

Variation of the midplane heat flux profiles with plasma current and heating power in the National Spherical Torus Experiment

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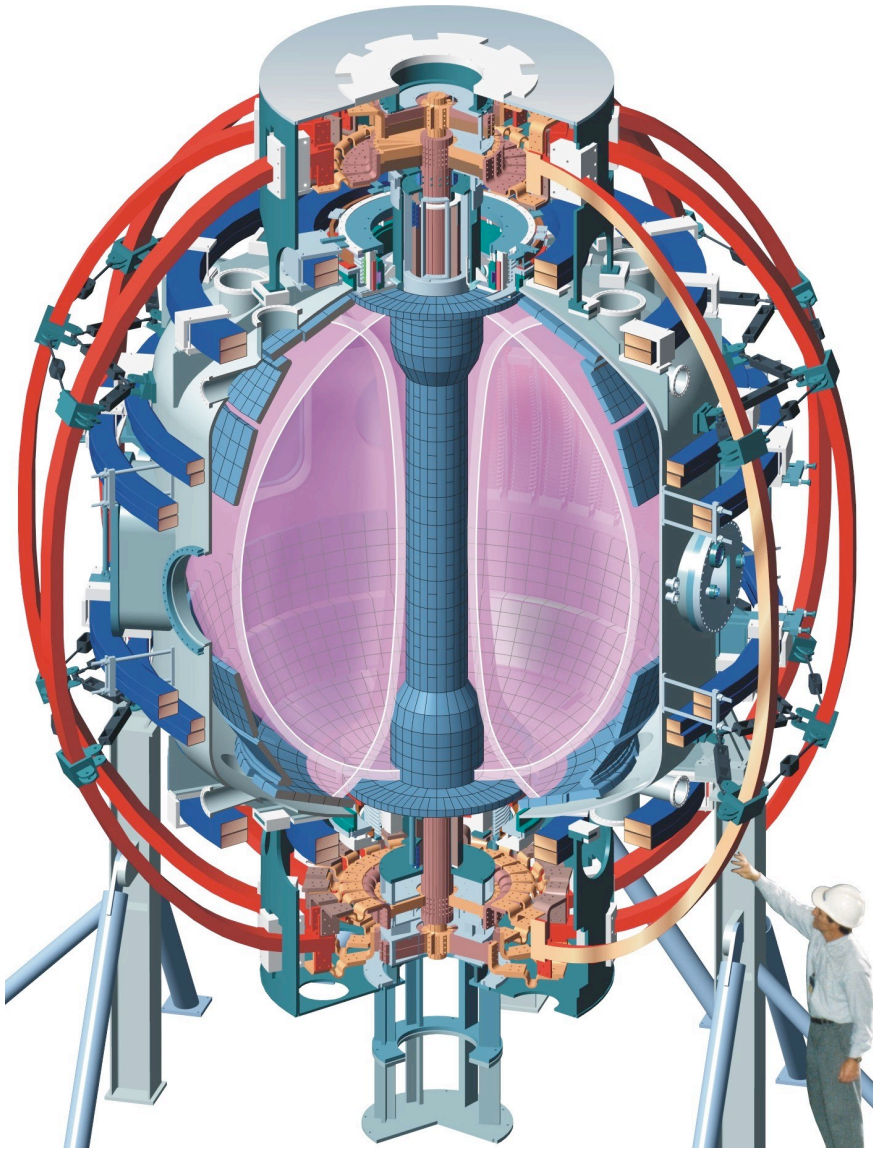


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NSTX Cross Section



NSTX Facility Parameters

Major Radius 0.86 m

Minor Radius 0.67 m

Elongation ≤ 3

Triangularity ≤ 0.8

Plasma Current ≤ 1.5 MA

Toroidal Field ≤ 0.6 T

NBI Heating ≤ 7.5 MW

RF Heating ≤ 6 MW

Pulse Length ≤ 1.6 sec

Heat flux management an important issue for Spherical Tori (ST)

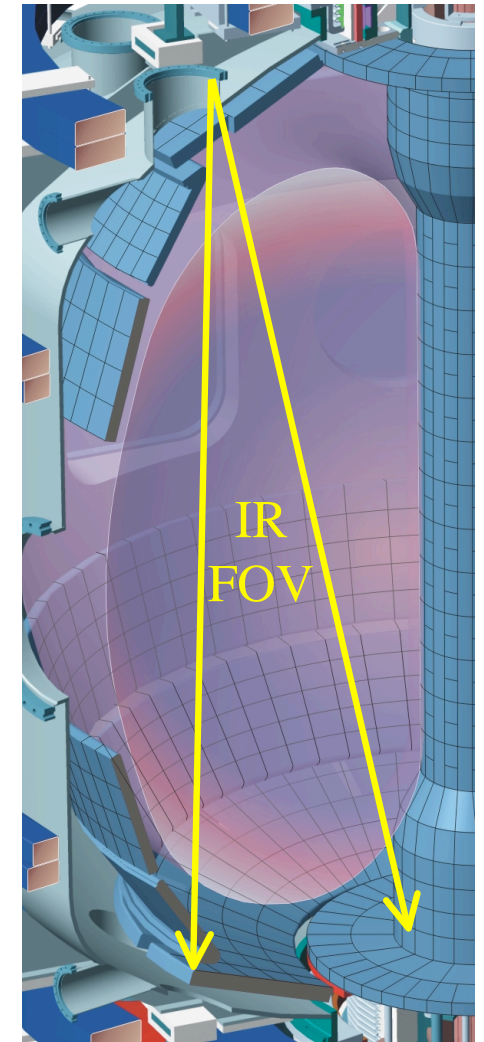
- Small major radius in ST implies small wall area, possibly high divertor power loading factor P/R
- High magnetic mirror ratio and large flux expansion in scrape-off layer may broaden power deposition to acceptable values
- In NSTX, plasma facing components are designed for a maximum transient temperature of $1200\text{ }^{\circ}\text{C}$
- Previous study indicates that a maximum pulse length of 2-3 sec can be tolerated at maximum observed peak heat flux of $\sim 10\text{ MW/m}^2$ before $1200\text{ }^{\circ}\text{C}$ will be reached on PFCs
- P_{NBI} and I_p scaling of outer divertor peak heat flux midplane width shown here
- *Dissipative divertor research: Soukhanovskii P2.023*

Summary and Conclusions

- Peak heat flux increases with P_{NBI} , with a break (stronger dependence) in the slope at $P_{\text{NBI}} \sim 3$ MW
 - Simulations with the 2-point Borass model suggest that at the lowest NBI power, the outer divertor may be on the verge of detaching
- The change in slope above at $P_{\text{NBI}} \sim 3$ MW could correlate with the onset of the high recycling regime
- Heat flux midplane profile width weakly dependent on P_{NBI} in high recycling regime
- Heat flux midplane profile width decreases rather strongly with I_p - much stronger than a simple connection length dependence
- Simple models predict narrower SOL widths than observed, but Bohm cross-field transport gives proper order of magnitude

