

Multiscale Phenomena of Plasma-Wall Interaction in TRIAM-1M

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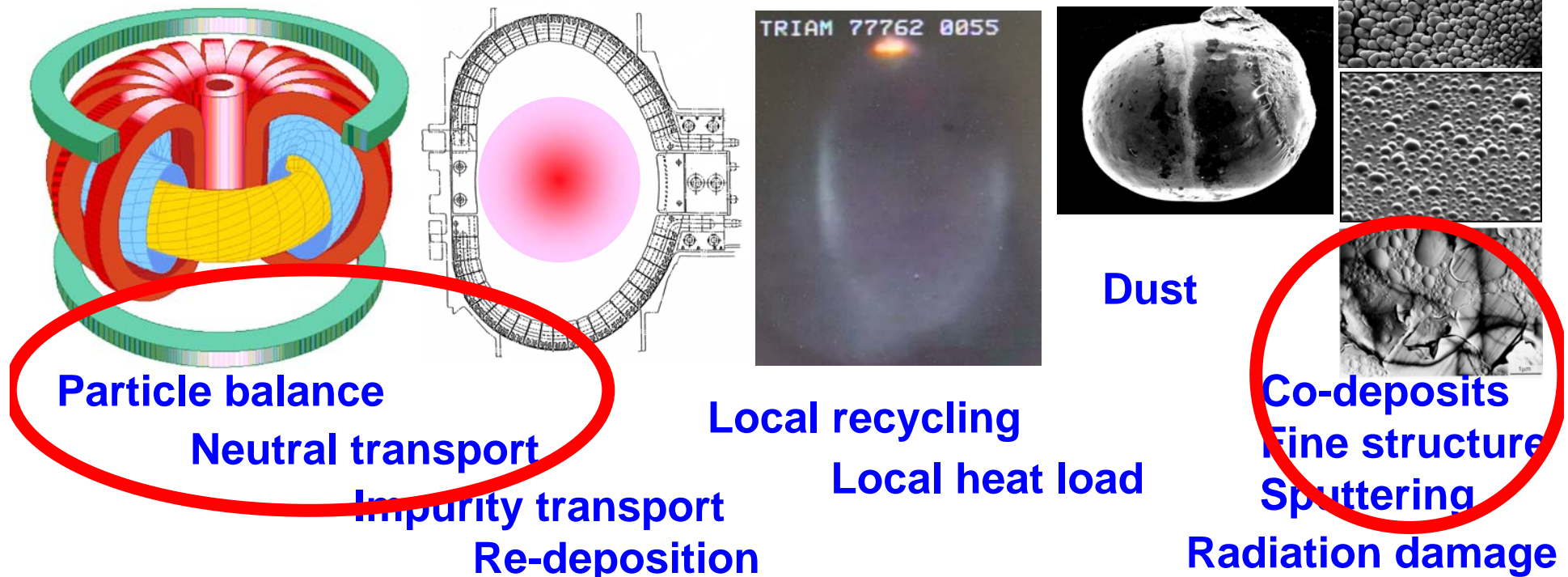
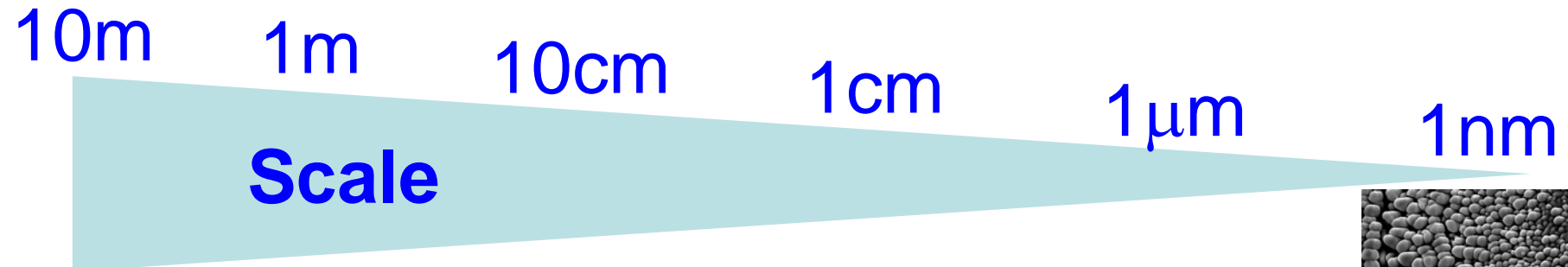
4 Shimane University

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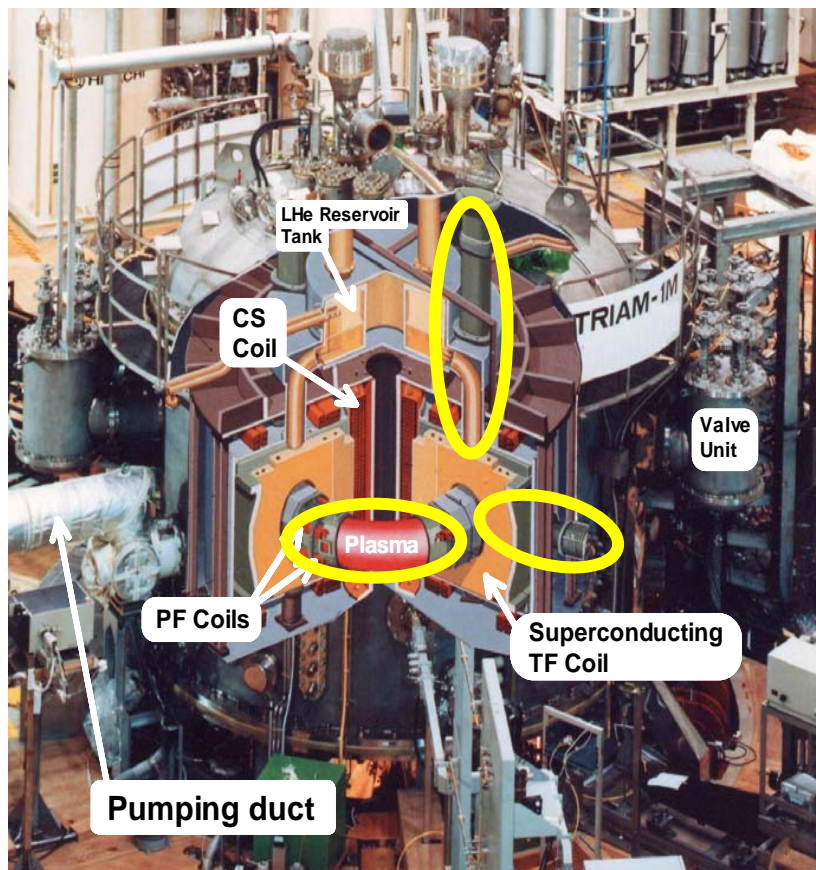
- **Introduction**
- **Wall Recycling Structure**
- **Global Particle Balance**
- **Hydrogen Retention in Co-deposits**
- **Impact of an interval time between discharges**
- **Summary**

Multiscale Phenomena in PWI

It is important to understand various phenomena related to the plasma-wall interaction from macroscopic and microscopic viewpoints



TRIAM-1M Tokamak



Bird's-eye view of TRIAM-1M

Major radius	0.84 m
Minor radius	0.12 m
Toroidal field	8 T (Steady State)

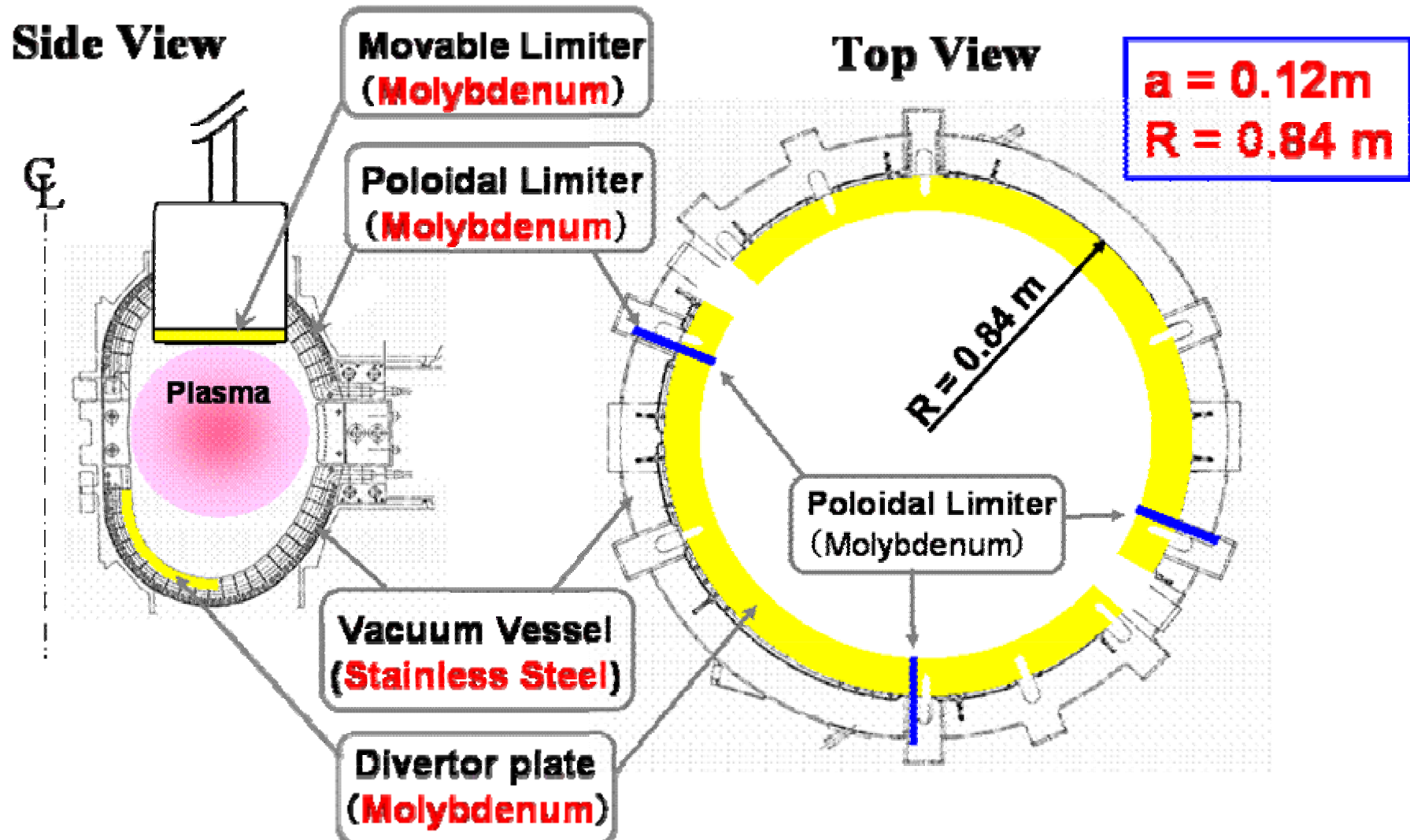
TF coils : Nb_3Sn (superconductor)
PF coils : Cu (normal conductor)

