI 2012



Net erosion rates have been explored over a limited parameter range

Experiment	lon Flux (m ⁻² s ⁻¹)	Magnetic Incidence	lon species	Target Material	Result
PISCES-B	8*10 ²¹	normal (90°)	D⁺, He⁺	Li/O mixed material	Complete removal of O layer after ~400s (unknown thickness) ¹
DIII-D (DiMES)	6*10 ²³	grazing angle	D+, C+	Мо	~0.8 nm/s net (1.4 nm/s gross) erosion rate ²
ASDEX-U (¹³ C Injection)	1-5*10 ²³	grazing angle	D+	Carbon	Re-deposition fraction ~0.28 (forward field), ~0.14 (reverse) ³

- 1. R. Doerner et al., JNM 2001
- 2. P. Stangeby et al., APS 2012
- 3. L. Aho-Mantila et al., JNM 2011

3D Monte Carlo codes have had limited success verifying net erosion rates in tokamaks

WBC/REDEP

Net Mo erosion in C-Mod: 10x higher than simulation

(J.N. Brooks, JNM 2011)

Mo deposition profile in DIII-D



ERO/SOLPS

¹³C deposition profile in ASDEX-U



toroidal coordinate (mm) toroidal coordinate (mm)

L. Aho-Mantila, JNM 2011

(downstream is relative to B field direction)



Motivates experiments with divertor plasma simulators with better diagnostic access

- Magnum-PSI
 - $\Gamma < 10^{24} \text{ m}^{-2}\text{s}^{-1} \text{ D}^+$, $T_e < 2 \text{ eV}$, $n_e < 5^*10^{20} \text{ m}^{-3}$
 - 5 s pulses, B~1 T (> 60 s, 2.5T superconducting- coming 2013)
 - Normal incidence: no magnetic pre-sheath
 - Evaporative Li coatings applied in-situ, calibrated with quartz crystal microblanace (QCM)



http://www.differ.nl/en/magnum_plasma_en



Diagnostic suite provides *spatially comprehensive, in-situ, real-time* re-deposition data

- Thomson Scattering provides n_e(r), T_e(r)
 - Single chord 2 cm from target, 1.8 mm resolution
- Visible Spectroscopy gives $I_{Li}(t)$, $I_{Oxygen}(t)$, $I_{H}(t)$
 - 350 nm < λ < 800 nm, 0.2 nm, 5-10 Hz resolution
- Fast camera w/ Li-I (671 nm) filter gives I_{Li}(r,t)
 - 0.285 mm x 0.285 m, ~2 kHz resolution





Fast-camera Image Li-I Emission



ionization (re-deposition) rates S_{iz,Li}(r,t) and S_{iz,O}(t)

Measure

M.A. Jaworski

ADAS Collisional-Radiative Model (CRM) predicts substantial local re-deposition of Li, negligible re-deposition of O







	ATJ Graphite	TZM Molybdenum	Tungsten
T _e (eV)	0.7 ↔ 1.7	0.6 ↔ 1.7	0.6 ↔ 1.7
n _e (10 ²⁰ m ⁻³)	1.0 ↔ 3.8	1.0 ↔ 4.0	0.8 ↔ 3.8
Γ _D (10 ²³ m ⁻² s ⁻¹)	0.6 ↔ 3.4	0.5 ↔ 3.6	0.4 ↔ 3.4
Li MFP (mm)*	31 ↔ 0.22	94 ↔ 0.21	137 ↔ 0.22
O MFP (mm)*	5.6e6 ↔ 250	7.0e7 ↔ 230	8.3e7 ↔ 250
# discharges	5 (bare) 3 (100 nm Li)	5 (bare) 8 (100 nm Li)	6 (bare) 6 (100 nm Li)

*calculated from ADAS Data Set (ADF11/SCD-96), www.adas.ac.uk, assuming E_{ejected}=1 eV



Li-I intensity continuously increased throughout discharge, while O-I intensity decays exponentially





Physical Interpretation: Difference in local re-deposition increases relative concentration of Li over time



Predict *net erosion* rates from *local* re-deposition with 1-D analytic/numerical model

- Areal impurity density *n(r,t)*
- Gross erosion rate *R*_{ero}(*r*,*n*)
 - Assume sputtering ~
 cosθ, yield Y₀ = 0.1
 - Ejection energy assumed to be 1 eV
- From a point source:
 - Sputtered distribution
 f_{sputter}(r',t')
 - Ionization distribution $f_{iz}(r',t')$

$$R_{ero}(r,t) = \begin{cases} Y_0 0.6n_e \left(\frac{T_e + \gamma T_i}{m_i}\right)^{1/2}, n > 0\\ 0, n = 0 \end{cases}$$

$$f_{sputter}(r',t') = \frac{1}{vt'}\Big|_{r' < vt'}$$

$$f_{iz}(r',t') = \frac{v}{\lambda_{iz}} \exp\left(-\frac{vt'}{\lambda_{iz}}\right)\Big|_{r' < vt'}$$

$$\mathbf{v}$$
 = ejected velocity
 λ_{iz} = ionization MFP

Predict *net erosion* rates from *local* re-deposition with 1-D analytic/numerical model (continued)

• Re-deposition distribution $f_{redep}(r')$:

$$f_{redep}(r') = \int_{r'/v}^{\infty} f_{sputter}(r',t') f_{iz}(r',t') dt' = \frac{1}{\lambda_{iz}} \Gamma\left(0,\frac{r'}{\lambda_{iz}}\right)$$