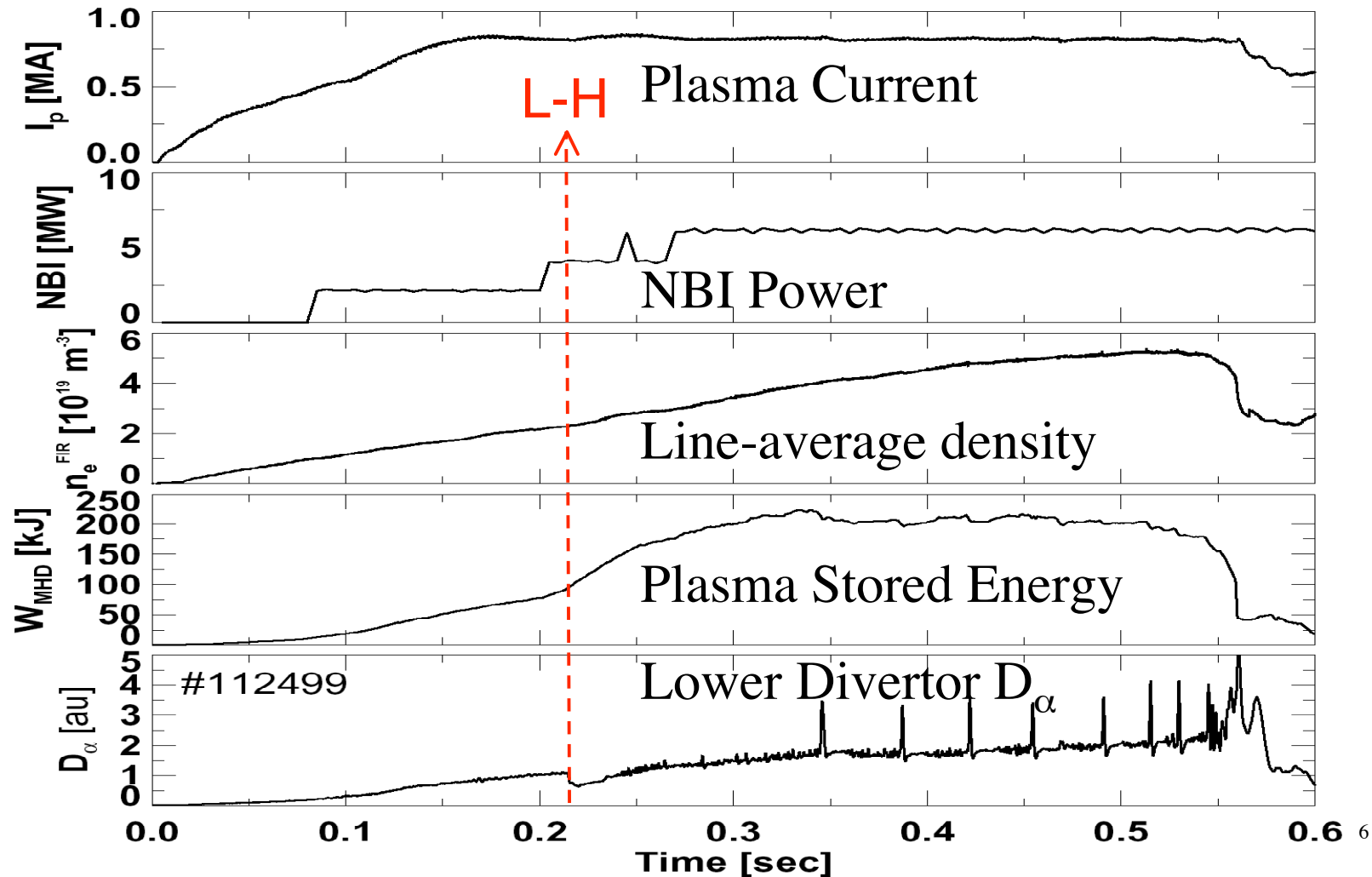
Lower divertor IR camera and 1-D conduction model used to compute heat flux

- Indigo ALPHA camera
 - I60 x 128 microbolometer array
 - 7-13 μm range
 - 30 Hz, 25ms thermal e-folding time
 - spatial resolution ~ 0.66 cm with present optics
 - 12-bit digital output, frame-grabbed on PC
 - Calibrated during in-situ bakes of the graphite tiles
- 1-D conduction model considers heat transport into tile bulk
 - temperature dependent ATJ graphite conductivity
 - neglects radial diffusion - ok for short pulses $<$ few sec