Plasma facing components: High Z

Wall Conditioning:

- (1) Baking of extension ports and then
- (2) ECR discharge cleaning for PFCs

All of the PFMs are made of **metals**

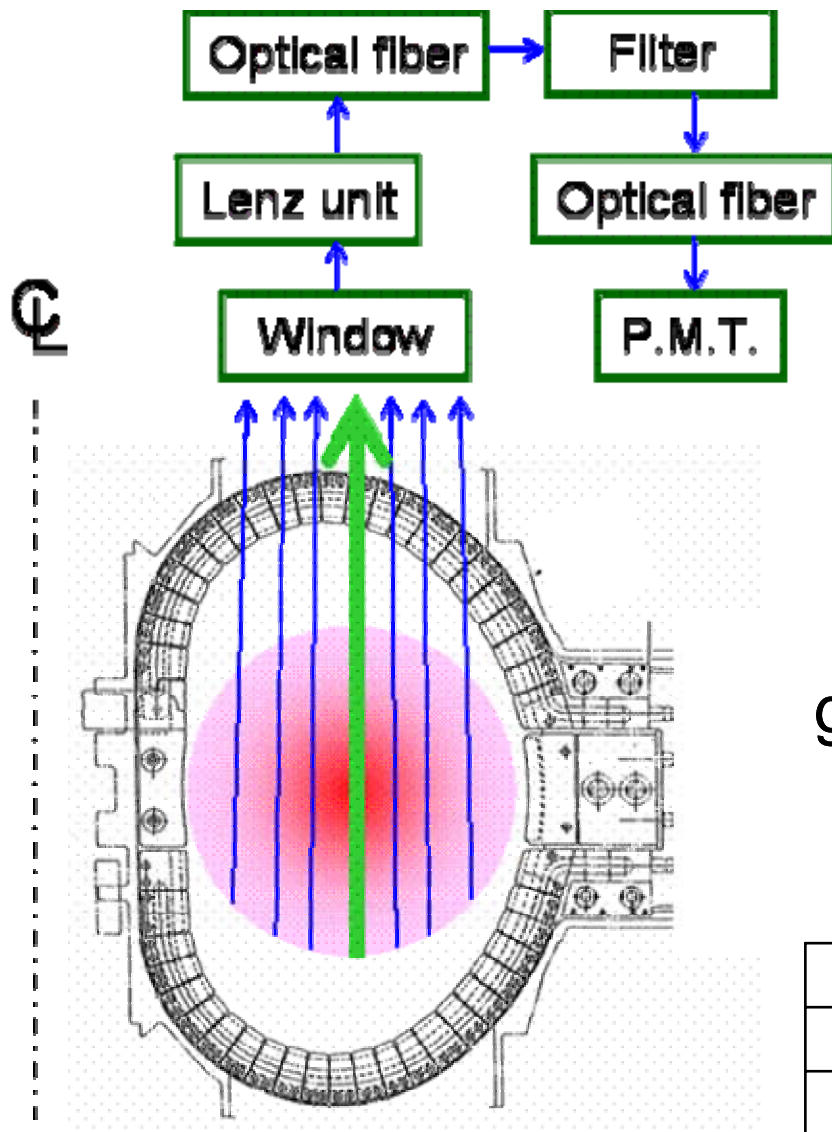


Without low Z material and coating

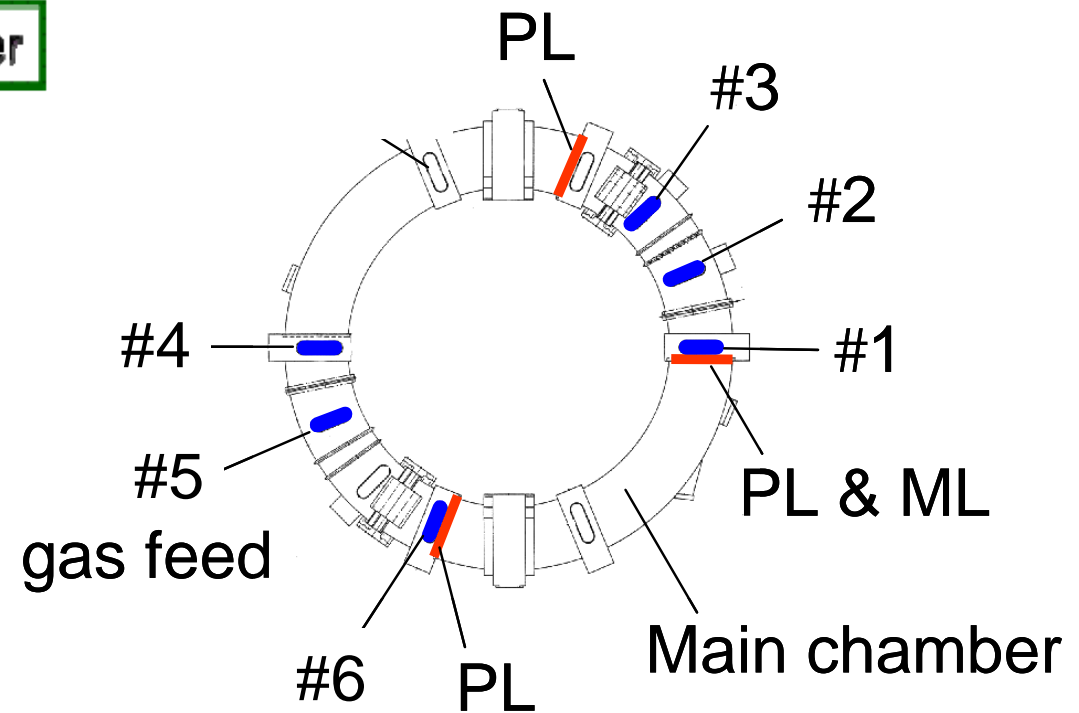
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Measurement system for H α profile



Toroidal Profile of H α intensity is measured at 6 positions.

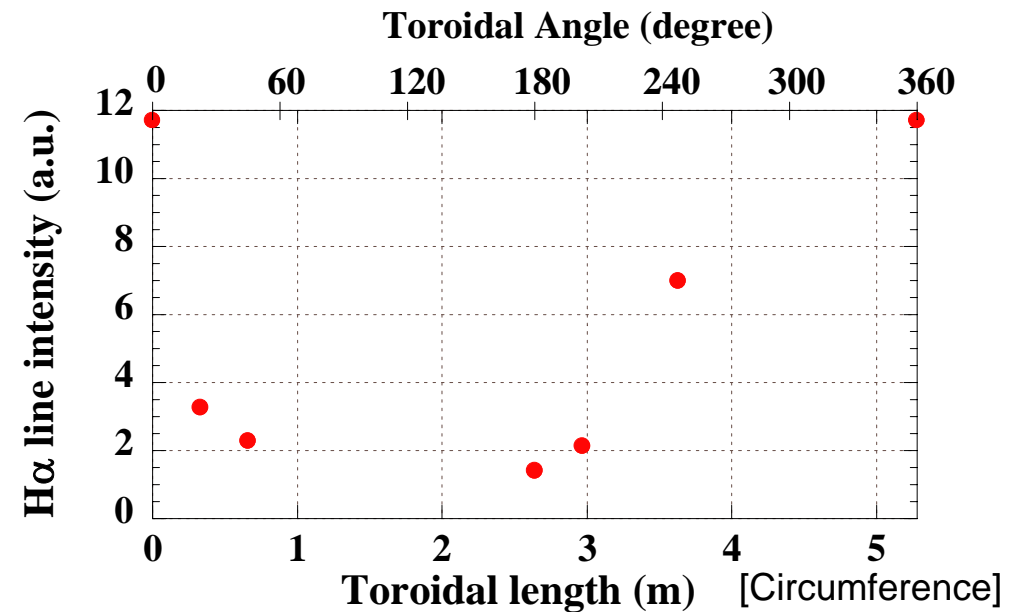
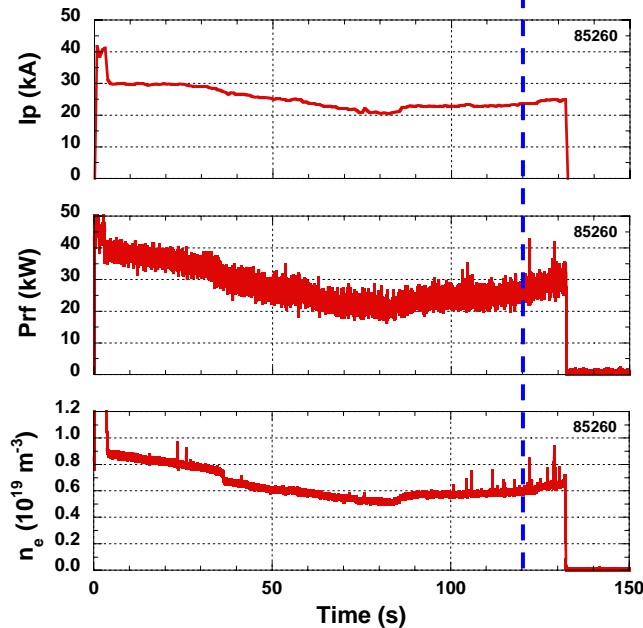


