



Modeling of ELM-pacing by Lithium Granule Injection (LGI) on NSTX-U with the M3D-C1 code

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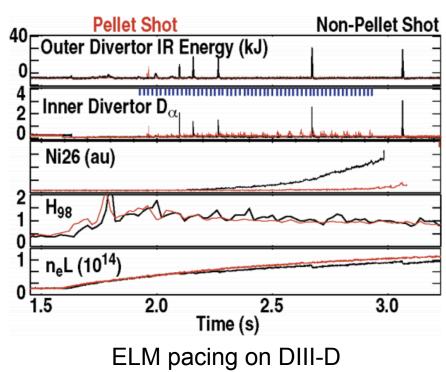
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Introduction and motivation

- The control and pacing of ELMs is needed in ITER
 - Need to have a tolerable peak heat flux on the divertor plates
 - Prevent impurity contamination, especially W
 - Need a larger ELMs frequency than "natural" one

 ELM pacing by D₂ pellet injection has been tested and proved to be effective in several devices



Introduction and motivation

- However, D₂ pellets also fuel the plasma
 - Need to decouple plasma fueling and ELM control
- ELM pacing by Lithium Granule Injection (LGI) has been demonstrated on EAST, DIII-D and NSTX and has potential for high injection rates
- Lack of physical understanding of the processes at play
- A modeling effort is needed to support next NSTX-U experiments

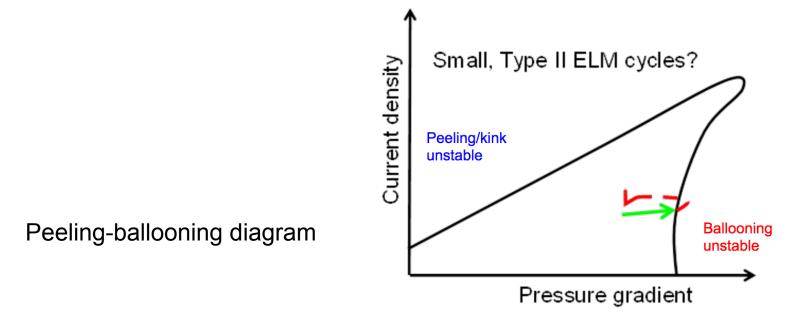


1. LGI principle and experiments

- 2. Pellet injection models
- 3. M3D-C1 modeling

ELM pacing principle

- Because of the 3D pressure perturbation due to the pellet ablation, medium/high-n ballooning modes become unstable.
- The ballooning modes are destabilized by the large local pressure gradients of the pressure perturbation.



Link between pellet parameters and profiles perturbation

- Need to link the pressure perturbation needed to trigger an ELM and the pellet parameters
 - Pellet size
 - Species (pure D₂, Li or even LiD)
 - Pellet velocity
 - Injection location (HFS vs. LFS)

Lithium Granule Injection principle

- Top part: granule dropper
- four separate reservoirs, 0.3-0.9 mm
- vibrating piezoelectric disk
- Average drop rate function of applied voltage (0-1000Hz)
- Bottom part: granule impeller
- rotary motor + ferro-fluidic feed-though,
 frot < 250 Hz
- Two-paddle impeller imparts 10-100 m/s finj=500 Hz

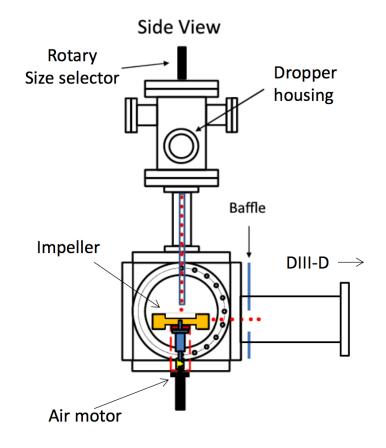


Figure from [A. Bortolon et al.]

Examples of edge perturbations induced by Lithium injection on NSTX

135064@ 272 ms 135064@280 ms 130389@ 353 ms 130389@ 356 ms 130387@ 191 ms 130387@ 197 ms 130385@ 393 ms 130385@ 400 ms ELM Triggered

Figure from [D. K. Mansfield et al.]