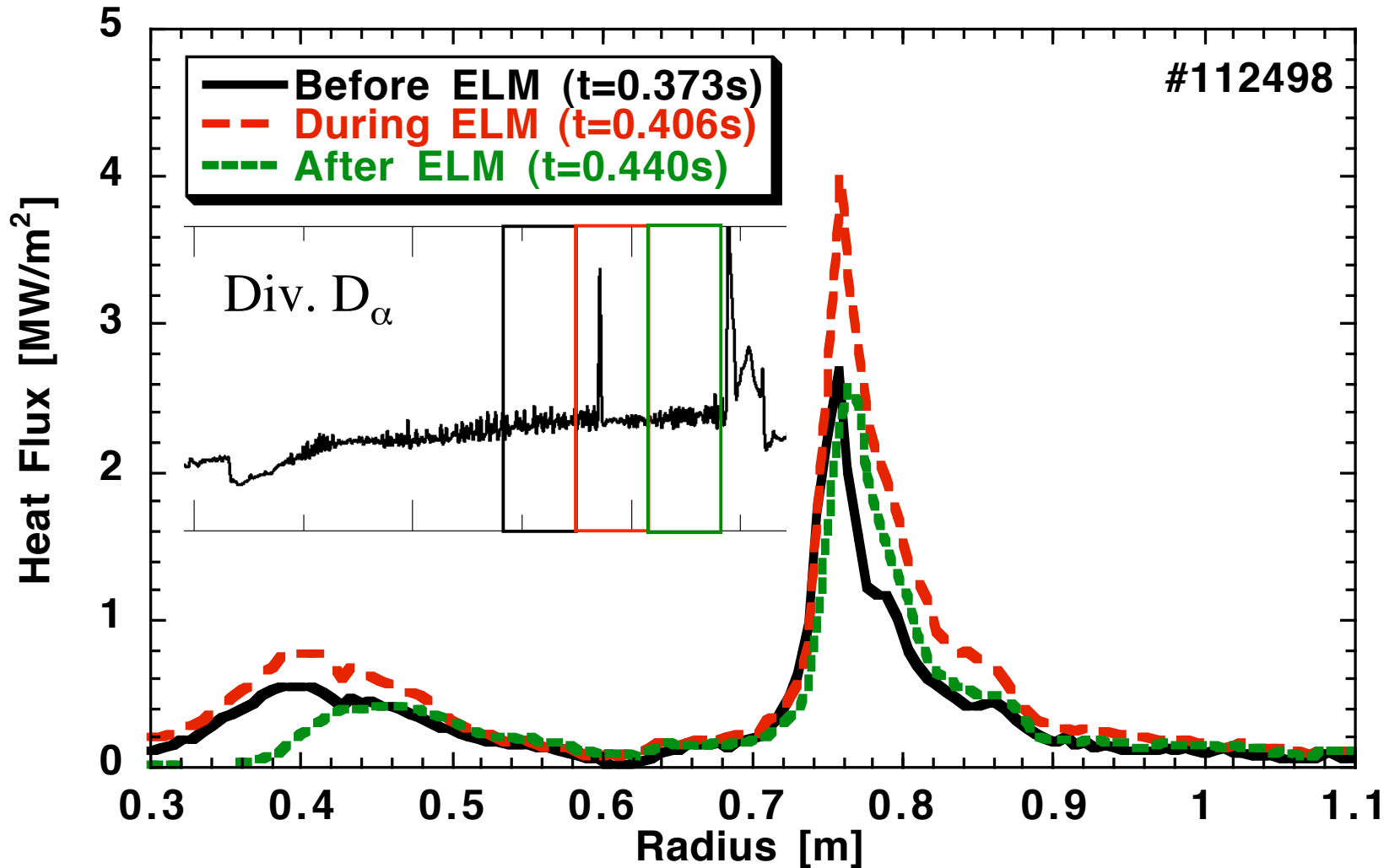


NBI-heated discharges used for heat flux scaling experiments (all with density ramping)

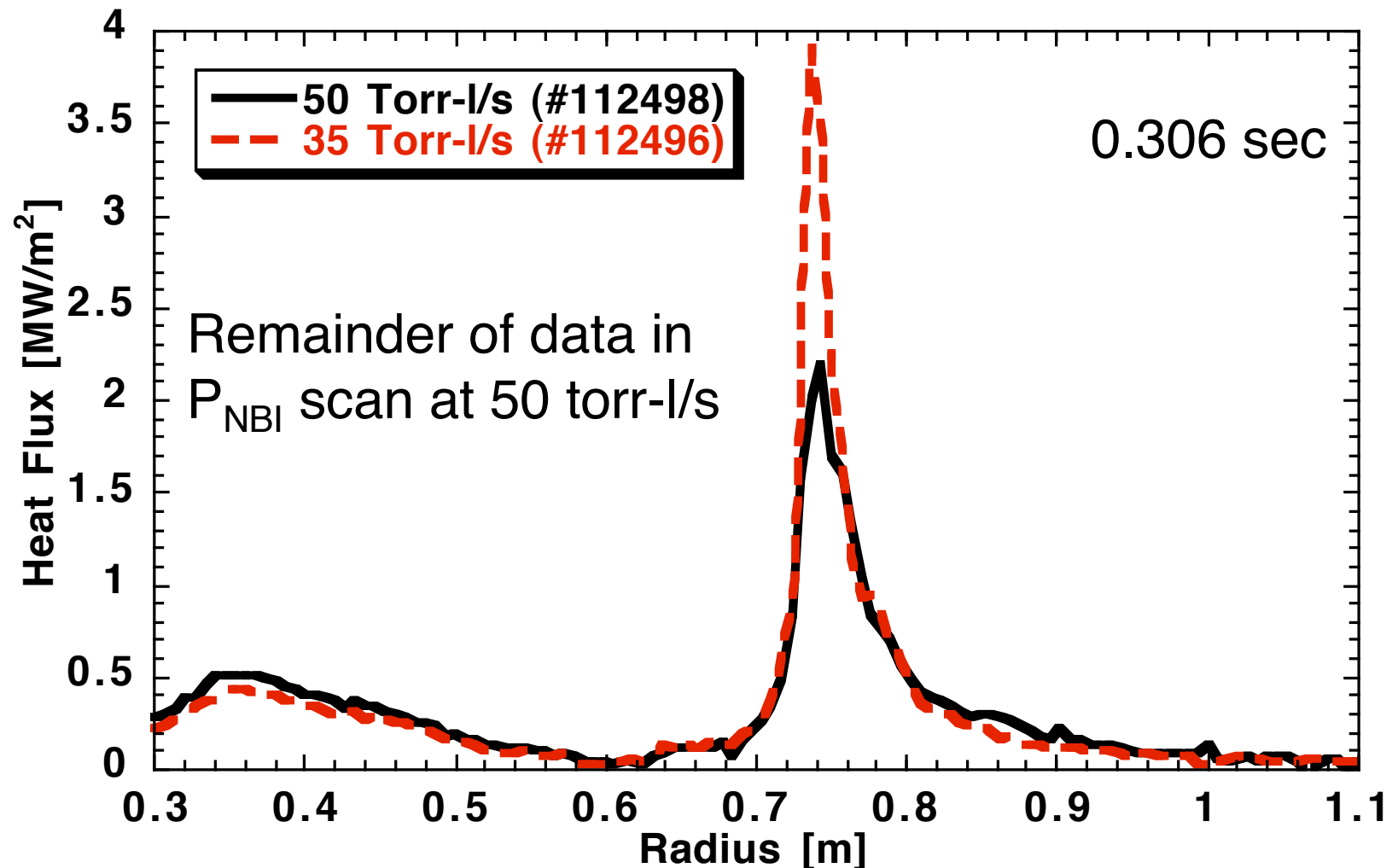
- Power accountability $\sim 70\%$ in these discharges (Paul, JNM 2005)



Heat flux profile changes moderately during Type I ELMs ($\Delta W/W < 10\%$), due to long integration time