#	1	2	3	4	5	6
Φ	0	22.5	45	180	202.5	247.5
L (m)	0	0.33	0.66	2.64	2.97	3.63

Toroidal profile of H α intensity

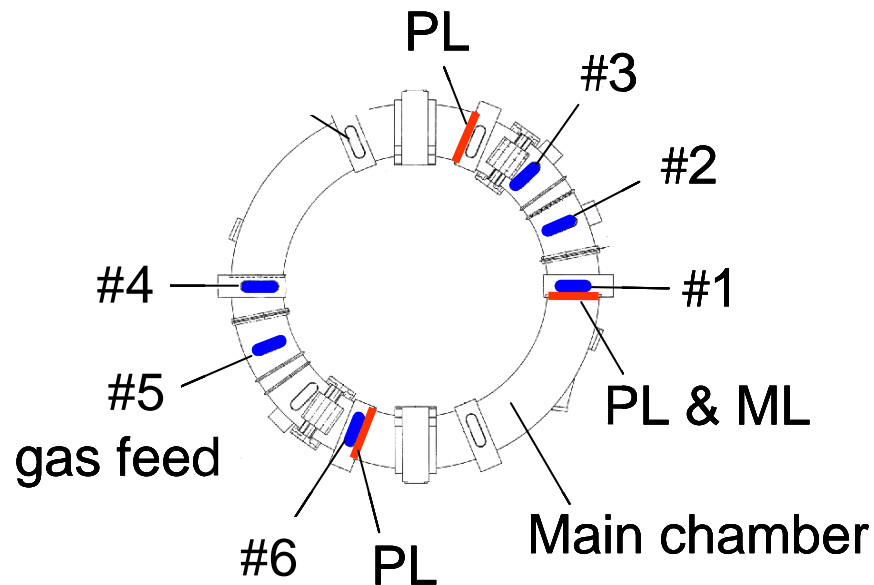
8.2 GHz LHCD

t=120 s

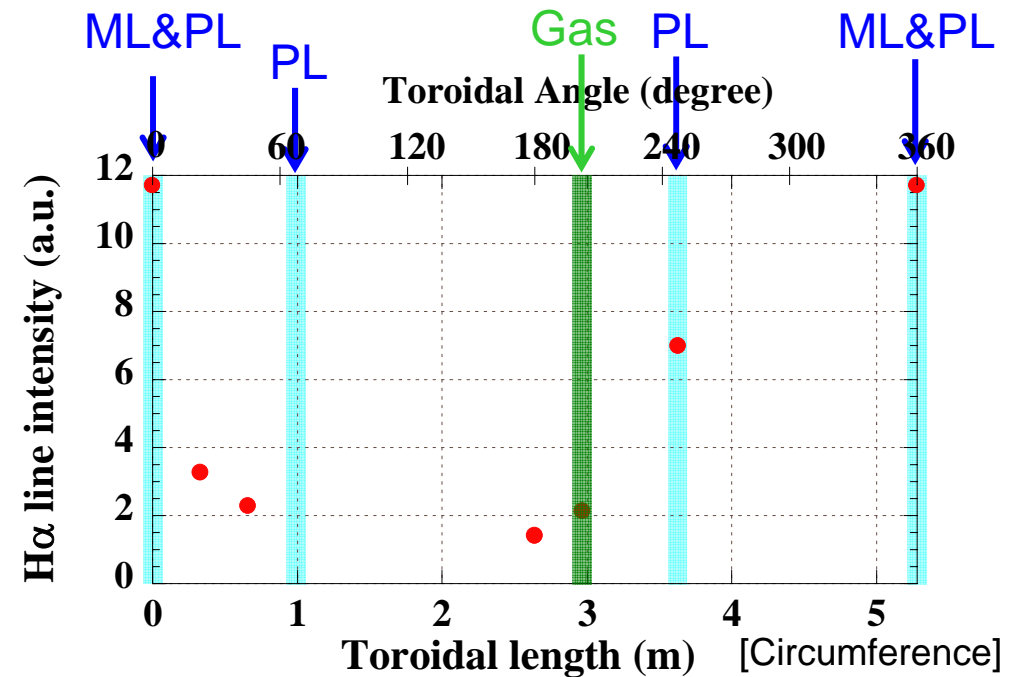


Data at the latter phase of the discharge is used to reduce an effect of gas puff on the toroidal profile.

Toroidal profile of H α intensity

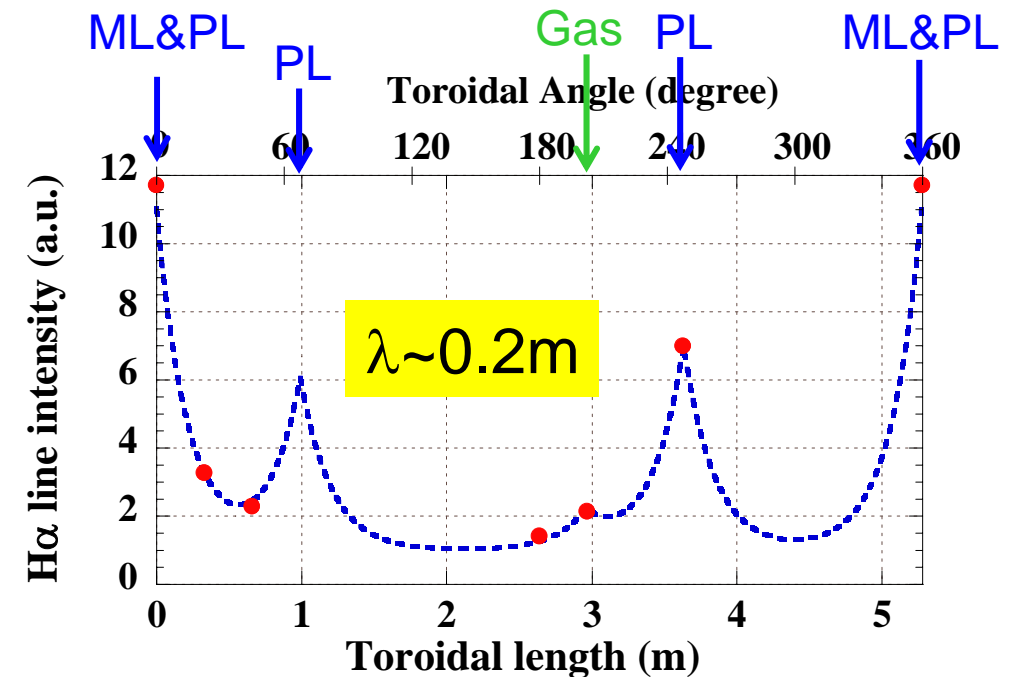
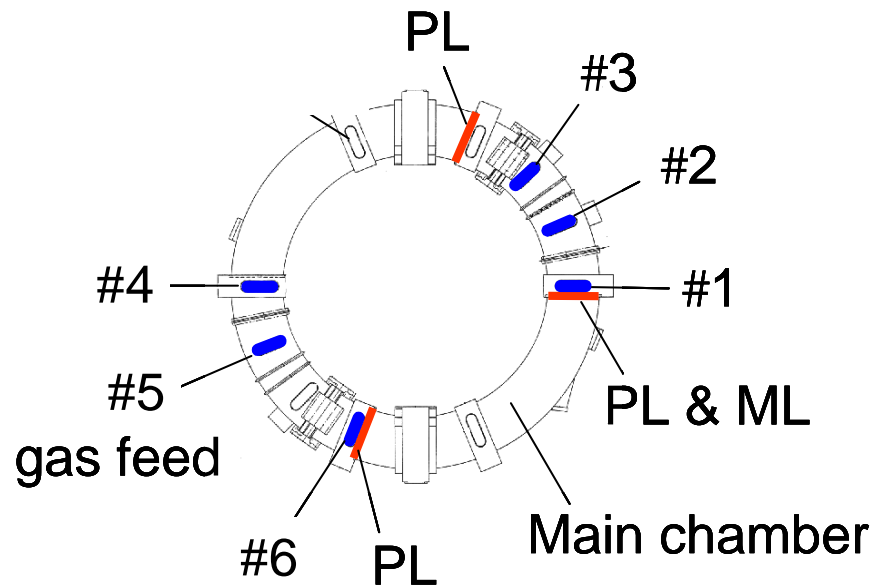


Wall recycling is enhanced at ML&PL



$$I_{H\alpha}(x) = P_{mc} + \sum_{i=1}^4 P_i \exp\left[\frac{-|x - x_i|}{\lambda}\right]$$

Toroidal profile of H α intensity



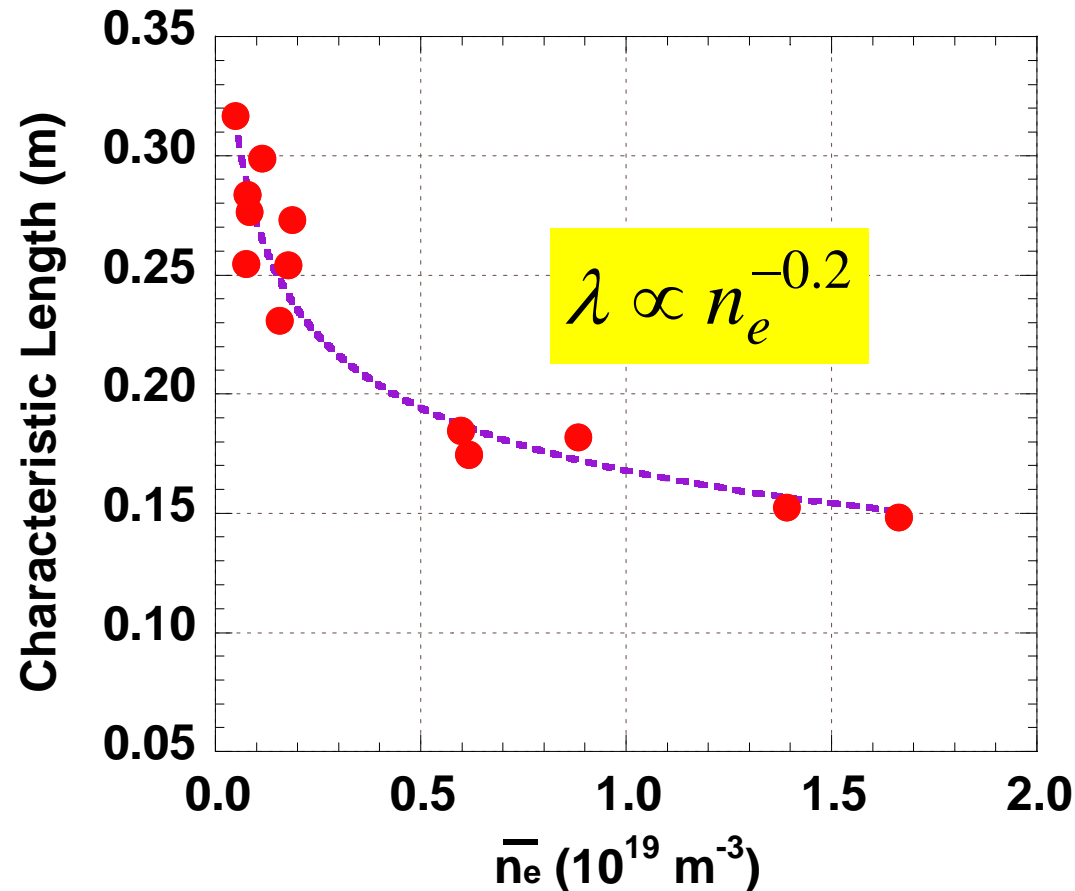
Almost all hydrogen is refueled by wall recycling. This means that recycling ratio is nearly unity. In another exp., the recycling ratio was more than 0.998.

[Ref.: M.Sakamoto et al. NF(2002)]

$$I_{H\alpha}(x) = P_{mc} + \sum_{i=1}^4 P_i \exp\left[\frac{-|x - x_i|}{\lambda}\right]$$

Hydrogen recycling is localized within $\lambda \sim 0.2\text{m}$.