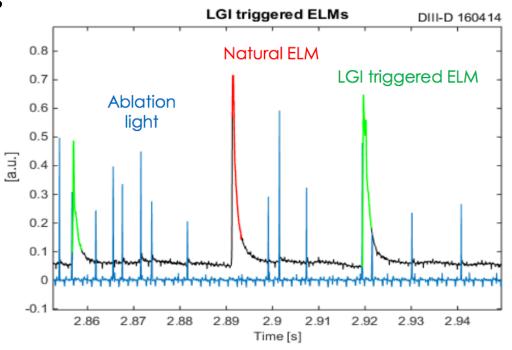
LGI triggered ELMs in DIII-D

Its key to identify which ELMs are associated with LGI

 Not all ablations are followed by ELMs

 ELMs can occur naturally during LGI phases

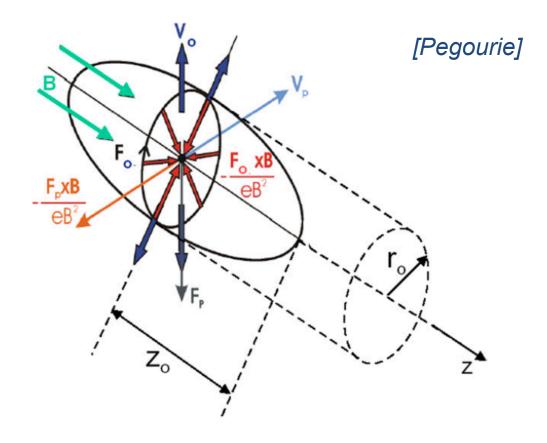
Modeling can provide some insight



LGI triggered ELMs in DIII-D

Pellet models: Shielding mechanisms

For both hydrogen or impurity pellets, ablation is a self regulated process, in the sense that the ablation cloud self-adapts for the heat flux at the pellet surface to be just enough to maintain the shielding capability of the cloud at the adequate value



Different types of shielding

- Gas dynamic shielding (dominant mechanism for D₂)
 - Due to the collisions between the incident plasma particles and that of the cloud, which is responsible for the ionization and heating of the ablatant.
- Electrostatic shielding
 - Due to the negative charge of the cloud with respect to the background plasma.
- Magnetic shielding
 - Due to the partial expulsion of the magnetic field from the cloud interior by the expanding plasma, and the associated reduction of the incident heat flux.

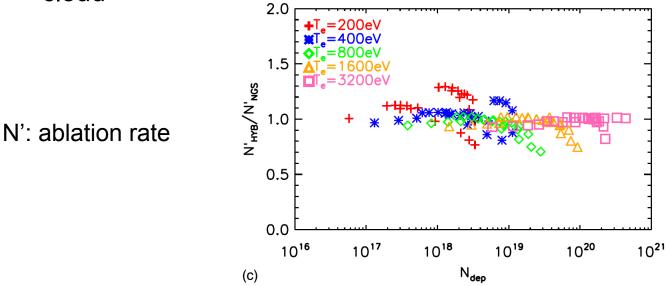
Pellet ablation model

- Neutral Gas Shielding (NGS) model:
 - Assume that the neutral gas shielding is the dominant process
 - Assume a constant pellet velocity
 - Gives a pellet ablation rate which depends on background plasma parameters

$$N' = 4.12 \times 10^{16} \cdot r_{\rm p}^{1.33} \cdot n_{\rm e}^{0.33} \cdot T_{\rm e}^{1.64}$$

Pellet model comparison [Gal2008]

- Comparison of Hybrid model, LLP model and NGS model
 - <u>LLP model</u>: takes into account channel flows and double electrostatic shielding
 - <u>Hybrid model</u>: same as LLP but assumes a spherical cloud



Additional shielding effects counteract each other. Ablation rate comparable to the NGS model, comparable to the experiment

M3D-C1 solves the 3D two-fluid MHD equations in a magnetized torus

$$\begin{aligned} \frac{\partial n}{\partial t} + \nabla \bullet (n\mathbf{V}) &= 0 \\ \frac{\partial \mathbf{B}}{\partial t} &= -\nabla \times \mathbf{E} \qquad \mathbf{B} = \nabla \times \mathbf{A} \qquad \mathbf{J} = \nabla \times \mathbf{B} \\ nM_i(\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \bullet \nabla \mathbf{V}) + \nabla \bullet \mathbf{P} &= \mathbf{J} \times \mathbf{B} - \nabla \bullet \mathbf{\Pi}_{GV} + \mu \nabla^2 \mathbf{V} \\ \mathbf{E} + \mathbf{V} \times \mathbf{B} &= \mathbf{R}_c + \frac{1}{ne} (\mathbf{J} \times \mathbf{B} - \nabla \bullet \mathbf{P}_e) - \lambda_H \nabla^2 \mathbf{J} \\ \frac{3}{2} \frac{\partial p_e}{\partial t} + \nabla \bullet \left(\frac{3}{2} p_e \mathbf{V}\right) &= -p_e \nabla \bullet \mathbf{V} + \eta J^2 + \frac{\mathbf{J}}{ne} \cdot \left[\frac{3}{2} \nabla p_e - \frac{5}{2} \frac{p_e}{n} \nabla n\right] - \nabla \bullet \mathbf{q}_e + Q_\Delta \\ \frac{3}{2} \frac{\partial p_i}{\partial t} + \nabla \bullet \left(\frac{3}{2} p_i \mathbf{V}\right) &= -p_i \nabla \bullet \mathbf{V} + \mu |\nabla V|^2 - \nabla \bullet \mathbf{q}_i - Q_\Delta \end{aligned}$$