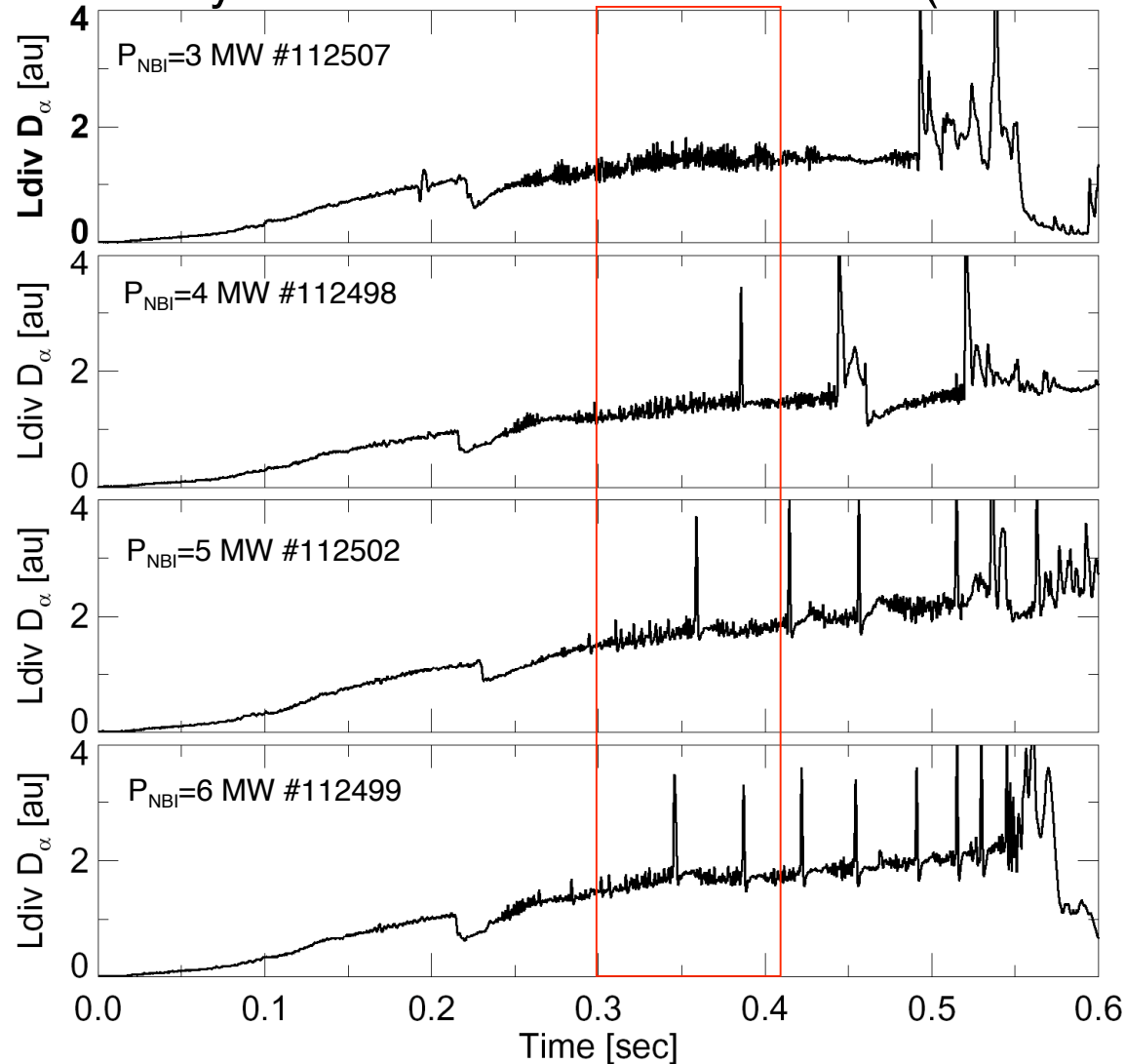
Peak Heat Flux Decreases with Center Stack Gas Fueling Rate ($I_p=0.8$ MA, $P_{\text{NBI}}=4$ MW, no big ELMs)



- Heat fluxes at lower gas fueling rates even higher

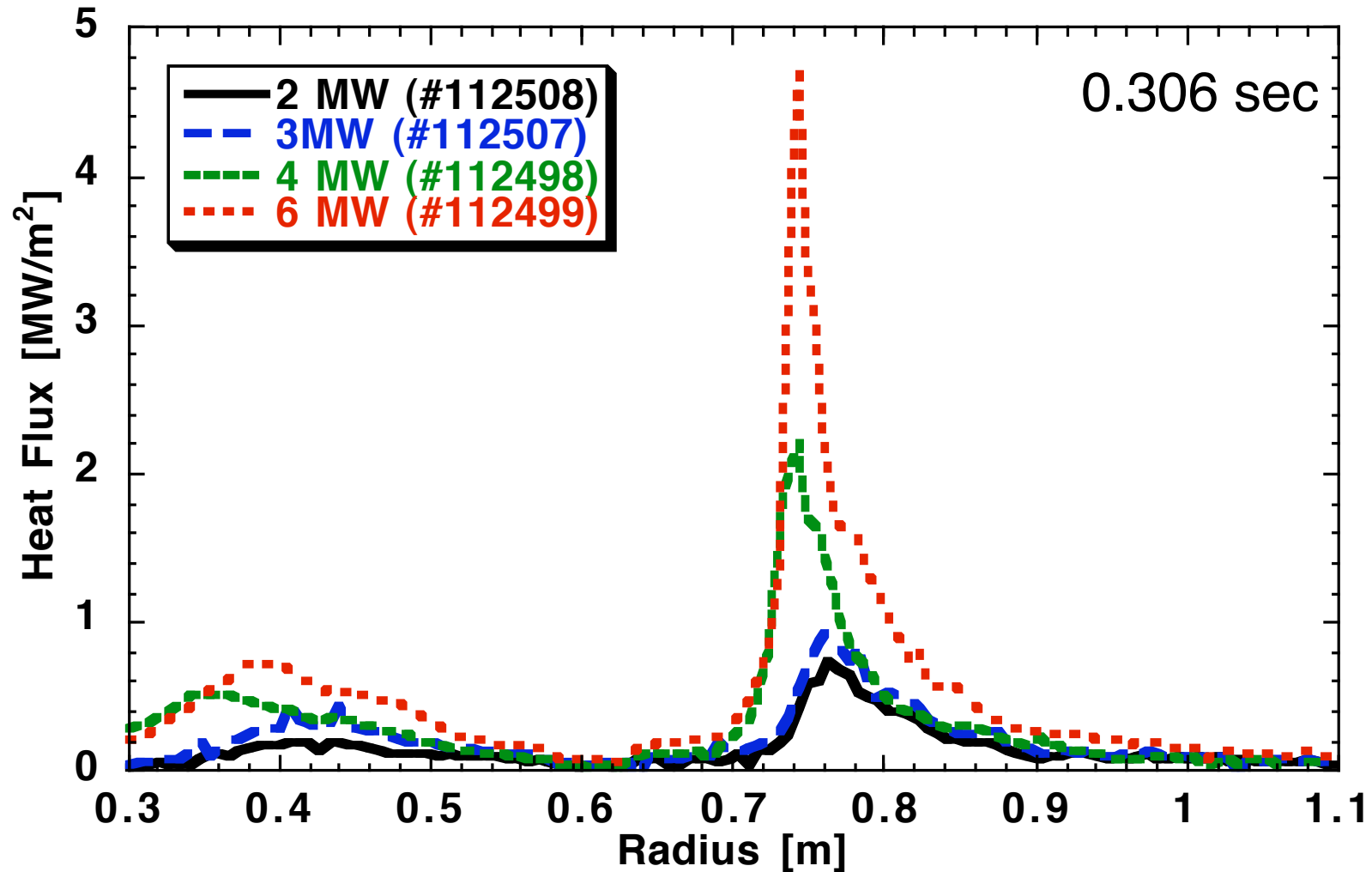
Discharges transition from small, Type V ELMs to mixed Type I V ELMs at $P_{\text{NBI}} \sim 4 \text{ MW}$ ($I_p = 0.8 \text{ MA}$)

- Time of analysis between 0.3 and 0.41 sec (4 IR camera frames)