Density dependence of λ



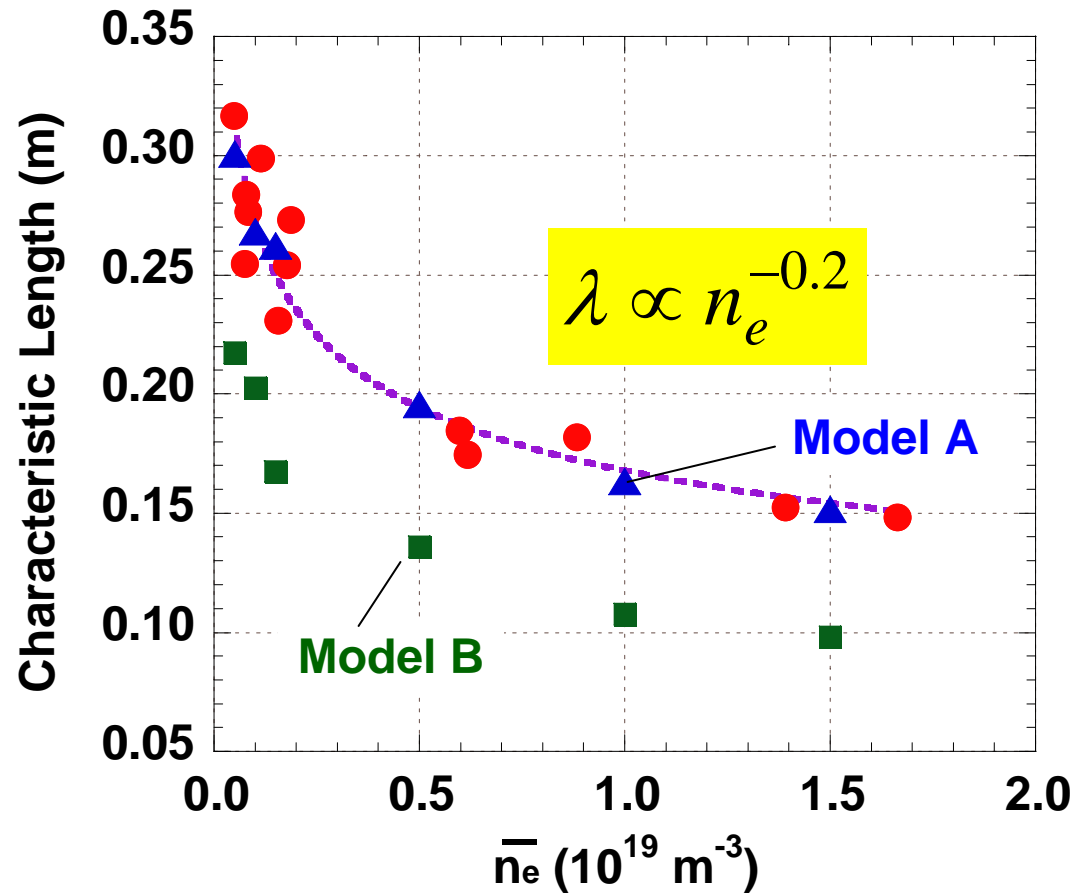
Density regime

$$0.05 \times 10^{19} < \bar{n}_e < 1.5 \times 10^{19} \text{ m}^{-3}$$

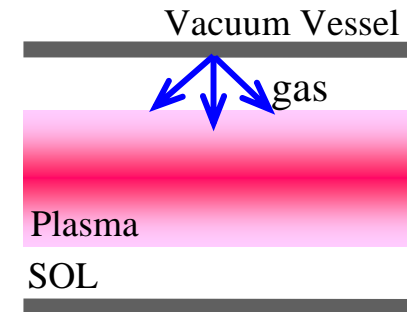
$$0.3 > \lambda > 0.15 \text{ m}$$

Although the density changes by 30 times, λ changes only twice.

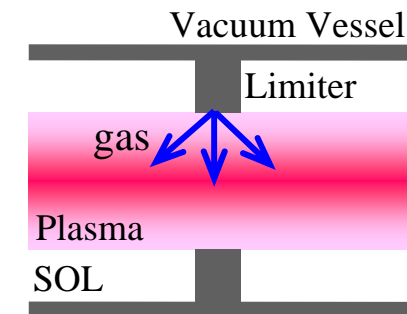
DEGAS simulation



Model A

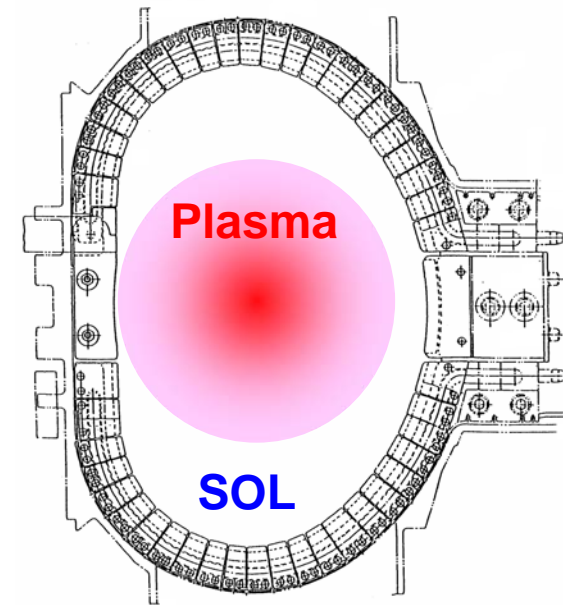
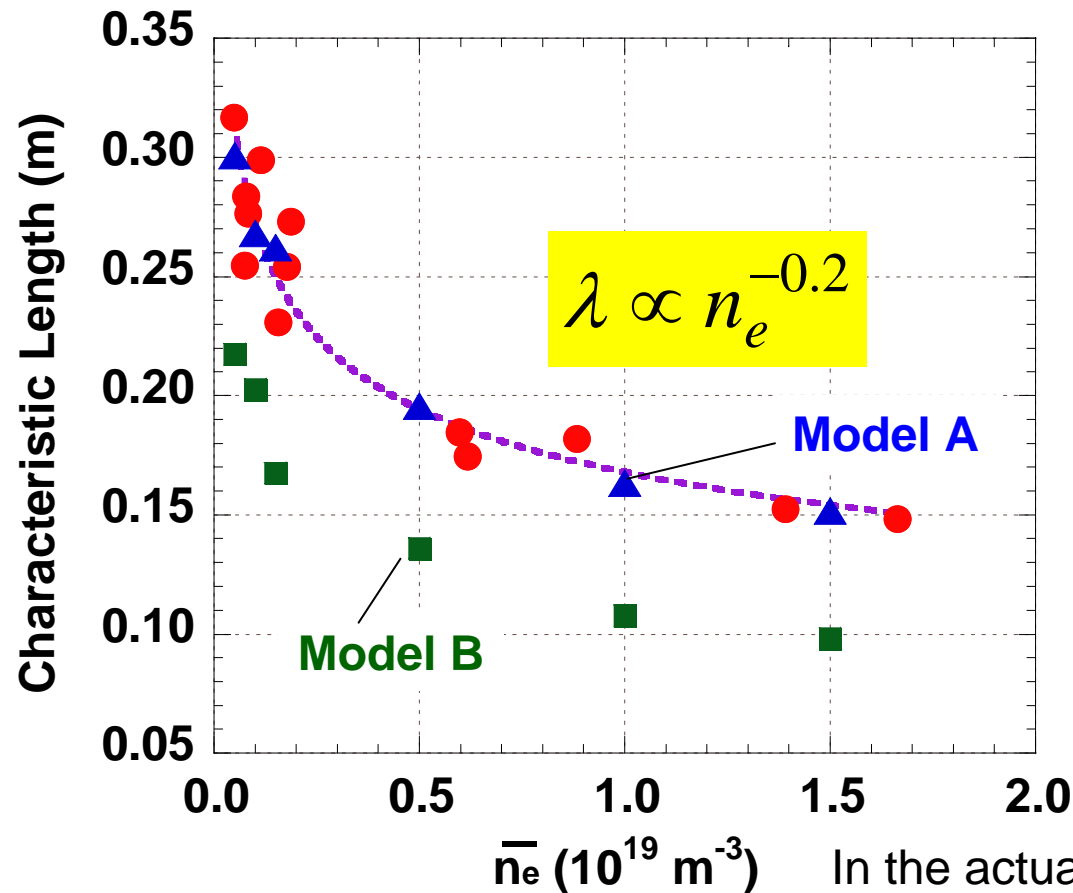


Model B



DEGAS simulation of the model A reproduces the exp. results.

Impact of SOL on the neutral transport



In the actual geometry, the limiter is D-shaped. Large SOL region exists above and below the plasma. Neutral transport in SOL seems to dominate the characteristic length of wall recycling structure.

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Particle Balance in Vacuum Vessel

$$dN_p / dt + dN_0 / dt = \Gamma_{\text{fuel}} - \Gamma_{\text{pump}} - \Gamma_{\text{wall}}$$

Γ_{fuel} : fueling rate, Γ_{pump} : pumping rate, Γ_{wall} : net wall pumping rate

Steady state condition:

$$\Gamma_{\text{wall}} = \Gamma_{\text{fuel}} - \Gamma_{\text{pump}}$$

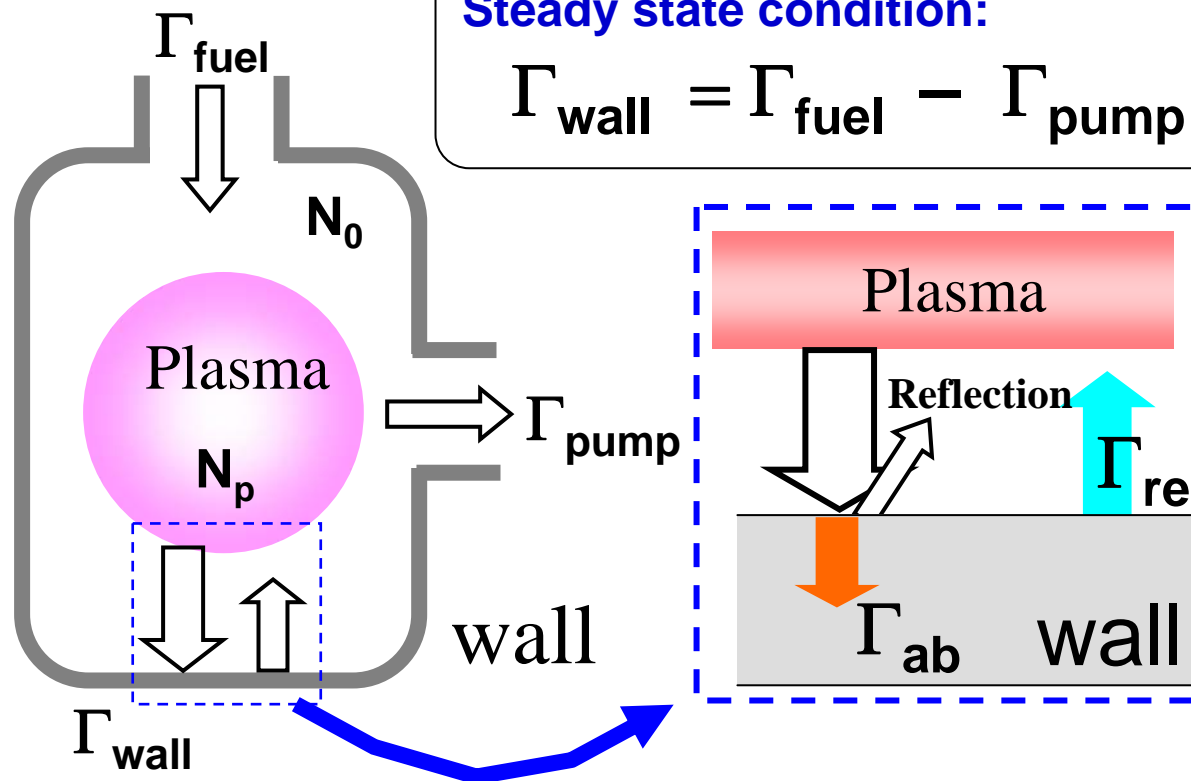
Two roles of wall

$$\Gamma_{\text{wall}} = \Gamma_{\text{ab}} - \Gamma_{\text{re}}$$

Positive : Sink
Negative : Source

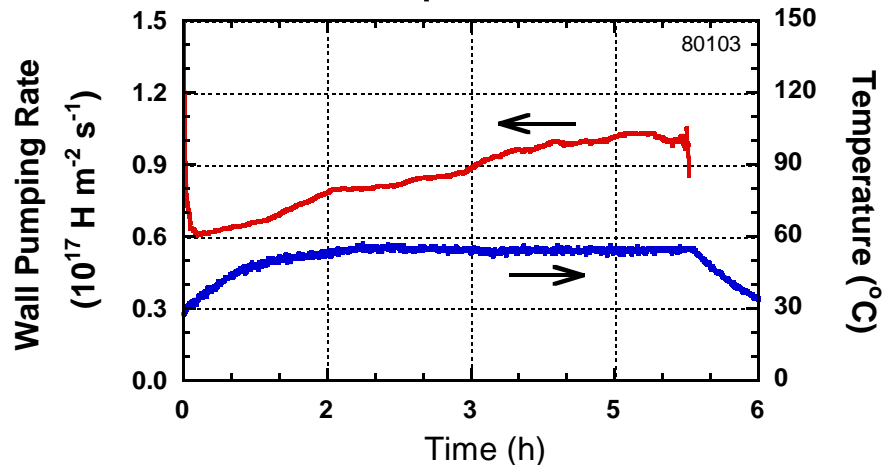
Γ_{ab} : H absorption

Γ_{re} : H re-emission



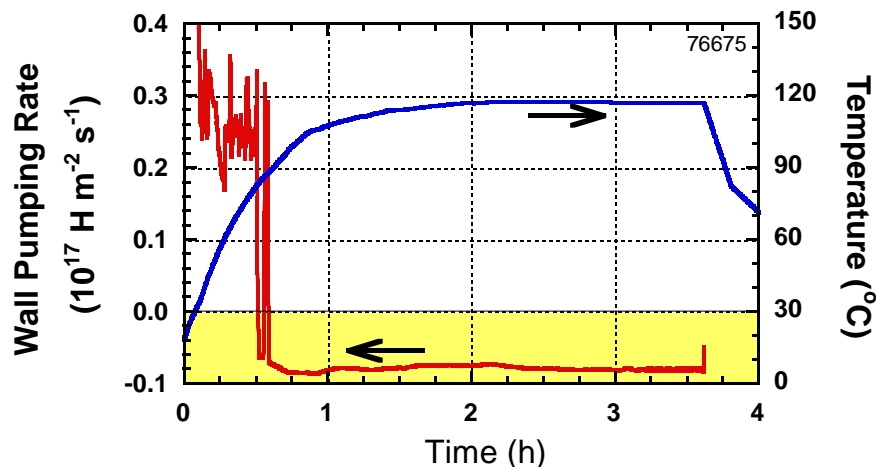
Impact of Wall Temperature on GPB

Low Temperature Wall



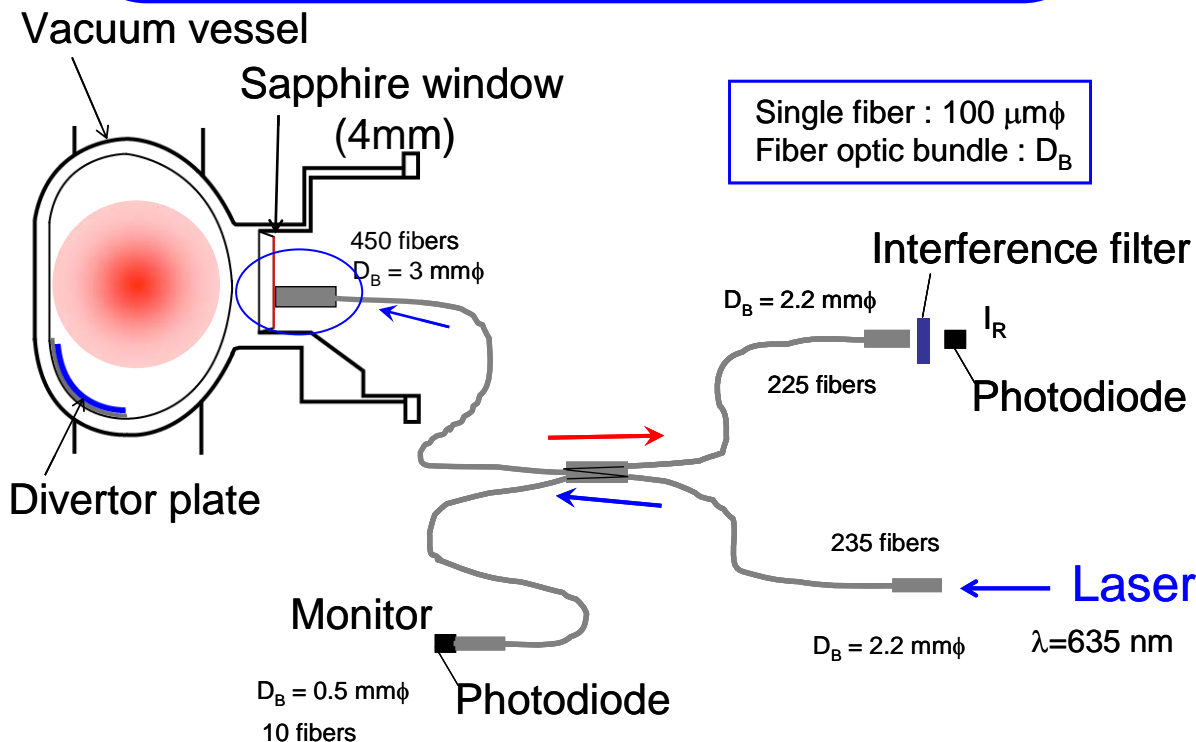
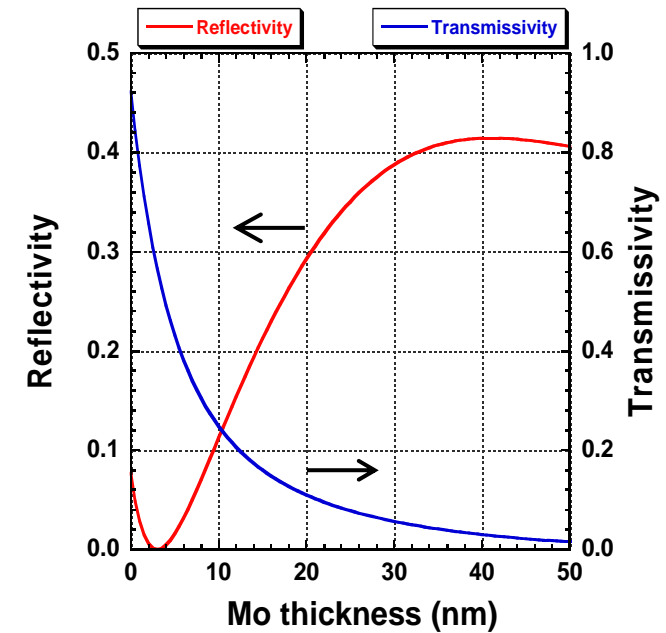
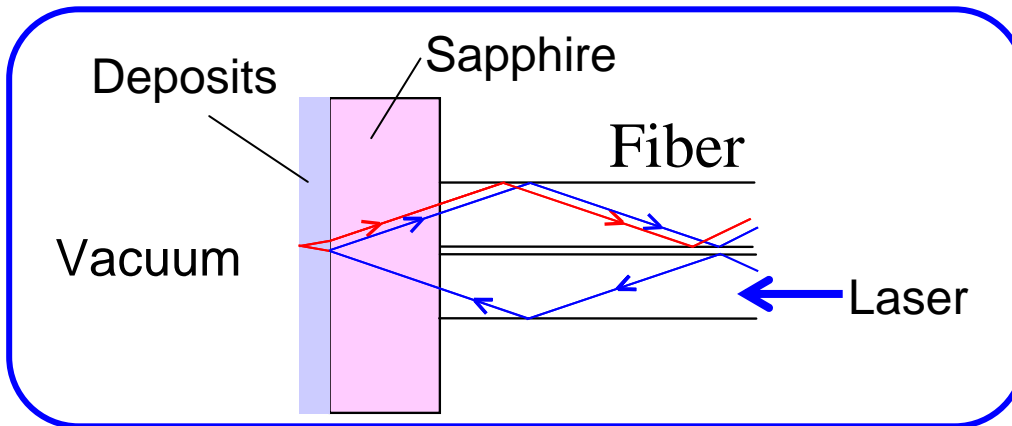
By using a movable limiter with good cooling capability, increase in the wall temperature was suppressed to less than 60 $^{\circ}\text{C}$. No wall saturation can be seen.

High Temperature Wall



Without the movable limiter, the wall temperature partly increased up to 120 $^{\circ}\text{C}$ due to heat load from the plasma. The wall pumping rate changed from positive to negative at $t \sim 30$ min.

In situ measurement of growth of deposited layer



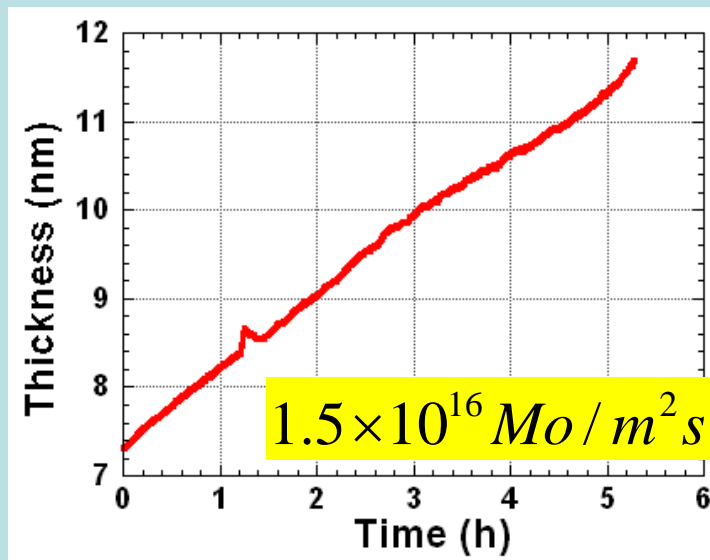
$$\delta = \frac{2\pi}{\lambda_0} n_1 2d \cos \phi \sim \frac{4\pi}{\lambda_0} n_1 d$$

$$r_1 = \frac{n_0 - n_1}{n_0 + n_1} \quad r_2 = \frac{n_1 - n_2}{n_1 + n_2}$$

$$r = \frac{r_1 + r_2 e^{-i\delta}}{1 + r_1 r_2 e^{-i\delta}}$$

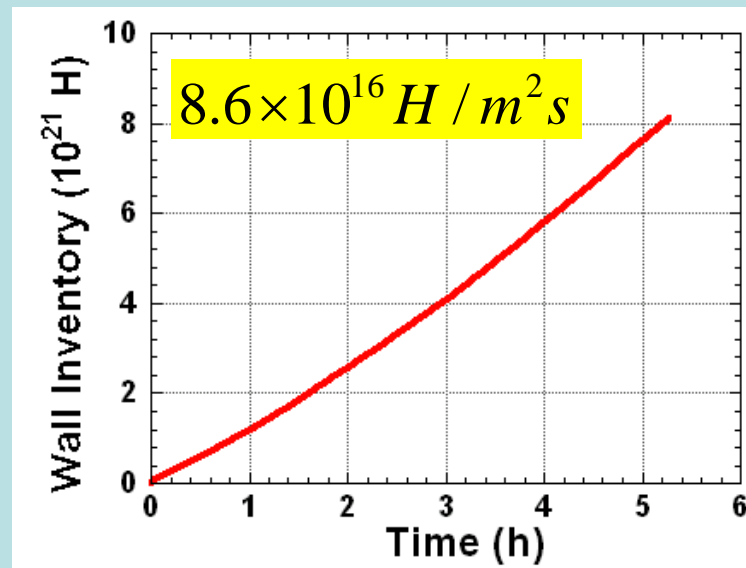
Continuous wall pumping related to codeposition

Growth of dep. layer



Time evolution of the thickness of the deposited layer.