[S. Jardin, N. Ferraro]

Resistive MHD 2-Fluid terms

Features of M3D-C1

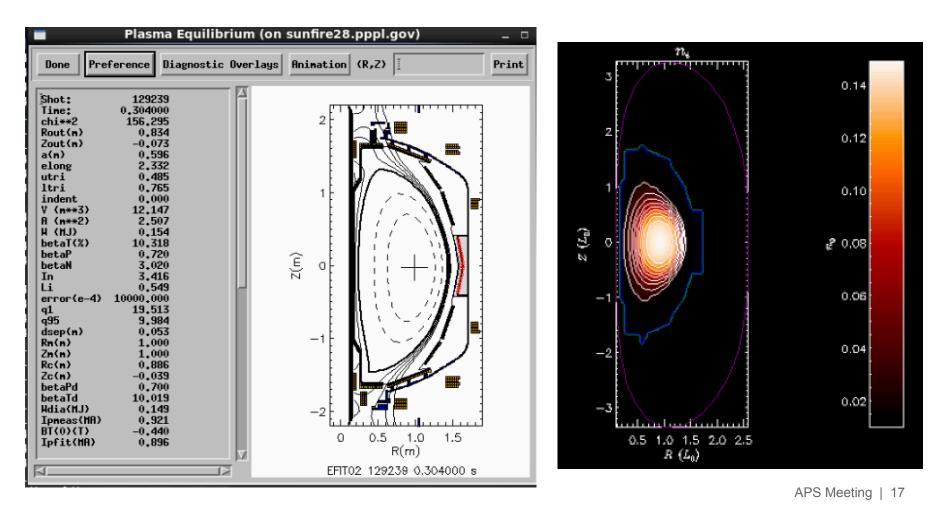
- High accuracy
 - High order 3D finite elements: crucial to get a spatially localized pellet
 - Full 2F MHD equations: diamagnetic terms very important for ELMs dynamic
- <u>Can perform long-time simulations</u>: ~ 10 ms
 - Fully implicit time-advance algorithm
 - Study of stability on the transport timescale
- <u>Geometrical flexibility</u>: mesh packing, realistic wall geometry

Pellet model in M3D-C1

- Neutral Gas Shielding (NGS) model currently being implemented in M3D-C1:
 - Density source term taking into account the pellet ablation
 - Pellet ablation process is approximated to be adiabatic: no heat sink in the temperature equation
- First simulations on-going
- Maxwellian model also being tested

Plan: to be able to make prediction for NSTX-U operation (pellet size, velocity, ...)

• Start from a NSTX-U high performance stable equilibrium and turn on pellets in the simulation.



First pellet injection test: 2D simulation Edge density increase

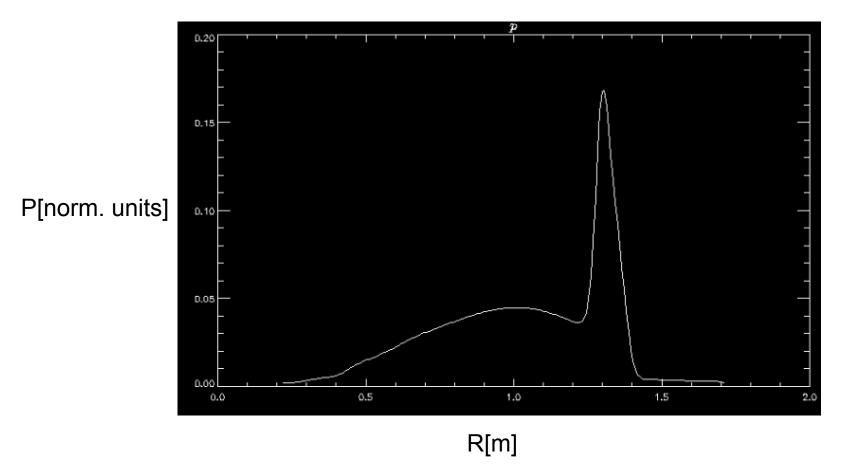
 n_{g} 1.0 1.0 0.9 0.50.50.8 (T_0) Z (L₀) 0.0 0.0 80 P 53 0.7 -0.5-0.5 2 -1.0-1.00.6-1.5 -1.5بابتيا يتبا تتبا تتبا تتبا تتبا 0.4 0.6 0.8 1.0 1.2 1.4 1.6 0.4 0.6 0.8 1.0 1.2 1.4 1.6 $R(L_0)$ $R(L_0)$