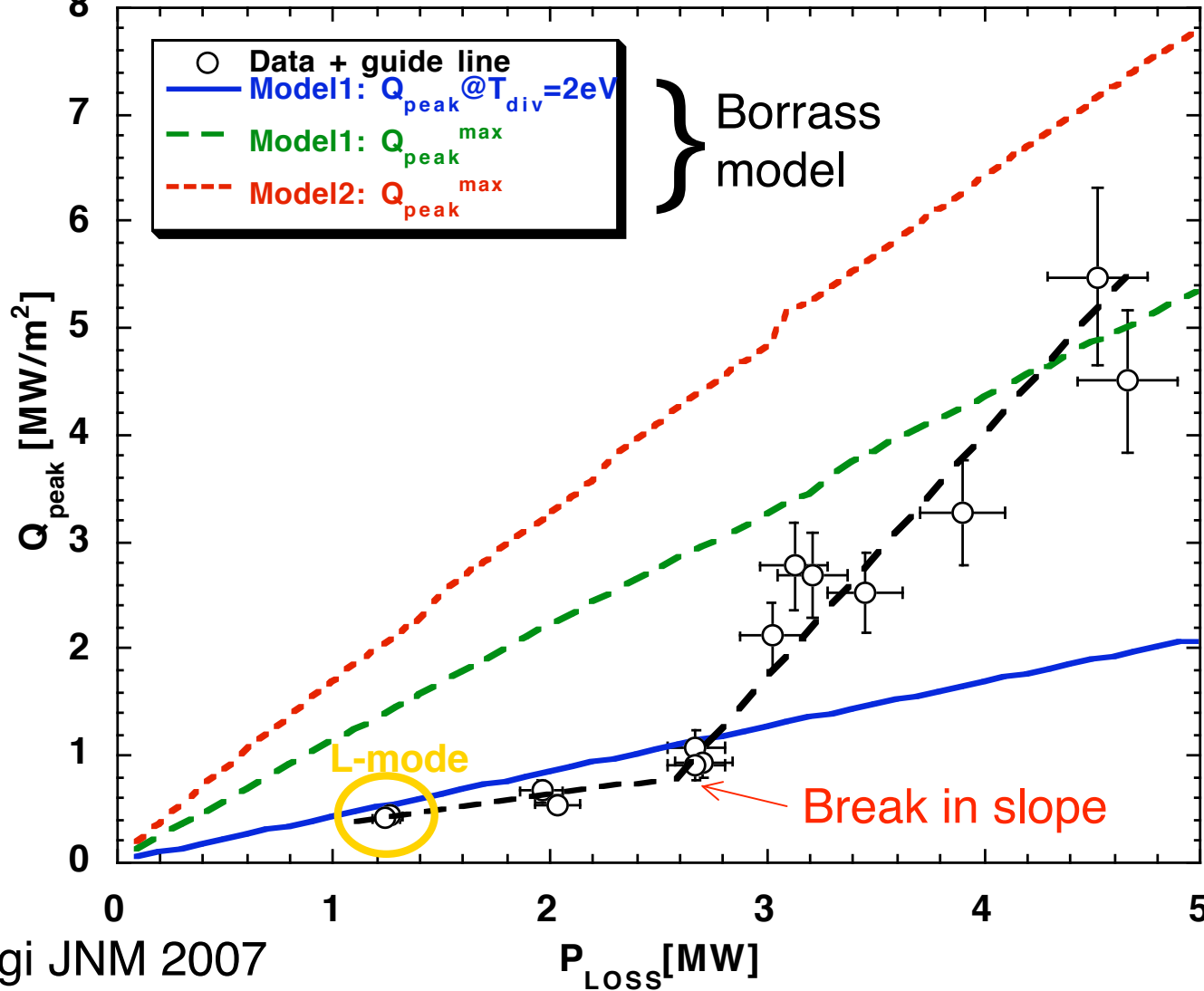
- Small, Type V ELMs
- Mixed small Type V + Type I ELMs
- Mixed small Type V + Type I ELMs
- Mixed small Type V + Type I ELMs

Heat flux profile becomes more peaked with increasing NBI power

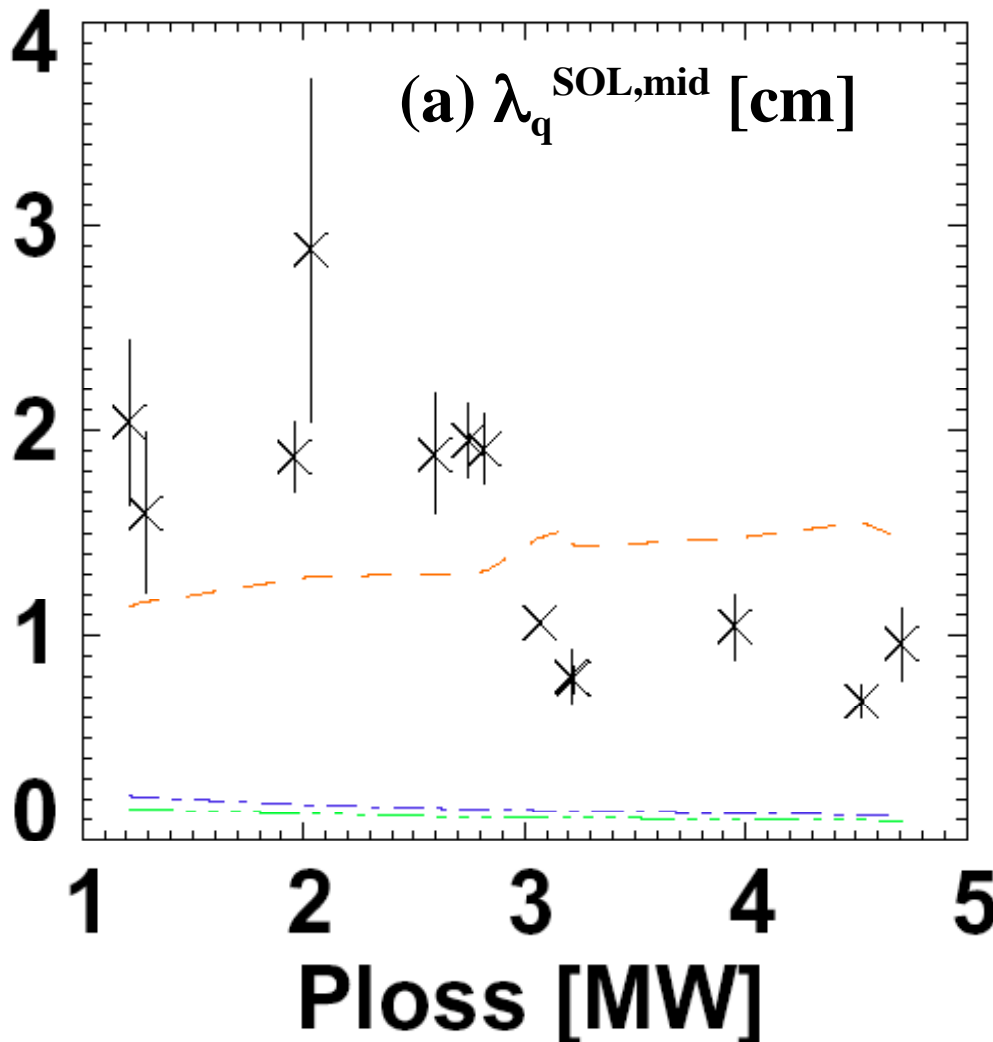


Peak Heat Flux increased with NBI power, with a change in the slope for $2 < P_{\text{loss}} < 3$ MW

$$P_{\text{LOSS}} = P_{\text{OH}} + P_{\text{NBI}} - dW_{\text{MHD}}/dt - P_{\text{rad}}^{\text{core}} - P_{\text{loss}}^{\text{fast ion}}; P_{\text{rad}}^{\text{core}} + P_{\text{loss}}^{\text{fast ion}} \sim 0.3(P_{\text{OH}} + P_{\text{NBI}})$$