Wall Inventory



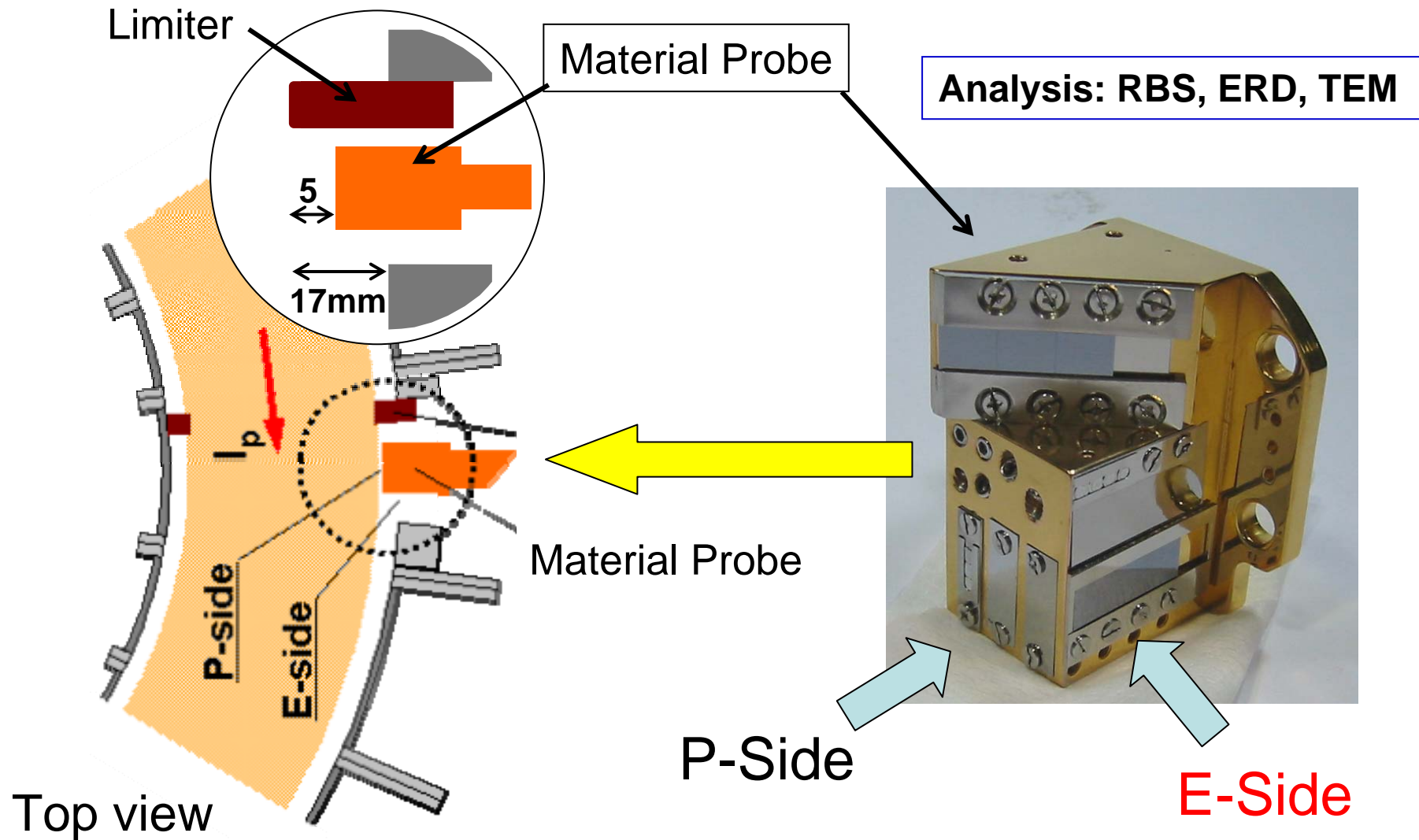
Time evolution of the wall inventory in 5 h 16 min discharge. No wall saturation can be seen.

Continuous codeposition can be expected.

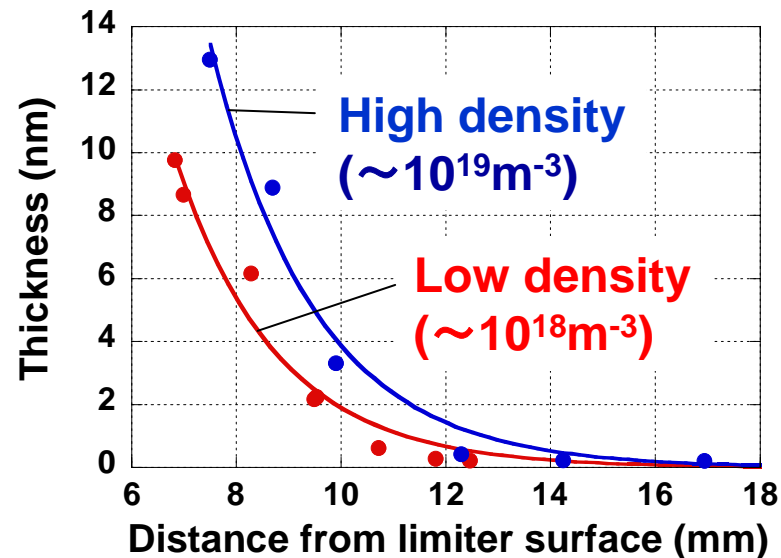
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Hydrogen retention & microstructure of co-deposit



Hydrogen retention & microstructure of Mo deposit

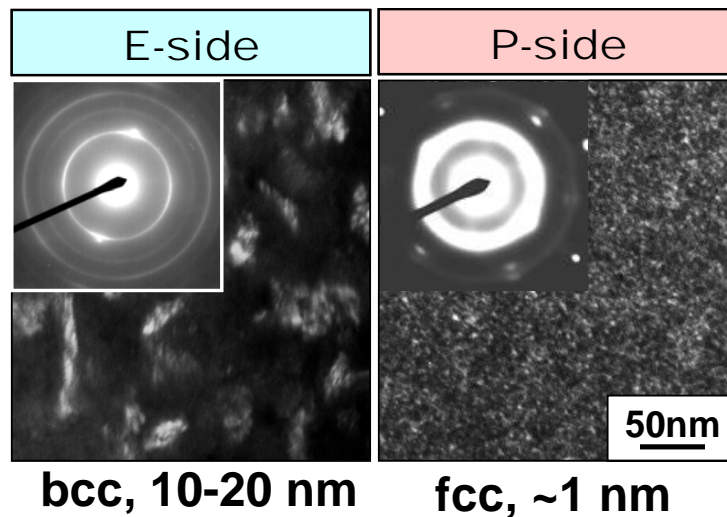


High density (10^{19} m^{-3})
 H/Mo ~ 0.17 @ E-side (8mm)
 H/Mo ~ 0.15 @ P-side

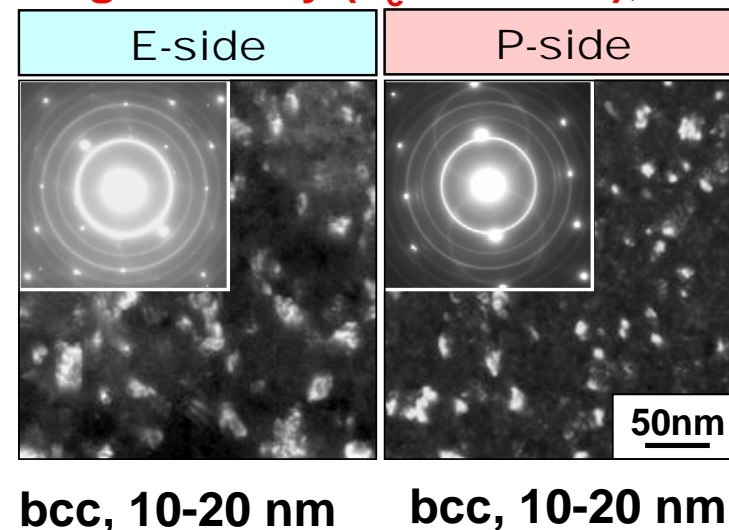
Low density (10^{18} m^{-3})
 H/Mo ~ 0.04 @ E-side (8mm)
 H/Mo ~ 0.10 @ P-side

Codeposition of hydrogen with sputtered Mo makes a substantial wall pumping.

