# **Development of a Lithium Vapor Box Divertor** for Controlled Plasma Detachment

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- **APS DPP 2018**



# **Divertor Detachment Front Can Run up to the Main Plasma**



### **Deleterious effect on H-Mode pedestal.**

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### Potzel, NF 2014, AUG

### **Lithium Vapor Box Divertor Localizes Radiation to Divertor Region**

- Provides a localized cloud of Li vapor away from main plasma
  - Creates a strong detachment front to keep radiation in the divertor
- Creates strong vapor gradient so that detachment front cannot run up to x-point.
  - **Detachment front location is resilient to** variable heat flux.
- Cannot be achieved with gaseous impurities pumping is too weak
- **Examined baffled configurations in the past but** • currently only considering no-baffle configurations





### **Two Codes to Capture Relevant Physics**

- Difficult to capture all divertor physics with one code
- Used UEDGE to understand plasma-Li interactions
  - Diffusive model for particle transport
- Used SPARTA to understand Li-Li interactions
  - Direct Simulation Monte-Carlo code



### **UEDGE Model with Lithium**

- UEDGE has a purely diffusive model for lithium vapor transport.
  - Based on collisions of lithium atoms with plasma ions.
    No Li-Li collisions.
  - Inaccurate in regions dominated by lithium convection/viscosity: Navier-Stokes regime.
- Transports lithium in plasma, calculates radiation self-consistently.
- Achieves detached plasma in Fusion National Science Facility (FNSF) with nearly 100% lithium radiated power and 66MW in outer divertor.
  - In "real" world would include other (seed) impurities.



## UEDGE Achieves Detachment in FNSF with Lithium

0.5 m Divertor leg, Open geometry

Localized evaporation, absorbing walls.

60 eV radiation per ionization

Divertor region heating ~ 2 MW/m<sup>2</sup>





## **UEDGE Provides Boundary Conditions To SPARTA**

- Recombination roughly equals ionization at a given Z position
- In effect, plasma acts like a mirror but with an increase in particle energy





# **SPARTA Simulation Set-Up and Lithium-Plasma Interactions**

- Using SPARTA Monte-Carlo Direct Simulation code for lithium vapor
  - Li-Li collision model based on known vapor viscosity vs. *T* makes this valid for regions outside of plasma.
- Lithium Plasma interaction taken from UEDGE results
  - Assume absorption of lithium at  $T_e = 0.2 \text{ eV}$
  - Recombination at the same point.
    - Lithium leaves along B with  $T_{Li} = E_{||,Li} = 0.2 \text{ eV}$
- Use SPARTA to design the vapor box to achieve detachment position resilience (explained on next slide)



### **Detachment Position Resilience**

### **High heat flux** (high T<sub>e</sub>) causes detachment front to extend towards divertor plate



### Low heat flux (low T<sub>e</sub>) causes detachment front $\widehat{E}^{1.0}$ to retract towards N X-point



Extended detachment front causes more lithium ionization due to vapor gradient

### **Detachment front** settles into, and resists changes to, equilibrium position

Retracted detachment front **causes** less lithium ionization due to vapor gradient







### **Using SPARTA to Demonstrate Detachment Position Resilience**



- Maintain constant evaporation rate
- Determine ionization rate of new configuration

R (m)

# - Incrementally change plasma shape to simulate higher or lower heat flux



 $10^{18}$ 



### **SPARTA Shows Vapor Box Has Very High Positional Resilience**



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### Conclusions

- UEDGE achieves detachment in FNSF with Li alone, shows lithium dynamics at detachment front.
- This provides a preliminary physics basis to optimize Lithium Vapor Box Divertor using SPARTA.
- A divertor with private-flux-side lithium evaporation near the bottom of the divertor leg –
  - Provides adequate lithium for detachment.
  - Provides strong positional resilience of the detachment front, without baffles. No issue of Li accumulation on 600 C surfaces.
- Integrated modeling, design, & experiments are needed.



### **Back-up Slides**



### **A Simplified Lithium Vapor Box Divertor Based on UEDGE Results**



Allows more Li efflux, but needs less total evaporation Makes experimental implementation easier, including starting with a toroidal segment



### High Wall Temperatures Prevent Lithium **Accumulation on First Wall**

- 140 g/s of lithium evaporated for  $P_{rad} = 66$  MW.
- Assume all of this is deposited on first wall,  $T_w \sim 600$  C.
- Evaporation rate at 600 C =  $2.66 \text{ g/s/m}^2$
- Area of first wall ~ 300 m<sup>2</sup>
- Total evaporation rate with multi-monolayer surface coverage = 800 g/sec
- Can't even accumulate a few monolayers of Li
- LiH decomposes in << 1 sec at 600 C.</li>



### **Two-Sided Injection Has Low Resilience**



# Little variation in Li absorption as leg moves away from evaporators. Same low resilience with bottom evaporation.



### Lithium Return Flow is Determined by Balance between Capillary Pull & MHD Drag

$$\Delta p_{capillary} = \frac{2\gamma \cos \alpha}{r_p} \ge \Delta p_{MHD}$$
$$\Delta p_{MHD} = \int \vec{j} \times \vec{B} \cdot \vec{dl} = \int v \sigma_{Li} B^2 dl \left(\frac{\sigma_{ij}}{\sigma_{Li} a_{Li}}\right)$$

 $\gamma \equiv surface \ tension$  $\alpha \equiv contact \ angle$  $r_p \equiv pore \ radius$ 







### **Sandwich Flow Channel Inserts Reduce** *AP***<b>MHD**



### Gap in Flow Channel Insert orients towards divertor surface. Works top and bottom, leaves margin for other effects.

Sandwich FCI: 0.5 mm steel 0.5 mm MgO insulator 1 mm steel

2 cm ID pipes spaced 10 cm apart toroidally  $\Delta p_{MHD} = 0.22 \,\Delta p_{Capillary}$  $@r_p = 40\,\mu m$  $v \leq 2.9 \ mm/s$  $\phi = 0.4 \, mV$ 



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## **Expected Lithium Cooling per Particle**



(Solid lines total cooling, dashed radiation only)

# Simple model for power dissipation based on ADAS Collisional-Radiative model







### **Evaporative Cooling & Heating**



**Divertor leg moving** in front of evaporator should enhance evaporation, positional resilience.



### **Mass Flows**