Midplane heat flux scale length depends weakly on P_{loss} in high recycling regime ($P_{\text{loss}} > 3$ MW)



Models (Counsell, JNM 1999)

- classical parallel transport
- different cross-field models

$$\lambda_q^{B1} = 0.3 q_{95}^{0.73} R_m^{0.27} a_m^{0.18} P_{\text{loss}}^{0.18} B_t^{-0.57} n_{\text{sep}}^{-0.18}$$

- Collisionless SOL
- Applies? NSTX SOL v_e^* 5-100

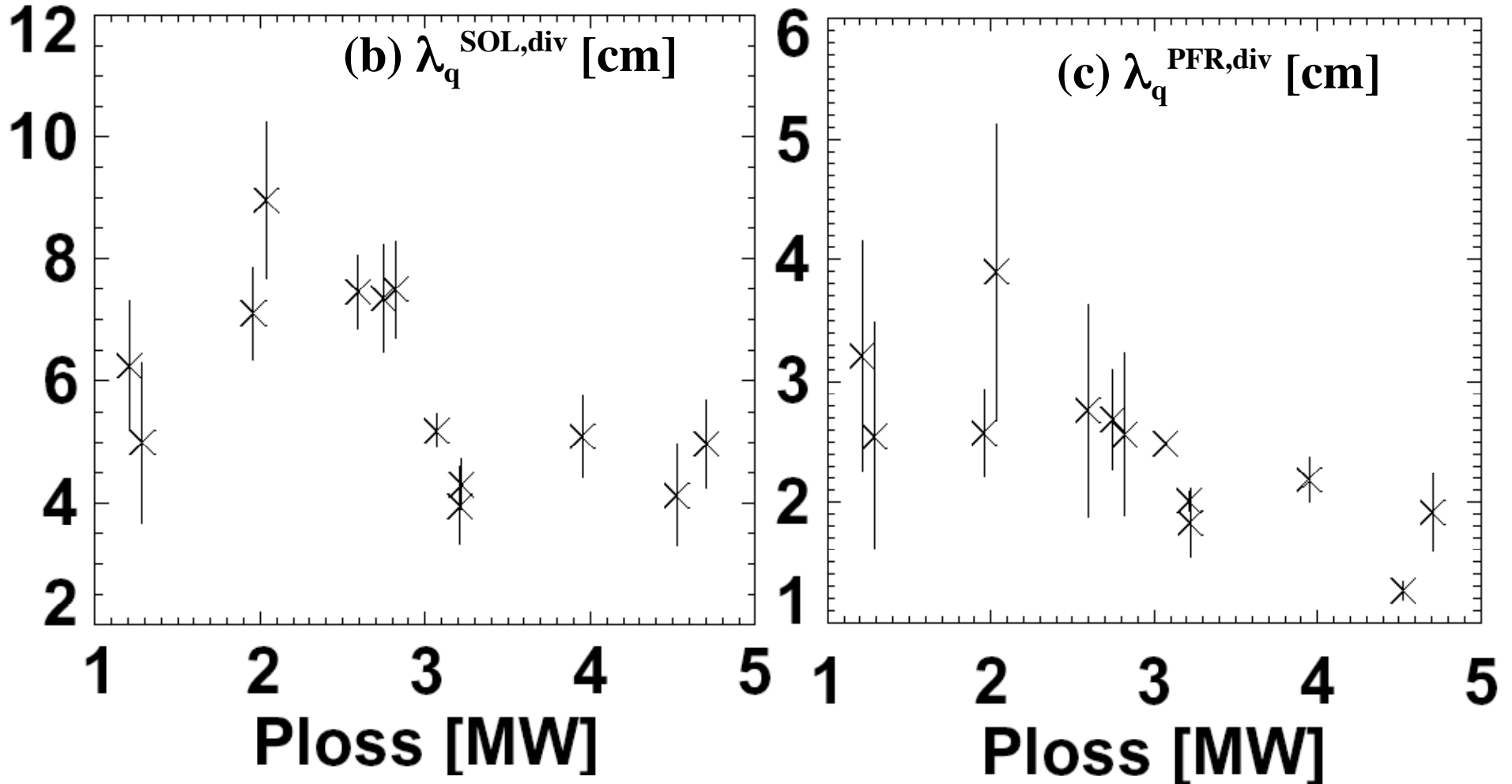
$$\lambda_q^D = 0.35 q_{95}^{-0.1} R_m^{0.3} a_m^{0.4} P_{\text{loss}}^{-0.4}$$

- collisional SOL
- cross-field from sheath resistivity

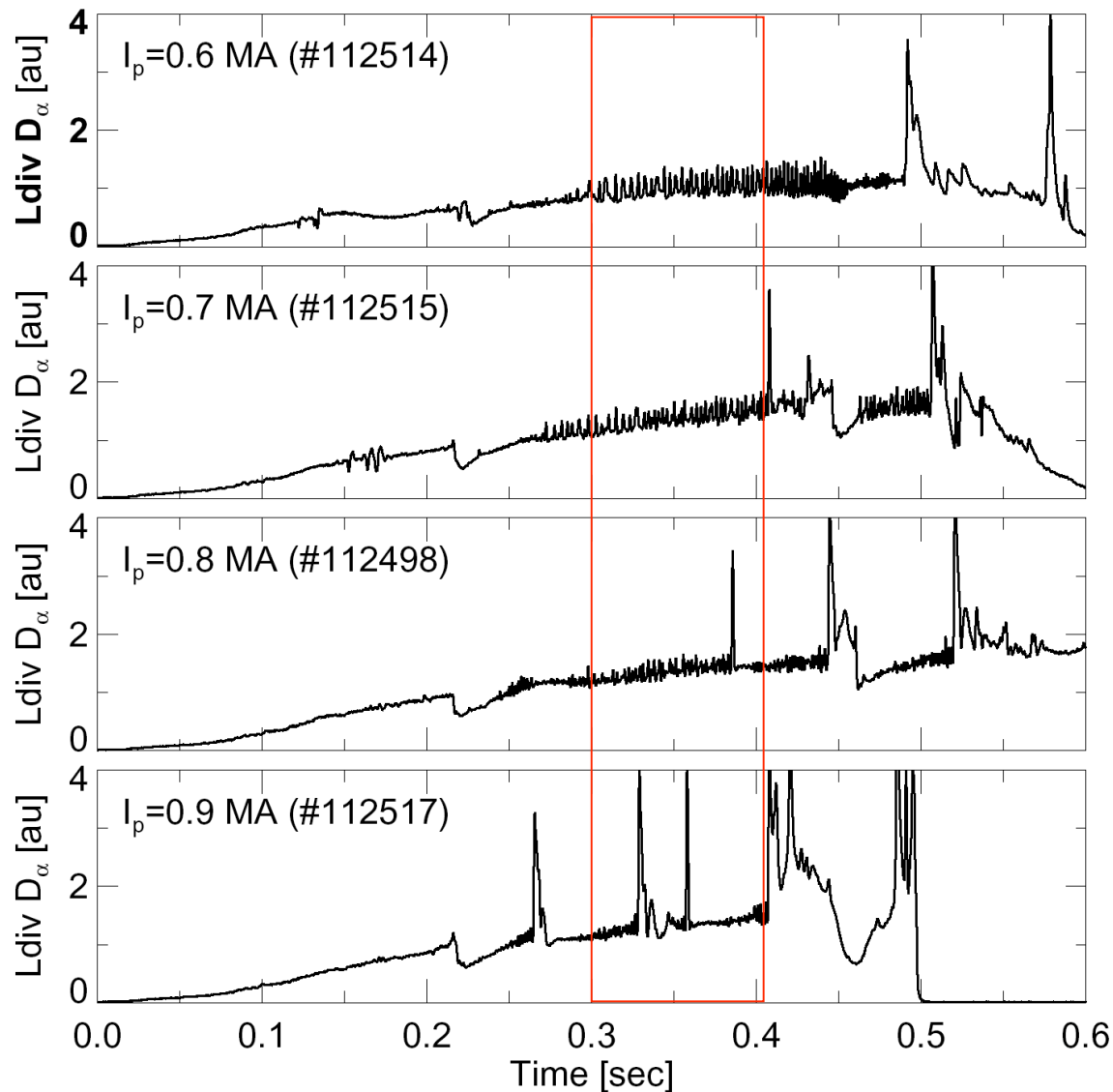
$$\lambda_q^M = 0.083 q_{95}^{0.6} R_m^{1.0} a_m^{0.4} P_{\text{loss}}^{-0.4}$$