● Low density ($n_e \sim 10^{18} \text{ m}^{-3}$), 4320s



◆ High density ($n_e \sim 10^{19} \text{ m}^{-3}$), 407 s



Summary of material probe results and GPB

	Low density ($\sim 1 \times 10^{18} \text{ m}^{-3}$)		High density ($\sim 1 \times 10^{19} \text{ m}^{-3}$)		note
	E-side	P-side	E-side	P-side	
Structure	bcc	fcc	bcc	bcc	
Grain size	10-20nm	1-2nm	10-20nm	10-20nm	
Mo depo. Rate	$3.6 \times 10^{17} \text{ Mo/m}^2\text{s}$	$6.4 \times 10^{16} \text{ Mo/m}^2\text{s}$	$(1.7 \times 10^{18} \text{ Mo/m}^2\text{s})$	$2.3 \times 10^{18} \text{ Mo/m}^2\text{s}$	$x=8\text{mm}$ @E-side
$\Gamma_{\text{wall}}(\text{MP})$	$1.3 \times 10^{16} \text{ H/m}^2\text{s}$	$6.4 \times 10^{15} \text{ H/m}^2\text{s}$	$(2.9 \times 10^{17} \text{ H/m}^2\text{s})$	$3.5 \times 10^{17} \text{ H/m}^2\text{s}$	
$\Gamma_{\text{wall}}(\text{GPB})$	$2 \times 10^{16} \text{ H/m}^2\text{s}$ (HTW)		$4.0 \times 10^{17} \text{ H/m}^2\text{s}$		Whole wall surface is used. ($S = 5 \text{ m}^2$)
	$8.6 \times 10^{16} \text{ H/m}^2\text{s}$ (LTW)				

- ➔ M. Sakamoto et al., Nuclear Fusion, 42 (2002) 588.
- ➔ M. Sakamoto et al., Nuclear Fusion, 442 (2004) 693.
- ➔ M. Miyamoto et al., J. Nucl. Mater. 337-339 (2005) 436-440
- ➔ M. Tokitani et al., 12th ICFRM, J. Nucl. Mater. (in press)

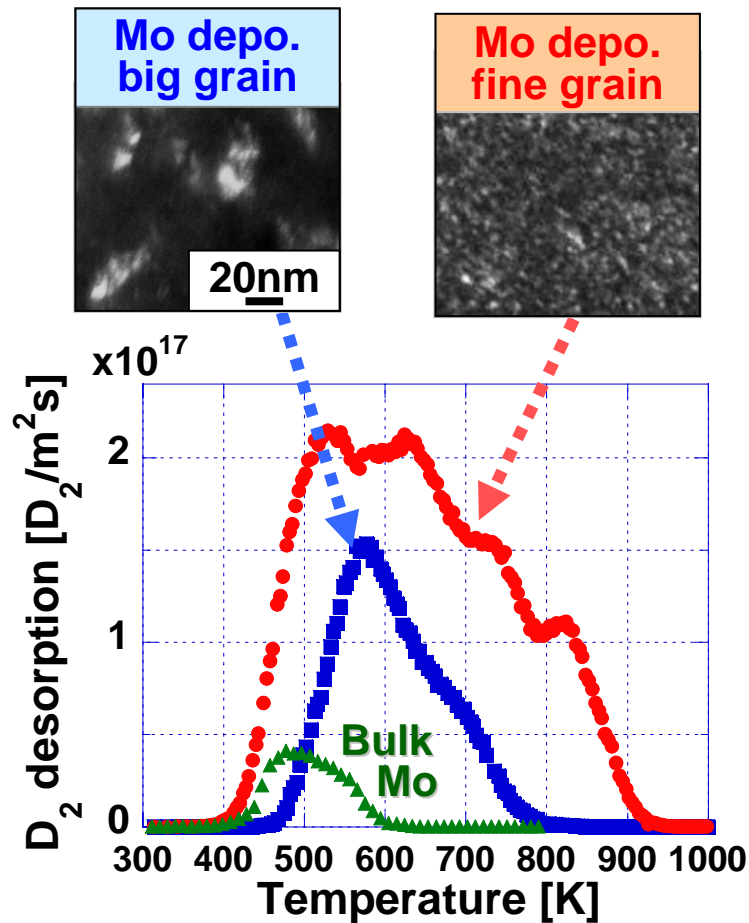
Summary of material probe results and GPB

	Low density ($\sim 1 \times 10^{18} \text{ m}^{-3}$)		High density ($\sim 1 \times 10^{19} \text{ m}^{-3}$)		note
	E-side	P-side	E-side	P-side	
Structure	bcc	fcc	bcc	bcc	
Grain size	10-20nm	1-2nm	10-20nm	10-20nm	
Mo depo. Rate	$3.6 \times 10^{17} \text{ Mo/m}^2\text{s}$	$6.4 \times 10^{16} \text{ Mo/m}^2\text{s}$	$(1.7 \times 10^{18} \text{ Mo/m}^2\text{s})$	$2.3 \times 10^{18} \text{ Mo/m}^2\text{s}$	$x=8\text{mm}$ @E-side
$\Gamma_{\text{wall}}(\text{MP})$	$1.3 \times 10^{16} \text{ H/m}^2\text{s}$	$6.4 \times 10^{15} \text{ H/m}^2\text{s}$	$(2.9 \times 10^{17} \text{ H/m}^2\text{s})$	$3.5 \times 10^{17} \text{ H/m}^2\text{s}$	
$\Gamma_{\text{wall}}(\text{GPB})$	$2 \times 10^{16} \text{ H/m}^2\text{s}$ (HTW)		$4.0 \times 10^{17} \text{ H/m}^2\text{s}$		Whole wall surface is used. ($S = 5 \text{ m}^2$)
	$8.6 \times 10^{16} \text{ H/m}^2\text{s}$ (LTW)				

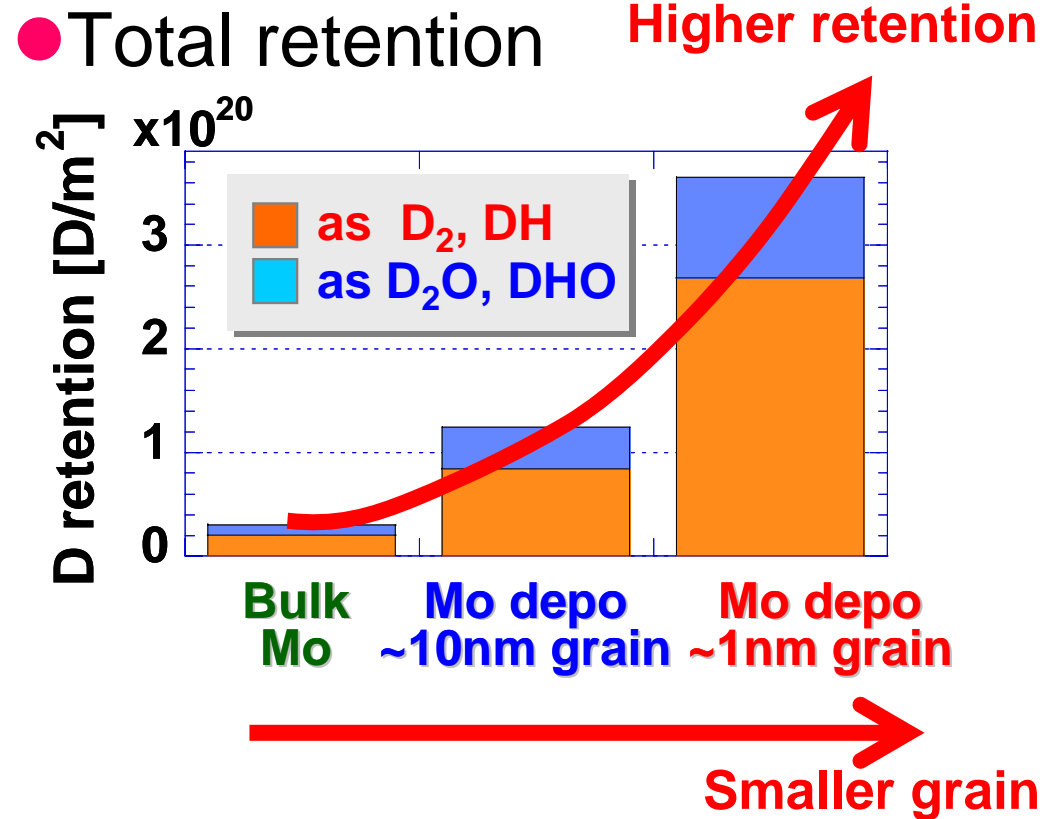
- ➔ M. Sakamoto et al., Nuclear Fusion, 42 (2002) 588.
- ➔ M. Sakamoto et al., Nuclear Fusion, 442 (2004) 693.
- ➔ M. Miyamoto et al., J. Nucl. Mater. 337-339 (2005) 436-440
- ➔ M. Tokitani et al., 12th ICFRM, J. Nucl. Mater. (in press)

Impact of grain size on hydrogen retention

D_3^+ with 6keV is implanted to Mo bulk and Mo deposits.



Thermal desorption spectra
Fluence : 1×10^{21} D/m²



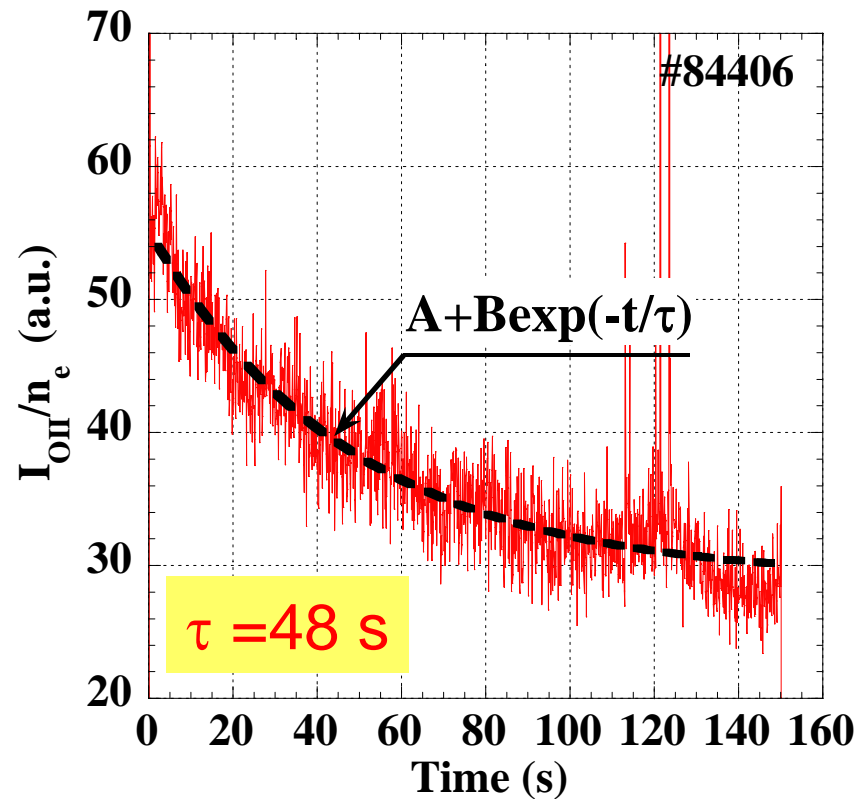
Note that the deposits with fine grains were made in a little oxygen atmosphere.