• Total re-deposition rate R_{redep}(r,t):

$$R_{redep}(r,t) = \int_0^\infty f_{redep}(r-r')R_{ero}(r',t)dr'$$

Incomplete Gamma function Γ(0,x)

• Differential equation for *n(r,t)*:

$$\frac{dn(r,t)}{dt} = \underbrace{R_{redep}(r,t) - R_{ero}(r,t)}_{R_{ero,net}(r,t)} = R_{ero} \begin{bmatrix} 1 - F_{redep} \end{bmatrix}$$

$$F_{redep} = re-deposition$$
fraction

Surface impurity density evolves quickly for high λ_{iz}/σ_{Te}

• $\lambda_{iz}/\sigma_{Te} = 185$ (typical for O in Magnum)

- High escape probability



Initial condition: **flat areal density profile** $n(r,t=0) = n_0$

Normalize time:

$$r = \frac{n_0}{R_{ero} (r = 0, t = 0)}$$

n = areal impurity density r = radial distance from axis of plasma column σ_{Te} = HWHM of T_e profile

Note: choice of σ_{Te} as normalization for r is arbitrary.



Surface impurity density evolves slowly for low λ_{iz}/σ_{Te}

• $\lambda_{iz}/\sigma_{Te} = 0.04$ (typical for Li in Magnum)

- Low escape probability



Average re-deposition fraction changes drastically between $5 < \lambda_{iz}/\sigma_{Te} < 100$

• Define
$$\langle F_{redep} \rangle = \frac{1}{a} \int_0^a F_{redep}(r, t=0) dr$$



Compare coating lifetime in model with experimental data

- Assume emission intensity ~ re-deposition rate
 - Fit an exponential curve to $\langle F_{redep}(t) \rangle$ when it begins decreasing





Initial comparison with data indicates importance of absolute sputter yield determination

• TRIM gives Y_0 =2e-4 for 20 eV D⁺ on O

- Does not take into account surface temperature

 τ calculated from spectroscopy data $I(t) = I_0 exp(-t/\tau) + I_1$



n_e (10 ²⁰ m ⁻³)	T _e (eV)	λ_{iz} / σ_{Te}
1.50	1.50	190
1.90	1.60	94
0.70	0.90	4.2e4
0.60	0.90	4.7e4
1.80	1.05	3400
2.70	1.05	2100
1.00	0.90	3.1e4
2.70	1.70	41
3.50	1.30	240
4.00	1.05	1400

Initial comparison with data indicates importance of absolute sputter yield determination (continued)

- Mixed-material surface (D, O, Li)
- Sputtering only occurs off first few monoloyers
 - Bulk n_{Li}, n_O unimportant
- Why does Li-I radiation increase continually?
 - Even after O-I intensity has saturated
 - If initially LiOH, should increase by factor of ~2 and stop





Caveats

- λ_{iz} will also vary with σ_{ne}
 - But σ_{ne} usually scales with σ_{Te}
- Other physics processes must be important
 - Adsorption/Desorption, Evaporation, etc.
 - Additional source/sink terms due to diffusion in the lithium material¹
- Code assumes slow variation of λ_{iz} with r
- ADAS data set contains limited resolution
 - Correct 2D interpolation between points is important

¹R. Bastasz, J.A. Whaley, Fus. Eng. Design 2004



- Refine analysis of spectroscopy data
 - Apply spectrometer calibration to directly model the line emission and compare with absolute brightness
 - Incorporate geometric factors accounting for sight line of spectrometer
 - Goal: obtain quantitative agreement between simulations and measurements over wide range of λ_{iz} / σ_{Te}
 - **f**_{redep} values
 - "coating lifetime" τ
- Improve accuracy of model:
 - Add in additional source/sink terms for specific materials
 - Refine sputtering yields using Bodhansky/TRIM
 - Time-resolved T_e measurement from D line ratios
- Longer term (new experiments):
 - Heated (liquid) samples, non-zero impact angle
 - Additional coating materials (B, Sn, Sn-Li?)

Obtained measurements of D⁺ sputtering yield on Li-coated TZM at room temperature



Obtained measurements of D⁺ sputtering yield on Li-coated TZM at room temperature (continued)

- 2 keV D⁺ ions, beam current ≈2.0 µA
- Li thickness ≈ 1.1 µm
- Sputtered Li measured with dual-crystal QCM





Obtained measurements of D⁺ sputtering yield on Li-coated TZM at room temperature (continued)

• Data Analysis:

$$M \equiv \frac{\sigma_f}{\sigma_q} \qquad F \equiv \frac{(f_q - f_c)}{f_q} = \frac{-\Delta f}{f_q} \qquad M = F$$

- Sputter Yield (atoms/ion)¹: $Y_0 = \frac{N_A \dot{m}_{net}}{M f_{cm} i_{im}} + \frac{N_A R Y_{ref}}{M}$. Note:
- Simplifying assumptions:
 - All Li converted to Li₂O (M=29.88 g/mol)
 - Reflection term is negligible
- Results in a sputter yield of 0.26 ± 0.10 for 2 keV D⁺ on Li
 - Previous work² finds Y_0 = 0.091 ± 0.033 for 700 eV D+ incident on D- saturated Li
 - VFTRIM-3D simulation² gives $Y_0=0.08$ at 1000 eV
 - This is a very preliminary data set that indicates higher erosion than previous studies. Further investigation is required.
- 1) M. Coventry, Ph.D. Thesis, 2007
- 2) J.P. Allain et. al, Nuclear Fusion, 2001

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