- collisional SOL
- cross-field due to charge exchange

Ratio of divertor private-flux region scale length to scrape-off layer heat flux scale length $\sim 2-3$

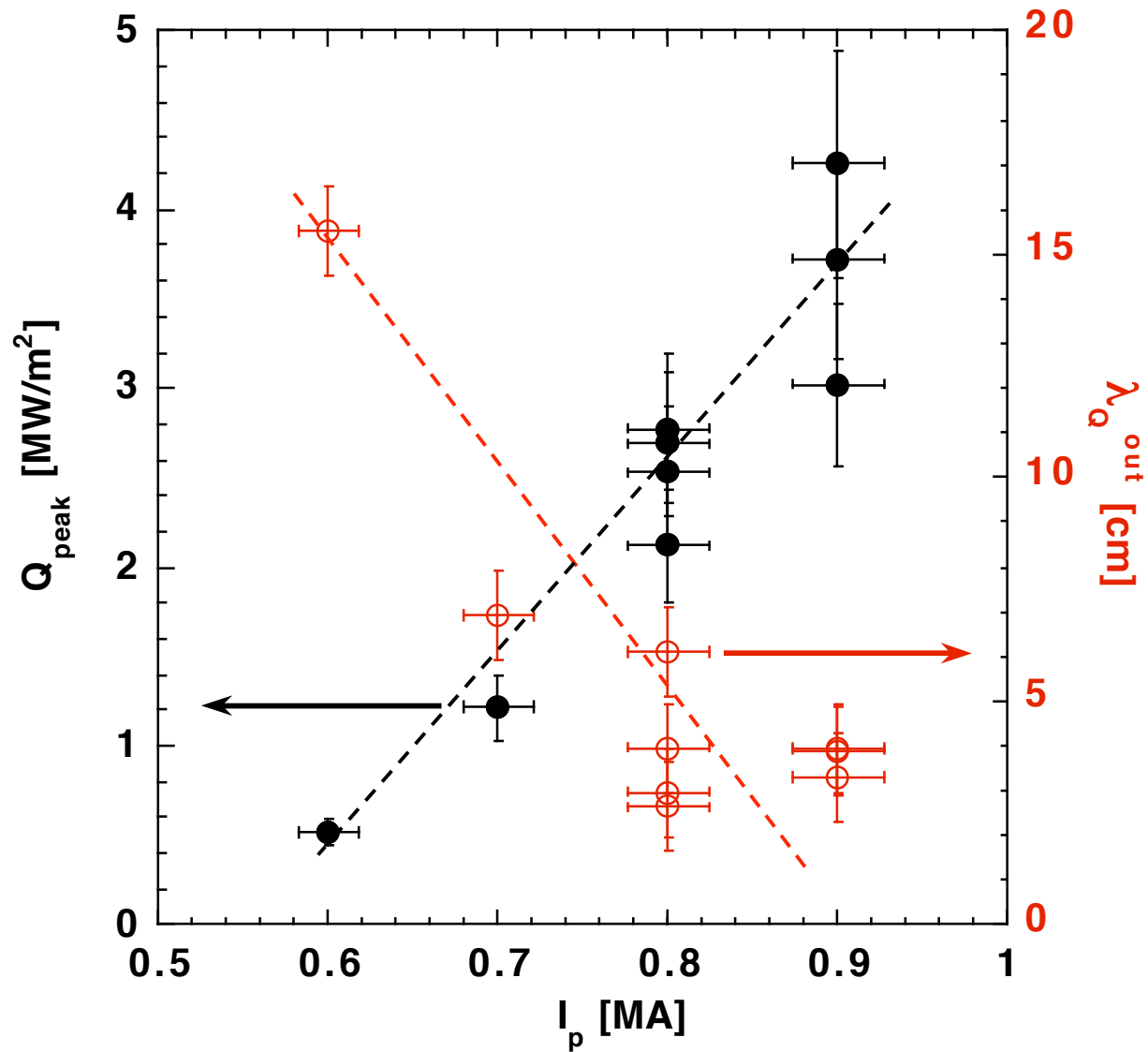


Larger ELMs and other MHD observed more frequently as I_p increased ($P_{\text{NBI}} = 4 \text{ MW}$)