Ion density

Equilibrium

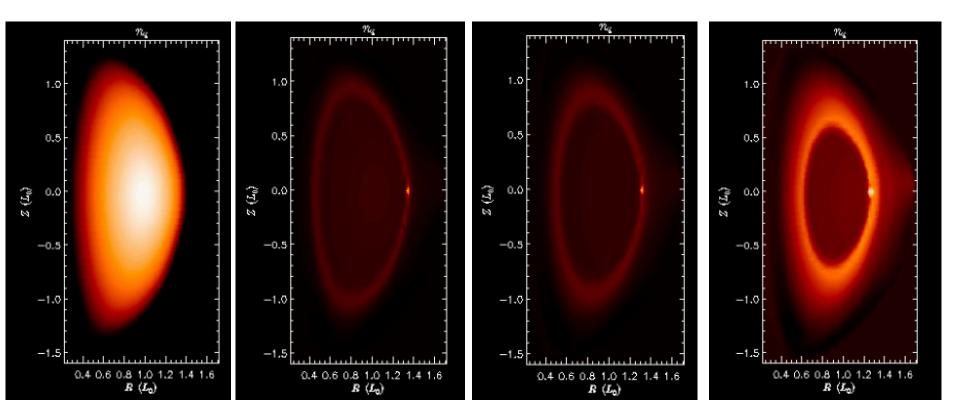
During pellet injection

Pressure profile



Density time evolution

Parameter scan on-going: pellet size, velocity



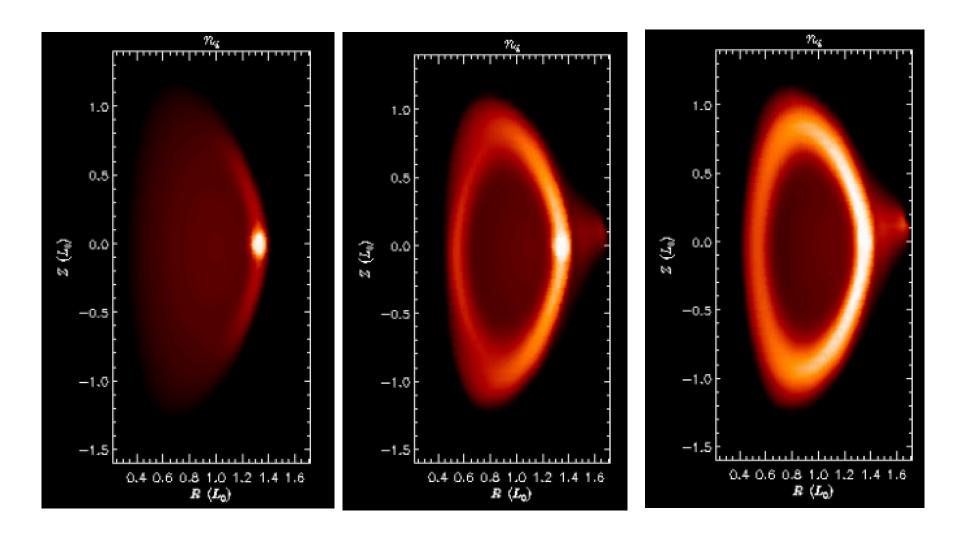
Pellet radius ~ 5 mm, pellet velocity ~ few 100m/s

Conclusion

- Lithium Granule Injection is a promising ELM pacing method
- New tool for ELM control
- First experimental results on several devices
- Modeling started with M3D-C1
 - First implementation of a deuterium moving pellet

Perspectives

- Implement a full LGI model in M3D-C1
 - Need a model including radiation, ionization, etc for Lithium.
 - Possibly taking into account additional shielding effects
 - Is NGS model good enough approximation for LGI or should we use a more complex model?
 - Comparison with experimental data
 - Application to NSTX-U scenarios and ELM control



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