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Impact of a repetition of discharges on wall condition is shown focusing on oxygen impurity behavior

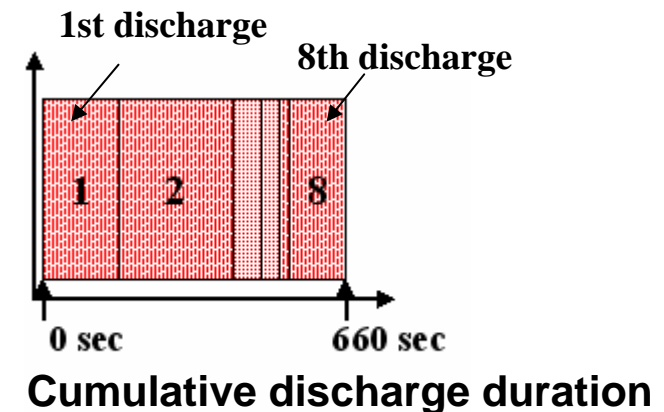
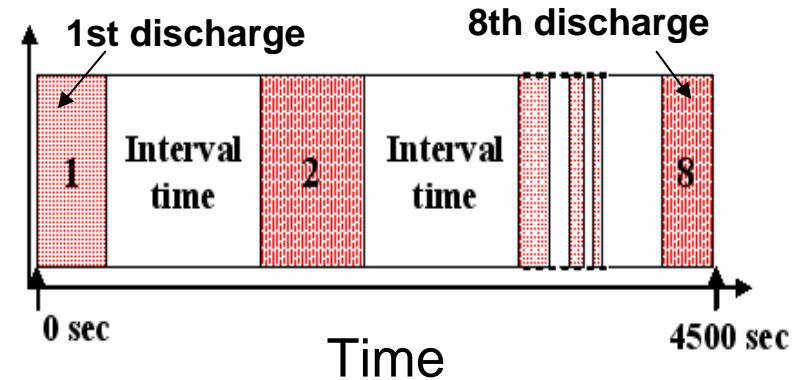
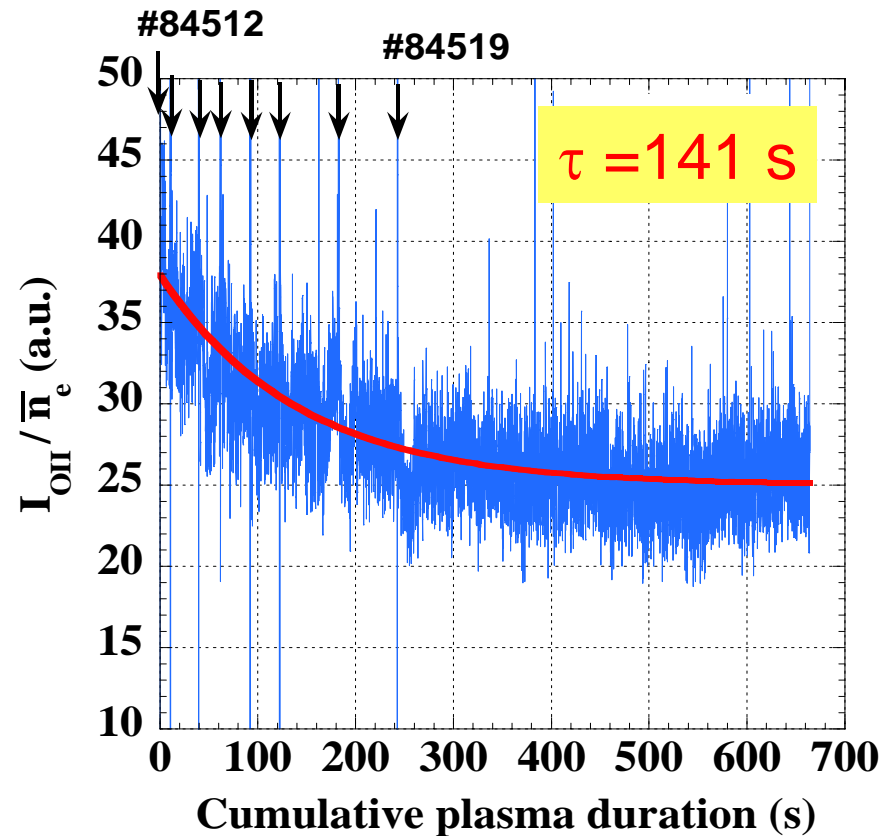
Single long duration discharge



Oxygen concentration of the wall surface gradually decreases during the discharge.

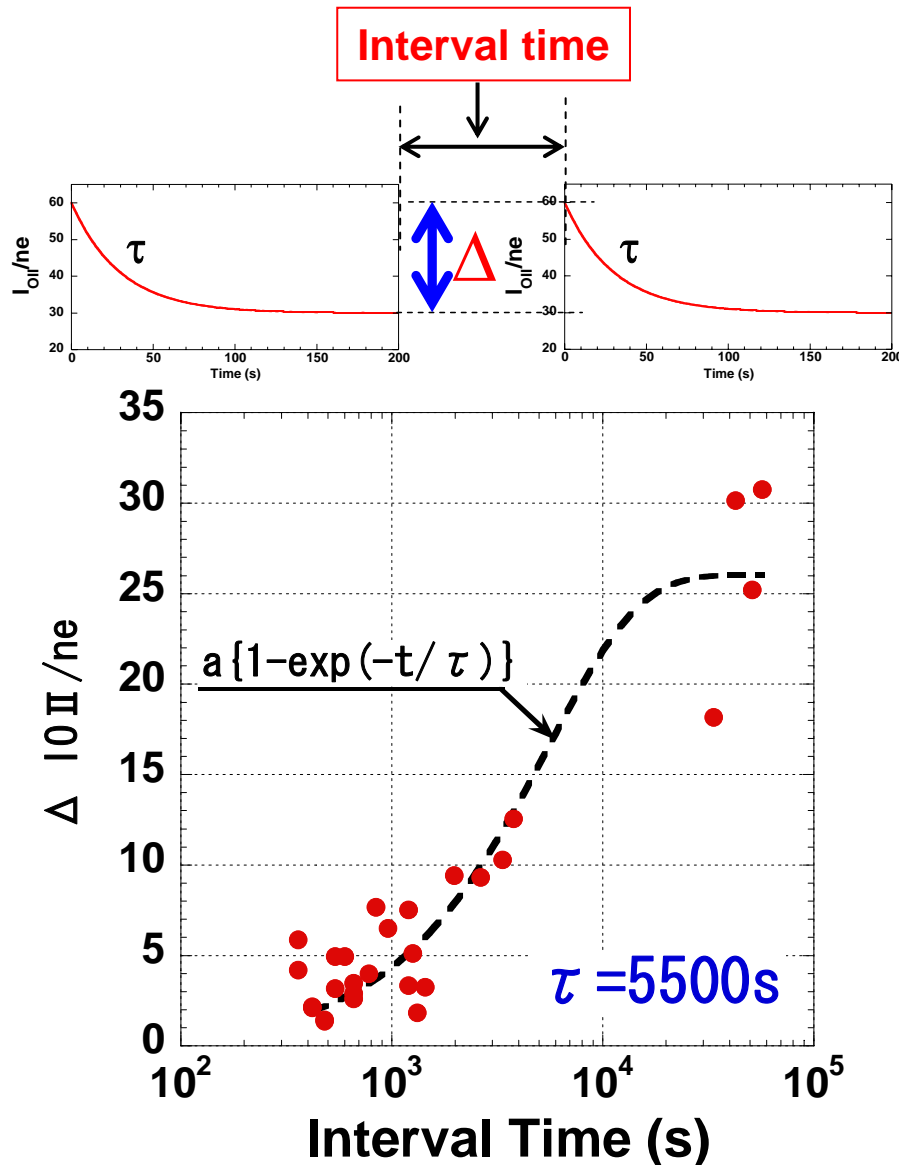
Note that the data were obtained in the initial phase of the campaign.

Oxygen behavior in the case of a repetition of discharges



The time constant τ is about 3 times longer than that of a single one.

Oxygen concentration on the wall surface increases during the interval time between discharges



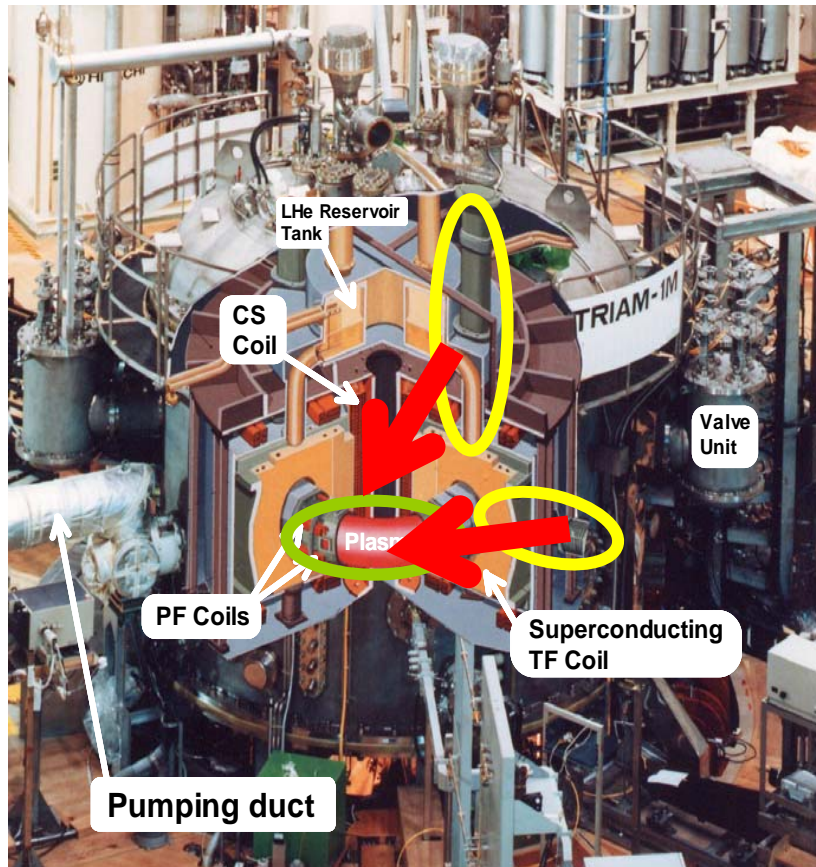
Langmuir adsorption equation

$$\frac{d\theta}{dt} = \frac{s(1-\theta)}{\sigma_m} \left(\frac{v}{4} \right) n - \frac{\theta}{\tau_a}$$

$$\Delta\theta = (1-\theta_0)\{1 - \exp(-t/\tau)\}$$

K. Akaishi, J. Plasma Fusion Res. 79(2003)518.

Oxygen comes from the surface which does not face the plasma during the interval time



Bird's-eye view of TRIAM-1M

Wall Conditioning:

- (1) Baking of extension ports and then
- (2) ECR discharge cleaning for PFCs

H₂O should come from the extension ports during the interval time.

Summary

PWI phenomena have been studied from macroscopic and microscopic viewpoints in long duration discharges on TRIAM-1M.

- (1) Wall recycling is localized within $\lambda \sim 0.3\text{m}$. λ is proportional to $n_e^{-0.2}$. Neutral transport in SOL should dominate the characteristic length λ .
- (2) Global wall pumping rates were estimated using a particle balance model in the case of LTW and HTW.
- (3) Wall temperature is a key to dominating a wall role: particle sink or particle source.
- (4) Codeposition of hydrogen with eroded metal makes a substantial wall pumping. H/Mo is comparable to that of carbon.
- (5) Capability of hydrogen retention depends on a grain size of the deposits. Oxygen strongly affects the structure formation of the deposits.
- (6) The wall condition continues to change not only during the discharge but also during an interval time between discharges. As for some PWI issues, a summation of short discharges can not reproduce a single long discharge.