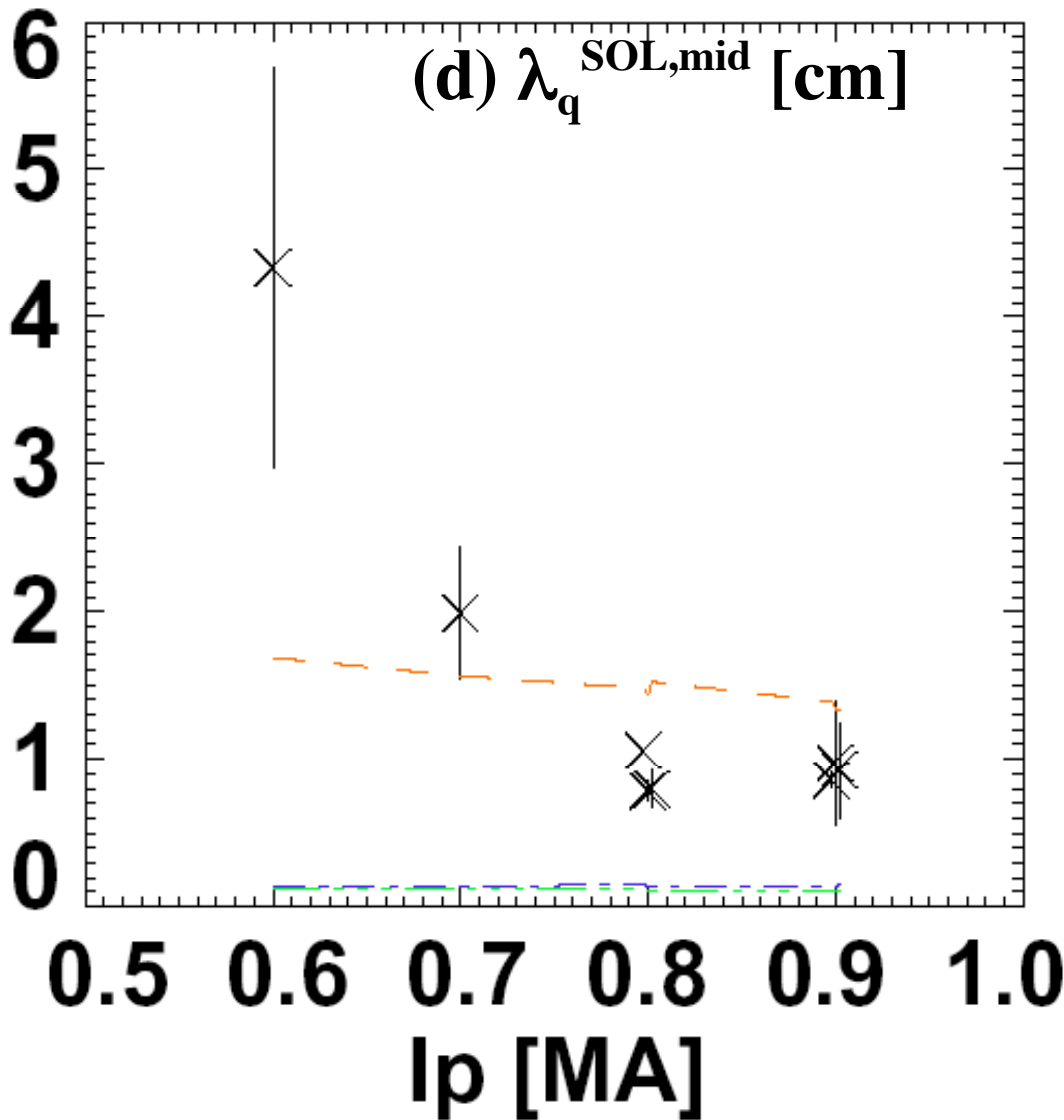


- Small, Type V ELMs
- Mixed small Type V + Type I ELMs
- Mixed small Type V + Type I ELMs
- Mixed small Type V + Type I ELMs

**Divertor peak heat flux (profile FWHM) increases
(decreases) with I_p**



Midplane heat flux scale length depends strongly on I_p ($P_{\text{NBI}} = 4 \text{ MW}$)



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- different cross-field models

$$\lambda_q^{B1} = 0.3 q_{95}^{0.73} R_m^{0.27} a_m^{0.18} P_{\text{loss}}^{0.18} B_t^{-0.57} n_{\text{sep}}^{-0.18}$$

- Collisionless SOL
- Applies? NSTX SOL v_e^* 5-100

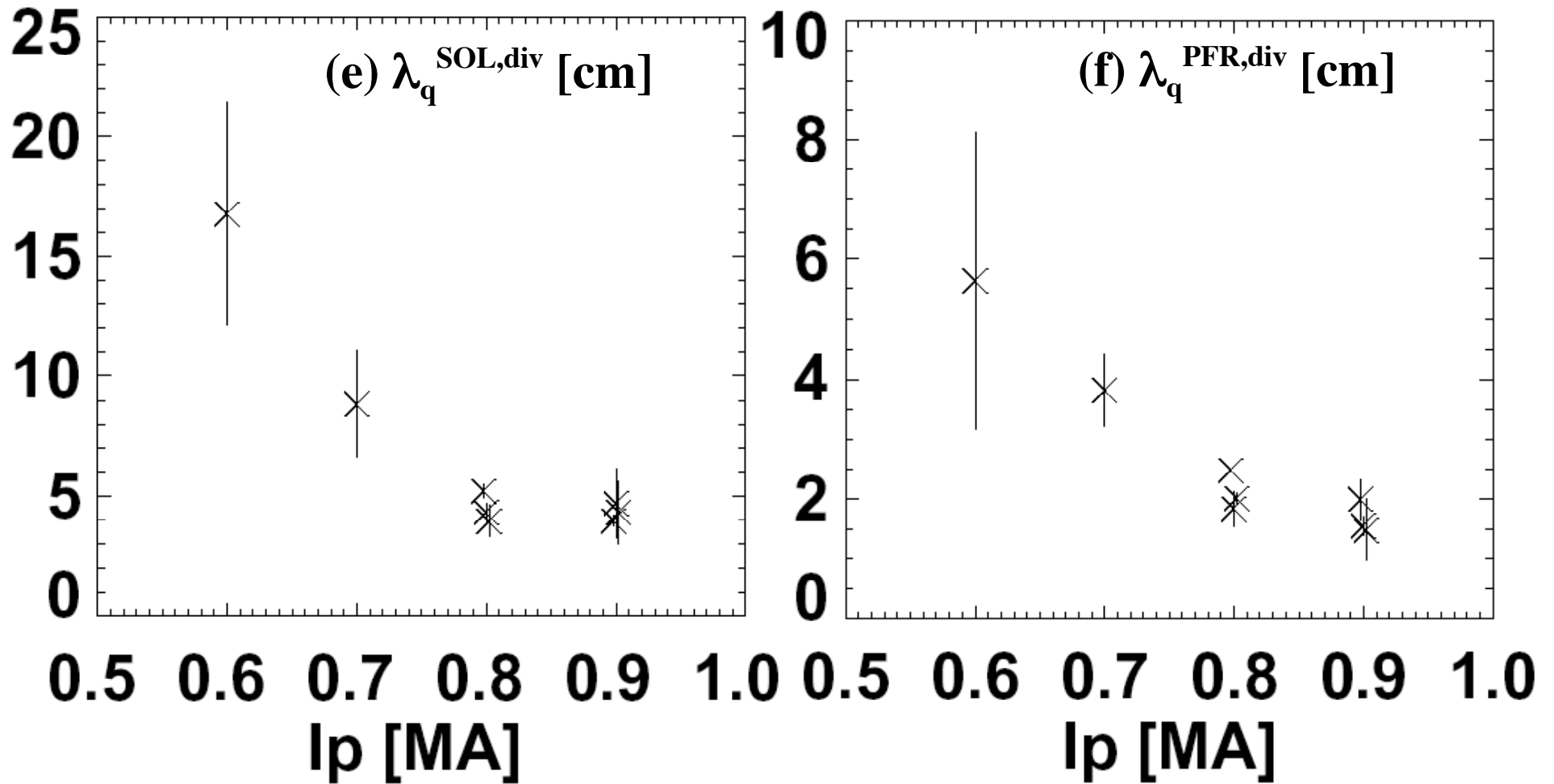
$$\lambda_q^D = 0.35 q_{95}^{-0.1} R_m^{0.3} a_m^{0.4} P_{\text{loss}}^{-0.4}$$

- collisional SOL
- cross-field from sheath resistivity

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- collisional SOL
- cross-field due to charge exchange

Ratio of divertor private-flux region scale length to scrape-off layer heat flux scale length ~ 2.5 -3



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